

339

E	L	A	N

Field Book

E 64-8x4

1 1 BS 2

0-0-0

91-12-20

255.81

77.923

255.756

3 50-15-10

92-44-25

74.68

22.763

74.595

2 0

70.00 03

1

TERRY DOVOT

GL 5-34-141-28

T @ 2 BS 1

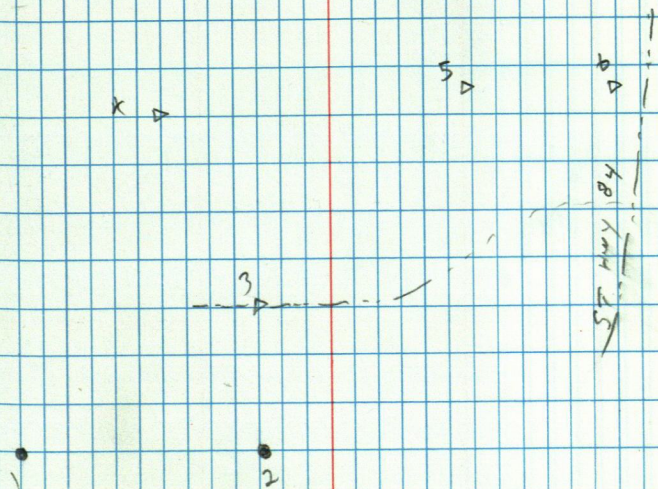
0-0-31			490.00	
100-0-38	84-0-31	91-48-02	149.351	489.87
84-01-02			203.29	
3 264-01-08	84-00-30	90-54-04	61.958	203.256

T @ 3 BS 2

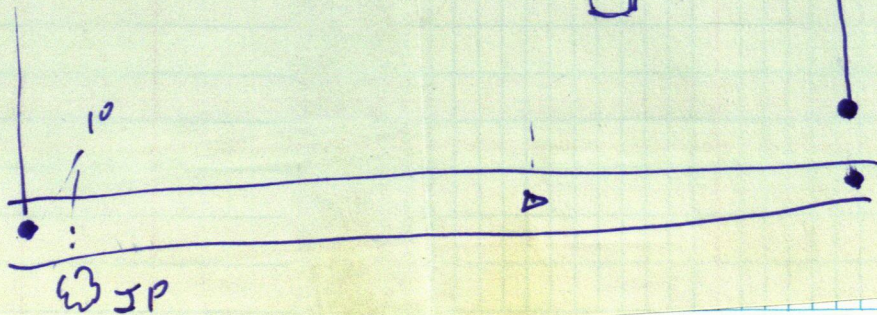
0-0-03				
181-0-06	123-54-47			
123-55-10				
4 303-55-15	123-55-09			
243-1-54	243-01-31			
5 63-01-55	243-01-49			

T @ 5 BS 2

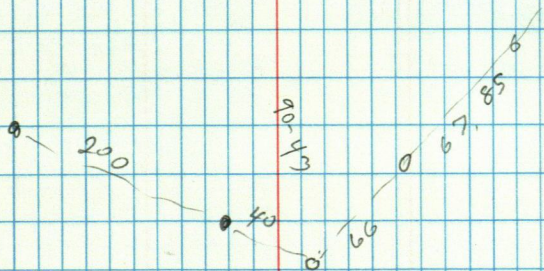
0-0-26			528.30	
180-0-25	210-00-33	82-53-33	160.746	527.809
210-01			255.30	
6 30-0-57	210-00-32	91-50-35	77.80	255.14



DICK JOHNSON



$$\begin{array}{r} 66 \\ 67.85 \\ \hline 133.85 \end{array}$$



179-18-10

98.04.30

96.90

95.948

29.541

92-18

251.63

251.427

6-21-76

Tom HASSER

T@ 2 BS 1

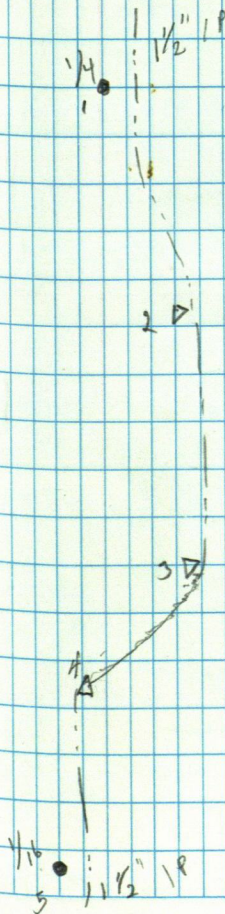
		91-12-54	382.20 116.496	382.114
3	173-24-54	173-24-54	90-47-18	446.25 136.017
	346-49-42			446.206

T@ 3 BS 2

	215-54-10	215-54-15
4	071-48-30	

T@ 4 BS 3

	166-02-57	90-15-44	262.47 80.006	262.467
5	166-03-06	91-46-54	219.02 66.757	218.913
	332-05-54			

