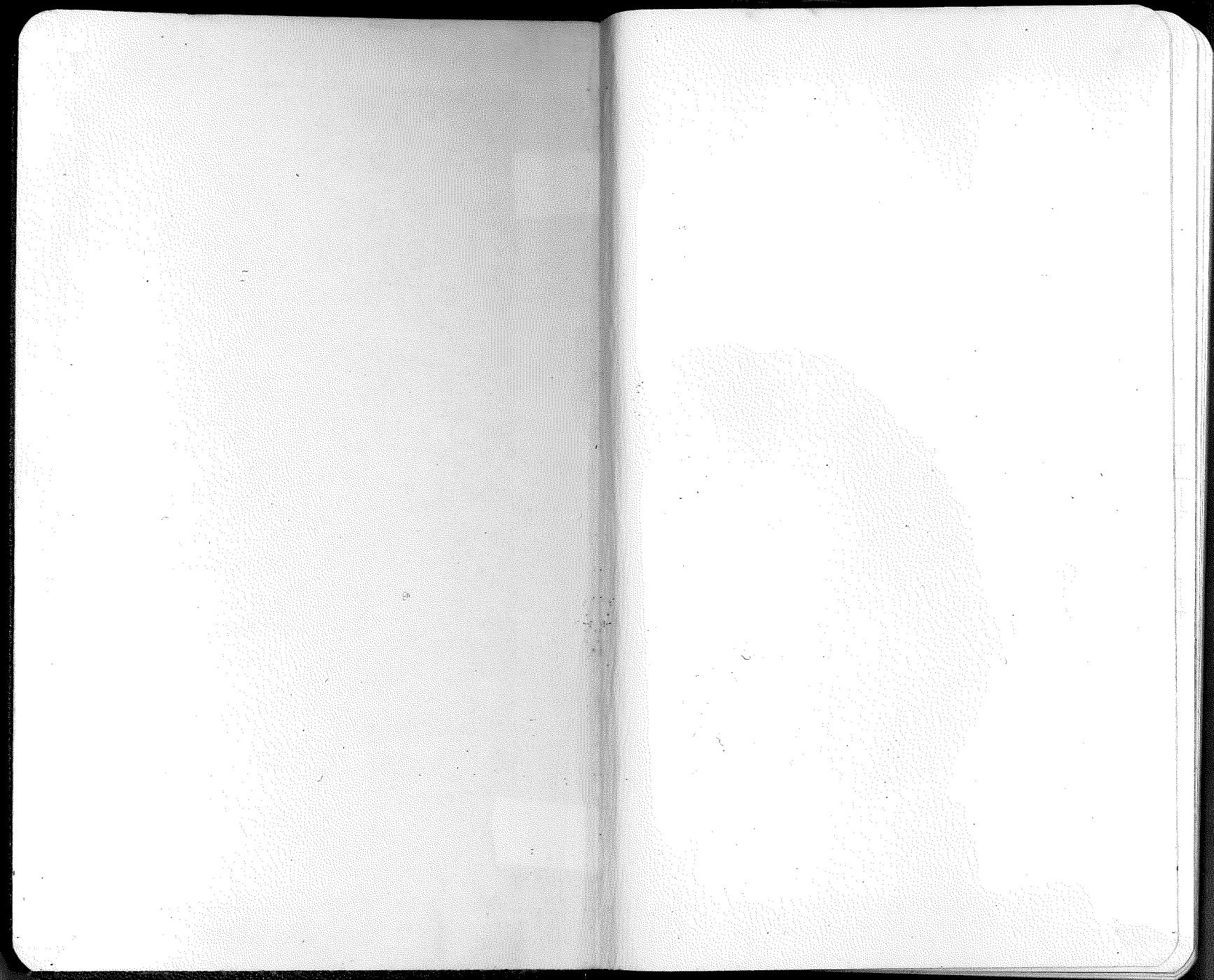
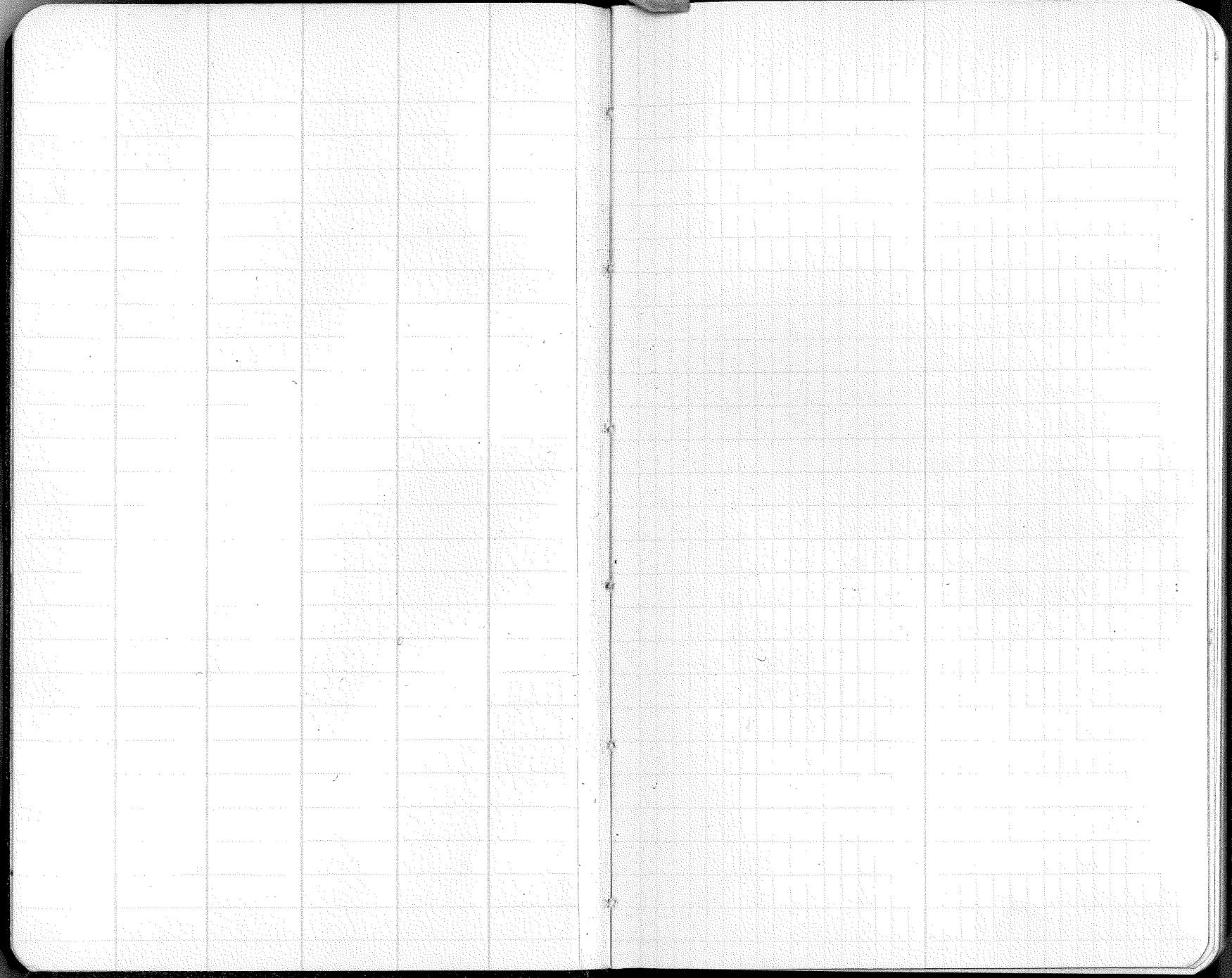


20

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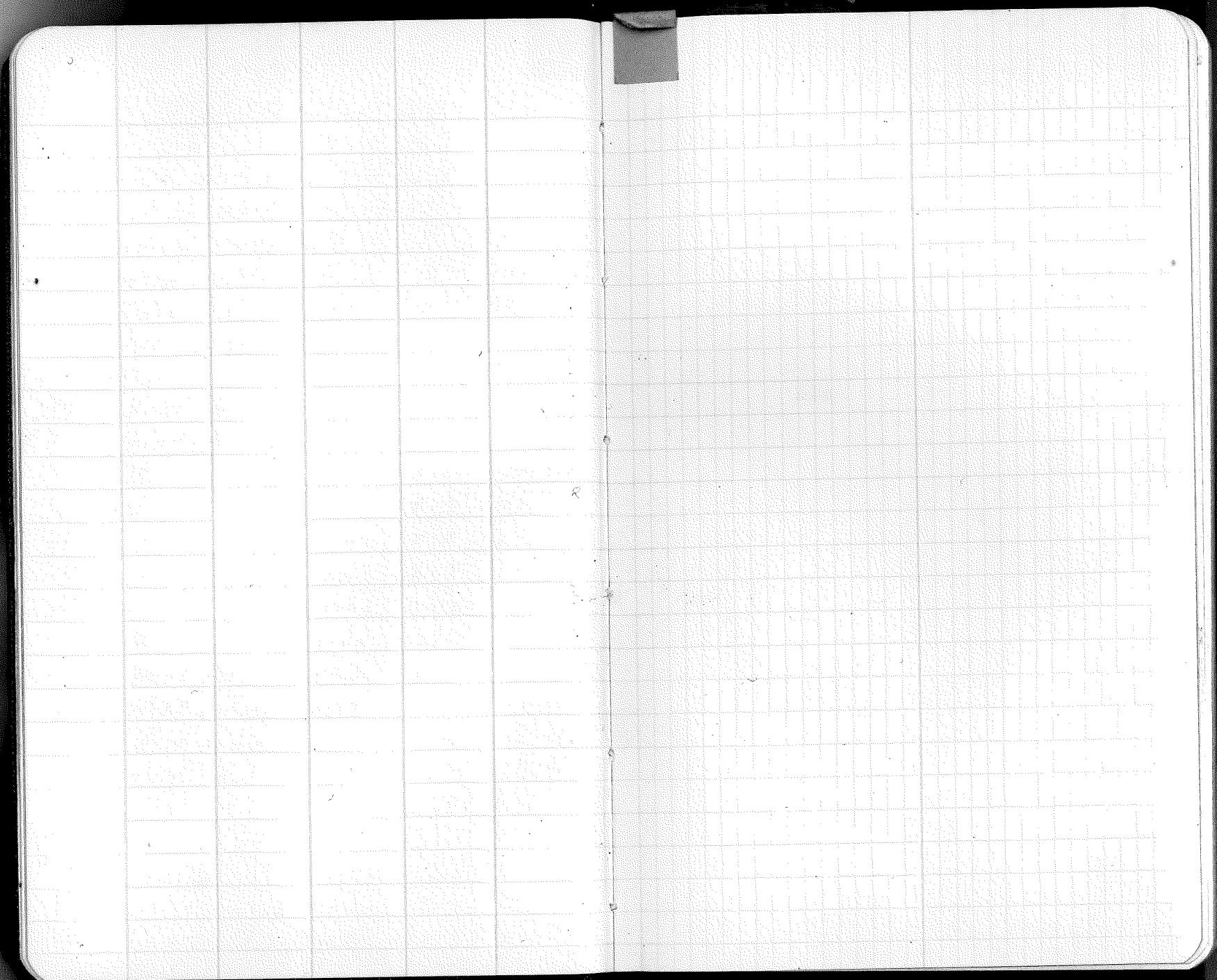
INDEX

T 14 N. R 26 W

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East on north side	1	3-9
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Data on Control Posts

112 Back of bk.



find under road
in road center is present but did not
Determined appr. position of N 60° E

25

24

23

22

21

20

19

18

17

16

15

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13

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3

2

1

0400 Start North from N 60° E Con. 1112 - 140-26

Look for:

Aspen-4"-551W-701ks

Birch-10"-517E-2031ks

Aspen 6-8"
Scattered sp.

1112-140-26

Road Intersection

Aspen 4-6"

Feb. 8, 1938

H. Wilson - Compass notes
M. Woods - Head chain
6. Constrictor chain
Found: Elm-10"

(New) N 67½° W - 46-3'

scribed 43 B.T.

Wh. oak-14"

368° E - 43.8 ft.

scribed 445 B.T.

Partially grown over

36

at stake to S.C. 211 - Closing corner.

31415 Intersect Standard Parallel 19 ft. west

30

49 48+79 Winter road NW & ERS.

48

47

46+00 Enke fence rail SW. NW & SE.

45

44

43

42

41

40

39 38+76 Woven wire fence appr 2.5 mi.

38

37

36

35

34

33 32+46 Woven wire fence runs W. short distance E - enter

32

31

30

29+07 Fence E 1W

28+42 Road to buildings runs East.

28+18 Narrow road runs N.W.

27

Look for:

Tam. 4-518W-92 lbs.

Tam. 4-N37E-59 lbs. "

Found: 2" square tam

stake, 2 ft. out of ground

scribed on west side

T 140 N 52

on east side

R 26W 51

from which

Tam stub - 4"

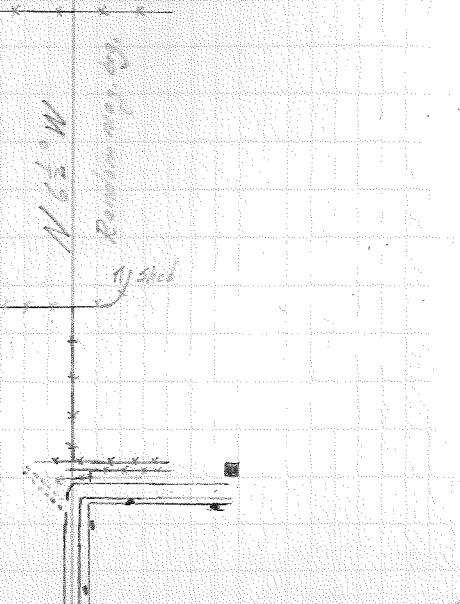
314°W - 63.6 ft.

face cut to

showing faint

evidence of surface

marks.



26446 App. E.C.W. 1195-2" Tam. stake.

24425 8 ft. 50. of 1/4" Finel 5" cedar with blaze opened up & backed face

24

23

22

21

20

19

18

17

16

15

14

13

12

11

10

9

8

7

6+55

6

5

4

3

2

1

0700 Start East from S.C. 211 140°26'

36

Tam. sh b-a-514W-636°

2" Tam. stake scribed
T14N 52, R26W 50

Feb. 8, 1938

3

H. Nelson - Compass - notes
H. Wood - road chain
G. Campbell - tape chain

W

W

W

W

W

W

W

W

W

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3" aspen state
712 to 14pt. ECU - C. 31

52028
53.
51600 Enter Highland - aspen
50 29150
49
48
47
46
45
44 449 018 winter road N15°
43
42100 Enter Cedar, birch, ash
41
40
39
38
37
36
35
34
33
32
31 30471 Enter black spruce 6'-8' NW 1/4
30
29
28
27

Look for:

Pine - 10-540E-10ths N
Pine - 6-530W-20ths S

4

Feb. 8, 1938 5
H. Wilson - Compass work
M. Woods - Head chain
G. Compton - Rear Chain

26
25

24

23

22

21
20166 Narrow road SE 1 NW
20

19

18

17

16

15

14

13

12

11

10

9

8
7437 Winter road NW & SE - often highest

7

6

5

4 to 0 Loc. low - cedar sp., ash, balsam

3

2
17867 with 40' 2" I.P. for standard corner 5. 35/36
1

0 to 0 start west from 50' 211 - 140-26

140-25 140-26

Loc. high - cedar sp.
Loc. low - cedar sp.

Tom. - 5" - N 63° W - 22.4 ft.
scribed 335 B.T.

Tom. stub - 5" - N 26° E - 5.2 ft.
scribed 536 B.T.

2" Tam. stake scribbled

for S.C. 318 140-26
to line from west 100 ft appr. State
Set state & offset 106.4 ft No.

52180

52

51

50

49467 Enter Island

49

48

47

46

45

44

43

42

41

40

39

38

37-42.7 State at east side of lake

36-40 Enter cattails

36

35

34

33100 Bottom of slope - cedar, ash

32

31

30

29 28-28 Narrow road SW 1/4 E

28 28124 - State road SW 1/4 E

27

140-25
34

140-26
34

♦ Appr. State.

6

Rice Lake

26
25
24
23
22
21
20
19
18

17
1600 Leave point

15
14
13160
13
12
11
10
9
8
7

6100 Leave Island

500 Start West from Ap 35 372 140-26

140-25
26

140-26

Feb. 8, 1956 7
H. Wilson - compass - notes
M. Woods - Head chain
G. Constant - rear chain.

