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N<sup>o</sup> 167

PASTS

FIELD BOOK

S.A.R. #10+5 Job #3002

No. 385

TRANSIT NOTES  
CASS Co.

Sta. 0+00 to 144+20



✓ Bena ✓ 248

[100' stationing ✓ stake on shoulder

1/2 Cost of detour.

3684  
296  
724 - 261 ✓

3684  
330  
484 - 260 d3  
41

3684  
327  
41

3684  
319  
49 54  
44

Time Book  
To Draper  
15" x 30

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
ENGINEERING and DRAFTING SUPPLIES  
IRVING PARK STATION  
CHICAGO, ILL.



Property of  
Cass County

Please return to  
Highway Engineer  
Walker,  
Minn.

8  
21



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D SR#10 Transit Notes  
At Intersection SR#10 & T.H.#8 Sec T R

12-4-29

Party { Prudlo  
Duncan Rod  
Duncan Chain

Res

R.P.

6+00 { 3" Ash 36.5E  
5" Birch 44NE

FE 8+10  
3+60  
FE

+882 45°10' 45°09' 15' to 2+89.6 P.T.  
+50 41°20' 41°12'  
2+00 36°20' 36°12'  
1+50 31°20' 31°12'  
1+00 26°20' 26°12' East Curve  
0+50 21°20' 21°12'  
0+00 16°20' 16°12'  
0-50 11°20' 11°12'  
0-100 6°20' 6°12'  
0-163.4 0-162.0

451.6 L=451.6

T 288.2 T=289.6

Δ 90°20' Δ=90°20'

C=20°R

2+83.8 P.T. → 99°34.8'  
+84.3 EC 44°35' 41°16' +50

2+00 36°09' 36°12'  
1+50 31°09' 31°12'  
1+00 26°09' 26°12' West Curve  
0+50 21°09' 21°12'

L 445.8 L=445.8

T 284.3 T=283.8

C 20°L C=20°L

0+00 16°09' 16°12'  
0-50 11°09' 11°12'  
0-100 6°09' 6°12'  
0-161.5 P.C. 0-162.0

Δ 89°10' Δ=89°10'

R.P.P.C. { T.P. 655 SE  
T.H. Sign Post 53.0 NE

R.P.E.C. { 14" W.P. 89.8 NE  
4" Bass W. 82.6 SE

R.P.P.C. { T.P. 44.1 SE  
T.H. Sign Post 47.5 SW

0+00 P.I. W Line Sec 15-T 145 N. R 30 W

R.P. { T.P. 42.6 SE  
18" Stump 60.0 SW

R of W Stake { P/W  
66' total R of W.



2

648

RP 34 { 3" Pop 398 SE  
3" Pop 380 NE

RP 30 { 4" Birch 568 SE  
3" NR 500 NE

RP 22 { 6" Pop 41.9 E  
3" Pop 42.2 NE

WILD PINE

Clay Soil

Clay Soil

WILD PINE

FE 14130

12+350 1/4 Line N9 Mon Δ0°15'R

R.P.S { 5" Poplar 601 SE  
8" Pop 574 SW



3

91+40 Sec Line  $\Delta 0^{\circ} 21' R$

P.I.  
 +956 2'57' ✓  
 67 2'26' ✓  
 66 1'56' ✓  
 65 1'28' ✓  
 64 0'58' ✓  
 63 0'28' ✓  
 62+039 P.C.

E 7.6  
 L 591.7  
 C 1° R  
 T 296.1

$\frac{1000}{3}$   
 333

65+00 1/4 Line P.I.  $\Delta 5^{\circ} 55' R$  N17°0'E

E.C. 15°-25°  
 +437 6'25'  
 41 ✓ 3'1" ✓ 0°-13'  
 40 - 2'4" ✓ 0°-03'  
 39 ✓ 2'1" ✓ 1'-0"  
 38 ✓ 1'2" ✓  
 37 ✓ 1'1" ✓  
 36 ✓ 0'4" ✓  
 35 0'1" ✓ 32.6'

E 10.2  
 L 683.3  
 T 342.1  
 C 1° L

38+025 Sec Line P.I.  $\Delta 6^{\circ} 50' L$

Sta 110-R.P. { 3" N.P. 58.9 SE  
 2" N.P. 46.5 NE  
 103-R.P. { 3" N.P. 54.4 SE  
 2" Pop. 74.8 NE

97+00 { 5" N.P. 53.6 SE  
 5" Stamp 71.8 NE

Sta 110 R.P. { 2" Green 56.6 SW  
 2" Pop 44.6 NW

85+00 R.P. { 2" N.P. 53.6 SE  
 2" Birch 46.8 NE

80+00 { 2" Birch 55.5 SE  
 124 Stamp 40.9 NE

73+00 R.P. { 5" J.P. 52.3 SE  
 4" J.P. 49.7 NE

R.P. { 4" J.P. 31.8 SW  
 4" J.P. 27.5 NW FE 61+20 FE

60+00 R.P. { 3" Birch 35.6 SE  
 2" Birch J.P. 42.8 NE  
 STK 16' R

53 R.P. { 5" J.P. 64.7 SW  
 3" J.P. 50.0 NW

48 { 5" Birch 48.3 W  
 5" J.P. 51.8 NE

43+00 R.P. { 4" Birch 43.5 W  
 5" J.P. 47.3 SW

R.P. { 3" Pop. 40.4 NE  
 3" Pop 30.4 SE

Wild Plum  
 Clay Soil To 42+00  
 Sandy " 42 To 144+00



4)

144+200 Co. Line

R.P. { 8" J.P. 35.0 SW  
5" Oak 73.9 NW

136+00

R.P. { 2" Oak 45.0 SE  
2" Oak 39.8 NE

131

R.P. { 3" Birch 36.4 SE  
3" Pop. 36.8 NE

125

R.P. { 3" J.P. 43.6 SE  
3" Oak 64.1 NE

P. 15x50 CM

Norway Beach Road

26+30

117+800 1/2 Line  $\Delta 0^{\circ}06'$  R  
65+00 P.I.  $\Delta 6^{\circ}55'$

R.P. { 2" Oak 60.3 SW  
2" Oak 43.8 NW







164.72

15		4.4	160.3
16		3.9	160.8
17		3.4	161.3
	2.40	3.45	161.27
18		3.9	159.8
19		5.8	157.9
20		6.4	157.3
	5.20	7.54	156.13
21		4.3	157.0
22		5.5	155.8
	5.75	5.85	155.48
23		5.8	155.4
24		5.6	155.6
25		5.4	155.8
26		5.2	156.0
27		4.8	156.4
28		4.9	156.3
	8.46	4.95	156.28
29		7.0	157.7
	+60	3.7	161.0
30		3.7	161.0
31		9.0	155.7
32		10.0	154.7
33		9.9	154.8
	5.25	9.91	154.83

Clay soil

$\frac{-03}{33}$	$\frac{-04}{17}$	$\frac{-25}{15}$	$\frac{-05}{10}$	44	$\frac{-02}{9}$	$\frac{-24}{15}$	$\frac{-10}{17}$	$\frac{-10}{34}$
$\frac{+03}{36}$	$\frac{00}{17}$	$\frac{-20}{15}$	$\frac{-03}{10}$	39	$\frac{-05}{11}$	$\frac{-26}{16}$	$\frac{-04}{17}$	$\frac{-05}{34}$
$\frac{00}{33}$	$\frac{-01}{15}$	$\frac{-26}{14}$	$\frac{-06}{9}$	34	$\frac{-04}{17}$	$\frac{-23}{16}$	$\frac{-04}{19}$	$\frac{-07}{31}$

$\frac{-03}{34}$	$\frac{-03}{15}$	$\frac{-23}{14}$	$\frac{-06}{9}$	39	$\frac{-04}{17}$	$\frac{-26}{19}$	$\frac{-06}{19}$	$\frac{-07}{31}$
$\frac{00}{31}$	$\frac{-03}{14}$	$\frac{-20}{13}$	$\frac{-05}{7}$	58	$\frac{-10}{14}$	$\frac{-23}{18}$	$\frac{-06}{20}$	$\frac{-10}{36}$
$\frac{-01}{29}$	$\frac{-04}{13}$	$\frac{24}{14}$	$\frac{-07}{7}$	64	$\frac{-07}{14}$	$\frac{-24}{19}$	$\frac{-10}{20}$	$\frac{-10}{35}$

Sp. in 12 Elm 50' R 20440

$\frac{+02}{30}$	$\frac{+05}{11}$	$\frac{-22}{10}$	$\frac{-06}{5}$	43	$\frac{-14}{14}$	$\frac{-30}{18}$	$\frac{-10}{19}$	$\frac{-17}{32}$	
$\frac{00}{30}$	$\frac{-04}{14}$	$\frac{-26}{10}$	$\frac{-07}{5}$	55	$\frac{+01}{5}$	$\frac{-06}{13}$	$\frac{-27}{13}$	$\frac{-10}{20}$	$\frac{-10}{31}$