E. Coto
R. Turner

6-21-96

JIM OATES

BLAIR WATER

T @ 2 BS 1

160-38-30

90-27-36

189.43

57.737

189.421

③ 301-16-48 160-38-24

90-34-54

116.72

35.568

116.700

T @ 2 BS 1

218-55-18

218-55-18

269-48-54

297.09

87.504

297.086

077-50-36

4

T @ 4 BS 2

274-20-06

274-20-27

5

188-40-54

T @ 1 BS 2

262-37-42

E. CURD

R. Turner

3

4

1305

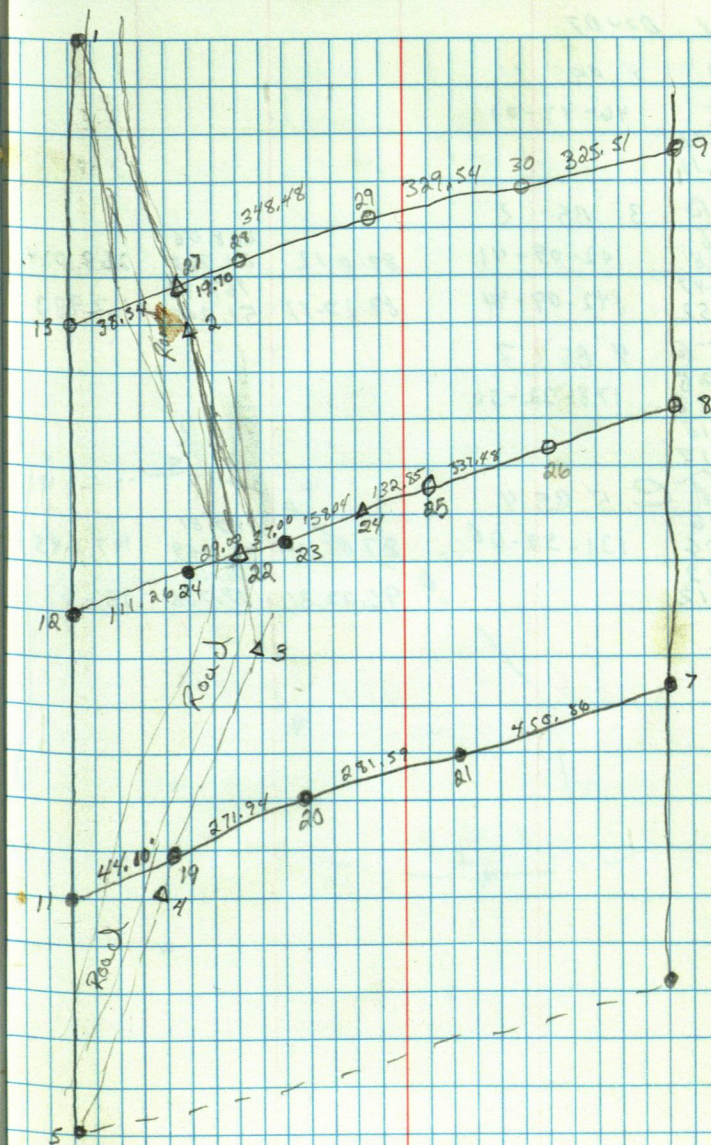
FRIR

1

Tom HASSER

6-24-56

	T@ 20 BS 19			
		89-54-06	271.94 82.887	271.938
21		268-58-36	81.59 85.823	281.525
	T@ 21 BS 20			
7		269-35-18	450.86	450.848
	T@ 22 BS 2			
23	84-14-00		37.00	
	T@ 22 BS 2			
24	84-14-00		29.00	
	T@ 22 BS 2			
12	84-14-00		111.26	
	T@ 23 BS 12			
24		270-30-06	158.04 48.169	158.022
	T@ 24 BS 12			
25		269-00-42	132.85 40.497	132.837 337.448
	T@ 25 BS 23			
26		269-38-30	337.48 102.849	337.448
	T@ 25 BS 23			
8		269-34-30	606.05 184.734	606.047
	T@ 27 BS 1			
13	77-38-54		38.34	
	T@ 27 BS 1			
29	77-38-54	91-19-48	348.48 106.218	348.387
	T@ 29 BS 27			
30		271-11-36	329.54 100.445	329.469
	T@ 30 BS 29			
9		269-01-54	325.51 99.230	325.486

R. Turner
T. Turner

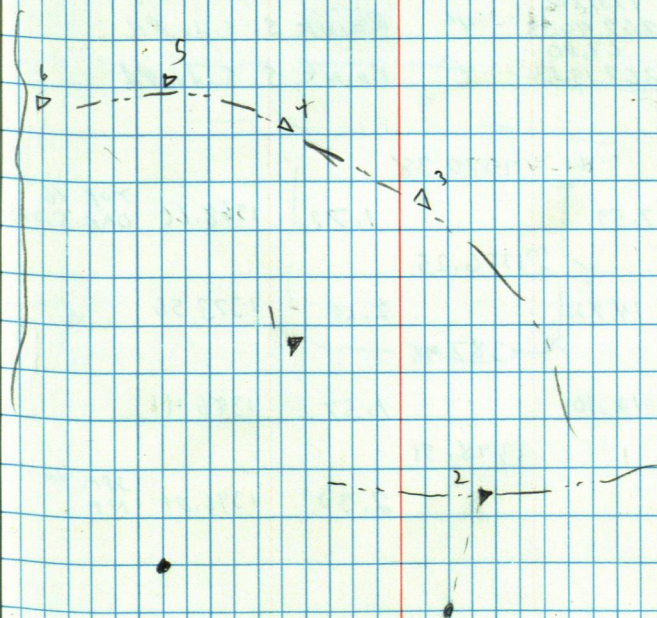
TERRY 00007

π 2 BS 1
 0-0-12
 180-0-12 46-43-00
 46-43-12
 ③ 126-43-12

π 3 BS 2
 0-0-06
 180-0-08 142-09-41 89-0-12 268.06 81.708 268.024
 142-09-47 167.99
 4 322-9-52 142-09-44 89-27-41 51.204 167.983

π 4 BS 3
 0-0-25
 180-0-27 178-22-50
 178-23-15
 3 353-23-17

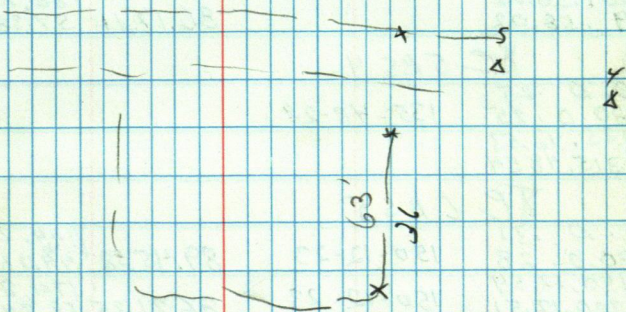
π 5 BS 4
 0-0-06
 180-0-06 131-59-06 87.05-04 147.81 45.069 147.645
 131-59-12 255.21
 6 311-59-12 96-22-36 77.788 253.63