West

Rice Lake

N

S

E

W

Up

Down

Rice Lake

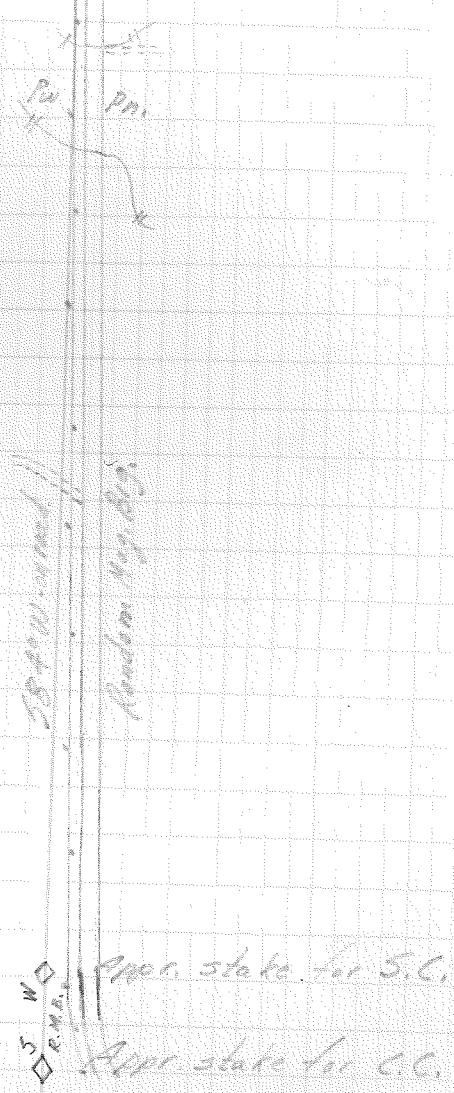
Appr. Stake

140-25
26

140-26

- 26
25
24
23
22
21 21454 End of mt 140-26
20
19 19402 Nor bush pine camp
18
17
16
15
14
13
12 12459 Private road ends 500.
11
10
9
8
7
6
5 run west.
4 offset north 81 ft to road &
3 app. 5 c. ft by U.S.G. and
2 10.2 ft red oak stake set to mark
1
0 000 Start westly app. 10-26

Feb. 9, 1938 9
H. Nilson - Comptor - not
M. Woods - Hood chain
G. Comstock - Rear chain



		140-25 26	140-26
2649	Continue west on 583 $\frac{1}{2}$ °W Offset north 10 ft. to 10 m. stub		
26			
25			
24			
23			
22			
21			
20			
19			
18			
17400	Enter tamarack swamp - 2"-4"		
16			
15			
14 13	Enter aspen-birch - 8"-10"		
12 11	Enter aspen-birch-mixed conifers		
10			
9 8	Enter cedar-spruce swamp		
7+20	Enter jack balsam		
6			
5+33	Enter jack pine ridge		
4			
3			
2			
1			
1730	St. sec. cor. 32 $\frac{1}{2}$ - 141-26		
0400	Start west from road int. 33 - 140-26		
Feb. 9, 1938 11 H. Nielsen - Compoes-Nide H. Woods - Hood Caren G. Comsigh - Rearchon			
585°W Rounding Nop. 32			
Found: Norway - 10" 581°E 3 ft. out of ground scribed Jack pine - 12" 547 $\frac{1}{2}$ °W 61.5 ft. - blazed ° West side - R26W S35 So. side - T140N S35 E. side - R26W S33 N. side - T141N S32 Road Intersection			

140-25
26

140-26

on ice.

52400 Set approx Sec Con. $\frac{34}{675}$ stroke

52

51

50

49

48

47

46

45

44

43

42

41

40

39

38

37

36

35

34

33

32

31

30

29

28400 Enter Lake Laura

27400 Beach

140-25
26

140-26

12

Lake
Laura

Rondon Mys. Eq.

Station

140-25
26

140-26

13

26

25

24

23

22

21

20

19

18

17

16

15

14

13400 Point 150 ft south

12

11

10

9

8

7

6

5

4

3

2

1

0400 Start west from appr. S.C. 32 675-140-26

Lake



Laura

32/675-140-26

Point 150 ft south

54424 Standard corner - 2" I.P. with cap
with nos 39

C.C. 116 - 2" I.P. open in cement block

52400 Enter open field

51 447 1 1/2" open I.P.

50 445 1 1/2" open I.P.

49

48 47491 Enter stockpile
47 47707 Fence runs NW below bank

46

45

44

43

42 41730 1 1/2" open I.P.

40

39

38

37 36449 Fence runs south - 30° E - enter brush

35 3448 offset No. 21 ft. to N.E. cor. at fence

33+58 END of fence

32

31

30

29

28

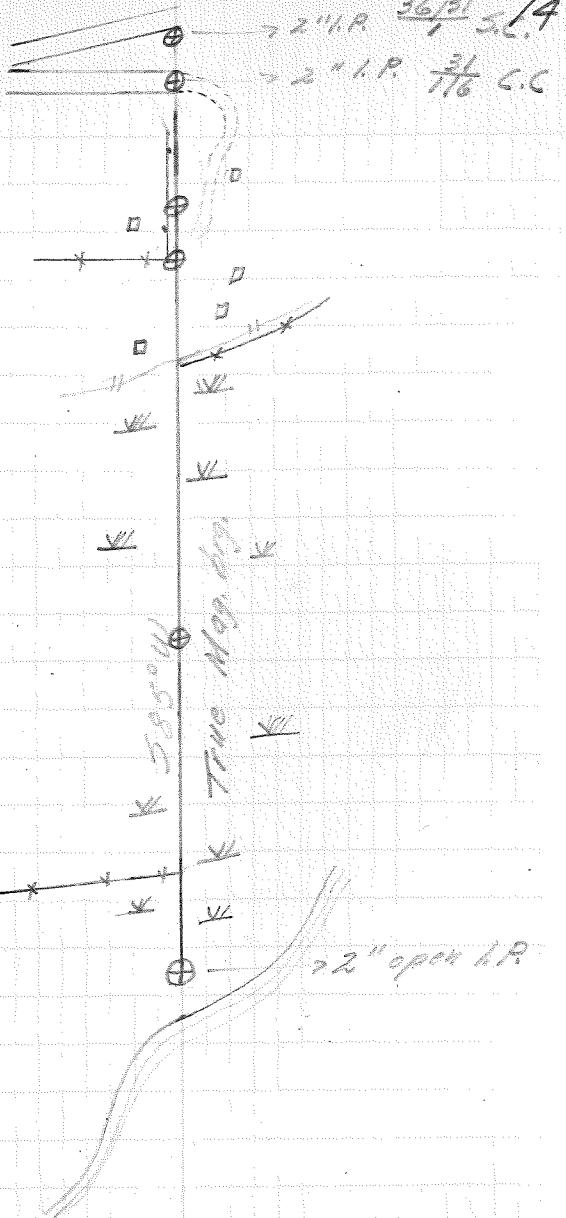
27

IHO-25
26

IHO-26

→ 2" I.P. 36/31 sc. 14

→ 2" I.P. 776 C.C.



at intersection of roads near ~~the~~
Center of road N.E.S., 130.7 ft. S.

49

51

50

49

48

47

46

45

44

43

42

41

40

39

38

37

Loc. Sol. sw.

Enter Sol. sw.

Leave Sw. swamp

33

Enter Sw. swamp

Loc. clump

32

Enter virgin N.W.P. clump

28

Leave Sw. N.W.P.

200' from road

Project

300' S.W.

300' S.E.

300' N.E.

300' N.W.

300' S.W.

26
25
24
23

Field NW
Lot 4 NE

23 410

Road No. 4 to Field 100 ft. No.

22
21

21 450 House 500 ft. No.

20

19

18

17

16

15

14

13

12

11

10

9

8

7

6 + 16

5

4

3

2

1

0400 Start west from intersection of roads

11 43

Fence ESW 1/4 E.
SW. 1/4 S. - enter H m.

2/11
11/12-140-26

Feb. 9, 1938 17

H. Nilson - Notes

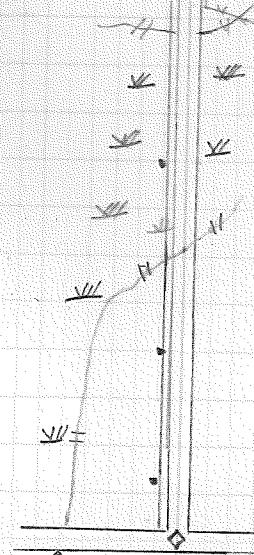
M. Woods - Head Chain

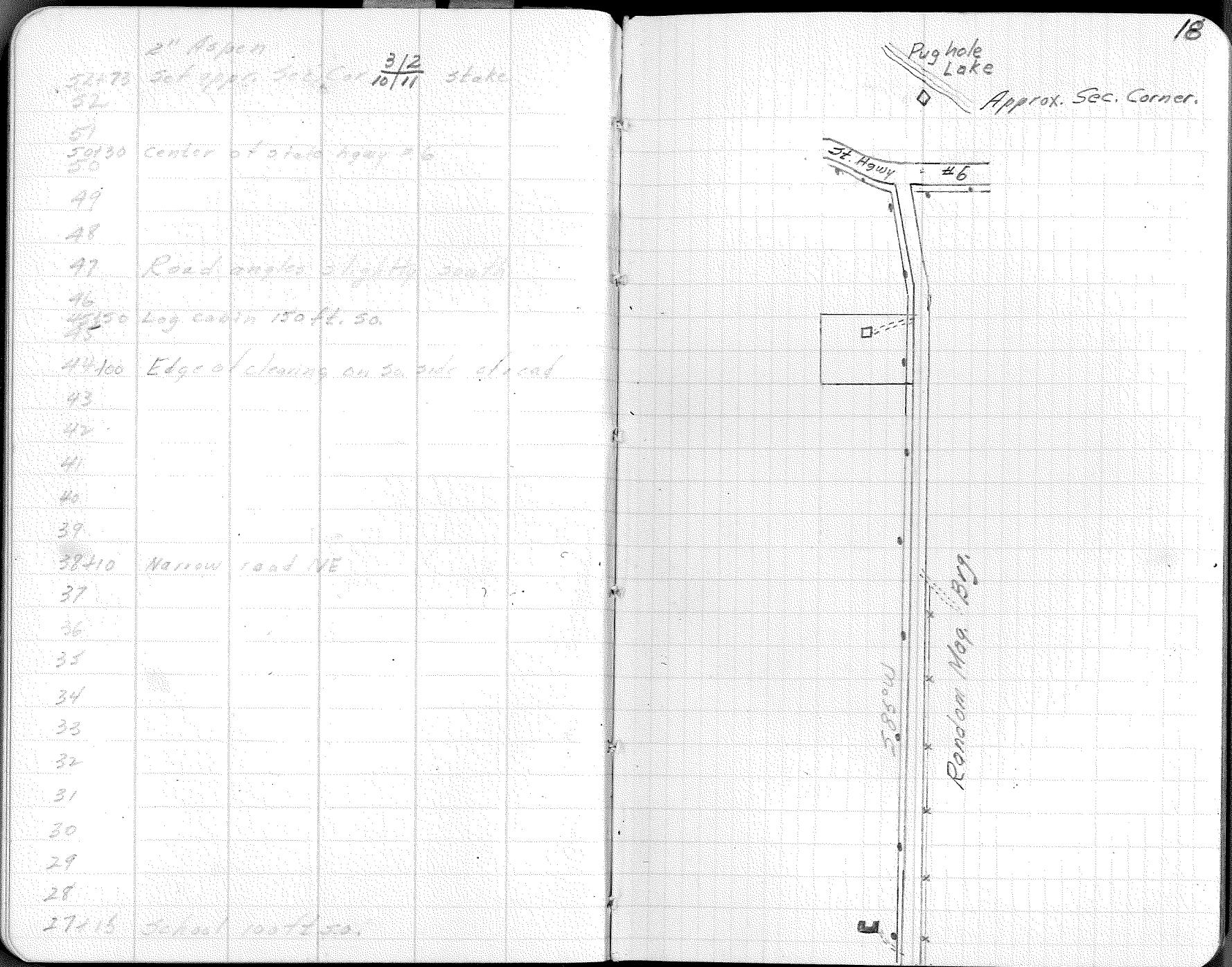
G. Constock - Poor Chain

field

585°W.

Randall Mfg. Squ.





July 10, 1936 19

M. Woods Notes
G. COMSTOCK, H. Chain
M. Bain Recheckin.

26+40 entered spruce swamp

25

24

23

22

21

20

19

18+25 left lake entered oak aspen-pine white

17

16

15

14+31 edge of lake & cedar system

13

12+00 entered cedar swamp

11

10

9+30 left cedar swamp entered aspen grove

8

7

6+50

6+29

5+14 LOST IN FOREST WITHIN CEDAR SWAMP

4

3

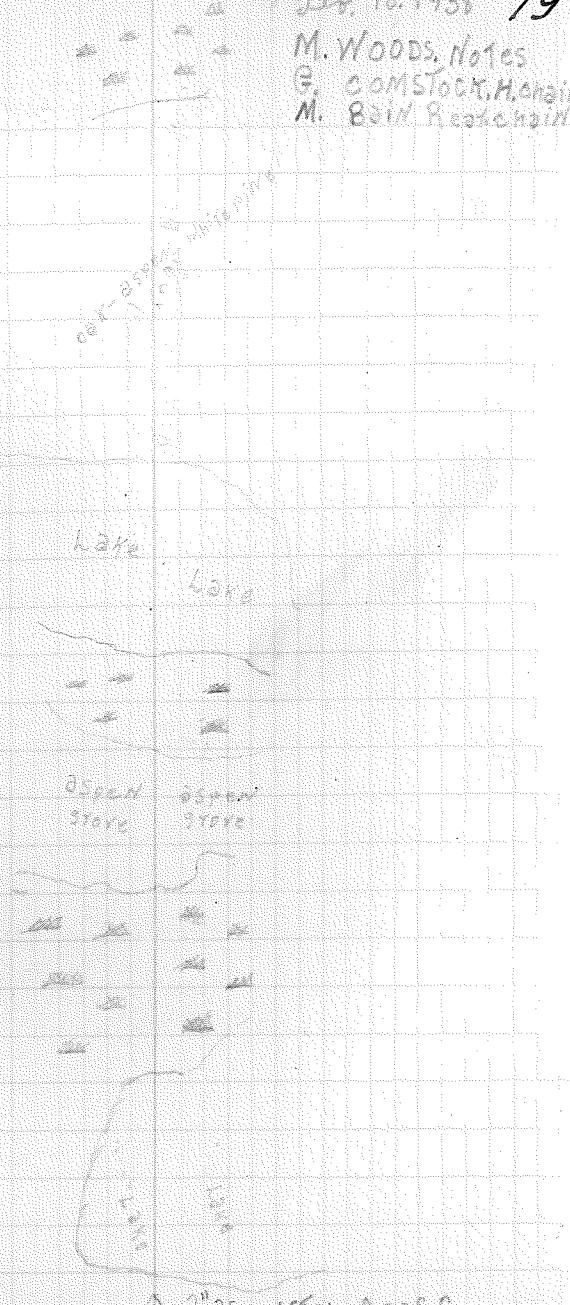
2

1+00 edge of lake

0+00 Start west from 10/11 - 140-26

593°W

Random Mag. Bearing S 83 1/2 W



Sut, 10.10.13

20

52+10.21' White oak Forest, ssp. 3/4

51

50

49

48

47

46

45

44

43

42

41

40

39+00 LEFT Spruce swamp, encl. old k. - sk.

38

37+92 LEFT Late cedar & spruce swamp

36

35+29 LEFT Spruce swamp, cedar & late

34

33+45 LEFT Old Spruce swamp - old k. - sk.

32

31

30

29+00 LEFT Spruce encl. old k. - sk.

28

27

58.98 N

App. sec. 10 of lot.

RANDY M. BEAUMONT 11/2013



000-25K

Feb 10, 1938

21

26

25

24

23 + 56

21 + 69 crossed R.R. S - NE.

22 + 26 CENTER OF BY RD. 10. E. WOODS AND LAKE

21 + 53 Roads to cabin. Big pine tree in middle

20

19 + 00

Gull River cabin app. Reservoir on side

18

17

16

15

14

13 + 10

EAST END OF LAKE APP. SPILL OVER ON SIDE

12

11 + 00, entered as per gage

10

9

8

7

6

5

4

3

2

1

0.00 Start west from 3 1/2 - Woods

LAKE
S 13 1/2 W

M. Woods. Notes.
G. Comstock, H. Chain
M. Bain Rear Chain



◇ 2" white oak post

Feb. 10, 1938

22

52 + 80 COTNERCAMPIN LAKE

51

50

49

48

47

46

45

44

43

42

41

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39

38

37

36

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S 83 $\frac{1}{2}$ ' W

Lake

Lake

Thunder Lake

Map Bearing S 21 $\frac{1}{2}$ W
Barom. Line.