$\frac{-02}{30}$	$\frac{+01}{10}$	$\frac{-19}{9}$	$\frac{-05}{5}$	58	$\frac{00}{5}$	$\frac{-09}{13}$	$\frac{-25}{19}$	$\frac{-10}{20}$	$\frac{-13}{31}$
$\frac{-07}{30}$	$\frac{-08}{13}$	$\frac{-23}{11}$	$\frac{-06}{6}$	56	$\frac{-07}{18}$	$\frac{-22}{19}$	$\frac{-01}{20}$	$\frac{00}{33}$	

$\frac{00}{30}$	$\frac{-04}{13}$	$\frac{-23}{11}$	$\frac{-06}{6}$	54	$\frac{-08}{13}$	$\frac{-25}{17}$	$\frac{-07}{19}$	$\frac{-09}{30}$	
$\frac{-03}{30}$	$\frac{-09}{11}$	$\frac{-27}{12}$	$\frac{-07}{7}$	52	$\frac{00}{6}$	$\frac{-11}{13}$	$\frac{-24}{17}$	$\frac{-07}{18}$	$\frac{-07}{34}$

$\frac{-04}{30}$	$\frac{-04}{13}$	$\frac{-22}{12}$	$\frac{-07}{7}$	48	$\frac{-09}{17}$	$\frac{-29}{17}$	$\frac{-07}{19}$	$\frac{-07}{30}$
$\frac{-09}{30}$		$\frac{-05}{13}$	$\frac{-20}{12}$	49	$\frac{-05}{13}$	$\frac{-20}{17}$	$\frac{-05}{19}$	$\frac{-07}{31}$

$\frac{-05}{30}$	$\frac{-04}{14}$	$\frac{-22}{12}$	$\frac{-06}{9}$	70	$\frac{-08}{12}$	$\frac{-25}{17}$	$\frac{-06}{18}$	$\frac{-08}{33}$
$\frac{-06}{30}$	$\frac{-04}{16}$	$\frac{-26}{14}$	$\frac{-06}{10}$	37	$\frac{-06}{11}$	$\frac{-20}{16}$	$\frac{-03}{18}$	$\frac{00}{30}$

		$\frac{-27}{33}$	$\frac{-20}{15}$	37	$\frac{-06}{11}$	$\frac{-23}{16}$	$\frac{-03}{17}$	$\frac{-07}{32}$
$\frac{-06}{31}$	$\frac{-03}{11}$	$\frac{-21}{15}$	$\frac{-01}{10}$	90	$\frac{-05}{11}$	$\frac{24}{16}$	$\frac{-10}{17}$	$\frac{-10}{30}$

$\frac{-02}{30}$	$\frac{-03}{16}$	$\frac{-26}{15}$	$\frac{-06}{10}$	100	$\frac{-04}{14}$	$\frac{-27}{17}$	$\frac{-03}{18}$	$\frac{00}{30}$
$\frac{00}{30}$	$\frac{-03}{17}$	$\frac{-22}{15}$	$\frac{-04}{16}$	99	$\frac{-07}{11}$	$\frac{-24}{15}$	$\frac{-07}{17}$	$\frac{00}{31}$



7

160.08

34		54	154.7
35		53	154.8
B.M		5.12	154.96
36		43	155.8
37		53	154.8
38		6.0	154.1
39		49	155.2
	504	160.24	4.88 155.20
40		6.5	153.7
41		7.0	153.2
42		33	156.9
43		4.6	155.6
44		7.3	152.9
	5.37	158.36	7.25 152.99
45		6.5	151.9
46		7.6	150.8
47		7.8	150.6
48		3.2	155.2
+40		2.7	155.7
49		6.2	152.2
50+35		7.7	150.7
50		6.5	151.9
	4.25	156.07	6.54 151.82
+40		4.1	152.0

Clay Soil

End Clay  
4.1.10

Sandy Soil

No Dr

No Dr

No Dr

-08/27	-10/16	-30/15	-10/11	54	-11/11	-30/16	-13/17	-20/20	
-10/31	-10/16	-23/14	-10/11	53	00/5	-19/9	-27/14	-12/16	-07/31

14" Oak 32' R. 35+50

-10/26	-09/15	-23/11	-05/3	43	-09/12	-27/16	-05/18	00/32	
-03/29	-05/17	-23/11	-07/7	53	-05/13	-23/19	-04/21	-04/31	
00/26	-01/17	14/3	00/3	60	+02/20	-20/25	00/28	00/35	
+06/30	+07/3	-20/16	-03/7	49	+04/6	-04/19	-23/23	-04/24	-05/27

-07/29	-01/14	-20/17	-06/7	65	+03/5	-03/15	-27/19	+04/21	-03/32
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-11/30	-09/17	-24/14	-09/10	70	-07/11	-20/16	-06/17	00/30
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-07/27	-03/18	-18/16	-05/11	33	-04/9	-16/14	+03/16	-04/32
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-04/27	-03/17	-19/16	-04/11	46	-03/11	-16/16	+02/18	+02/31
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-04/30	-03/17	-20/16	-05/11	73	-04/17	-13/16	00/18	00/35
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+03/29	00/16	-18/15	00/10	65	-05/12	-16/17	00/18	+03/32
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-06/30	-03/15	-20/14	-04/9	76	-02/13	-20/17	-04/19	00/30
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-20/34	-10/16	-25/14	-05/9	78	-04/17	-15/17	00/18	+05/31
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-20/30	-13/16	-24/14	-04/9	32	-06/9	-09/16	+13/17	+23/31
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-10/31	-06/15	-20/14	-04/8	27	-03/9	-10/15	+14/17	+20/28
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-07/29	-04/16	-20/15	-03/10	62	00/9	-13/15	00/17	+05/33
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-03/30	-07/16	-20/15	-03/11	77	-04/9	-26/15	-13/17	-12/31
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00/30	00/16	-11/14	-06/10	65	-05/9	-23/15	-06/16	-10/28
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-03/30	-03/16	-20/15	-05/11	41	-04/9	-20/14	00/16	-02/29
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15607

51		6.2	149.9
BM		5.30	150.77
52		5.2	150.9
+50		4.9	151.2
53		6.3	149.8
54		8.4	147.7
55		12.4	143.7
	1.44	145.11	12.40 143.67
56		4.1	141.0
57		5.5	139.6
58		5.2	139.9
<del>57</del>	7.74	147.75	5.10 140.01
59		5.7	142.1
+50		4.1	143.7
60		5.0	142.8
61		9.3	138.5
62		7.0	140.8
	5.05	145.81	6.99 140.76
63		4.6	141.2 D-E
64		5.8	140.0 24" CM
65		5.6	140.2
66		5.4	140.4
67		4.9	140.9
	5.83	146.72	4.92 140.89
<del>68</del> +50		4.8	141.9

$+0.5/30$	$-0.1/17$	$-1.6/14$	$0.0/2$	62	$-0.4/9$	$-1.5/14$	$+0.1/16$	$+0.3/30$
5" Papi 56" R 52+0.0								
$+0.7/27$	$0.0/21$	$-1.3/18$	$-0.3/11$	52	$-0.2/11$	$-1.0/16$	$+0.1/18$	$-0.2/32$
$+1.6/35$	$+1.3/19$	$-0.4/11$	$+0.5/14$	49	$-0.6/10$	$-2.5/16$	$-1.5/18$	$-1.8/34$
$+1.3/33$	$+1.1/16$	$-1.0/16$	$+0.2/11$	63	$-1.0/9$	$-2.4/15$	$-1.0/17$	$-1.0/21$
$+0.3/25$	$+0.3/14$	$-1.3/16$	$+0.3/11$	8.4	$-0.1/10$	$-2.0/15$	$-0.5/17$	$-0.7/32$
$+0.8/24$	$+0.9/14$	$-1.1/13$	$-0.1/3$	12.4	$-0.4/11$	$-1.7/16$	$0.0/18$	$0.0/32$
$-0.2/27$	$0.0/15$	$-1.7/14$	$-0.3/9$	4.1	$0.0/11$	$-1.7/16$	$-0.4/18$	$0.0/34$
$0.0/30$	$+0.1/3$	$-1.4/14$	$-0.2/9$	5.5	$-0.3/13$	$-2.9/16$	$-0.2/18$	$0.0/30$
$+0.3/24$	$0.0/13$	$-2.0/14$	$-0.5/6$	5.2	$-0.3/13$	$-1.7/19$	$-0.2/21$	L.0
$+1.0/31$	$+0.4/15$	$1.3/14$	$-0.1/9$	5.7	$-0.6/13$	$-2.0/19$	$-0.6/21$	$-0.7/30$
$+0.1/20$	$+0.3/15$	$-2.0/13$	$0.0/8$	4.1	$0.0/11$	$-2.0/15$	$-0.3/19$	$-0.5/26$
$+0.3/22$	$+0.7/15$	$-1.3/15$	$+0.3/9$	5.0	$-0.2/12$	$-1.7/17$	$0.0/19$	$-0.3/30$
$-0.4/16$	$-0.2/15$	$-1.4/14$	$-1.0/9$	9.3	$-0.2/11$	$-1.5/14$	$-0.3/19$	$0.0/30$
$-0.3/22$	$-0.1/17$	$-1.5/15$	$-0.1/11$	7.0	$+0.1/10$	$-2.0/15$	$-0.7/18$	$0.0/31$
$+0.3/30$	$0.0/9$	$-1.3/18$	$-0.3/14$	4.6	$-0.9/5$	$-2.0/10$	$-0.5/12$	$-0.3/27$
$+0.2/24$	$0.0/22$	$1.1/12$	$0.0/5$	5.8	$-0.7/5$	$+0.0/6$	$+0.3/30$	
$0.0/31$	$0.0/25$	$-1.4/11$	$0.0/5$	5.6	$-0.3/5$	$-2.0/9$	$-0.5/10$	$0.0/30$
$-0.1/20$	$-0.1/12$	$-1.5/19$	$-0.3/13$	5.4	$-0.3/7$	$-1.7/12$	$0.0/14$	$0.0/30$
$+0.2/21$	$-0.2/14$	$-2.0/16$	$-0.1/11$	4.9	$-0.4/9$	$-1.8/15$	$-0.1/16$	$+0.3/30$
$-0.1/30$	$-0.1/17$	$-2.0/15$	$-0.5/10$	4.8	$-0.3/10$	$-2.0/15$	$0.0/17$	$+0.3/30$