TOP	BS	4		
0.0.07				
L	DIST	ROD	REMARKS	
170.22.30	23.15			
	V.263.0433	4'	TOE + N SIDE RD	
118.40.10	29"	4'		
	263.04.37		TOE + S SIDE RD	
	94.39			
113.22.14	263.03.06	4'	TOE TH HILL	
	147.61			
120.14.53	262.26.25	4'	TOE TH HILL	
	199.24			
127.15.36	262.25.28	4'	TOE TH HILL	
	123.30			
137.51.08	262.40.33	4'	BRINK S. SIDE RD	
	67.80			
151.17.55	262.19.53	4'	BRINK S. SIDE RD	

HI = 1370.38

BM ¹ L	7.59	1.72	1368.66	TOP 16" OAK STUMP
			1376.25	
TP	14.42	2.69	1373.56	
			1387.98	
TP	12.10	1.57	1386.41	
			1398.51	
BM ¹ I		2.50	1396.01	SPR IN NP



0000 MUNSOW

AC 2 B5 1	
0.0.08	
180.0.08	244-45-04
244.45.12	
364.45.14	
91.57.00	153.44
91.30.01	46.766
	153.346
	160.99
	49.066
	160.926

AC 3 B5 2	
0.0.27	
180.0.28	165-20-28
165.20.55	
4245.20.57	

AC 4 B5 3	
0.0.20	
180.0.20	189-57-42
189.58.02	
9.58.02	
91.54.22	174.57
86.17.11	53.207
	174.47
	188.28
	57.388
	187.884

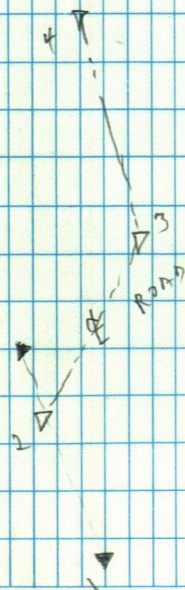
AC 5 B5 4	
0.0.25	
180.0.25	135-48-28
135.48.53	
6315.48.54	

AC 6 B5 5	
0.0.31	
180.0.28	150-12-23
150.12.54	
7330.12.51	150-12-23
89.45.58	144.24
86.21.25	44.035
	174.89
	53.340
	144.36
	174.60

AC 7 B5 6	
0.0.15	
180.0.20	185-25-28
185.25.48	
8.5.25.53	

AC 8 B5 7	
0.0.15	
180.0.15	172-45
172.45.15	
9352.45.15	172-44-55
90.34.17	191.13
93.40.04	58.260
	127.48
	38.865
	191.126
	127.217

AC 9 B5 8	
0.0.20	
180.0.20	112-40-50
112.41.10	
10292.41.10	



10 B 5 9

0.0.10		180.10	
180.0.10	219-29-54	93.32.47	54.897 179.759
219.30.04		125.11	
11 39.30.04		87.43.15	38.133 125.10

11 B 5 10

0.0.28	
180.0.28	154-34-13
154.34.41	
12 334.34.39	154-34-13

12 B 5 11

0.0.0		113.02	
180.0.0	218-32-02	85.48.01	34.448 112.715
218.32.02		106.48	
13 38.32.01		99.38.45	82.459 104.981

BILL SMITH

T@ 2 BS 1

3 024-41-18 24-41-03
049-22-06

T@ 3 BS 2

4 028-14-30 28-14-21	90-01-06	1540.92 469.672	1540.913
056-28-42	90-30-24	215.99 65.835	215.983