Lake

Lake

Feb 10 1938

24

56+64 APP SEC. COYNE in center of road. North - south
56+48 - crossed fence north - south, LEFT SPYKE SWAMP

52

51

50

49

48

47

46

45

44

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41

40

39+48 entered spruce swamp.

fence runs north

37

36

35

34

33+39 crossed road North - south.

32

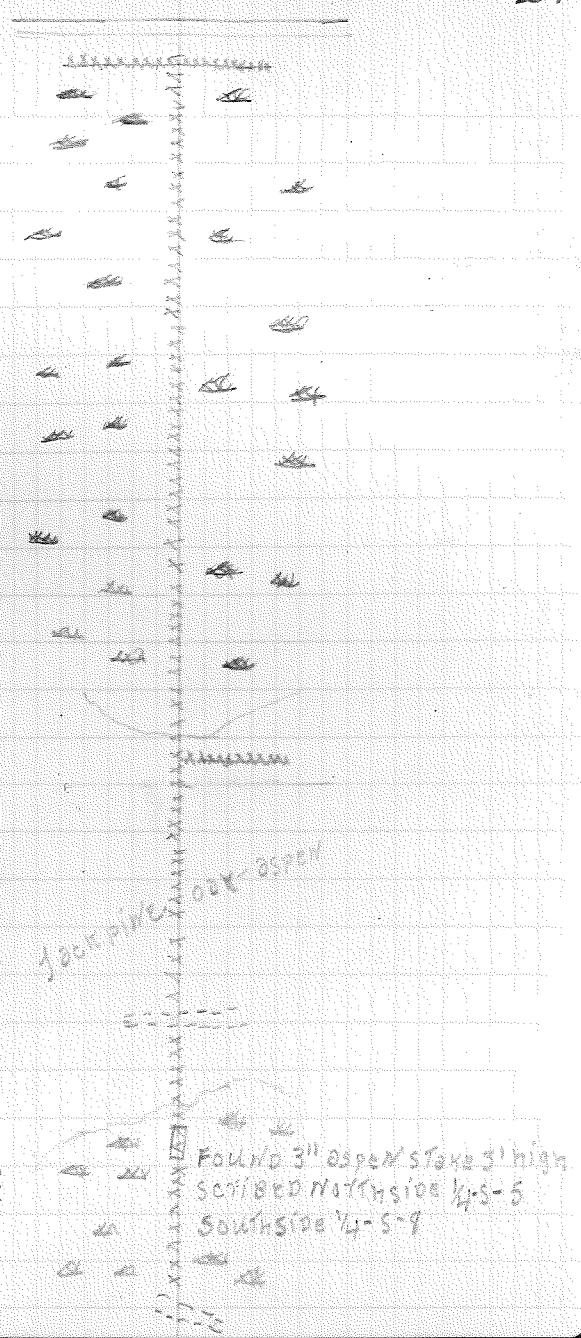
31+17 LEFT RED WILLOW SWAMP ENTR'D 100' JACK PINE CEDARS
1/4 COYNE 3" 250 ft N Stake.

29

28

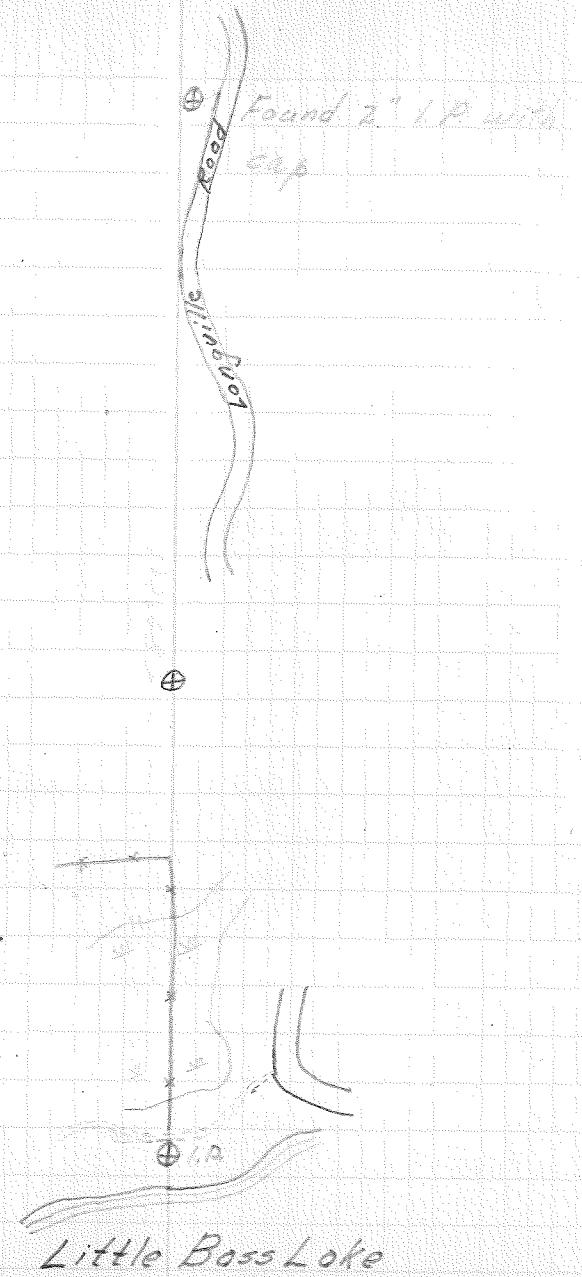
27+23 crossed road N - S

S 82°W



26

- | | |
|--------|---------------------------------------|
| 52 | to 300 S. 121 ^{1/2} - 140-26 |
| 31-466 | Intersect N13 Line 10.6 ft soot cor. |
| 31 | |
| 50 | |
| 49 | |
| 48-100 | 16 ft south edge of road |
| 47 | |
| 46 | |
| 45 | |
| 44 | |
| 43 | |
| 42 | |
| 41-150 | Long grass road 12 18 ft. north |
| 41 | |
| 40 | |
| 39-30 | 12' open l.l. 18' soot cor. |
| 38 | |
| 37 | |
| 36 | |
| 35-58 | Fence runs 38' soot cor. |
| 35 | |
| 34-40 | Edge of low swamp - edge No. pine |
| 33 | |
| 32 | |
| 31 | |
| 30-462 | Brush 20' tall 10' 5 |
| 29-73 | cent. 20' tall 10' 5 |
| 29-76 | M.C. 16' open P. |
| 28-78 | Edge of 20' tall N13 |
| 26 | |
| 27 | |



53+22 $\frac{1}{2}$ inch p. with 2" top Postec. corner. $\frac{1}{2} \times \frac{1}{2}$
52
51

49+34 Left open fields. scattered aspen

48

47

46+46 open field West of Line

45

44

43

42

41+00 Fence east.

40

39

38

37

36

35

34

32+81 Fence east.
32+36 Road to House

31+36 House app 50' east - trailer house 75' west of line

30

29+16 Fence east open field

28

27

aspen

Open field

aspen

open field

line
aspen

Sept. 11, 1938

29

M. Woods. Notes

G. Comstock McHain

M. Bain Rear. chair

36

35

34

33

32

31

30

29

28

27

26

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242

243

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247

248

249

250

251

252

253

Feb. 11 1939 30

52+91

CENTER OF HIGHWAY IN S. SEC. CORN IN ROAD CENTER.

52+67

2" ASPEN STAKE 3' TOS. FOR SEC. CORNER. 10/1
15/14

51

50

49

48

47

46

45

44

43

43+00

LEFT S.S. SWAMP. ENTERED LONGHORN SWP.

42

41

40

39+22

ENTERED S.S. SWAMP.

38

37

36

35

34+61

LEFT S.S. SWAMP. ENTERED LONGHORN SWP.

33

32

31

30+00

ENTERED YAM. SWAMP.

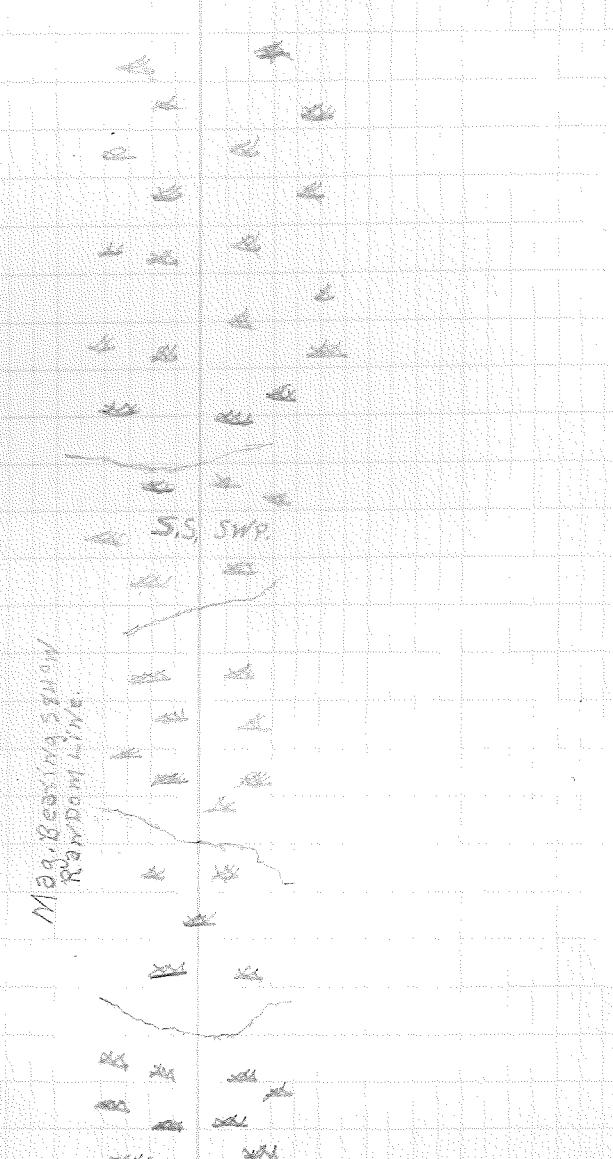
29

28

27

Highway 206

S 84° W



31

Feb 11, 1938
 M. Woods Notes
 E. Comstock, H. chain
 M. Bain. Read chain.

S 83¹⁰' W.

Pine areas
 Pine areas

Map, Beginning S 83¹⁰' W.
 from 1/2 mile

Open
 Open

Highway line

26

25

24

23

22

21

20

19

18

17

16

15

14

13

12

11

10

9

8

7

6

5

4

3

2

1

5+51.

Entered S.S. Swamp

4

3

2

1

0 + 24

0 + 00

0 + 00

App. Sec. corner stone
 Started West from App. sec. cor. 9-11-5 T-14-6 R-2-6
 Offset 11 ft North to Line running West

Ref. 11. 1938

32

52+80 S. 07 W. C. main lake S.C. 7/10
12/15

51

50

49

48

47

46

45

44

43

42

41

40

39

38

37

36

35

34

33

32+30

edge of lake.

31+00

foot of hill.

30+75

offset 8.3' south 6.21(9.2) high

29+75

top of hill, offset 37.5' south to 2" stake

28

27

S. 43 1/2 W

Thunder Lake

132.300 ft. 583' 4" N.
Random line

Φ 2" iron pipe.

square on one side 1 1/2" high.
open pipe

open pipe

Feb 14, 1938 33

M. Woods Notes.
E. Comstock H. Chain
M. Bain. Rear chain

S 81 $\frac{1}{2}$ W

pin-as-pot pin-as-pen

2" stakes squared on 4 sides
or 50 $\frac{1}{2}$ " iron rod with handle

Thunder Lake

26

25

24 + 00 entered cedar swamp

23

22

21

20

19

18

17

16

15

14

13 + 30

Crossed R 20 NW - SE.
edge of lake offset 70' south to

12 + 16

11

10

9

8

7

6

5

4

3

2

1

0 + 00 started West from App Sc. 9 $\frac{1}{2}$ 1613 1142 R. 26

Feb 1st, 1938. 39

52480 corner of sheep trap enclosure
+ 35 edge of pig hole hole

2

19

18

17

16

15

14

13

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1

0

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278

279

280

281

26+79.

CROSSED ROAD N.W. SE.

26+77

NEV. M.C. 4" ASPEN 8133 ON TWO SIDES. b' NORTH OF LINE

26+34

LEFT LAKE ENTERED PINE ASPIRE

25

24

23

22

21

20

19

18

17+17

EDGE OF LAKE

16

15

14

13+89

LEFT LAKE ENTERED 2 ASPEN

12

11

10

9

8

7+15

EDGE OF LAKE.

6+

5+66

1 1/2" WOODEN STAKE 2' TALL.

4

3+72

~~FOUND M.C. CORNER.~~

2

1

0+00

STAYED WEST FROM APP.S.C. $\frac{19}{16}$ TAD. R. 26

ASPIRE

Feb 14, 1938
M. Woods. Notes,
C. Comstock. H. chain
M. Bain. Rear chain

35

S 82°W.

THUNDER LAKE.

ASPIRE

THUNDER LAKE

Mag. Bearing S. 82°W.
From Dog Line

1 1/2" Wooden Stake 2' tall.

PINE STAKE
1 1/2" WOODEN STAKE 2' TALL.

Feb. 14, 1938. 36

56+45 fence twins North Found

52+80 Blazed 4" cedar post on 2 sides Keene App. S.C.

51

50

49

48

47

46

45

44+46

CROSSED ROAD N.W. 5.E

Fence West-North

CROSSED FENCE North-South

43

42

41

40

39

38

37

36

35

34

33+71

CROSSED FENCE North East-W

32

31

30+39

FOUND $\frac{1}{4}$ CORNER

29

28

27+33 FOUND ORIGINAL M.C. CORNER

S 82° W.

Major Bearing S 82° W.

2" 1.9, 3" STAKES SCRIBED
S-7-5-8-5-18-5-17
8" ASPEN 83 YRS 5.64" E
DISTANCE 125.1"

PINE-ASPEN

5 1/2 I.P. 2/13/31

PINE-ASPEN

3" ASPEN STAKE 2' TALL BLAZED
ON 2 SIDES. SCRIBED.

NORTH SIDE 1/4-5-8
SOUTH SIDE 1/4-5-17

10" JACKPOIN BEADS, S. 16° E

SCRIBED 1/4-5-17-B.T. DISTANCE 20.8

6" WHITE PINE BEADS N 32° W

SCRIBED 5-8-B.T. DISTANCE 6.8"

4" ASPEN STAKE SQUARED ON 2

SIDES. NORTH SIDE M.C. 5-8
SOUTH SIDE M.C. 5-9,

8" ASPEN BEADS S 20° E

DISTANCE 7.9'

PINE-ASPEN

26
 25
 24
 23
 22+71 ~~Entered Spruce swamp.~~
 21+75 ~~Entered Spruce swamp.~~
 20 19+00 LEFT SPRUCE SWAMP.
 19+05 ~~Entered Spruce swamp.~~
 18+00 ENTERED SPRUCE SWAMP.
 17+54 ~~Entered Spruce swamp.~~
 16+16 LEFT SPRUCE CEDAR SWAMP.
 15
 14+60 LEFT SPRUCE CEDAR SWAMP.
 13+91 ENTERED SPRUCE CEDAR SWAMP.
 12
 11+70 ~~Entered lowland swamp.~~
 10+97 LEFT LOWLAND SWAMP.
 9
 8+00 ENTERED LOWLAND SWAMP.
 7
 6
 5
 4
 3+72 F
 2
 1
 0+00 STARTED WEST FROM APP. SC. 7th 1140 R 26

58 1/2 W

aspen pine

aspen

aspen pine

2" in. 2 aspen staves
 Sawed down - 20' long
 Slabbed & packed
 Distilled

Feb. 14, 1938 38

52+80 Set 3" Hardwood Stake

51+20 Line runs North

50

49

48

47

46

45

44+88

43

42

41

40

39

38

37

36

35

34

33

32+44

31+15

230+00

ENCL 100' MIXED Hardwood
FOUN

29

28+64 crossed road NW - S.E.

27+22 FOUND 4 corner, offset 4 ft south to line.