9

146.72

68		4.5	142.2
+50		5.4	141.3
69		5.1	141.6
BMI		5.20	141.52
70		4.8	141.9
71	1	3.4	143.3
72		5.6	141.1
	8.25	149.37	5.60 141.12
73		6.7	142.7
74		4.9	144.5
75		3.8	145.6
+45		3.3	146.1
76		6.7	142.7 Dr. W.
+50		9.3	140.1 15"
77		8.5	140.9
78		2.8	146.6
	8.24	154.78	2.83 146.54
+50		8.1	146.7
79		9.6	145.2
+50		8.0	146.8
80		5.8	149.0
+55		2.4	152.4
81		5.2	149.6
+50		8.4	146.4

-02/0	-03/10	-16/15	00/17	+03/30	4.5	-03/10	-16/15	00/17	+03/30
+03/10	+02/15	-14/15	-03/9	5.4	00/10	-14/15	00/16	00/30	
+04/14	-01/15	-17/13	-06/9	5.1	-06/11	-17/15	-01/16	-03/31	
4" Poplar 6.5" R 6.9 +00									
-07/14	-02/14	-18/13	-06/8	4.8	-03/9	-17/15	00/16	+03/31	
-02/30	-02/16	-19/13	-04/6	3.4	00/10	-15/15	+0/17	+04/31	
00/31	-03/16	-17/15	-02/10	5.6	-03/11	-17/16	-04/17	-04/30	
-03/30	-03/16	-17/13	-03/10	6.7	-05/9	-20/15	-03/16	-05/30	
-10/30	-05/16	-18/15	-05/10	4.9	-04/11	-16/16	00/17	-03/31	
-02/29	-08/18	-24/15	-01/10	3.8	-03/11	-19/15	+05/17	+08/30	
+03/17	+04/17	-09/14	-02/9	3.3	-03/10	-10/14	+14/17	+15/30	
+10/30	+03/16	-11/14	-02/9	6.7	00/9	-15/14	-09/16	-02/30	
-07/16	-17/15	-25/15	-05/8	9.3	-07/9	-25/14	-20/16	-13/30	
+08/30	-02/16	-24/14	-06/8	8.5	-05/9	-20/13	-13/16	-07/30	
+05/30	+05/16	-14/14	-02/9	2.8	00/10	-10/15	+08/17	+13/30	
00/30	+03/17	-12/16	-07/11	8.1	-03/10	-10/14	+13/17	+14/30	
00/30	-03/17	-20/15	-03/10	9.6	-03/10	-17/14	-08/16	-10/30	
-07/30	-01/17	-21/16	-07/11	5.0	-04/9	-18/14	-02/16	-07/31	
-03/30	-01/17	-17/14	-03/10	5.8	00/9	-11/14	+06/15	+03/31	
-03/30	-01/11	-15/15	-07/11	2.4	-06/10	-10/14	-01/17	00/30	
+16/31	+10/17	-07/16	+08/16	5.2	+05/9	-07/14	+08/15	+16/30	
-10/30	-11/19	-22/17	-05/12	8.4	-06/8	-17/13	-08/14	-07/30	



	154.78		
82		98	145.0
	4.19	149.13	9.84 144.94
83		54	143.7
84		4.1	145.0
85		6.0	143.1 Dr. W
+50		7.1	142.0 15"
86	1	6.9	142.2
87		5.4	143.7
	7.10	150.79	5.44 143.69
88		5.2	145.6
+35		4.6	146.2
89		5.4	145.4
+50		3.9	146.9
90		5.7	145.1
BM		7.60	143.19
+50		8.0	142.8
91		8.5	142.3
92		8.0	142.8 Dr. W
	7.30	150.06	8.03 142.76 15"
93		5.8	144.3
+50		5.0	145.1
94		5.1	145.0
95		5.5	144.6
	5.61	150.02	5.65 144.41

	$\frac{00}{20}$	$\frac{-03}{19}$	$\frac{-20}{18}$	$\frac{+06}{17}$	98	$\frac{00}{7}$	$\frac{-16}{16}$	$\frac{+03}{14}$	$\frac{00}{27}$
	$\frac{-03}{24}$	$\frac{-01}{20}$	$\frac{-18}{18}$	$\frac{-03}{13}$	54	$\frac{-03}{7}$	$\frac{-20}{11}$	$\frac{-01}{13}$	$\frac{-07}{29}$
	$\frac{-03}{25}$	$\frac{-01}{20}$	$\frac{-20}{18}$	$\frac{-03}{13}$	41	$\frac{-01}{5}$	$\frac{-20}{10}$	$\frac{+01}{11}$	$\frac{+04}{28}$
	$\frac{+03}{25}$	$\frac{-03}{24}$	$\frac{-17}{18}$	$\frac{-02}{14}$	6.0	$\frac{00}{7}$	$\frac{-16}{10}$	$\frac{+03}{12}$	$\frac{+09}{30}$
	$\frac{00}{21}$	$\frac{00}{20}$	$\frac{-20}{18}$	$\frac{-01}{13}$	7.1	$\frac{-05}{5}$	$\frac{-17}{9}$	$\frac{-02}{11}$	$\frac{-02}{30}$
	$\frac{+03}{24}$	$\frac{+02}{21}$	$\frac{16}{19}$	$\frac{-01}{13}$	6.9	$\frac{-07}{5}$	$\frac{-17}{9}$	$\frac{-04}{10}$	$\frac{-06}{27}$
	$\frac{+05}{30}$	$\frac{+05}{21}$	$\frac{-15}{20}$	$\frac{00}{16}$	5.4	$\frac{-02}{6}$	$\frac{-20}{10}$	$\frac{-04}{12}$	$\frac{-02}{26}$
	$\frac{-05}{30}$	$\frac{-05}{21}$	$\frac{-21}{20}$	$\frac{-03}{15}$	5.2	$\frac{-03}{6}$	$\frac{-15}{10}$	$\frac{00}{12}$	$\frac{+03}{30}$
	$\frac{00}{30}$	$\frac{+03}{21}$	$\frac{-17}{21}$	$\frac{00}{16}$	4.6	$\frac{-04}{5}$	$\frac{-17}{10}$	$\frac{+03}{11}$	$\frac{+03}{20}$
	$\frac{+03}{31}$	$\frac{01}{21}$	$\frac{-17}{20}$	$\frac{00}{15}$	5.4	$\frac{-06}{5}$	$\frac{-19}{10}$	$\frac{-07}{11}$	$\frac{-10}{29}$
	$\frac{00}{21}$	$\frac{-02}{20}$	$\frac{-16}{18}$	$\frac{00}{15}$	3.9	$\frac{-03}{5}$	$\frac{-18}{9}$	$\frac{+02}{10}$	$\frac{00}{30}$
	$\frac{+03}{30}$	$\frac{+05}{21}$	$\frac{-10}{24}$	$\frac{+03}{16}$	5.7	$\frac{-01}{5}$	$\frac{-12}{9}$	$\frac{00}{10}$	$\frac{+02}{30}$
	3" Poplar 70' R 90+40 (cannot find)								
	$\frac{00}{20}$	$\frac{00}{24}$	$\frac{-16}{21}$	$\frac{00}{17}$	8.0	$\frac{-01}{3}$	$\frac{-15}{8}$	$\frac{00}{9}$	$\frac{00}{26}$
	$\frac{00}{20}$	$\frac{00}{24}$	$\frac{-17}{21}$	$\frac{00}{17}$	8.5	$\frac{-03}{3}$	$\frac{-11}{7}$	$\frac{-01}{8}$	$\frac{00}{30}$
	$\frac{00}{20}$	$\frac{-03}{24}$	$\frac{-20}{20}$	$\frac{00}{16}$	8.0	$\frac{-03}{2}$	$\frac{-17}{7}$	$\frac{00}{8}$	$\frac{+06}{30}$
	$\frac{00}{27}$	$\frac{-20}{24}$	$\frac{-04}{20}$		5.8	$\frac{-14}{7}$	$\frac{+03}{8}$	$\frac{+10}{29}$	
	$\frac{00}{25}$	$\frac{-18}{23}$	$\frac{00}{19}$		5.0	$\frac{-04}{3}$	$\frac{-20}{8}$	$\frac{-01}{9}$	$\frac{+01}{30}$
	$\frac{-03}{21}$	$\frac{-01}{12}$	$\frac{00}{19}$		5.1	$\frac{-03}{3}$	$\frac{-20}{7}$	$\frac{00}{8}$	$\frac{00}{30}$
	$\frac{00}{41}$	$\frac{00}{24}$	$\frac{-20}{23}$	$\frac{-04}{15}$	5.5	$\frac{-04}{3}$	$\frac{-20}{7}$	$\frac{-03}{8}$	$\frac{-03}{30}$