5 210-11-30 210-11-36	90-06-06	133.46 40.678	133.456
060-23-12			

6 176-57-30 176-57-33	89-55-36	241.95 73.748	241.951
353-55-06			

T@ 4 BS 3

7 165-34-06

T@ 5 BS 3

8 178-14-48

T@ 6 BS 3

9 114-50-24 114-50-09	89-43-12	174.53 53.196	174.526
229-40-18			

T@ 9 BS 6

10 215-45-12 215-44-54	90-11-06	129.59 39.499	129.588
071-29-48			

T@ 10 BS 9

11 159-23-06 159-22-57	89-44-42	137.15 41.803	137.147
318-45-54			

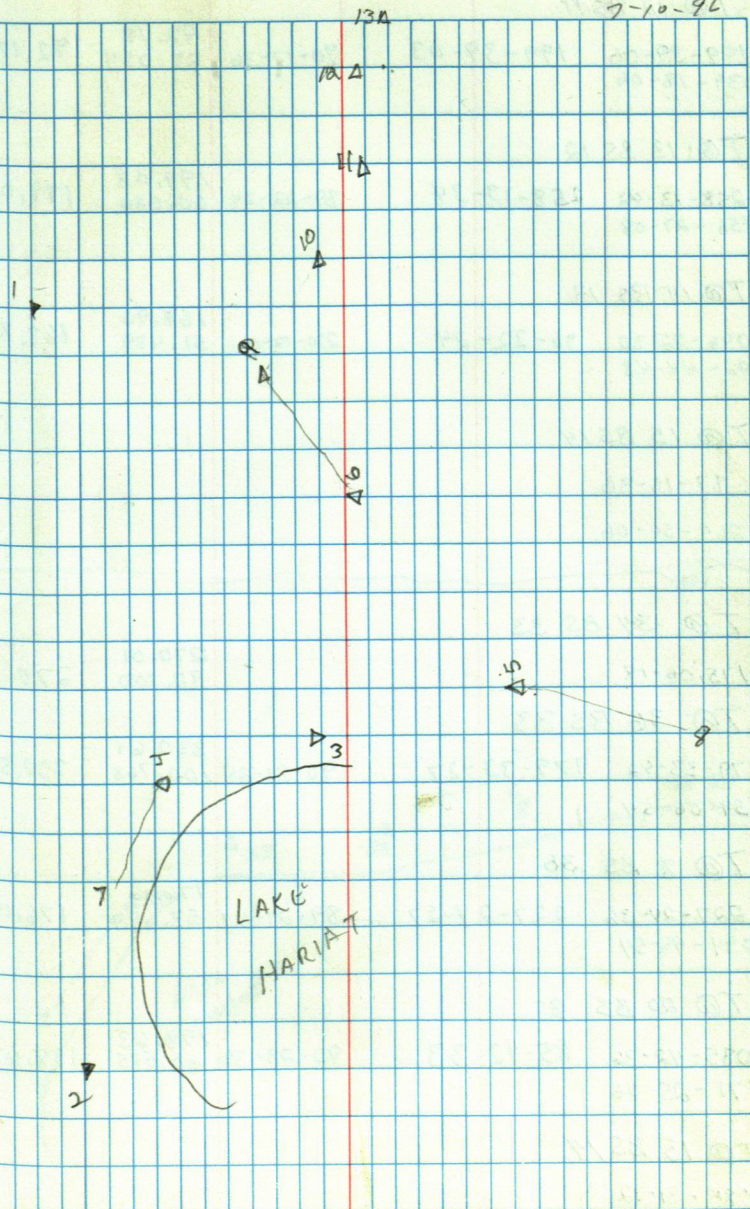
T@ 11 BS 10

12 208-21-12 208-21-18	89-19-06	146.09 44.527	146.077
056-42-36			

17 15 D. 18 E CUR-
R. TURNER

14 A

7-10-96



Bill Smith

T@ 12 BS 11

13 199-39-06	199-39-03	90-17-36	92.18 28.094	92.174
039-18-06				

T@ 13 BS 12

14 258-13-42	258-13-34	89-22-24	199.08 60.680	199.068
156-27-09				

T@ 14 BS 13

15 096-22-30	96-22-24	270-12-06	168.90 51.479	168.895
192-44-48				

T@ 15 BS 14

17 87-10-36

18 264-50-06

T@ 34 BS 33

7 175.06-18

270.01
80.300 270.01

T@ 36 BS 33

8 179-33-42 179-33-27

90-31-24

330.61
100.768 330.592

359-06-54

T@ 8 BS 36

20 227-24-36 227-24-27

89-21-49

176.16
53.694 176.149

094-48-54

T@ 20 BS 8

19 085-42-36 85-42-33

90-28-30

198.63
60.545 198.627

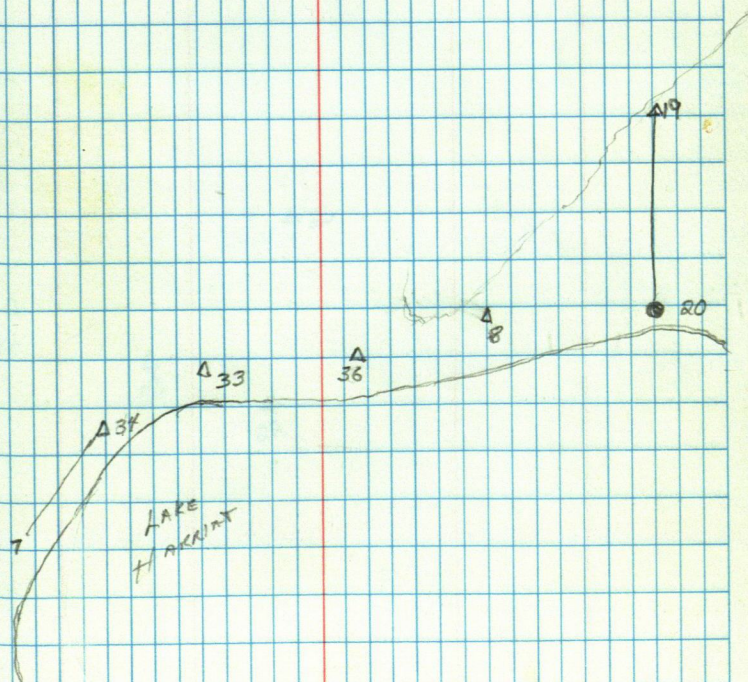
171-25-06

T@ 15 BS 14

17 085-31-12

R. Turner
T. Turner

7-19-96



Bill Smith

7-18-96

T@ 43 BS 42

22 181-53-12	181-53-12	90-55-24	88.75 27,050	88.796
003-46-24				

T@ 22 BS 43

23 098-27-06	98-26-57	268-51-00	205.05 62,500	205.009
196-53-54				

T@ 23 BS 22

24 155-57-06	155-57-12	89-50-48	383.57 116,913	387.568