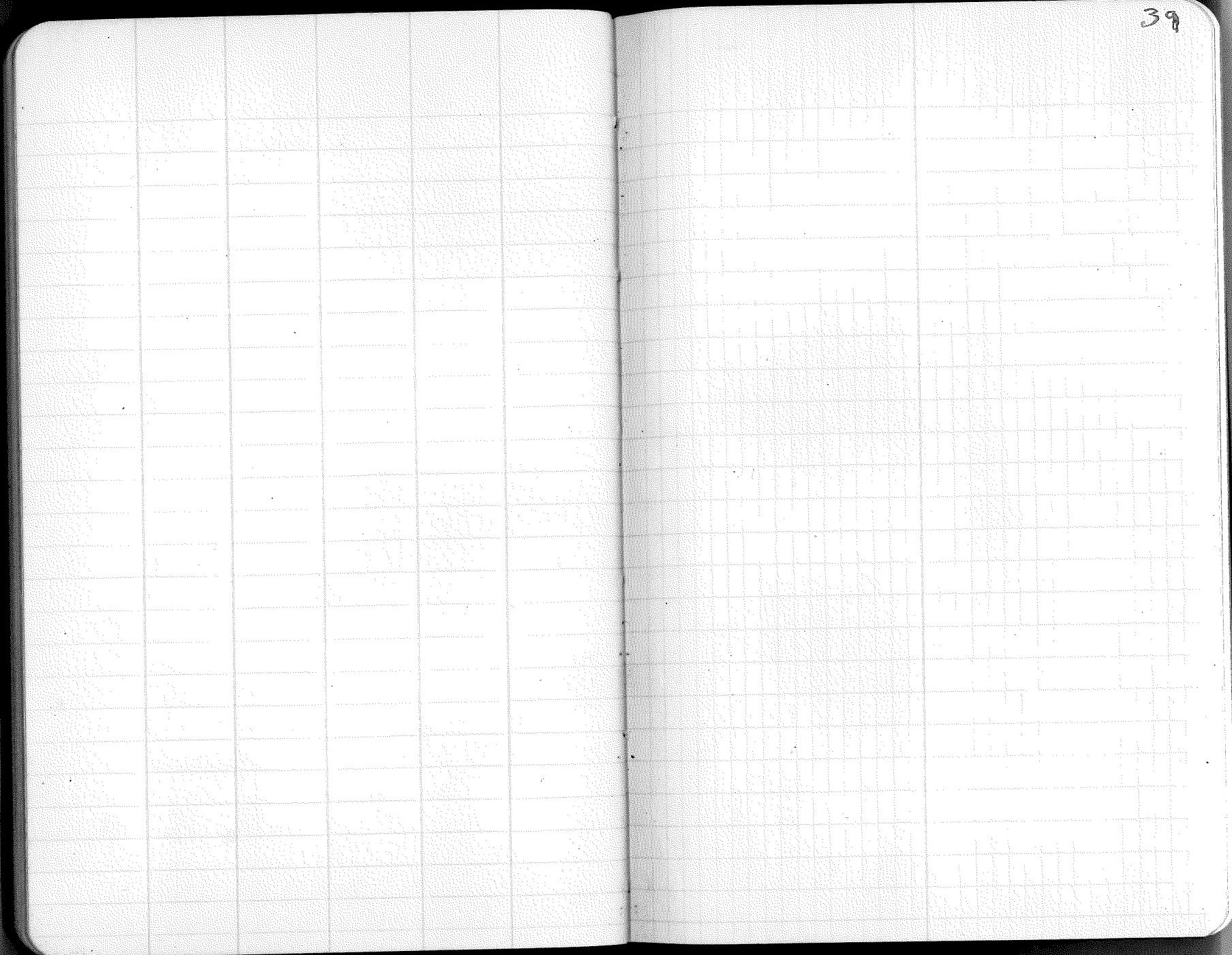
S8 $\frac{1}{2}$ ° W.

Mog. Bedrock Stake
Hardwood

Mixed

3" aspen stake scribed on
West side 1/4 - S - 8
East side 1/4 - S

8" N.W. pine boots 512 ft distance
Mog. bedrock 1/4 - S - 8
112" pine stump bedrock 1/4 - S - 8
Boiler pipe 34" scribed - S - 8



Nov. 1 1938 40

Setting up Controls. ~~3/2~~ ^{Road} 139-26

Distance from ~~3/2~~ 139-26 east
to road 100 feet Var. 62°
Highway 6.

Distance from ~~3/2~~ ³⁴ 139-26 east
to Fein's road 100 feet Var. 62°

2. Distance to Road From ~~3/2~~ ^{3/2} 139-26 Var. 62°

To Fein's Road 21+27 feet

Distance From ~~3/2~~ 10 Puchs Road 50°

~~3/2~~ ^{3/2} 8+94 feet

Distance From ~~3/2~~ 139-26 Var. 62°

25+20 feet Var. 62°

Distance west from ~~3/2~~ to highway

No. 6 3+66 Var. N 94 W 139-2

Distance West From ~~3/2~~

0+28.1 Var. 62°

Distance From West From ~~3/2~~ 139-26

0+28 Var. 62°

Distance N 62° W 139-26 0+52 feet

Distance W To ~~3/2~~ Var. 62° 15'

Distance N to ~~3/2~~ 139-26 1+00 feet Var.

Nov. 1 1938

Nov. 2 1938

Distance from ~~41/2~~ ^{6 1/2} To Muchoh's Road

10+45 139-26-Ya $0^{\circ} 30'$

Distance from ~~West~~ ^{W.E.} from ~~2 1/2~~ to Lake George

Road 20+81 Ya 11/2 E

Distance ~~East~~ ^{E.W.} ~~41/2~~ to Lake George Road

36 ft. ~~1 1/4~~ COXLEY ^{2 1/2}

Distance North to Camp Road ~~1 1/2~~ ^{1 1/5} ~~1 1/2~~

18' ~~1 1/2~~

Distance North from ~~1 1/2~~ ^{1 1/2} to Camp Road

518 ft. $0^{\circ} 6 \frac{1}{2}'$

Distance South from ~~1 1/2~~ ^{3 1/2} to Fall Creek

1835' Ya $0^{\circ} 6'$

Distance North from ~~1 1/2~~ ^{3 1/2} to Highway 6 F

16+75 Ya 11/2 E

NOV. 7, 1938

Woods

Schwartz

Yieldings

Setting 1930 controls

Set Post For ~~13 1/2~~ ~~13 9 - 26~~Distance West $\frac{3}{4} \text{ mi}$ $19^{\circ} 30'$ to Mitchell Lake
Road 28.49' - 129-26 Va. S. 13 $\frac{1}{2}$ W.

Distance East From 25 1/2 To center

~~30 31~~

of Mitchell Lake Road 18.6' Va. S. 70 W.

13 9 - 26

set post for $\frac{3}{4} \text{ mi}$ 13 9 - 27 1/2 N 5° Eset post for $\frac{1}{2} \text{ mi}$ 13 9 - 27

Set No. 1939 #3.
M. Woods Notes.
G. Comstock H. Chain.
M. Bain Rer. 2 Chain.

26

25

24

23

22

21

20

19

17+18

EDGE OF LOKO
BUTTING 30' SOUTH OF LINE
OFFSET 14' SOUTH TO M.C. CORNER.

16+43

HOUSE 75' SOUTH OF LINE LEFT OPEN

15

13+27

CROSSED FENCE N-S. BUILDING ALONG SIDE OF RIVER
ROAD SWINGS TO SOUTH

12+16

FENCE SOUTH.

11

10+15

OPEN FIELD SOUTH OF LINE

9

8

7

6

5

4+08

FENCE SOUTH - WEST

3

2

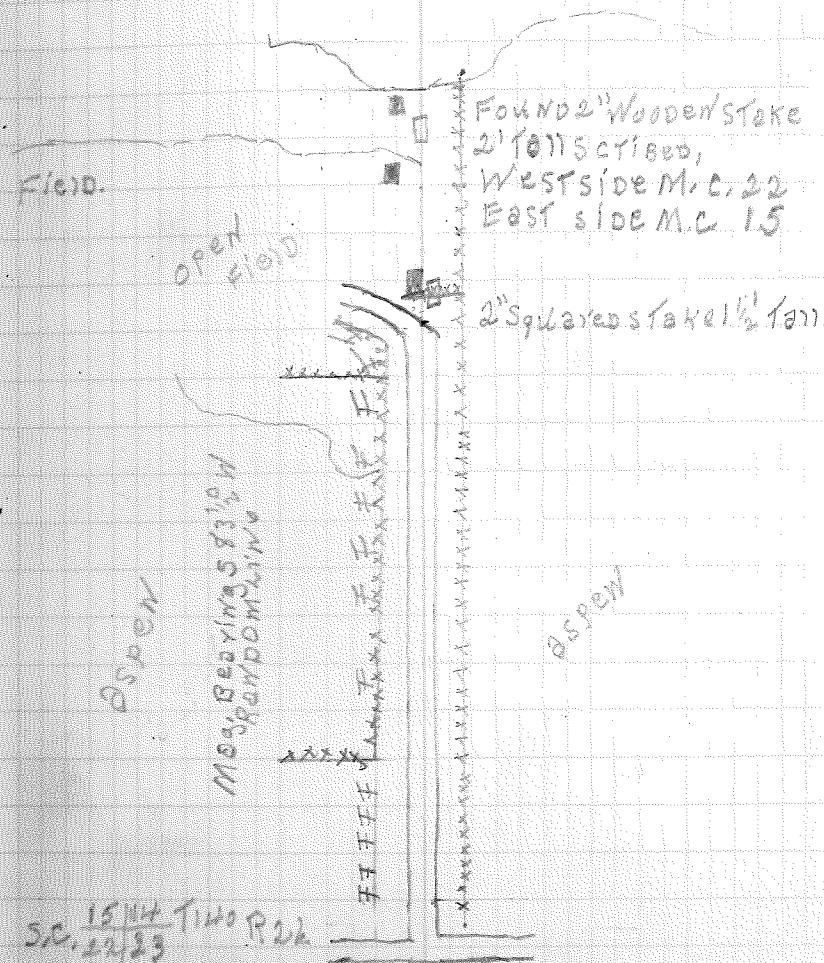
1

0+00

STAKED WEST PLAT S.C. IN ROAD INTERSECTION

S 83 3° W

THUNDER LAKE



Feb 16, 1938. 44

54+84.5 FOUND 4" spruce logs from which bears.

53

52

51+22 LEFT spruce swamp entered. 25 pen.

50

49

48

47

46+63 entered spruce swamp

45-

44

43

42

41

40

39+82

CROSSED ROAD NE-SW.
FOUND M.C. CORNER.

38+89

LEFT lake entered 35 pen. Oak.

37

36

35

34

33

32

31

30

29

28

27

S 83° 3' W

aspen

8" aspen/bears S 51° W
distance 23' 8"

SCRIBED B.T.

6" pine STUMP BEARS

N 63° 0' N SCRIBED B.T.
Distance 36' 4"
8" aspen BEATS N 35° E
SCRIBED S-5 B.T.
Distance H 1' 4"

6" aspen BEARS S 62° E
SCRIBED S-24-B.T.
Distance 20'

aspen 20R

Ø 1/2 i.p. about 11' tall 3' Stake
5' (2) square on 4 sides.

Mug. Bearing S 83° 3' W
Pond & me

THUNDER LAKE

26+99 LEFT from S. side SW 1/4

25

24

23

22+50 ENTERED from S. side SW 1/4

21

20

19

18+00 LEFT going to enter SW 1/4 sec - Blych.

17

16

15

14

13+20 ENTERED pine grove

12

11

10

9

8

7

6

5

4

3

2

1

0+00 Started West from S.C. 1615 2122 140.R26

583 $\frac{1}{2}$ W

Feb 16, 1938 H5.
M. Woods. Notes
G. Comstock. H. Chair
M. Bain. F. Chair

about
B1Km

Single
before

May. Beg. 1/14 S 4 $\frac{1}{2}$ W
R 1/2 N Dm Lines
3500 ft 1,000 ft

4' Squared Stake

Sept 16, 1938 H6.

52 + 85 Appr. S. C. 512 to 4" squared on H sides.

51

50

49 + 49 NE 1/4 plug hole lake entered spruce 5 n 2 m p

48 + 00 edge of plug hole lake

47

46

45

44 + 69
43 + 12

NE 1/4 plug hole lake entered spruces same...
edge of plug hole

42

41

40

39

38

37

36

35

34

33

32

31

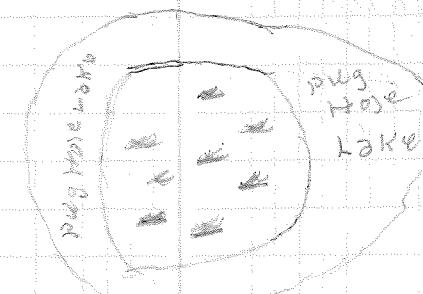
30

29

28

27

S 83 1/2 W.



Mag. Bearing S 83 1/2 W.
Par 0003, 1/16

aspen pine

aspen pine

Ref. Job 1938, 41.
M. Woods, Notes
B. Comstock H. chain
M. Bain Rear chain.

26+40 LEFT lake

25

24

23

22+92 edge OF lake.

21

20

19

18

17

16+91 east end of lake Htco North of Line

15

14

13+20 left Spruce Swamp

12

11+00 entered Spruce Swamp

10

9

8+31 LEFT Spruce Swamp entered Mixed

7

6

5

4

3+31 entered Spruce Swamp

2

1

0+00 offset line North to Line From East.

S 82° W.

PLK HOLE
LAKE

MIXED HTW

MIXED HARDWOOD

Aug 19, 1938 S 82° W

Started West From A.P.A. S.C., 17^{1/2} T. 14 R. 26
2021

Feb. 16 1938 Hg.

52 83.7" FOUND 3" SQUARED STAKES CEDS 5-17 519-S-18x 520 S 82°W

51

50

49

48

47

46

45

44

43

42

41+99 LEFT PLUG HOLE S.W. OF CEDAR 5' IN THE SWAMP

40

39

38

37+00 PLUG HOLE SWAMP

36

35

34

33

32

31

30

29

28

27+63 OLD TRAIL N.E.-SW.

□ 10" SPRUCE BEARS S 62°W
5' CEDS 5-17-B1.

DISTANCE 31.8

6" SPRUCE BEARS S 86°W
SCIBED 5-17-B1.

DISTANCE 32.4

4" SPRUCE BEARS S-35°E
SCIBED 5-20-B1.

DISTANCE 12.8

PLUG HOLE
SWAMP.

MIXED H.W.
PINE-ASPEN.

49.

Setting Board Controls

T. 139-26

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

I.P.
 Controls

100' Distance from I.P. @ $\frac{3}{2}$ 139-26
east to Highway #6 - $6\frac{1}{2}^{\circ}$

100' Distance from $\frac{1}{4}$ cor. $\frac{34}{3}$ 139-26
east to Fehr's road ~~road~~ - $6\frac{1}{2}^{\circ}$

2127' Distance to $\frac{1}{4}$ cor $\frac{33}{4}$ 139-26
(R,

894' Distance from $\frac{32}{5} \frac{33}{4}$ 139-26
south to Fehr's road $6\frac{1}{2}^{\circ}$

2520' Distance from $\frac{1}{4}$ cor. $\frac{33}{4}$ 139-26
south to Fehr's road $6\frac{1}{2}^{\circ}$

366' Distance from $\frac{3}{10} \frac{12}{11}$ 139-26
west to Highway #6 $6\frac{1}{2}^{\circ}$

28' Distance from ~~10/11~~ 139-26 $\frac{1}{4}$ cor. 10/11
west to Highway #6

52' Distance from $\frac{15}{20} \frac{14}{23}$ 139-26
N. 66 $\frac{2}{3}$ W. to Control post

Intersection of camp road & #6.

15' Distance from ~~22~~²³/₂₇ 139-26
west to control post. $6\frac{1}{2}^{\circ}$

100' Distance from ~~28~~²⁷/₃₃³⁴ 139-26 $6\frac{1}{2}^{\circ}$
south to control post on road

1045' Distance from ~~35~~³⁵/₃₈ 139-26 $\frac{1}{4}$ $7\frac{1}{8}$
north to Muchow's road. 6°

2088' Distance from ~~31~~³²/₆⁵ 140-26
west to Lake George road $6\frac{1}{2}^{\circ}$

36' Distance from $\frac{1}{4}$ $\frac{7}{8}$ 139-26
east to Lake George road.

18' Distance from ~~16~~¹⁵/₂₁ 139-26
north to camp road

518' Distance from $\frac{1}{4}$ $\frac{16}{21}$ 139-26
north to camp road.

1835' Distance from ~~33~~³⁴/₄³ 139-26
south to Fehr's road. $6\frac{1}{2}^{\circ}$

1675' Distance from ~~10~~¹¹/₁₅¹⁷ 139-26 $\frac{3}{10}\frac{2}{11}$
north to High # 6.

0' set control post by corner $\frac{13}{24}\frac{18}{19}$ 139-26
139-27

corner ~~edge~~ ~~at~~ ~~in~~

in road.— control east of road-High # 6

2847' Distance from ~~18 10
30 29~~ 139-26 3883'

west to Mitchel Lake rd.

18.6' Distance from ~~28 30
36 31~~ 139-26

west to control post.