150.02

96	6.1	143.9
97	6.2	143.8
+50	6.8	143.2
98	6.4	143.6
99	5.1	144.9
100	5.5	144.5
101	4.4	145.6

4.66 150.21 4.47 145.55

102	5.2	145.0
103	5.2	145.0
104	6.8	143.4
105	8.5	141.7

10.97 152.65 8.53 141.68

1 +50	10.3	142.4
106	7.5	145.2
107	6.4	146.3
108	5.2	147.5
+50	5.1	147.6

B.M 4.34 148.31

109	4.0	148.7
+75	3.7	149.0
110	5.2	147.5
+50	8.4	144.3
111	10.4	142.3

3.60 145.87 10.38 142.27

6.1	$\frac{-02}{31} \frac{00}{24} -18 \frac{-05}{22} \frac{-03}{18}$	6.1	$\frac{-03}{3} \frac{-19}{7} \frac{-03}{8} \frac{00}{30}$
6.2	$\frac{-06}{23} \frac{-02}{24} \frac{-21}{22} \frac{-03}{13}$	6.2	$\frac{00}{24} \frac{-18}{9} \frac{+03}{8} \frac{-02}{30}$
6.8	$\frac{-03}{24} \frac{-19}{22} \frac{-03}{17}$	6.8	$\frac{-05}{5} \frac{-13}{8} \frac{00}{9} \frac{+02}{30}$
6.4	$\frac{-02}{35} \frac{00}{24} \frac{-17}{22} \frac{00}{17}$	6.4	$\frac{-03}{4} \frac{-14}{4} \frac{+04}{10} \frac{00}{30}$
5.1	$\frac{00}{33} \frac{00}{24} \frac{-19}{21} \frac{00}{16}$	5.1	$\frac{-04}{4} \frac{-20}{9} \frac{-05}{10} \frac{-01}{30}$
5.5	$\frac{-02}{31} \frac{-04}{21} \frac{-20}{20} \frac{-01}{15}$	5.5	$\frac{-03}{3} \frac{-19}{8} \frac{-02}{10} \frac{+02}{29}$
4.4	$\frac{-02}{31} \frac{-01}{21} \frac{-21}{20} \frac{-04}{14}$	4.4	$\frac{-03}{5} \frac{-15}{9} \frac{+01}{11} \frac{+02}{30}$

5.2	$\frac{-05}{31} \frac{-05}{22} \frac{-20}{21} \frac{-03}{16}$	5.2	$\frac{-02}{4} \frac{-14}{8} \frac{+03}{9} \frac{+03}{30}$
5.2	$\frac{-01}{33} \frac{+03}{24} \frac{-20}{21} \frac{-03}{17}$	5.2	$\frac{-04}{3} \frac{-19}{9} \frac{-01}{9} \frac{+01}{29}$
6.8	$\frac{-01}{31} \frac{00}{24} \frac{-20}{20} \frac{-04}{15}$	6.8	$\frac{-04}{4} \frac{-19}{9} \frac{-02}{11} \frac{-04}{31}$
8.5	$\frac{-01}{33} \frac{-01}{21} \frac{-19}{19} \frac{-03}{14}$	8.5	$\frac{-05}{5} \frac{-12}{9} \frac{-01}{11} \frac{00}{31}$

10.3	$\frac{-03}{31} \frac{-06}{21} \frac{-20}{20} \frac{-08}{15}$	10.3	$\frac{-06}{5} \frac{-20}{9} \frac{-06}{11} \frac{-07}{33}$
7.5	$\frac{00}{21} \frac{-01}{21} \frac{-20}{20} \frac{-06}{15}$	7.5	$\frac{00}{4} \frac{-14}{9} \frac{+06}{10} \frac{+02}{30}$
6.4	$\frac{+05}{24} \frac{00}{21} \frac{-17}{20} \frac{-05}{16}$	6.4	$\frac{-04}{4} \frac{-18}{9} \frac{-01}{10} \frac{+03}{30}$
5.2	$\frac{00}{34} \frac{+05}{22} \frac{-17}{20} \frac{+01}{15}$	5.2	$\frac{-03}{5} \frac{-14}{9} \frac{00}{10} \frac{-03}{30}$
5.1	$\frac{-05}{30} \frac{-07}{19} \frac{-19}{19} \frac{-04}{14}$	5.1	$\frac{-02}{5} \frac{-14}{10} \frac{00}{11} \frac{00}{30}$

4" J. Pine 65' R 108+50

4.0	$\frac{-05}{31} \frac{00}{19} \frac{-20}{18} \frac{-05}{13}$	4.0	$\frac{-04}{6} \frac{-17}{11} \frac{00}{13} \frac{+03}{30}$
3.7	$\frac{00}{29} \frac{+01}{19} \frac{-15}{17} \frac{-03}{13}$	3.7	$\frac{-03}{5} \frac{-11}{12} \frac{+02}{12} \frac{+05}{30}$
5.2	$\frac{+01}{29} \frac{+03}{19} \frac{-14}{18} \frac{-01}{15}$	5.2	$\frac{-02}{7} \frac{-11}{12} \frac{+03}{14} \frac{00}{31}$
8.4	$\frac{+01}{27} \frac{+02}{19} \frac{-14}{17} \frac{00}{13}$	8.4	$\frac{-02}{8} \frac{-12}{10} \frac{00}{12} \frac{00}{32}$
10.4	$\frac{-02}{30} \frac{-01}{19} \frac{-20}{18} \frac{-05}{13}$	10.4	$\frac{-05}{6} \frac{-15}{12} \frac{00}{13} \frac{00}{30}$







153.36

125+50		5.1	148.3
126		7.2	146.2
+35		8.5	144.9
127		9.0	144.4
10.45	154.81	9.00	144.36
128		10.8	144.0
129		7.0	147.8
130		4.8	150.0
131		5.5	149.3
132		6.4	148.4
133		10.6	144.2
189	146.08	10.62	144.19
134		6.8	139.3
+50		8.4	137.7
135		9.5	136.6
136		7.3	138.8
238	141.21	7.25	138.83
+50		3.2	138.0
137		6.1	135.1
138		11.0	130.2
2.70	132.93	10.98	130.23
139		4.6	128.3
+50		5.9	127.0
140		6.0	126.9
+50		5.3	127.6