311-54-24				

R. Turner
T. Turner

Δ 24

Δ 23

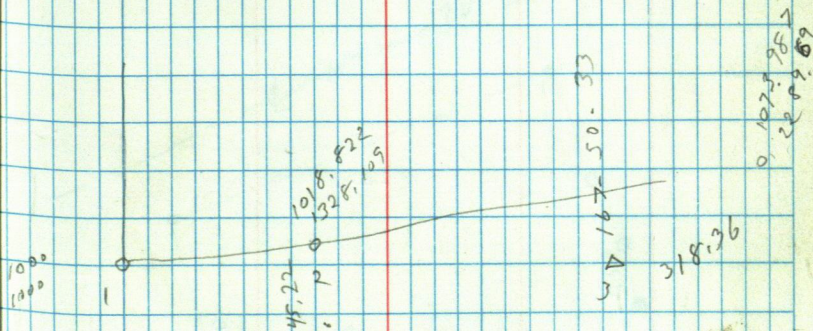
Δ
42Δ
43Δ
22

DAVE STEVERT

TR 2 BS 1

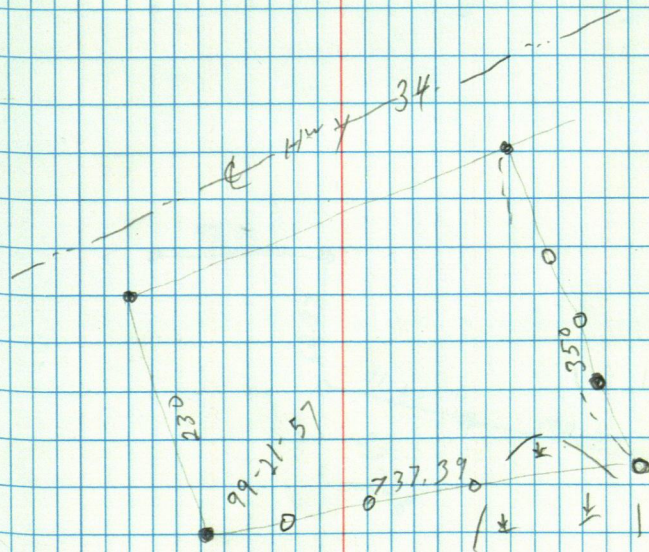
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180-00-10	183-59-21	92-13-53	100.248	328.648
183-59-30			649.60	
3-59-30	183-59-20	89-15-40	197.994	649.536

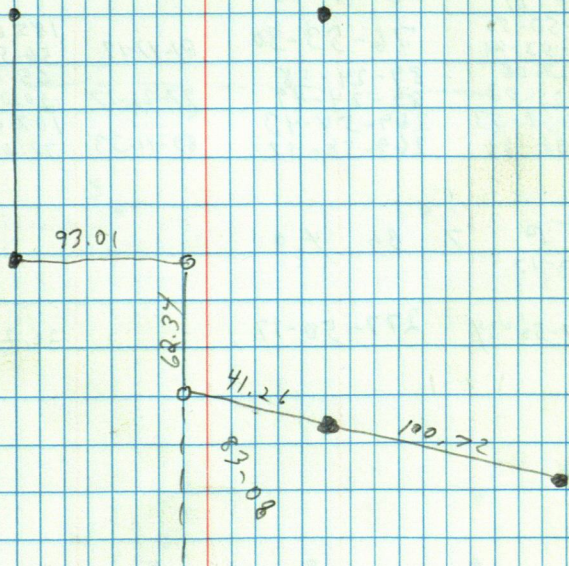
94-43-25 319.10



VFW

93-55.50 350,83





101

BS 2

0-0-0			168.96	168.954
179-59-48		90-31-48	51.500	
35-12-23	35-12-23		67.00	
115-12-30	35-12-42	98-01-29	20.425	66.349
82-33-02	82-33-02		202.24	
4 261-33-11	82-33-23	91-31-17	61.643	202.168
107-13-43	107-13-43		37.05	
5 282-13-48	107-14-0	93-29-15	11.294	36.983
160-37-43	160-37-43		136.59	
6 340-37-48	160-38-0	89-38-02	41.632	136.586

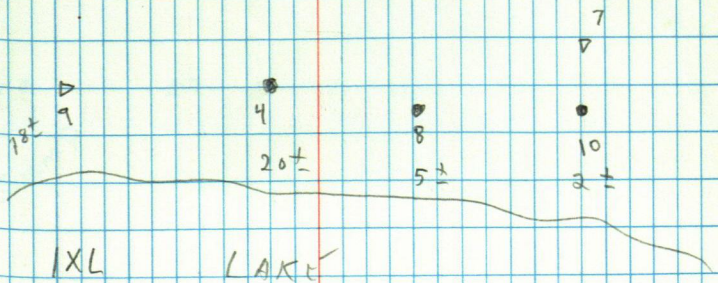
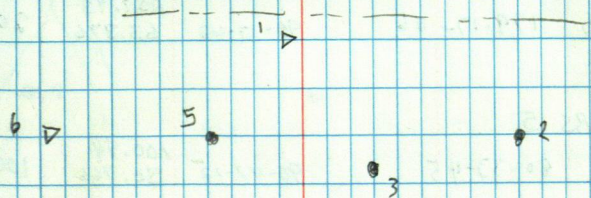
102 4 BS 1

0-0-10	76-50-40			
180-0-19				
76-53-50	76-53-30	91-42-19	185.69	185.597
256-53-49			56.597	
89-25-08	89-24-58		65.76	
8 264-25-08	89-24-49	97-26-17	20.043	65.205
264-58-53	269-58-43		107.09	
9 89-58-36	269-58-17	89-11-33	32.643	107.082

103

7 BS 4

0-0-17				
10 277-50-34	277-50-17		20.28	



Don B. Riddle

7-30-96

R. Turner
T. Turner

T@ 2 BS 1

175-48-12	175-48-08	89-57-24	901.02 274.634	901.021
351-36-00		89-53-06	1134.28 345.729	1134.274

				PT
T@	3	BS	2	

700-5552				
4 093-19-06	93-19-03	91-42-30	204,96 62,471	204,866
186-38-06				

T@ 4 BS 3

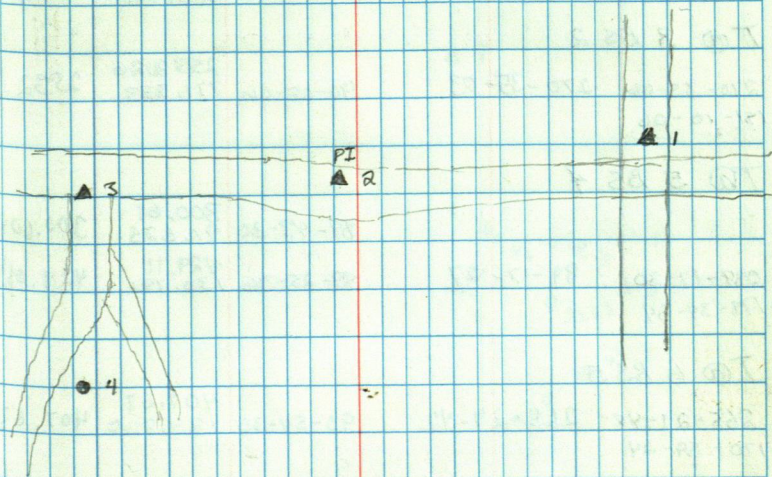
5/181-37-54	181-37-42	92-31-24	206.78 63.027	206.579
003-15-24				