~~Set control post for 21/11/12 139-27
" " " 11/12 139-27
" " " 11/13 139-27~~

28.1' Distance from ~~10 11
15 17~~ 139-26

west to control post

Narrow's

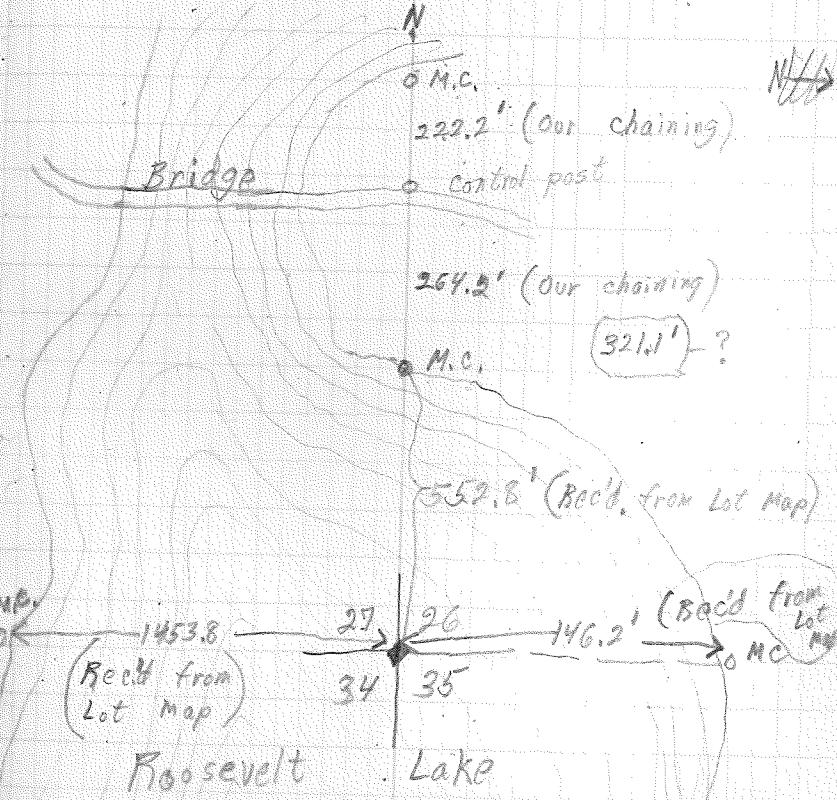
~~10'~~ Distance control post is set
Only a south of iron pipe found
Lot Pipe just north of High. #6
at "Narrow's".

391' Control post set 391' sooth
of iron pipe. Found on
shore of Roosevelt
Lake - M.C. corner.

corner in center of road.

-Narrows-

Information received on M.C. at Narrow's.



Controls on Swatara Road.

1141.4' Distance from cor. ~~24~~
to Swatara road ~~25~~ 139-26

At cor. Also set control at corner
~~24~~ which is at side
~~25~~ of resort road to
Manning's place.

Party:

Woods, Chopka

Schartz, Anbeam

Date: 12/14/38

Par

control/s on crooked Lake Rd.

T 139-26

At cor. Bet control at cor. $\frac{26}{35} \frac{25}{36}$
12/14/38At cor. Set control at cor. $\frac{25}{36}$
12/14/38

Co.

Party:

Woods

Schwartz

Chopka

Anderson, R.

Date:

12/14/38

Controls on Cedar Spring Rd.

At cor. Set control at cor. $\frac{23}{24} \frac{24}{25}$ 139-26
 $\frac{26}{25}$

Party:

Johnson, R.

Schwartz

Chopka

Date:

12/14/38

Setting Road Controls

T. 139-27

6	5	4	3	2	1	X
7	8	9	10	11	12	
18	17	16	15	14	13	
19	20	21	22	23	24	
30	29	28	27	26	25	
31	32	33	34	35	36	

Controls on Trelipi Roads

Set control post for $\frac{21}{11/12}$ 139-27 corner

Set control post for $\frac{11/12}{11/12}$ 139-27

Set control post for $\frac{14}{23} \frac{13}{24}$ 139-27 same corner described on next page.

Set control post for $\frac{23}{26} \frac{24}{25}$ 139-27

Controls on the Dog Lake Spur.

Distance:

At cor. set control post at $\frac{13}{27}$ 139-27 corner is on south side of road.

At cor. Set control post at $\frac{19}{23} \frac{13}{21}$ 139-27 " " " " " " "

At cor. Set control post at $\frac{15}{23} \frac{14}{23}$ 139-27 " " " " " " "

2300' Distance south from $\frac{18}{19}$ 139-27
to Dog Lake Spur. St Contd

Controls on the Old Grade

16.9' Distance from $\frac{6}{6}$ 139-27
south to control post on ^{Brosco's} side $\frac{6}{6}$ rod 63' Iron pipe in center of road.

17.3' Distance from $\frac{6}{6}$ 139-27
west to control on Old Grade. 63'

17.9' Distance from $\frac{6}{7}$ 139-27
west to control on old grade 63'

18.4' Distance from $\frac{7}{7}$ 139-27
west to control on old grade. 63'

18' Dis. from $\frac{7}{8}$ 139-27
west to con. on old grade.

18' Dis. from $\frac{18}{19}$ 139-27
west to old grade.

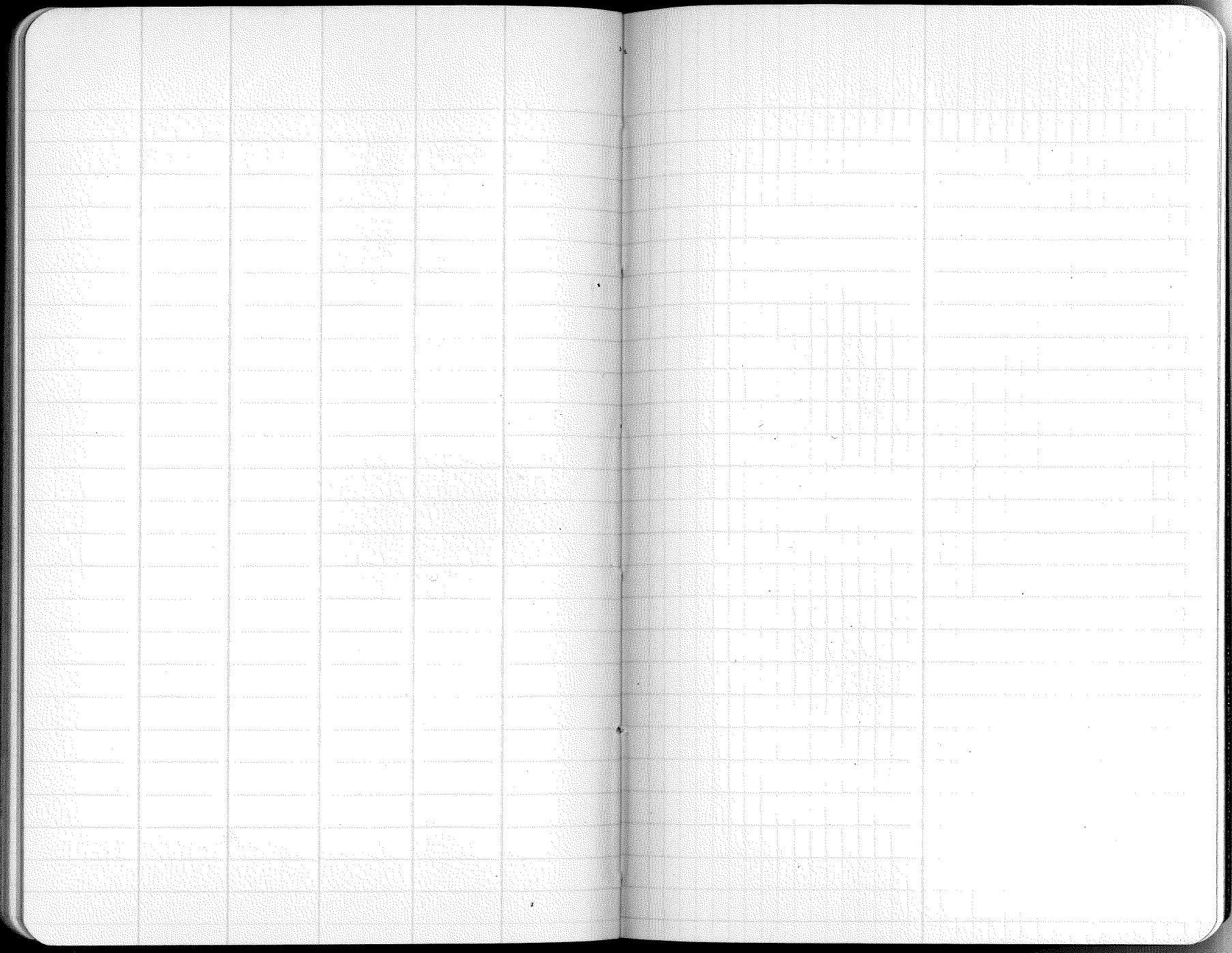
18.3' Distance from $\frac{18}{18}$ 139-27
west 10.00' with old grade.

14' Distance from $\frac{30}{31}$ 139-27
west to old grade.

No post

| 31 | 139-27

1200' distance from ~~31~~ 139-27 ~~to~~ V
nest to off grade.



T 140 -27

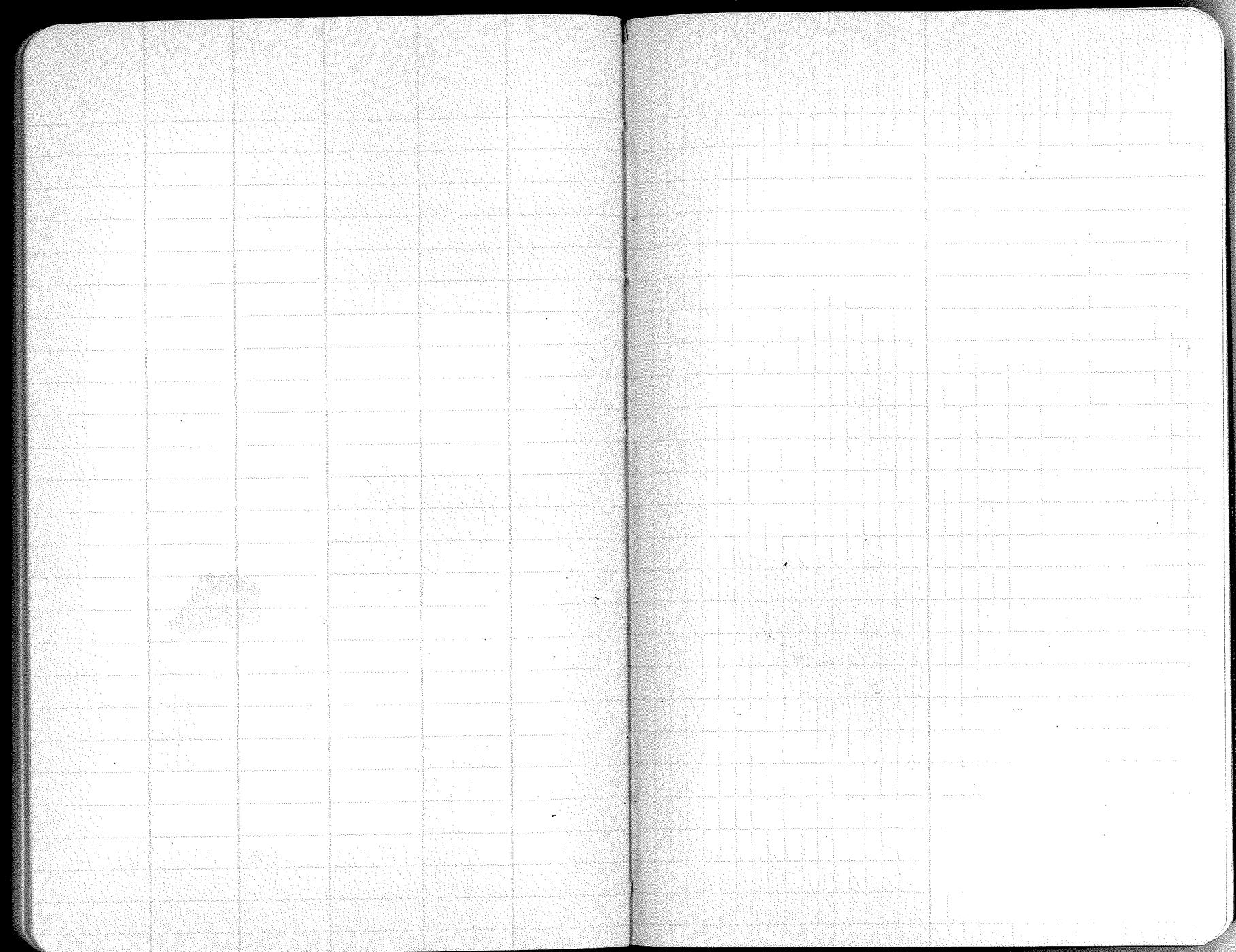
Controls on Old R.R. Grade

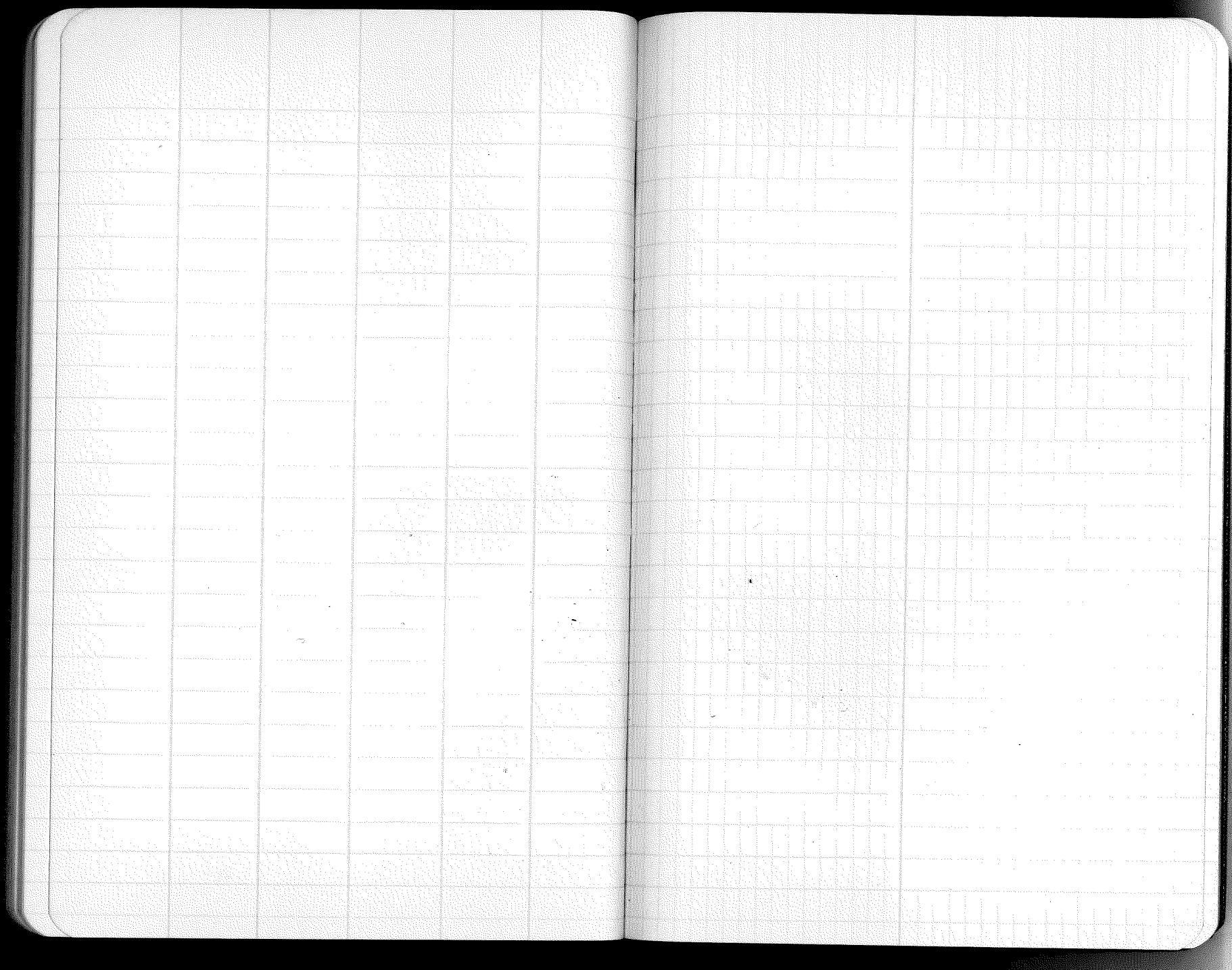
375' Distance from ~~30~~¹³⁰/₃₁ 140-27
south to control post on grade