DrW

Dr.E  
15" CM

$\frac{-01}{30} \frac{-03}{18} \frac{-20}{10} \frac{-02}{11}$	5.1	$\frac{-04}{7} \frac{-12}{12} \frac{00}{13} \frac{-04}{31}$
$\frac{+03}{30} \frac{+03}{17} \frac{-09}{16} \frac{00}{12}$	7.2	$\frac{00}{8} \frac{-06}{12} \frac{10}{13} \frac{-04}{26}$
$\frac{+05}{30} \frac{+08}{16} \frac{-07}{12} \frac{+04}{11}$	8.5	$\frac{00}{12} \frac{+06}{12} \frac{+04}{30}$
$\frac{+07}{30} \frac{+07}{18} \frac{-08}{16} \frac{+04}{11}$	9.0	$\frac{+02}{9} \frac{-04}{13} \frac{+04}{14} \frac{+03}{30}$
$\frac{-02}{30} \frac{-01}{18} \frac{-09}{15} \frac{+04}{12}$	10.8	$\frac{+03}{8} \frac{-09}{12} \frac{+04}{14} \frac{+06}{28}$
$\frac{-06}{30} \frac{-03}{18} \frac{-10}{11} \frac{-03}{14} \frac{-02}{3}$	7.0	$\frac{+07}{7} \frac{-07}{16} \frac{+03}{13} \frac{+03}{25}$
$\frac{00}{30} \frac{+06}{19} \frac{-04}{19} \frac{+02}{13} \frac{-03}{8}$	4.8	$\frac{-03}{7} \frac{-11}{11} \frac{+04}{12} \frac{00}{30}$
$\frac{+07}{30} \frac{+05}{20} \frac{-10}{18} \frac{+04}{14}$	5.5	$\frac{+03}{7} \frac{-10}{11} \frac{+02}{13} \frac{+05}{26}$
$\frac{+10}{33} \frac{+06}{21} \frac{-04}{19} \frac{+01}{15} \frac{-03}{3}$	6.4	$\frac{+04}{7} \frac{-11}{12} \frac{00}{13} \frac{-06}{30}$
$\frac{+23}{32} \frac{+17}{19} \frac{+01}{16}$	10.6	$\frac{+02}{7} \frac{-21}{13} \frac{-09}{15} \frac{-22}{30}$
$\frac{+12}{32} \frac{+16}{20} \frac{+01}{16} \frac{+03}{15}$	6.8	$\frac{-01}{7} \frac{-20}{12} \frac{-12}{14} \frac{-22}{28}$
$\frac{+16}{32} \frac{+18}{19} \frac{00}{17} \frac{+02}{14}$	8.4	$\frac{+01}{6} \frac{-16}{12} \frac{-12}{12} \frac{-20}{28}$
$\frac{+15}{35} \frac{+10}{19} \frac{-04}{15}$	9.5	$\frac{-02}{6} \frac{-11}{13} \frac{-20}{25}$
$\frac{+07}{35} \frac{+04}{21} \frac{-04}{19} \frac{-01}{15}$	7.3	$\frac{+01}{7} \frac{+17}{13} \frac{-03}{15} \frac{-17}{28}$
$\frac{+16}{38} \frac{+09}{19} \frac{-03}{18} \frac{-01}{15}$	3.2	$\frac{+01}{7} \frac{-20}{13} \frac{-10}{14} \frac{-22}{29}$
$\frac{+14}{31} \frac{+08}{19} \frac{-04}{18} \frac{+00}{14}$	6.1	$\frac{+04}{8} \frac{+18}{13} \frac{-06}{15} \frac{-17}{27}$
$\frac{+10}{35} \frac{+04}{18} \frac{00}{17} \frac{+03}{13}$	11.0	$\frac{00}{8} \frac{+18}{13} \frac{-09}{14} \frac{-20}{30}$
$\frac{+33}{39} \frac{+26}{17} \frac{+10}{17} \frac{+05}{16} \frac{+07}{13}$	4.6	$\frac{+04}{8} \frac{-20}{13} \frac{-16}{15} \frac{-22}{31}$
$\frac{+33}{30} \frac{+17}{17} \frac{+15}{17} \frac{00}{16} \frac{+03}{13}$	5.9	$\frac{00}{7} \frac{-20}{13} \frac{-20}{13}$
$\frac{+23}{36} \frac{+05}{19} \frac{-07}{17} \frac{00}{13}$	6.0	$\frac{-02}{9} \frac{12}{14} \frac{-04}{15} \frac{-06}{30}$
$\frac{+16}{38} \frac{+09}{19} \frac{-04}{17} \frac{00}{13}$	5.3	$\frac{+07}{9} \frac{-06}{14} \frac{+10}{16} \frac{+10}{31}$



14

132.93

141		40	128.9
14V		18	131.1
T.P	9.60	140.69	1.84
143		74	133.3
144		52	135.5
145+20		52	135.5
145		55	135.2
146		54	135.3
147		22	138.5
148		+30	143.7
149		+80	148.7
BM		3.45	137.24

$\frac{+15}{35}$	$\frac{+83}{17}$	$\frac{-10}{16}$	$\frac{+02}{11}$	40	$\frac{+06}{18}$	$\frac{-07}{15}$	$\frac{+06}{16}$	$\frac{+11}{31}$
$\frac{+03}{14}$	$\frac{00}{16}$	$\frac{-12}{15}$	$\frac{+03}{11}$	18	$\frac{+05}{11}$	$\frac{-05}{15}$	$\frac{+13}{17}$	$\frac{+23}{35}$

$\frac{-03}{33}$	$\frac{00}{16}$	$\frac{-10}{15}$	$\frac{+01}{11}$	74	$\frac{+03}{18}$	$\frac{-07}{14}$	$\frac{+01}{17}$	$\frac{-02}{32}$
$\frac{00}{40}$	$\frac{+05}{16}$	$\frac{-11}{15}$	$\frac{00}{10}$	52	$\frac{00}{10}$	$\frac{-10}{14}$	$\frac{00}{15}$	$\frac{-10}{30}$
$\frac{00}{34}$	$\frac{+03}{16}$	$\frac{-10}{14}$	$\frac{+03}{9}$	52	$\frac{+03}{10}$	$\frac{-10}{15}$	$\frac{00}{16}$	$\frac{-28}{34}$

6" X Pine 110' L 144+40



15

S.A. Road No. 10 C&G.

0+00-12+35 0.9 Ac. C&G Heavy

12+35 26+40 1.8 Ac C&G Heavy

38+0.25-65+00 1.8 Ac C&G Heavy

65+00 75+00 0.7 Ac C&G Heavy

75+00 91+40 - 1.1 C&G Light

91+40 117+80 1.8 C&G Light

117+80-144+20 1.8 C&G Light



17) Transit Notes Co. Aid Road No. 2  
 Smokey Hollow Twp Job # 294

Party { Prudlo  
 Bodo  
 Lester

April 16-1938

23

20

16

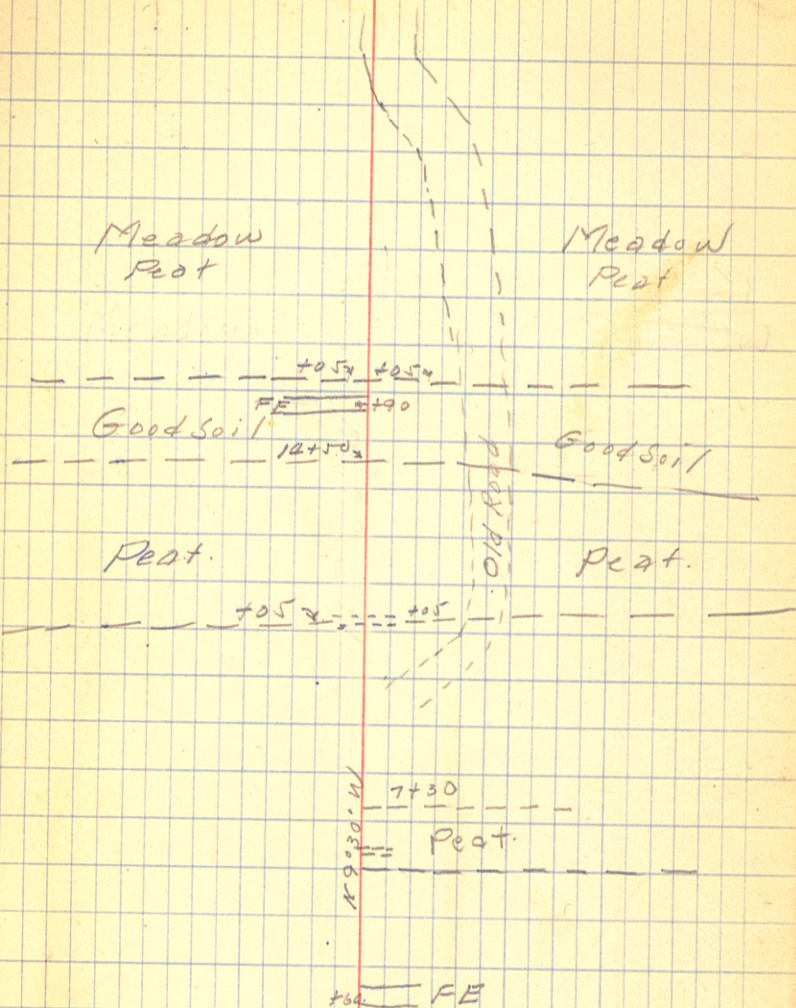
15

11+05. 30 x 26 C.M. in p O.K.

6+68 8 x 24 C.M. Dr. E. O.K.

3

0+00 1/4 Cor. Sec 2-3-140-25.



R.P. 5" Pop 705 SW  
 3" " 1018 NW.