T@ 5334

6	179-17-12	179-17-06	90-37-42	207.93 63.376	207.914
	358-34-12				

T @ 6 BS 5

780-34-06	80-33-45	90-47-12	100,94 30,766	100,929
161-07-30				



45

46

 ΔT

Swamp

HAEN SECORA

T@ 2 BS 1

89-56-42 2758.16
840.688 2758.148

3 179-01-18 179-01-09
358-02-18

90-05-42 1979.16
603.251 1979.153

T@ 3 BS 2

270-35-06 270-35-03

90-02-06 2532.26
771.883 2532.249

4 181-10-06

T@ 5 BS 4

89-43-30 300.61
91.625 300.604

089-17-30 89-17-27

89-25-36 429.11
130.791 429.084

6 178-34-54

T@ 6 BS 5

7 265-29-48 265-29-42
170-59-24

90-54-36 407.67
124.260 407.62

8-14-96 R. Turner
T. Turner

St
Col

24

30

47

40-44-15 0.43.15
0.33.03 45

19-03
25.8

40

90-42-33
6 2 99.06 23.99
5.23 5

Dick Johnson

T@ 1 BS 2

88-40-12 1301.76
396.775
27.38
90-25-12 8.345

4 89-30-36
179-00-54

T@ 3 BS 1

92-01-36 201.00
61.264
287.56
90-05-24 87.648

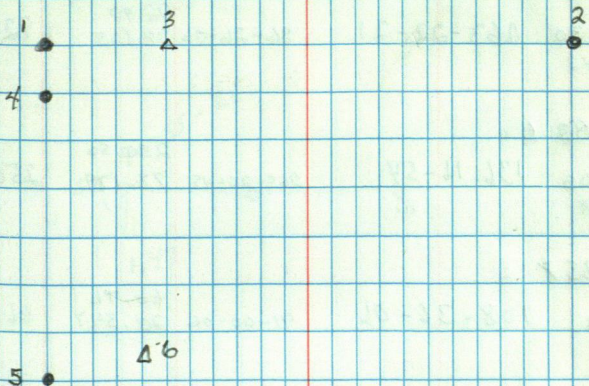
6 273-18-42
186-37-06

T@ 6 BS 3

5 252-16-42 185.21
144-33-12 56.451
89-29-24

8-15-56

R. Turner
T. Turner



DON BRIDGELL

T@ 1 BS 2

90-04-06

900.97
274.615
553.65

900.964

3 270-28-54 270-20-51
180-41-42

90-26-54

168.755

553.634

T@ 6 BS 5

7 263-22-30 263-22-21
166-44-42

86-26-06

92.40
28.163

92.219

T@ 7 BS 6

8 136-17-06 136-16-54
272-33-48

268-20-48

256.50
78.179

256.389

T@ 8 BS 7

9 108-36-18 108-36-06
217-12-12

91-00-06

66.76
20.347

66.747

T@ 6 BS 5

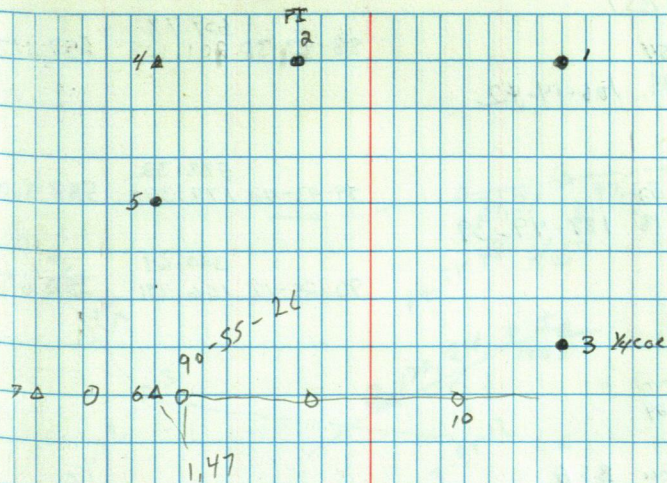
10 90-55-26

90-20-54

504.72
153.838

504.707

8-15-96 R. Turner
T. Turner



KEN SECORIT

T@ 2 BS1

3	106-14-54	88-43-30	659.78 201.103	659.617
	212-29-24	106-14-42		

4	188-49-42	89-43-42	588.32 179.326	588.310
	017-39-18	188-49-39		

5		90-29-18	350.69 106.891	350.677
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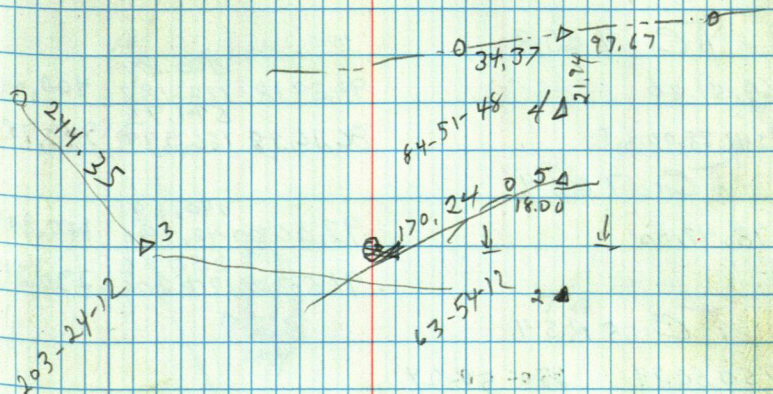
003-54-12
127-48-24

T@ 1/4 cor BS6

7	274-50-36	274-50-39		
	189-41-18			

T@ 7 BS 1/4 C

8	173-02-24	173-02-06	286.53 87.337 1045.53	286.53 1045.502
	346-04-12	270-23-12	318.678	