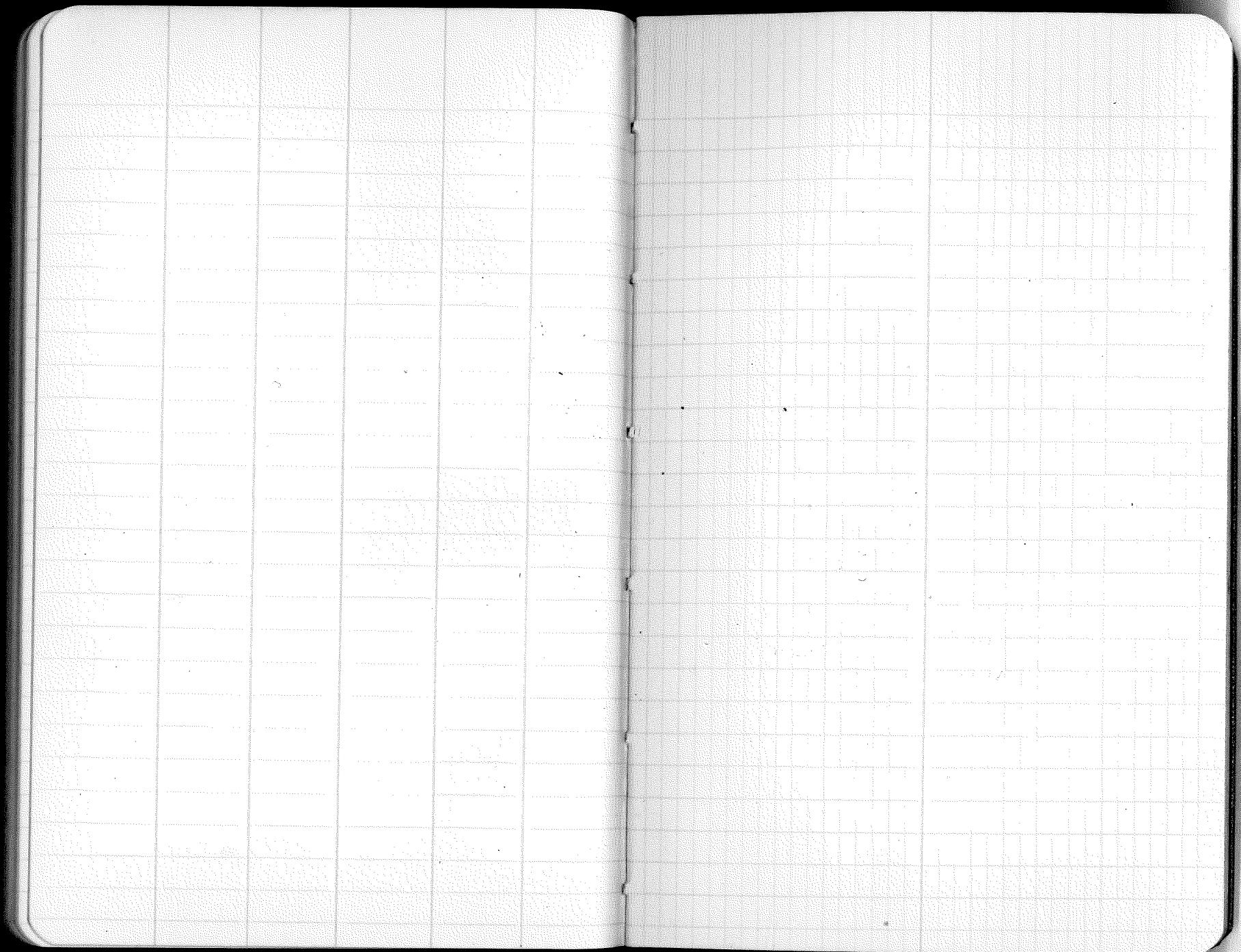
380' Distance from ~~30~~¹³⁰/₃₁ 140-27
east to control post on
Old grade

530' Dist. from ~~30~~³⁰/₃₁ cor 140-27
north to control post on

888' Distance from ~~30 29~~^{30 29}/_{31 32} 140-27
north to control post on
old grade







T 139-25

Johnson &
Party: Woods, M.
Chyka, J.
Schwartz, C.

Date: Dec. 16, 1938

Swatara Road

{ Control for 4 139-25 is

1340' south of sec. cor.

cor. in { Control for 11/12 139-25 is
road. edge of intersection - S.E. side. Found: Two wood post; one at N.W. cor. S.E. cor.

Found: Iron pipe E.C.W. Reest, 6" dia.
old wood post

Cor. in { Control for 131 139-25 is found: Yellow tag on
road. (southeast side of curve in road. Settler said

Telephone post.
it is the corner.

Party: Johnson, R
Woods, M
Schwartz
Chupka

Date:
Dec. 16 '38

Morrison Lake Trail

Cor. in { Control for
road

30/29 139-25
31/32

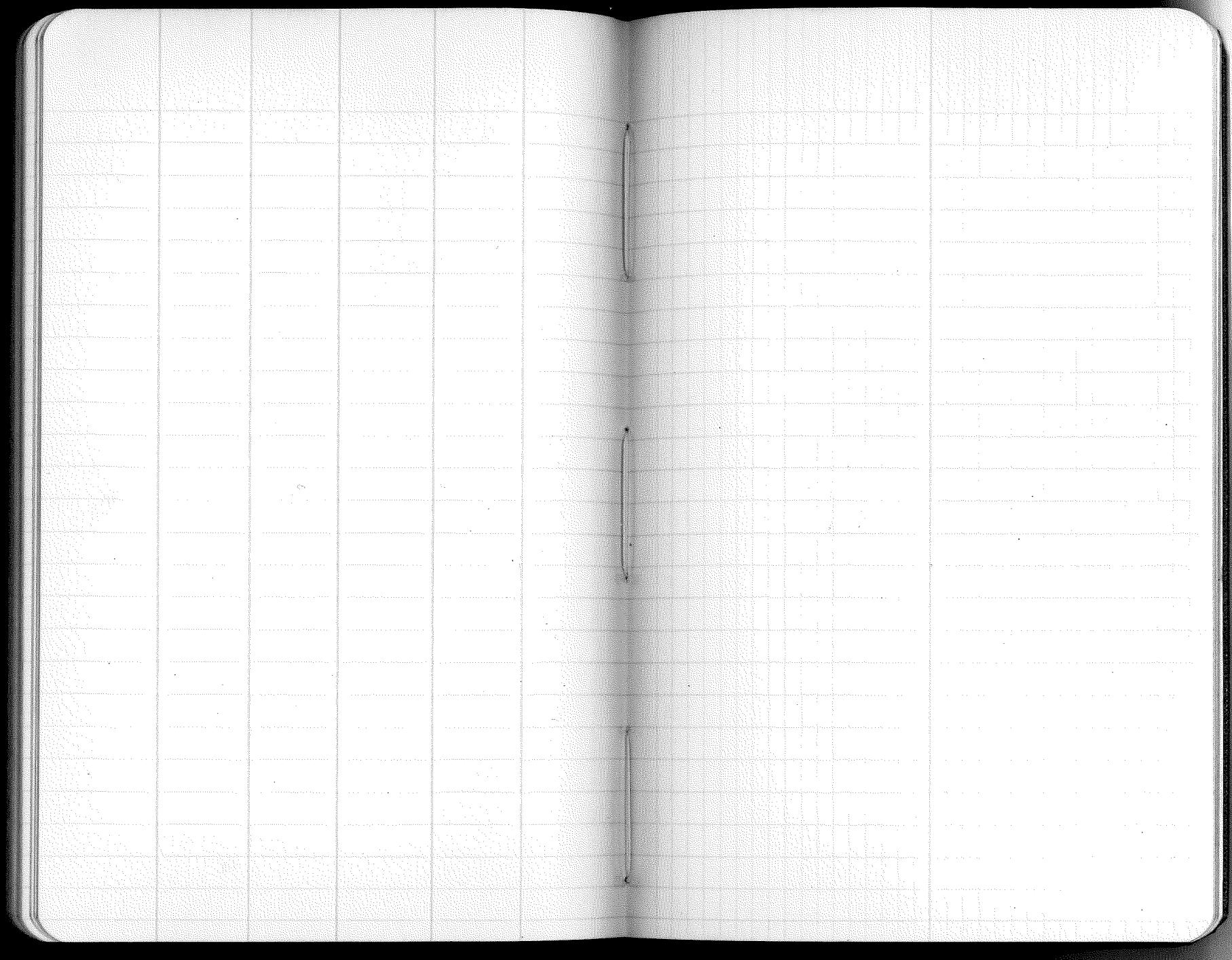
Found: Iron pipe & wood post in the
center of road & 2" under.