18

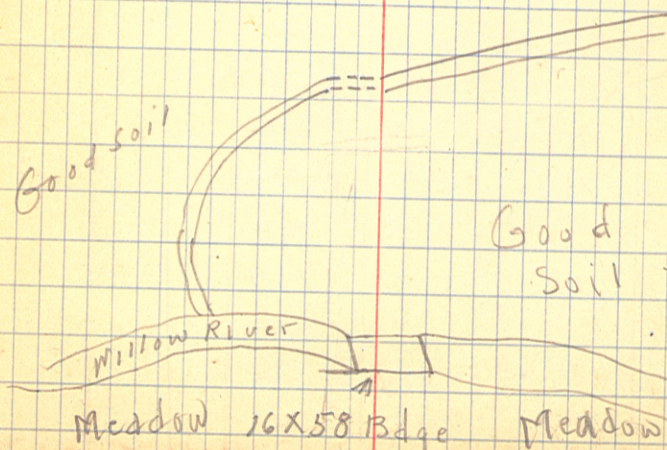
31+463 PI

30

26+10 Sec Line -

24

RP { 6" Pop 60.7 E  
7" Ash 500 NE





Level	Notes	Co. A. & Road No. 2	Smoky Hollow Trwp. Job #294	
BM	6.68	1306.68	1300.00	
0+00			11.0	95.7
1+00			11.7	95.0
2+00			10.7	96.0
+50			7.4	99.3
3			5.7	01.0
+50			4.6	02.1
4			5.1	01.6
+50			6.9	99.8
5			10.2	96.5
+40	225	9871	1022	1296.46
6			9.2	89.5
7		CMC	9.0	89.7
+65			4.0	94.7
8			3.7	95.0
+50			5.8	92.9
9			5.8	92.9
10			7.4	91.3
11			9.2	89.5
BM	165	9470	5.66	93.05
12			9.3	85.4
+05	36 x 28	CMC	10.9	83.8
13			10.0	84.7
14			9.5	85.2
	6.98	9228	9.40	85.30

Radio  
Bodo's  
Kester.

April 17-1980

5" Pop 40 L 3+20

102 33	107 20	117 17	112 14	11.0	117 12	129 15	120 17	128 30
122 30	122 20	122 18	125 15	11.7	125 12	148 17	132 19	135 30
129 30	127 19	135 17	119 13	10.7	106 13	116 17	100 19	100 30
90 30	82 17	74 16	77 10	7.4	78 12	82 15	71 19	67 30
77 30	71 18	77 16	65 16	5.7	61 11	68 15	60 18	54 30
54 30	50 18	63 16	51 12	4.6	45 12	42 17	41 30	
62 30	54 18	63 16	53 13	5.1	57 15	40 18	30 36	
85 30	73 18	88 16	72 12	6.9	70 14	74 16	53 19	42 30
125 30	113 17	125 15	109 11	10.2	109 15	118 17	95 20	82 31
76 30	76 16	84 14	72 10	6.2	62 14	72 18	58 20	52 30
95 30	98 16	111 14	98 11	9.2	85 17	94 21	100 30	
88 30	93 17	110 15	97 11	9.0	87 17	104 20	100 30	
33 30	38 18	48 16	34 12	4.0	56 18	64 20	47 27	49 30
37 30	36 18	52 15	36 12	3.7	51 18	57 20	37 26	36 30
40 30	50 18	63 15	58 12	5.8	60 16	63 16	67 21	71 30
50 30	54 17	68 15	56 11	5.8	66 19	73 21	73 30	
		83 30	80 15	75 11	7.4	75 22	74 30	
		88 30	71 19	76 11	9.2	74 24	96 30	
		91 30			9.3	94 30		
		98 30			10.0	102 11	96 16	94 30
96 30	97 16	112 15	91 12	9.5	101 14	90 19	90 31	

5" Poplar 502 9+50



9228

15		5.6	86.7
16		5.1	87.2
+70		3.6	88.7
17		4.6	87.7
+40		6.1	86.2
18		6.9	85.4
19		6.9	85.4
	5.91 91.74	6.45	85.83
20		6.3	85.4
21		7.8	83.9
22		7.1	84.6
23		6.0	85.7
+43	Edge Bdgc	4.4	87.3
24+01	Edge Bdgc	3.4	88.3
WL		10.7	81.0
Bot Creek		12.9	78.8
+40		4.6	87.1
BM	5.27 94.19	2.82	88.92
25		6.8	87.4
26		6.7	87.5
27		5.6	88.6
28		5.4	88.8
29		6.0	88.2
+01	36x24 CM New	8.4	85.8

57/30	54/15	68/10	47/11	5.6	56/20	4.9/30			
48/30	43/16	70/15	55/11	5.1	54/14	63/18	47/21	47/31	
51/30	52/18	59/17	47/12	3.6	55/15	52/18	48/30		
			51/30	4.6	49/14	52/31			
54/30	58/18	70/17	59/12	6.1	62/13	68/16	56/19	59/30	
68/30	70/18	84/16	70/12	6.9	71/13	84/17	60/19	65/30	
68/30	68/17	82/15	70/11	6.9	71/13	79/16	63/18	63/30	
63/30	66/19	76/18	61/14	6.3	70/8	63/11	62/25	65/31	
69/30	65/18	83/17	74/11	7.8	77/6	68/9	67/20	78/28	LO
73/30	76/18	80/16	75/13	7.1	64/3	64/15	74/21	73/30	
73/30	77/15	79/19	69/12	6.0	58/12	81/20	70/23	70/30	
	66/30	64/10	44/4	4.4	44/9				
LO	129/10	34/1	3.4	34/10	54/14	34/16	34/30		
	42/30	42/17	27/9	4.6	54/14	61/18	52/22	55/30	

(15" Elm. 70' R. 24+10

95/30	79/15	84/13	74/9	6.8	71/8	80/14	75/17	76/30
74/31	75/17	82/15	69/19	6.7	78/5	71/7	70/30	
54/30	55/17	67/14	55/12	5.6	54/30			
58/30	52/14	64/18	56/15	5.4	42/30			
70/27	46/23	45/10	64/5	6.0	48/30			



21

9919

30

5.1

89.1

31

3.6

90.6

$\frac{50}{30}$	$\frac{53}{24}$	$\frac{62}{22}$	$\frac{44}{17}$	$\frac{43}{4}$	5.1	$\frac{64}{5}$	$\frac{55}{7}$	$\frac{53}{30}$	
	$\frac{40}{30}$	$\frac{42}{16}$	$\frac{54}{14}$	$\frac{38}{2}$	3.6	$\frac{39}{5}$	$\frac{56}{13}$	$\frac{46}{15}$	$\frac{46}{30}$

0+00-22+00 05 AC CTG

26+60-29+00 02 AC "



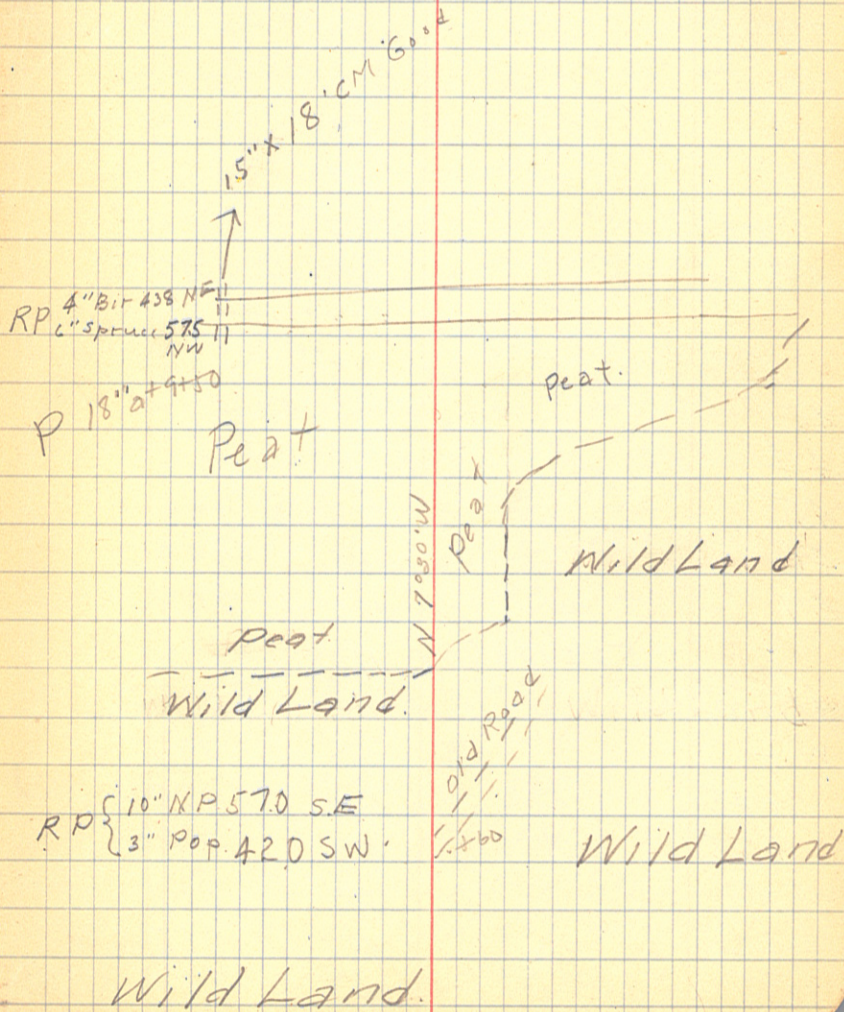
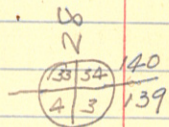
23

Transit Notes Co. A. I. R. #7

Rudlo  
Bodoh  
Lester

April 19-1930.