7

1314.87

7A

330.18

88-28-13

14

DAVE OLSEN PETER

XC 1 B 5 2

(3) 209.30 → 92.42.34 408.89 408.427
124.627

XC 3 B 5 1 ← 89.16.48 143.40 143.386
43.707

(4)

XC 4 B 5 3

(5) 60.51.30 93.39.18 400.87 400.049
122.183

(6) 241.38.00 86.16.48 544.93 543.787
166.049

XC 7 B 5 4

178.47.00 92.00.00 140.39 140.304
42.791

(8) 91.55.00 230.36 230.217
70.206

XC 5 B 5 4

(9) 250.50.24 250-50-24

141.40.48

XC 9 B 5 5

(10) 31.56.48 31-56-54 93.37.00 168.46 68.324
20.867

1163.53.48 87.10.00 129.77 129.611
39.554

(10) 221.14.36 221-14-12 89.22.48 162.99 162.976
49.677

82.28.24

(12) 128.32.36 126.50.12 23.46 18.78

(13) 268.58.12 86.21.00 52.29 52.18

(14) 317.34.24 83.07.24 45.73 45.40

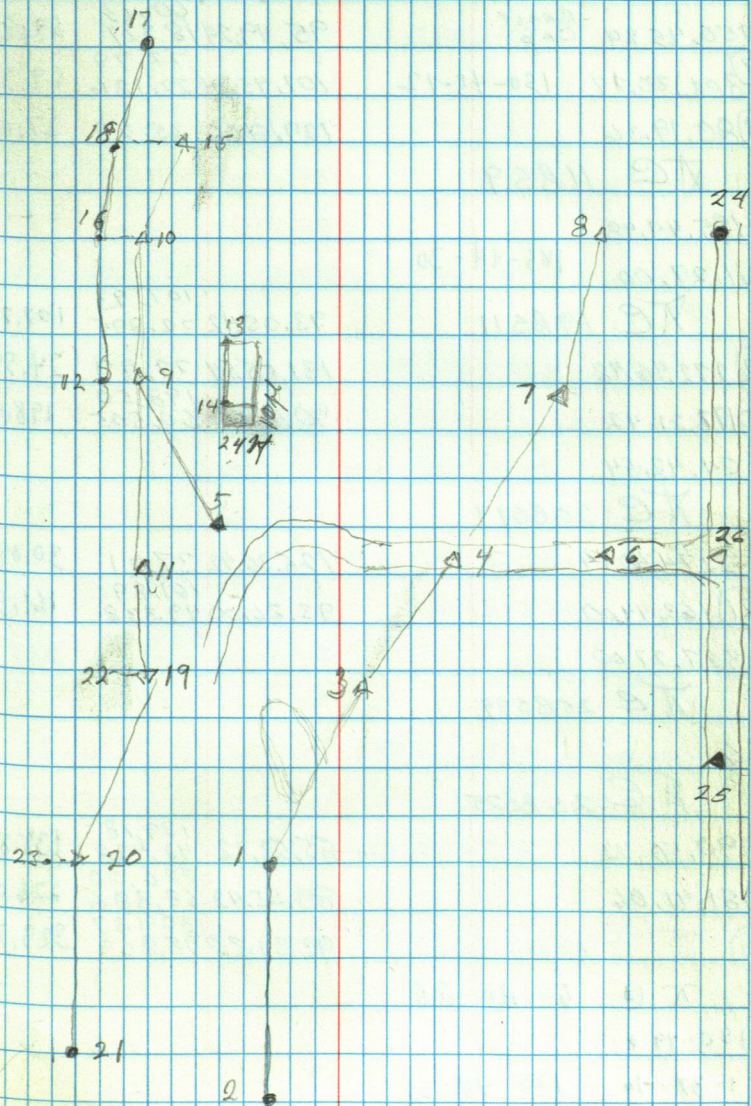
XC 10 B 5 9

(15) 162.34.54 162-34-48

325.09.36

(16) 90.30.36 120.05.36 30.50 26.39

B. CURT
R. TURNER
9-15-96



AB 15BS10

150.45.24 ^{BRASS} Cap 95.49.24 ^{60.13} 18.327 59.818

(17) 301.30.24 150-45-12 107.45.24 ^{72.79} 22.186 69.321

(18) 80.19.36 129.51.00 35.20 27.02

AC 11BS9

(19) 185.44.48
11.29.00 185-44-30

AC 19BS11 93.05.42 ^{107.93} 32.895 107.768

(22) 272.46.48 131.55.54 32.99 24.543

(20) 197.21.42 90.53.00 ^{198.50} 60.505 198.479

34.42.54

AC 20BS19

(23) 274.40.54 125.36.42 37.01 30.09

(21) 163.44.00 93.26.00 ^{161.89} 49.338 161.589

327.27.00

AC 25BS24

24

AC 26BS25

(6) 90.50.42 85.53.12 ^{139.18} 42.428 138.831

181.41.06 89.55.42 ^{226.00} 68.886 226.001

(24) 93.34.80 ^{324.37} 98.869 323.739

AC 6 BS 26

180.49.0

4 1-37-40 180-48-50

DARYL WILSON

TC 1852

130,25.06 130-24-51 90,09.42 ^{185.06} 56,407 185.06

③ 260.49.42 90,56.30 ^{914,44} 126,320 414,380

④ 65,03.06 89,50.24 ^{139.22} 139,22

⑤ 70,10.30 90,15.36 117,61

⑥ 80,43.30 90,27.54 134,23

⑦ 92,31.06 90,35.30 204,38

TC 3851

239,17.30 239-17-27 91,10.48

⑧ 118,34.54 ~~86.40~~ 86,40

81,49.30 81-49-18

⑨ 163,28.36

TC 9853

153,35.12 153-35-06 268,01.42 ^{184.43} 56,214 184.32

307,10.12 86,39.54 ^{257.65} 78,530 257,165

TC 10859

135,18.06 135-17-48

⑪ 270,35.36 66,40

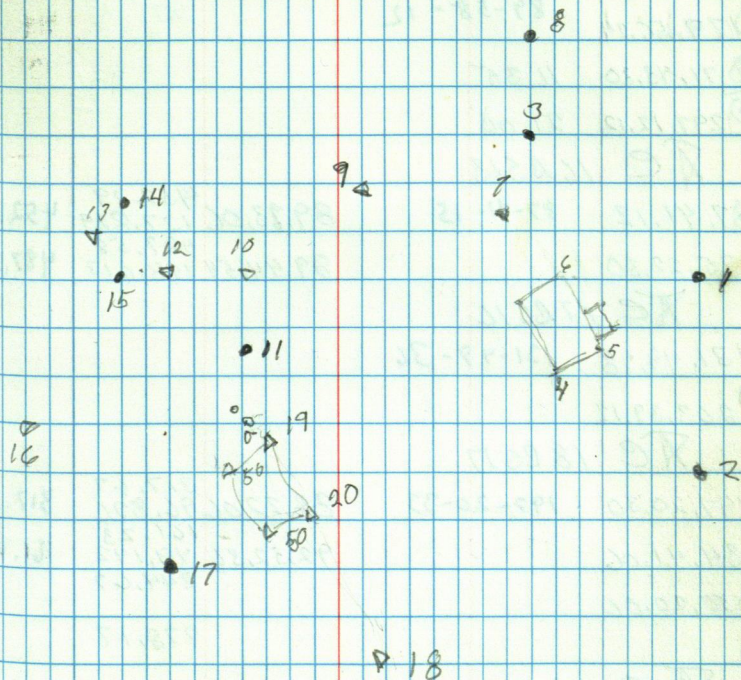
229,04.48 229-04-51

1298,09.42

TC 128510

199,12.30 199-12-18 89,17.00 ^{187.98} 57,297 187,966

⑬ 38,24.36 ~~71,41.06~~ ^{235.12} 71,665 235,018



DAYE WILSON
Xc 13. B512

89.58.12

(16) 79.56.24 89-58-12

(14) 71.43.30 11.35

(15) 297.12.12 21.00

Xc 16. B513

87.41.12 87-41-15

89.83.06 ^{452.19}
^{137.829} 452.164

175.22.30