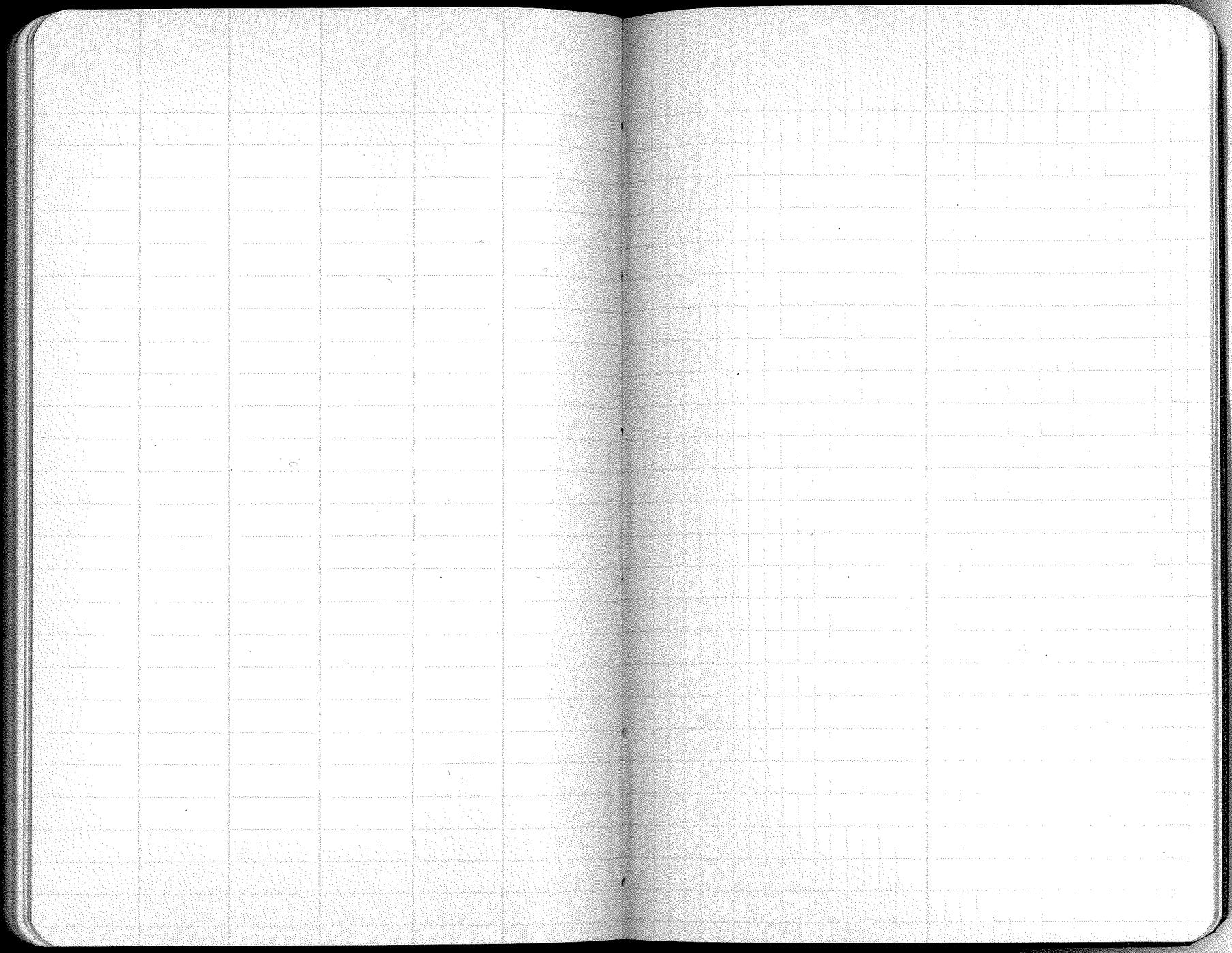
8/9
17/16

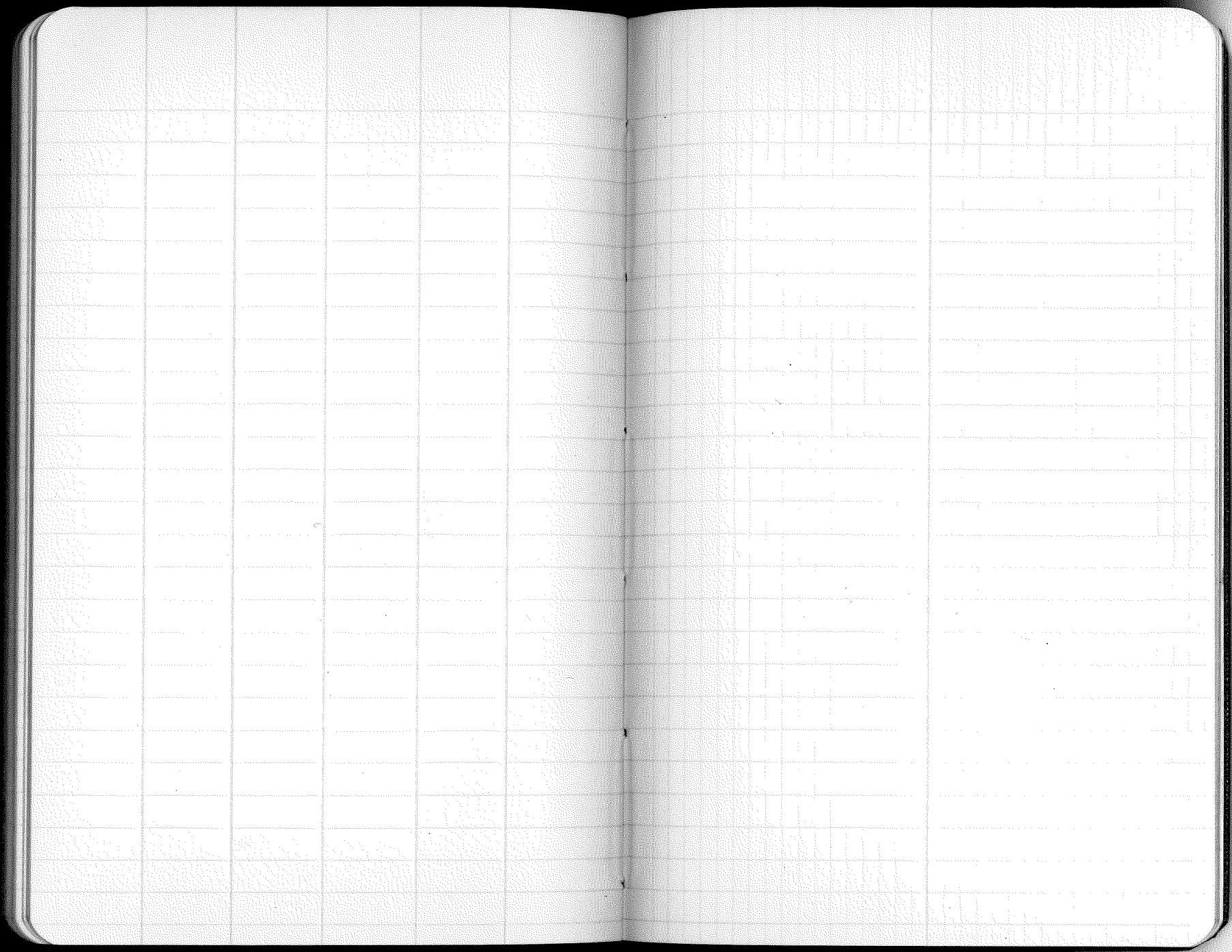
T 140 R 27

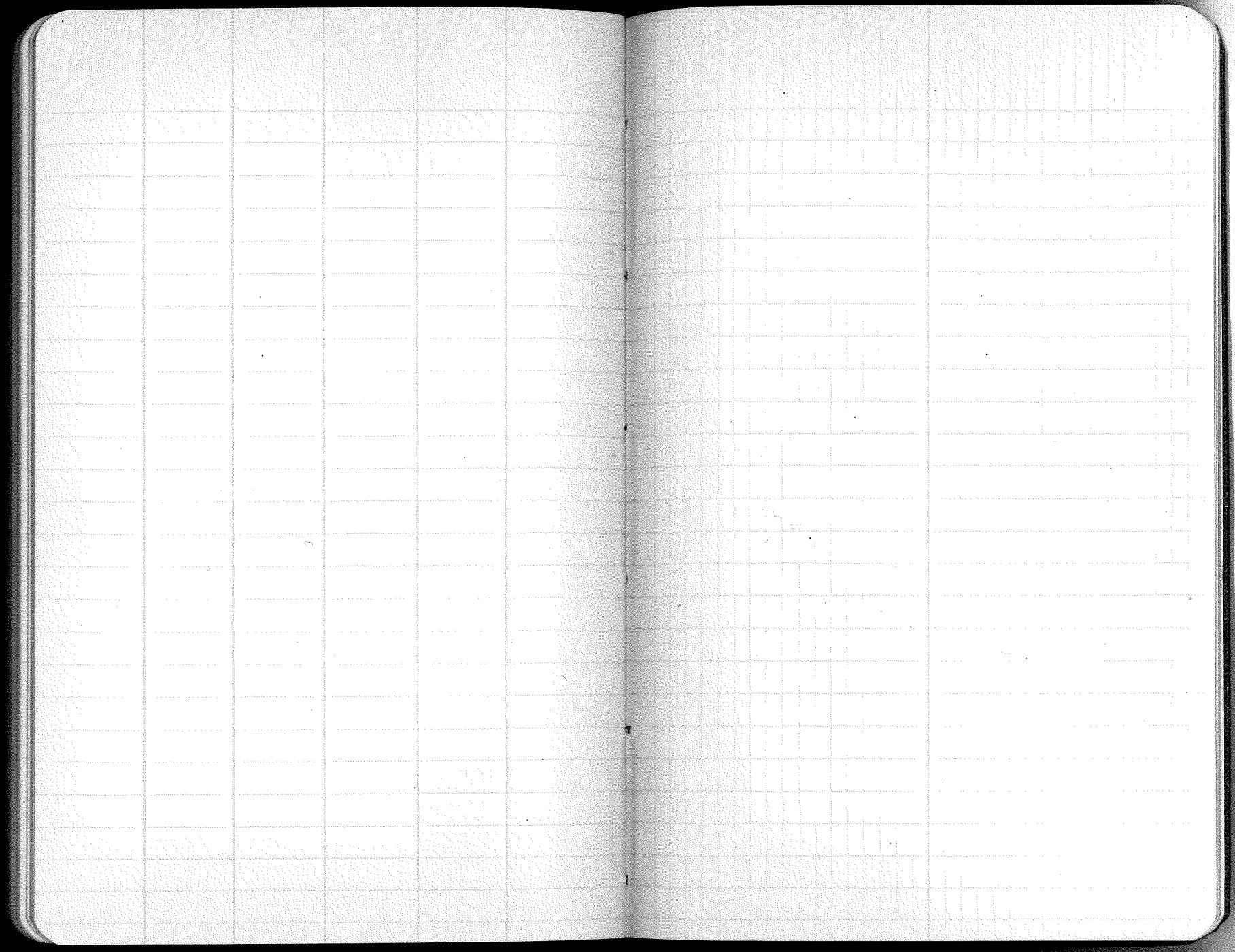
374'
loc 7
220' wood post
2 BT's

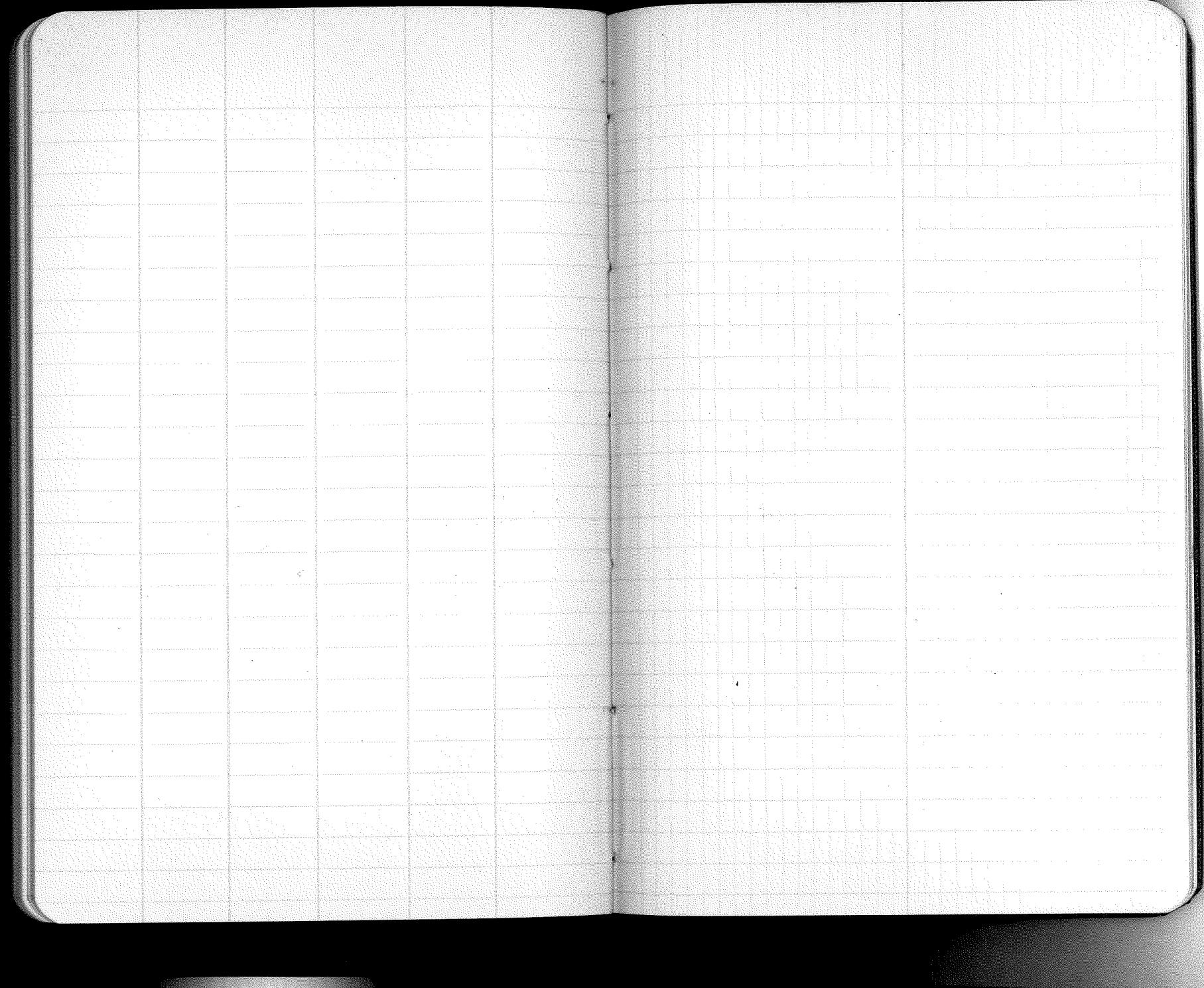
June 20, 1940

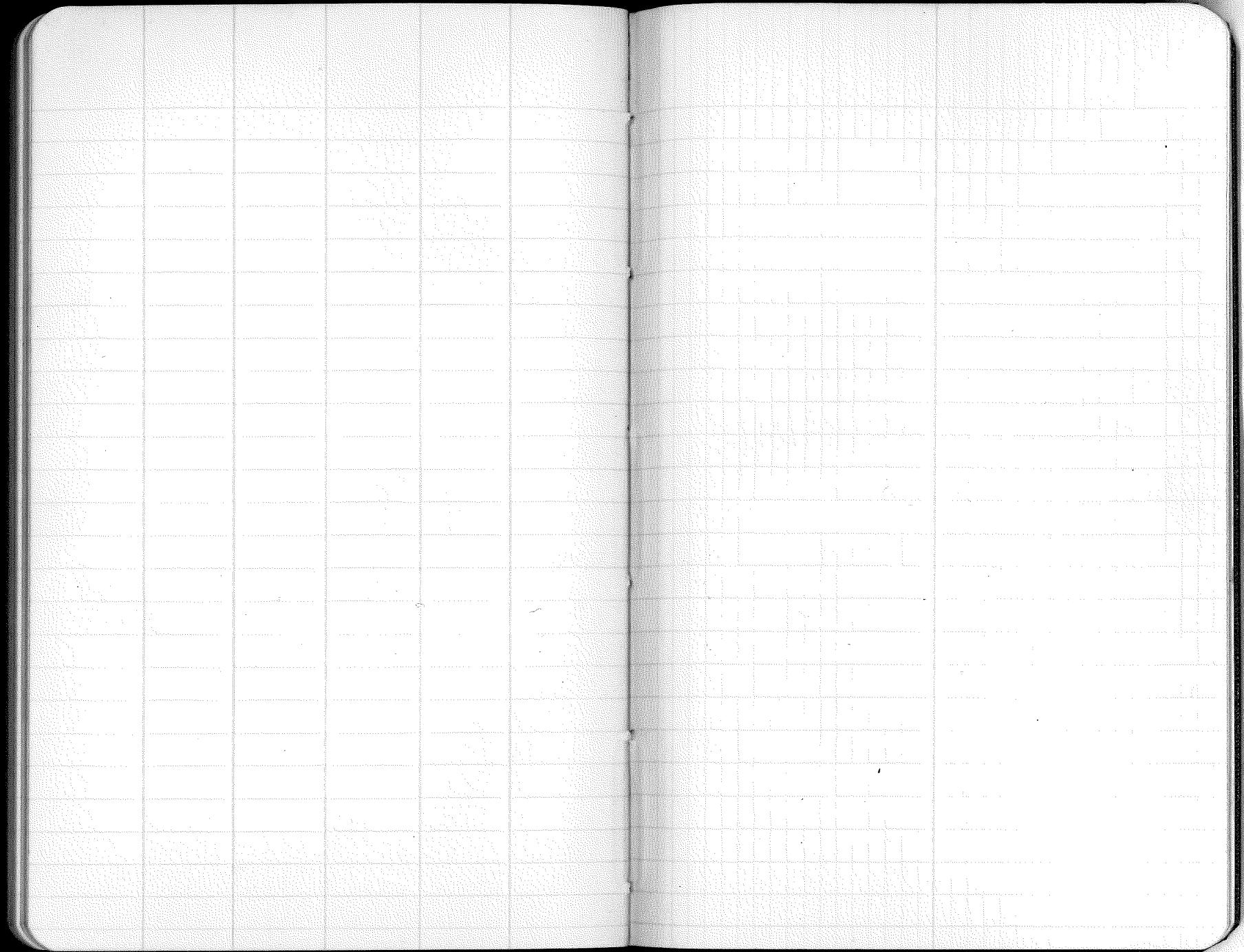












IMPROVED TABLES AND INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

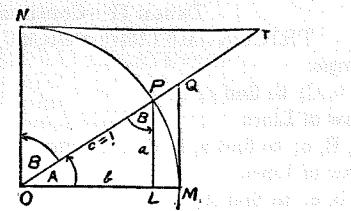


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2 ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2}A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2}A = \frac{r}{s-a}$$

$$\tan \frac{1}{2}B = \frac{r}{s-b}$$

$$\tan \frac{1}{2}C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2}ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}(B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	$\times .00019$	= miles
Lineal yards	$\times .0006$	= miles
Square inches	$\times .007$	= square feet
Square feet	$\times .111$	= square yards
Square yards	$\times .0002067$	= acres
Acres	$\times 4840$	= square yards
Cubic inches	$\times .00058$	= cubic feet
Cubic feet	$\times .03704$	= cubic yards
Links	$\times .22$	= yards
Links	$\times .66$	= feet
Feet	$\times 1.5$	= links

$$360^\circ = 21600' = 1296000"$$

Radius = arc of 57.2957790°

Arc of 1° (radius = 1) = .017453292

Arc of $1'$ (radius = 1) = .000290888

Arc of $1''$ (radius = 1) = .000004848

$$\pi = 3.141592654$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163$$

$$\sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776$$

$$\pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{3} = 0.523598776$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in $1\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet

2. Alignment. One end 1.4 feet out of line

3. Sag of tape at centre of 0.61 feet.

4. Temperature difference of 15°

5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ

Horizontal Distance = $R - R \sin^2 a + C \cos a$

Vertical Distance = $R \frac{1}{2} \sin 2a + C \sin a$

distance from Object glass to cross hairs

R = Reading \times distance between cross hairs

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

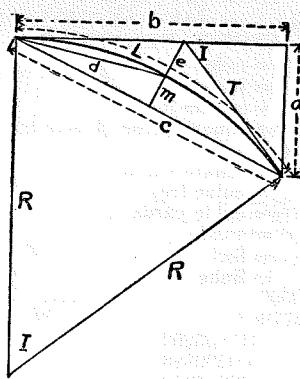


TABLE V
CURVE FORMULAE FOR SIMPLE CURVES
COMPILED BY J. CALVIN LOCKE, C.E.

$$(1) c = \sqrt{2Ra} \quad (2) c = \sqrt{a^2 + b^2}$$

$$(3) c = \sqrt{2R(R - \sqrt{(R+b)(R-b)})} = \sqrt{2R(R - \sqrt{R^2 - b^2})}$$

$$(4) c = 2\sqrt{m(2R-m)}$$

$$(5) c = 2R \sin \frac{1}{2}I \quad (6) c = 2T \cos \frac{1}{2}I$$

$$(7) e = R \operatorname{exsec} \frac{1}{2}I$$

$$(8) e = R \tan \frac{1}{2}I \tan \frac{1}{4}I \quad (9) e = T \tan \frac{1}{4}I$$

$$(10) b = \sqrt{a(2R-a)}$$

$$(11) b = \sqrt{\left(c + \frac{c^2}{2R}\right)\left(c - \frac{c^2}{2R}\right)} = \sqrt{c^2 - \frac{c^4}{4R^2}}$$

$$(12) b = R \sin I \quad (13) b = a \cot \frac{1}{2}I$$

$$(14) R = \frac{a^2 + b^2}{2a} = \frac{c^2}{2a} \quad (15) R = \frac{d^2}{2m} = \frac{c^2 + 4m^2}{8m}$$

$$(16) d = \sqrt{R(2R - \sqrt{(2R+c)(2R-c)})} = \sqrt{R(2R - \sqrt{4R^2 - c^2})}$$

$$(17) d = \sqrt{2Rm} \quad (18) d = 2R \sin \frac{1}{4}I \quad (19) m = \frac{d^2}{2R}$$

$$(20) m = R \mp \sqrt{\left(R + \frac{c}{2}\right)\left(R - \frac{c}{2}\right)} = R \mp \sqrt{R^2 - \frac{c^2}{4}}$$

$$(21) m = R \operatorname{vers} \frac{1}{2}I \quad (22) m = R \sin \frac{1}{2}I \tan \frac{1}{4}I \quad (23) m = \frac{1}{2}ct$$

$$(24) a = \frac{c^2}{2R} \quad (25) a = R - \sqrt{(R+b)(R-b)} = R - \sqrt{R^2 - c^2}$$

$$(26) a = 2R(\sin^2 \frac{1}{2}I)^2 \quad (27) a = R \operatorname{vers} I \quad (28) a = R \sin I \operatorname{ta}$$

$$(29) a = b \tan \frac{1}{2}I \quad (30) a = T \sin I \quad (31) T = R \tan \frac{1}{2}I$$

$$(32) I = \frac{L}{R} \times 57.295780 \quad (33) R = \frac{L}{I} \times 57.295780$$