- +556 E Road
- 48
- 47
- 46
- 45
- 44
- 43
- 42
- 41
- 40
- 39
- 38+00





24

Level Notes CAR #7 Blind Lake Twp.

Prudlo  
Bodoh  
Lester

Apr. 19-1930

Total 1.10 Acct G.

B.M.	2.66	1302.66	1300.00
37+00		35	99.2
+40		35	99.2
38		6.1	96.6
+40		5.4	97.3
39		5.2	97.5
40		9.0	93.7
	1.55	1295.26	8.95 1293.71
41		3.9	91.4
+50		6.7	88.6
42		10.5	84.8
	6.35	1291.13	10.48 1284.78
+50		8.5	82.6
43		9.6	81.5
44		10.2	80.9
45.		11.3	79.8
46		11.4	79.7
47		12.0	79.1
	5.34	1285.39	11.08 1280.05
48		6.9	78.5
WL		5.8	79.6
+45.		6.6	78.8
+55.		4.9	80.5
50' L		5.3	80.1
100' L		4.9	80.5
150		4.5	80.9

Spid 4" Birch 45' L 0+45

42	53	72	57	6.1	70	89	80	81
30	19	16	12		12	17	20	31
38	40	69	50	13.54	64	89	72	54
40	19	16	12		12	17	19	40
42	57	74	55	5.2	54	77	58	50
40	18	16	12		12	17	19	40
116	110	127	104	9.0	86	102	77	63
40	21	19	13		12	17	19	40

42	52	67	44	3.9	43	63	25	23	09
40	20	17	12		13	16	20	26	40
106	83	102	75	6.7	67	91	43	24	
40	20	18	12		12	17	22	43	
142	132	141	116	10.5	105	123	78	52	41
40	21	18	12		11	15	20	41	

104	103	113	96	8.5	88	103	77	36	40
38	16	15	11		12	15	19	40	
106	106	110	100	9.6	93	102	79	24	47
40	17	15	9		13	17	24	47	40
108	105	102	102	10.2	112	92			
40	20	20	20		20	40			
108	111	111	113	11.3	112	84			
40	20	20	20		20	40			
109	113	113	114	11.4	110	104	88		
39	20	20	20		23	30	40		
110	115	115	120	12.0	117	108			
40	24	24	20		20	40			

56	54	62	6.9	60	60	54
80	40	20		20	40	70

5.7	6.0	6.6	5.6
120	70		70
		4.9	5.3/50

64	64	53	5.3	53	68	67
30	10	7		7	10	30
56	61	53	4.9	52	69	57
30	13	8		8	13	15
42	44	48	4.5	47	65	46
33	14	12		9	13	15

Bottom



25)

128539

200' V

4.0 81.4  
4.0 81.4

50' R

4.6 80.8

100' R

2.7 82.7

B.M.

184 1283.55

$\frac{45}{33}$   $\frac{50}{16}$   $\frac{64}{13}$   $\frac{48}{10}$  4.0  $\frac{45}{9}$   $\frac{69}{15}$   $\frac{53}{17}$   $\frac{56}{33}$   
4.0

$\frac{58}{30}$   $\frac{64}{12}$   $\frac{52}{8}$  4.6  $\frac{48}{7}$   $\frac{60}{10}$   $\frac{60}{30}$   
 $\frac{21}{30}$   $\frac{22}{17}$   $\frac{36}{12}$   $\frac{25}{9}$  2.7  $\frac{27}{9}$   $\frac{37}{12}$   $\frac{23}{14}$   $\frac{17}{30}$   
4" Birch 80' R 10+10



26

Co. A #7 Blind Lake

24 ✓

23

22

21+58.0

P.I A 9°00' L

19

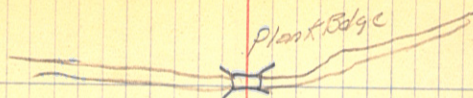
12

11

2+0.0

P.I A 9°00' L

0+0.0



Wild Land

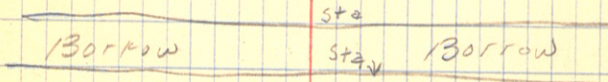
RR 3<sup>rd</sup> Pop 428 SE  
5<sup>th</sup> Pop 355 E

Wild Land

19+40

Swamp  
Peat

Swamp  
Peat.



Swamp  
Peat

Swamp  
Peat

3+50

Field

Field

R.P. { F.P. 32.5 SE  
F.P. 360 NE



27

Sta 38+00 - 0+00

33+140

32

31

30

29

28

27

26

25

RP { 3" Pop. 503 W  
3" Pop. 68.3 NW

Wild Land

Wild Land

Swamp ~~30+12~~

29+00

Swamp

27+30



B.M.	186	130186		1300.00
0-100			0.5	014
0+00			0.8	011
1+00			0.9	010
2+00			2.7	99.2
2+50			3.9	98.0
3			5.2	96.7
4			7.6	94.3
5			7.8	94.1
	230	9636	7.80	94.06
6			3.0	93.4
7			4.7	91.7
8			4.9	91.5
9			5.3	91.1
10			5.7	90.7
11			5.6	90.8
	235	9307	5.64	90.72
12			4.2	88.9
B.M.			2.75	
13			6.1	87.0
14			6.6	86.5
15			7.0	86.1
	465	9091	6.81	86.26
16			5.0	85.9

6" J.P. 60'R 2+90

Same x sec	0.5	Same x sec	
$\frac{-13}{30}$ $\frac{-07}{18}$ $\frac{-30}{76}$ $\frac{-07}{10}$	0.8	$\frac{-02}{10}$ $\frac{-28}{16}$ $\frac{-05}{19}$ $\frac{00}{30}$	
$\frac{-12}{30}$ $\frac{-08}{18}$ $\frac{-32}{76}$ $\frac{-06}{11}$	0.9	$\frac{-04}{12}$ $\frac{-28}{17}$ $\frac{-05}{20}$ $\frac{-05}{30}$	
$\frac{+10}{30}$ $\frac{+12}{19}$ $\frac{-24}{15}$ $\frac{-03}{10}$	2.7	$\frac{00}{12}$ $\frac{-26}{17}$ $\frac{-16}{20}$ $\frac{-09}{30}$	
$\frac{+28}{36}$ $\frac{+30}{22}$ $\frac{-23}{76}$ $\frac{-04}{11}$	3.9	$\frac{-03}{14}$ $\frac{-23}{18}$ $\frac{-12}{21}$ $\frac{-12}{30}$	
$\frac{00}{30}$ $\frac{-03}{19}$ $\frac{-26}{77}$ $\frac{-05}{11}$	5.2	$\frac{-04}{14}$ $\frac{-28}{20}$ $\frac{-14}{20}$ $\frac{-02}{30}$	
$\frac{-13}{30}$ $\frac{-17}{11}$ $\frac{-05}{8}$	7.6	$\frac{-02}{8}$ $\frac{-11}{11}$ $\frac{-10}{30}$	
$\frac{-15}{30}$ $\frac{-20}{12}$ $\frac{-02}{8}$	7.8	$\frac{-04}{8}$ $\frac{-13}{10}$ $\frac{-12}{30}$	
$\frac{-13}{30}$ $\frac{-15}{11}$ $\frac{-03}{7}$	3.0	$\frac{-03}{17}$ $\frac{-15}{10}$ $\frac{-15}{30}$	
$\frac{-08}{30}$ $\frac{-10}{10}$ $\frac{-02}{7}$	4.7	$\frac{-02}{7}$ $\frac{-13}{11}$ $\frac{-13}{30}$	
$\frac{-10}{30}$ $\frac{-14}{10}$ $\frac{-03}{7}$	4.9	$\frac{00}{7}$ $\frac{-14}{10}$ $\frac{-14}{30}$	
$\frac{-07}{30}$ $\frac{-10}{10}$ $\frac{-02}{7}$	5.3	$\frac{-03}{7}$ $\frac{-13}{9}$ $\frac{-14}{30}$	
$\frac{-10}{30}$ $\frac{-12}{10}$ $\frac{-04}{6}$	5.7	$\frac{-02}{7}$ $\frac{-09}{11}$ $\frac{-08}{30}$	
$\frac{+03}{30}$ $\frac{-04}{18}$ $\frac{-19}{15}$ $\frac{-11}{10}$ $\frac{-02}{6}$	5.6	$\frac{-06}{8}$ $\frac{-17}{16}$ $\frac{-10}{18}$ $\frac{-12}{30}$	

$\frac{-07}{30}$   $\frac{-16}{13}$   $\frac{-19}{9}$  4.2  $\frac{-05}{9}$   $\frac{-14}{14}$   $\frac{-10}{19}$   $\frac{-08}{30}$

5" Poplar 40' L 12+00

$\frac{-12}{30}$ $\frac{-11}{10}$ $\frac{-05}{7}$	6.1	$\frac{-04}{8}$ $\frac{-17}{11}$ $\frac{-19}{30}$
$\frac{-14}{30}$ $\frac{-13}{9}$ $\frac{-03}{7}$	6.6	$\frac{-02}{7}$ $\frac{-12}{10}$ $\frac{-19}{30}$
$\frac{-17}{30}$ $\frac{-13}{10}$ $\frac{-02}{7}$	7.0	$\frac{-02}{7}$ $\frac{-11}{10}$ $\frac{-10}{30}$
$\frac{-10}{30}$ $\frac{-10}{10}$ $\frac{+01}{6}$	5.0	$\frac{00}{7}$ $\frac{-15}{10}$ $\frac{-12}{30}$



9091

17			50	85.9
18			53	85.6
19			54	85.5
	768	9327	5.32	85.59
20			6.1	87.2
+40			52	88.1
21			45	88.8
+50			54	87.9
22			80	85.3
BM			6.85	
	151	8686	7.92	85.35
+60			3.9	83.0
23			4.8	82.1
24			5.0	81.9
24	Bridge	WL	74 - Bot creek	87
+60			4.6	82.3
25			3.0	83.9
	6.50	9040	2.96	83.90
+60			3.3	87.1
26			3.4	87.0
+40			4.6	85.8
27			8.0	82.4
+40			10.2	80.2
28			11.2	79.2
	420	8348	11.12	79.28

$-\frac{11}{30}$	$-\frac{10}{10}$	$\frac{00}{7}$	50	$-\frac{04}{7}$	$-\frac{14}{9}$	$-\frac{12}{30}$
$-\frac{10}{30}$	$-\frac{11}{10}$	$\frac{00}{7}$	53	$\frac{00}{6}$	$-\frac{10}{9}$	$-\frac{09}{30}$
$-\frac{16}{30}$	$-\frac{14}{9}$	$-\frac{02}{6}$	54	$-\frac{03}{7}$	$-\frac{11}{10}$	$-\frac{10}{30}$

$-\frac{20}{30}$	$-\frac{12}{8}$	$-\frac{02}{6}$	6.1	$-\frac{02}{8}$	$+\frac{04}{8}$	$+\frac{17}{30}$
$-\frac{23}{32}$	$-\frac{17}{7}$	$+\frac{00}{12}$	52	$\frac{00}{12}$	$\frac{00}{19}$	$+\frac{30}{25}$
$-\frac{09}{30}$	$+\frac{23}{9}$	$+\frac{03}{13}$	45	$+\frac{20}{23}$	$+\frac{52}{27}$	$+\frac{89}{31}$
$+\frac{24}{30}$	$+\frac{42}{17}$	$\frac{00}{12}$	54	$+\frac{02}{12}$	$+\frac{23}{16}$	$+\frac{12}{30}$
$+\frac{90}{35}$	$+\frac{50}{22}$	$+\frac{10}{16}$	80	$-\frac{02}{7}$	$-\frac{31}{30}$	

4" Pop. 50' L 20+25

$+\frac{33}{30}$	$+\frac{15}{19}$	$\frac{00}{15}$	3.9	$-\frac{06}{6}$	$-\frac{20}{9}$	$-\frac{23}{30}$
$+\frac{12}{30}$	$\frac{00}{16}$	$-\frac{04}{8}$	4.8	$-\frac{06}{6}$	$-\frac{19}{9}$	$-\frac{17}{30}$
$-\frac{16}{30}$	$-\frac{15}{14}$	$-\frac{02}{9}$	5.0	$-\frac{05}{5}$	$-\frac{24}{15}$	$-\frac{24}{30}$

Dr. E

$-\frac{13}{30}$	$-\frac{14}{16}$	$-\frac{20}{15}$	$-\frac{02}{8}$	4.6	$-\frac{02}{4}$	$-\frac{30}{15}$	$-\frac{28}{30}$
$-\frac{36}{30}$	$-\frac{37}{15}$	$-\frac{05}{8}$	3.0	$-\frac{04}{6}$	$-\frac{30}{15}$	$-\frac{42}{30}$	

$+\frac{40}{30}$	$+\frac{43}{15}$	$+\frac{09}{9}$	3.3	$-\frac{03}{11}$	$+\frac{18}{15}$	$-\frac{25}{30}$	
$+\frac{59}{30}$	$+\frac{70}{19}$	$\frac{00}{10}$	3.4	$-\frac{04}{13}$	$+\frac{40}{19}$	$+\frac{18}{30}$	
$+\frac{124}{39}$	$+\frac{129}{30}$	$+\frac{47}{17}$	$+\frac{01}{10}$	4.6	$-\frac{02}{15}$	$+\frac{20}{15}$	$-\frac{31}{30}$
$+\frac{86}{30}$	$+\frac{52}{23}$	$+\frac{22}{15}$	$+\frac{02}{7}$	8.0	$-\frac{04}{9}$	$-\frac{37}{14}$	$-\frac{40}{30}$
$+\frac{50}{30}$	$+\frac{18}{15}$	$-\frac{01}{7}$	10.2	$\frac{00}{8}$	$-\frac{23}{15}$	$-\frac{25}{30}$	
$+\frac{35}{31}$	$-\frac{03}{16}$	$-\frac{02}{7}$	11.2	$-\frac{05}{8}$	$-\frac{18}{11}$	$-\frac{18}{30}$	



30

83.48

29		5.1	78.4
30 +00		52	78.3
+12		73	76.2
31		4.9	78.6
	8.54	87.14	488 78.60
31+60		77	79.4
32		5.9	81.2
+55		0.6	86.5
	9.84	96.44	054 86.60
33		5.7	90.7
+50		50	91.4
34		5.3	91.1
+50		7.2	89.2
35		5.5	90.9
BM		6.91	89.53

Borrow

350 1287.05 1283.55

0+00		6.7	80.4
+85		5.4	81.7
1+00		4.5	82.6
	7.41	129.46	000 1287.05
+50		8.3	86.2
2		5.5	89.0
+50		4.9	89.6
3		6.0	88.5

$\frac{-06}{32} \frac{-14}{11} \frac{-02}{7} 5.1 \frac{-03}{7} \frac{-14}{9} \frac{-15}{30}$   
 $\frac{-18}{30} \frac{-12}{10} \frac{-02}{7} 5.2 \frac{-03}{7} \frac{-18}{10} \frac{-17}{30}$

Plank B49c 4' No Dr.

$\frac{-12}{30} \frac{-14}{9} \frac{-04}{7} 4.9 \frac{-02}{7} \frac{-15}{11} \frac{-17}{30}$

$\frac{-19}{30} \frac{-19}{10} \frac{-02}{11} 7.7 \frac{-05}{11} \frac{-21}{10} \frac{-22}{30}$

60  $\frac{-25}{17} \frac{-10}{11} 5.9 \frac{-18}{20} \frac{-07}{25} \frac{-10}{33}$

$\frac{+25}{34} \frac{+20}{17} \frac{-10}{15} \frac{00}{11} 0.6 \frac{00}{11} \frac{-10}{14} \frac{+20}{17} \frac{+20}{37}$

$\frac{-05}{37} \frac{+05}{17} \frac{-23}{15} \frac{-05}{10} 5.7 \frac{-07}{12} \frac{-20}{16} \frac{+12}{18} \frac{+20}{35}$

$\frac{-22}{36} \frac{-10}{18} \frac{-30}{15} \frac{-10}{11} 5.0 \frac{00}{11} \frac{-18}{14} \frac{+20}{17} \frac{+25}{34}$

$\frac{-27}{38} \frac{-10}{18} \frac{-32}{11} \frac{-07}{11} 5.3 \frac{-02}{11} \frac{-25}{16} \frac{-07}{19} \frac{00}{34}$

7.2

5.5

4" Pop 65' L 32+80

89/30 80/10 72/7 6.7 72/7 76/9 76/30

Req. Borrow 79/30 63/13 53/9 5.4 59/9 65/12 68/30

44/33 42/16 52/13 44/8 4.5 44/9 54/12 42/15 43/32

67/30 68/16 95/12 82/9 8.3 83/7 95/11 75/13 81/30

38/30 40/15 66/12 56/8 5.5 55/9 66/12 50/14 54/30

42/30 43/15 62/12 51/10 4.9 51/6 60/12 43/16 42/30

52/30 53/15 44/8 6.0 60/7 70/12 54/16 53/30

+50

7.2