$$(34) L = IR \times 0.01745329 \quad (35) L = \frac{8d - c}{3}$$

$$(36) \text{Area Seg.} = \frac{LR - R^2 \sin I}{2} = \frac{LR - Rb}{2}$$

TABLE VI

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches								
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches										
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3.84	69	45- 6.48	86	56- 9.12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11.76	70	46- 2.40	87	57- 5.04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7.68	71	46-10.32	88	58- 0.96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3.60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11.52	73	48- 2.16	90	59- 4.80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10.08	91	60- 0.72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3.36	75	49- 6.00	92	60- 8.64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11.28	76	50- 1.92	93	61- 4.56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7.20	77	50- 9.84	94	62- 0.48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3.12	78	51- 5.76	95	62- 8.40
11	7- 3.12	28	18- 5.76	45	29- 8.40	62	40-11.04	79	52- 1.68	96	63- 4.32
12	7-11.04	29	19- 1.68	46	30- 4.32	63	41- 6.96	80	52- 9.60	97	64- 0.24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8.16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1.44	99	65- 4.08
15	9-10.80	32	21- 1.44	49	32- 4.08	66	43- 6.72	83	54- 9.36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2.64	84	55- 5.28	101	66- 7.92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	+	10'	580.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	5° C.	20'	568.53	28.137	5° C.	20'	1079.2	100.75	5° C.
30'	75.01	.491	T	30'	576.95	28.974	T	30'	1087.8	102.35	T
40'	83.34	.606	.03	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	E	50'	593.79	30.686	E	50'	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024		10'	610.64	32.447		10'	1122.4	108.90	
20'	116.68	1.188		20'	619.07	33.347		20'	1131.0	110.57	
30'	125.02	1.364		30'	627.50	34.259		30'	1139.7	112.25	
40'	133.36	1.552		40'	635.93	35.183		40'	1148.4	113.95	
50'	141.70	1.752		50'	644.37	36.120		50'	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425		20'	669.70	39.006		20'	1183.1	120.87	
30'	175.06	2.674	.06	30'	678.15	39.993	.13	30'	1191.8	122.63	.19
40'	183.40	2.934	E	40'	686.60	40.992	E	40'	1200.5	124.41	E
50'	191.74	3.207	.003	50'	695.06	42.004	.011	50'	1209.2	126.20	.025
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10'	208.43	3.790		10'	711.97	44.066		10'	1226.6	129.82	
20'	216.77	4.099		20'	720.44	45.116		20'	1235.3	131.65	
30'	225.12	4.421		30'	728.90	46.178		30'	1244.0	133.50	
40'	233.47	4.755		40'	737.37	47.253		40'	1252.8	135.35	
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10'	258.51	5.829	.09	10'	762.80	50.554	.19	10'	1279.0	141.01	.29
20'	266.86	6.211	E	20'	771.29	51.679	E	20'	1287.7	142.93	E
30'	275.21	6.606		30'	779.77	52.818		30'	1296.5	144.85	
40'	283.57	7.013	.004	40'	788.26	53.969	.017	40'	1305.3	146.79	.038
50'	291.92	7.432		50'	796.75	55.132		50'	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10'	308.64	8.307		10'	813.75	57.498		10'	1331.6	152.69	
20'	316.99	8.762		20'	822.25	58.699		20'	1340.4	154.69	
30'	325.35	9.230		30'	830.76	59.914	20° C.	30'	1349.2	156.70	20° C.
40'	333.71	9.710		40'	839.27	61.141		40'	1358.0	158.72	
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	T
7°	350.44	10.707	.13	17°	856.30	63.634	E	27°	1375.6	162.81	E
10'	358.81	11.224	E	10'	864.82	64.900		10'	1384.4	164.86	
20'	367.17	11.753	.006	20'	873.35	66.178	.022	20'	1393.2	166.95	.051
30'	375.54	12.294		30'	881.88	67.470		30'	1402.0	169.04	
40'	383.91	12.847		40'	890.41	68.774		40'	1410.9	171.15	
50'	392.28	13.413		50'	898.95	70.091		50'	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10'	409.03	14.582		10'	916.03	72.764	25° C.	10'	1437.4	177.55	25° C.
20'	417.41	15.184		20'	924.58	74.119		20'	1446.3	179.72	
30'	425.79	15.799	T	30'	933.13	75.488	T	30'	1455.1	181.89	T
40'	434.17	16.426	.16	40'	941.69	76.869	.32	40'	1464.0	184.08	.49
50'	442.55	17.065	E	50'	950.25	78.264	E	50'	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10'	459.32	18.381		10'	967.38	81.092		10'	1490.7	190.74	
20'	467.71	19.058		20'	975.96	82.525		20'	1499.6	192.99	
30'	476.10	19.746		30'	984.53	83.972		30'	1508.5	195.25	
40'	484.49	20.447		40'	993.12	85.431		40'	1517.4	197.53	
50'	492.88	21.161		50'	1001.7	86.904		50'	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	.19	20'	1027.5	91.399	.39	20'	1553.1	206.77	.59
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	E
40'	534.89	24.913		40'	1044.7	94.462		40'	1571.0	211.48	
50'	543.29	25.700	.008	50'	1053.3	96.013	.034	50'	1580.0	213.86	.078

 $T = R \tan \frac{1}{2} I$ $E = R \operatorname{exsec} \frac{1}{2} I$ TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	T	30'	2170.8	397.4	T	30'	2763.7	631.7	T
40'	1624.9	226.0	.13	40'	2180.3	400.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	404.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.5	645.2	.056
10'	1652.0	233.4		10'	2209.0	411.1		10'	2804.9	649.7	
20'	1661.0	235.9		20'	2218.6	414.5		20'	2815.2	654.3	
30'	1670.0	238.4		30'	2228.1	418.0		30'	2825.6	658.8	
40'	1679.1	241.0		40'	2237.7	421.4		40'	2835.9	663.4	
50'	1688.1	243.5		50'	2247.3	425.0		50'	2846.3	668.0	
33°	1697.0	246.1	10° C.	33°	2257.0	428.5	10° C.	33°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.26	20'	2276.2	435.6	.34	20'	2877.5	682.0	.42
30'	1724.4	253.9	E	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	E	40'	2295.6	442.8	E	40'	2898.4	691.4	E
50'	1742.6	259.1	.046	50'	2305.2	446.4	.075	50'	2908.9	696.1	.112
34°	1751.7	261.8		34°	2314.9	450.0		34°	2919.4	700.9	
10'	1760.8	264.5		10'	2324.6	453.6		10'	2929.9	705.7	
20'	1770.0	267.2		20'	2334.3	457.3		20'	2940.4	710.5	
30'	1779.1	269.9		30'	2344.1	461.0		30'	2951.0	715.3	
40'	1788.2	272.6		40'	2353.8	464.6		40'	2961.5	720.1	
50'	1797.4	275.3		50'	2363.5	468.4		50'	2972.1	725.0	
35°	1806.6	278.1	T	35°	2373.3	472.1	T	35°	2982.7	729.9	T
10'	1815.7	280.8	.40	10'	2383.1	475.8	.51	10'	2993.3	734.8	.63
20'	1824.8	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	E	30'	2402.6	483.4	E	30'	3014.5	744.6	E
40'	1843.3	289.2	.070	40'	2412.4	487.2	.116	40'	3025.2	749.6	.168
50'	1852.5	292.0		50'	2422.3	491.0		50'	3035.8	754.6	
36°	1861.7	294.9		36°	2432.8	494.8		36°	3046.5	759.6	
10'	1870.9	297.7		10'	2441.9	498.7		10'	3057.2	764.6	
20'	1880.1	300.6		20'	2451.8	502.5		20'	3067.9	769.7	
30'	1889.4	303.5		30'	2461.7	506.4		30'	3078.7	774.7	
40'	1898.6	306.4		40'	2471.5	510.3		40'	3089.4	779.8	
50'	1907.9	309.3		50'	2481.4	514.3		50'	3100.2	784.9	
37°	1917.1	312.2	E	37°	2491.3	518.2	E	37°	3110.9	790.1	.84
10'	1926.4	315.2	.093	10'	2501.2	522.2	.151	10'	3121.7	795.2	
20'	1935.7	318.1		20'	2511.2	526.1		20'			

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVETABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2		71°	4086.9	1308.2		81°	4893.6	1805.3	
10'	3386.3	925.9	+	10'	4099.5	1315.6	+	10'	4908.0	1814.7	+
20'	3397.5	931.6	5° C.	20'	4112.1	1322.9	5° C.	20'	4922.5	1824.1	5° C.
30'	3408.8	937.3	T	30'	4124.8	1330.3	T	30'	4937.0	1833.6	T
40'	3420.1	943.1	.25	40'	4137.4	1337.7	.30	40'	4951.5	1843.1	.36
50'	3431.4	948.9	E	50'	4150.1	1345.4	E	50'	4966.1	1852.6	E
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10'	3454.1	960.6		10'	4175.6	1360.1		10'	4995.4	1871.8	
20'	3465.4	966.5		20'	4188.5	1367.6		20'	5010.0	1881.5	
30'	3476.8	972.4		30'	4201.2	1375.2		30'	5024.8	1891.2	
40'	3488.3	978.3		40'	4214.0	1382.8		40'	5039.5	1900.9	
50'	3499.7	984.3		50'	4226.8	1390.4		50'	5054.3	1910.7	
63°	3511.1	990.2	10° C.	73°	4229.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10'	3522.6	996.2	T	10'	4252.6	1408.7	T	10'	5084.0	1930.4	T
20'	3534.1	1002.3		20'	4265.6	1413.5		20'	5099.0	1940.3	
30'	3545.6	1008.3	.51	30'	4278.5	1421.2	.61	30'	5113.9	1950.3	.72
40'	3557.2	1014.4	E	40'	4291.5	1429.0	E	40'	5128.9	1960.2	E
50'	3568.7	1020.5	.159	50'	4304.6	1436.8	.220	50'	5143.9	1970.3	.299
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10'	3591.9	1032.8		10'	4330.7	1452.5		10'	5174.1	1990.5	
20'	3603.5	1039.0		20'	4343.8	1460.4		20'	5189.3	2000.6	
30'	3615.1	1045.2		30'	4356.9	1468.3		30'	5204.4	2010.8	
40'	3626.8	1051.4		40'	4370.1	1476.4		40'	5219.7	2021.1	
50'	3638.5	1057.7	15° C.	50'	4383.3	1484.4	15° C.	50'	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10'	3661.9	1070.2	.76	10'	4409.8	1500.5	.91	10'	5265.6	2052.1	.109
20'	3673.7	1076.6	E	20'	4423.1	1508.6	E	20'	5281.0	2062.5	E
30'	3685.4	1082.9		30'	4436.4	1516.7		30'	5296.4	2073.0	
40'	3697.2	1089.3	.240	40'	4449.7	1524.9	.332	40'	5311.9	2083.5	.450
50'	3709.0	1095.7		50'	4463.1	1533.1		50'	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10'	3732.7	1108.6		10'	4489.9	1549.7		10'	5358.6	2115.3	
20'	3744.6	1115.1		20'	4503.4	1558.5		20'	5374.2	2126.0	
30'	3756.5	1121.7		30'	4516.9	1566.3		30'	5389.9	2136.7	
40'	3768.5	1128.2	20° C.	40'	4530.4	1574.7	20° C.	40'	5405.6	2147.5	20° C.
50'	3780.4	1134.8	T	50'	4544.0	1583.1	T	50'	5421.4	2158.4	T
67°	3792.4	1141.4	E	77°	4557.6	1591.6	1.22	87°	5437.2	2169.2	1.45
10'	3804.4	1148.0		10'	4571.2	1600.1	E	10'	5453.1	2180.2	E
20'	3816.4	1154.7	.321	20'	4584.8	1608.6	.445	20'	5469.0	2191.1	.603
30'	3828.4	1161.3		30'	4598.5	1617.1		30'	5484.9	2202.2	
40'	3840.5	1168.1		40'	4612.2	1625.4		40'	5500.9	2213.2	
50'	3852.6	1174.8		50'	4626.0	1634.4		50'	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10'	3876.8	1188.4		10'	4653.6	1651.7		10'	5549.2	2246.7	
20'	3889.0	1195.2	25° C.	20'	4667.4	1660.5	25° C.	20'	5565.4	2258.0	25° C.
30'	3901.2	1202.0	T	30'	4681.3	1669.2	T	30'	5581.6	2269.3	T
40'	3913.4	1208.9	1.28	40'	4695.2	1678.1	1.53	40'	5597.8	2280.6	1.83
50'	3925.6	1215.8	E	50'	4709.2	1686.9	E	50'	5614.2	2292.0	E
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10'	3950.2	1229.7		10'	4737.2	1704.7		10'	5646.9	2315.0	
20'	3962.5	1236.7		20'	4751.2	1713.7		20'	5663.4	2326.6	
30'	3974.8	1243.7		30'	4765.3	1722.7		30'	5679.9	2338.2	
40'	3987.2	1250.8		40'	4779.4	1731.7		40'	5696.4	2349.8	
50'	3999.5	1257.9		50'	4793.6	1740.8		50'	5713.0	2361.5	
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9		90°	5729.7	2373.3	
10'	4024.4	1272.1	T	10'	4822.0	1759.0	T	10'	5746.3	2385.1	T
20'	4036.8	1279.3	1.54	20'	4836.2	1768.2	1.84	20'	5763.1	2397.0	2.20
30'	4049.3	1286.5	E	30'	4850.5	1777.4	E	30'	5779.9	2408.9	E
40'	4061.8	1293.6		40'	4864.8	1786.7		40'	5796.7	2420.9	
50'	4074.4	1300.9	.485	50'	4879.2	1796.0	.671	50'	5813.6	2432.9	.910

T = R tan $\frac{1}{2} I$ E = R exsec $\frac{1}{2} I$

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	
10'	5847.5	2457.1		10'	6971.3	3294.1	5° C.	10'	8362.7	4407.6	+
20'	5864.6	2469.3		20'	6992.0	3310.1	5° C.	20'	8388.9	4429.2	5° C.
30'	5881.7	2481.5	T	30'	7012.7	3326.1	T	30'	8415.1	4450.9	T
40'	5898.8	2493.8	.43	40'	7033.6	3342.3	.51	40'	8441.5	4472.7	.62
50'	5916.0	2506.1	E	50'	7054.5	3358.5	E	50'	8468.0	4494.6	E
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10'	5950.5	2531.0		10'	7096.6	3391.2		10'	8521.3	4538.8	
20'	5967.9	2543.5		20'	7117.8	3407.7		20'	8548.1	4561.1	
30'	5985.3	2556.0		30'	7139.0	3424.3		30'	8575.0	4583.4	
40'	6002.7	2568.6		40'	7160.3	3440.9		40'	8602.1	4606.0	
50'	6020.2	2581.3		50'	7181.7	3457.6		50'	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10'	6055.4	2606.8	T	10'	7224.7	3491.3	T	10'	8684.0	4674.7	T
20'	6073.1	2619.7		20'	7246.3	3508.2		20'	8711.5	4697.2	
30'	6090.8	2632.6		30'	7268.0	3525.2		30'	8739.2	4720.3	1.25
40'	6108.6	2645.5	E	40'	7289.8	3542.4	E	40'	8767.0	4743.0	E
50'	6126.4	2658.5	.401	50'	7311.7	3559.6	.536	50'	8794.9	4766.9	.721
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10'	6162.2	2684.7		10'	7355.6	3594.2		10'	8851.0	4814.1	
20'	6180.2	2697.9		20'	7377.8	3611.7		20'	8879.3	4837.8	
30'	6198.3	2711.2		30'	7399.9	3629.2		30'	8907.7	4861.1	
40'	6216.4	2724.5		40'	7422.2	3646.8		40'	8936.3	4885.7	
50'	6234.6	2737.9	15° C.	50'	7444.6	3664.5	15° C.	50'	8965.0	4909.9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10'	6271.1	2764.8	1.30	10'	7489.6	3700.2	1.56	10'	9022.7	4958.6	1.93
20'	6289.4	2778.3	E	20'	7512.2	3718.2	E	20'	9051.7	4983.1	E
30'	6307.9	2792.0		30'	7534.9	3736.2		30'	9080.9	5007.6	
40'	6326.3	2805.6	.604	40'	7557.7	3754.4	.806	40'	9110.3	5032.6	1.09
50'	6344.8	2819.4		50'	7580.5	3772.6		50'	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10'	6382.1	2847.0		10'	7626.6	3809.4		10'	9199.1	5107.9	
20'	6400.8	2861.0		20'	7649.7	3827.9		20'	9229.0	5133.3	
30'	6419.5	2875.0		30'	7672.9	3846.5		30'	9259.0	5158.3	
40'	6438.4	2889.0	20° C.	40'	7696.3	3865.2	20° C.	40'	9289.0	5184.5	20° C.
50'	6457.3	2903.1	T	50'	7719.7	3884.0	T	50'	9319.5	5210.3	T
97°	6476.2	2917.3	E	107°	7743.2	3902.9	E	117°</			

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C o / Feet	R Inch	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o / Feet	R Inch	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot	
35	10	16-26	8-13	49.3	
45	10	12-46	6-23	38.3	
50	15	17-16	8-38	34.5	
60	15	14-22	7-11	28.8	
75	15	11-30	5-45	23.0	
100	20	11-30	5-45	17.3	
120	20	9-34	4-47	14.3	
150	20	7-39	3-49	11.5	
190	25	7-32	3-46	9.15	
200	25	7-10	3-35	8.6	
225	25	6-25	3-12	7.7	
240	25	5-58	2-59	7.2	
250	25	5-44	2-52	6.9	
275	25	5-12	2-36	6.2	
288	50	9-58	4-59	6.0	
300	50	9-32	4-46	5.7	
350	50	8-12	4-06	4.9	
376	50	7-40	3-50	4.6	
400	50	7-10	3-35	4.3	
410	50	7-00	3-30	4.2	

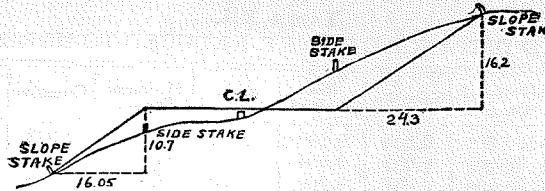
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.023	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10°30'	.17500	20°30'	.34167	30°10'	.50833	40°30'	.67500	50°10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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