89.44.54 ^{487.58}
^{148.613} 487.571

Xc 17. B514

131.49.48 131-49-36

(18) 263.39.12

Xc 18. B517

197.20.30 197-20-33

88.22.06 ^{317.67}
^{96.826} 317.54

(2) 34.41.06

92.52.36 ^{161.23}
^{49.142} 161.024

(19) 50.20.06

344.67

(20)

278.17

Xc 2. B51

220.54.48 220-54-45

(18) 81.49.30

RALPH YEAGER

70 3 BS 1

87-35-42

9000-18

2669.93

813.796

2669.92

4 175-11

87-35-30

1335.18

406.960

1335.08

2

1 • sph in comb.

2 •

3 •

4 •

TE 1852

214.00.00

③ 68.00.00 214-00

TE 3851

241.00.00

④ 122.00.00 241-00

TE 4853

⑤ 174.42.12

93.18.06

104.53

104.353

349.24.24 174-42-12

89.50.00

31859

1765.93

1755.92

535.213

TE 5854

180.00.48

⑥ 000.01.12 180-0-36

TE 6855

⑦ 179.52.36

89.47.36

1743.37

1743.35

359.45.06 179-52-33

90.41.18

531.879

1560.36

1560.236

475.595

TE 7854

183.21.18 183-21-06

91.42.48

169.97

51.807

169.894

⑧ 06.42.12 RR Sample

⑨ 183.21.18

268.15.48

153.78

46.872

153.709

3.60

⑩ COIP NAIL

TE 9857

263.41.36 263-41-18

⑪ 167.22.34

TE 11859

181.07.06 181-07-03

89.20.42

576.22

175.632

576.18

729.84

222.208

728.83

⑫ 007.14.06

16 Fence Post

A15

A14

A13

A12

A11

22 pipe

19 3/4 pipe

18

20

A2

A21

A17

A1

RR 10 9 8 7 6 5 4 3

Te 12 B 511

177.56.42 177-56-30

(13) 355.58.00

Te 13 B 512

184.44.48 184-44-39 90.44.00 205.84
62.741 205.824

(14) 009.29.18

89.01.24 415.76
126.723 415.697

Te 14 B 513

179.14.48 179-14-45

(15) 358.29.24

Te 15 B 514

180.29.30 180-29-18 92.38.48 253.05
77.134 252.786

(16) 0.58.34

89.32.24 485.70
148.040 485.68

Te 4 B 53

244.30.34 244-30-30

(17) 129.01.00

Te 17 B 54

142.11.04 142-11-09 87.02.12 74.98
22.855 74.882

(18) 284.22.18

91.28.06 195.81
59.683 195.745

Te 18 B 517

117.39.34 117-39-30 88.15.54 197.64
60.239 197.546

(19) 235.19.00

203.54.42 203-54-36 91.54.48 221.23
67.431 221.106

(20) 47.49.12

286.35.12 286-35-21 94.02.18 166.51
50.750 166.021

(21) 213.10.42

7e 19B517

255,29.18 255-29-09 91,01.30 ^{404,130} 123,243 404,254

(22) 150,58.18

7e 22B519

137,26.24

(23) 224,52.24 137-26-12

7e 23B522

183,47.18

90,37.30 ^{185,03} 56,400 185,023

(24) 107,34.00 183-47

94,21.30 ^{136,12} 41,489 135,725

7e 24B523

232,27.18 232-27-06

(25) 104,54.12

91,24.48 ^{199,69} 60,864 199,626

7e 4B55

171,04.30

(1) 342,09.36 171-04-48

94,12.18 ^{125,54} 38,245 125,202

7e 1B54

99,14.42 99-14-45

(2) 198,29.30

7e 26B55

53,09.36 53-09-24

(9) 106,18.48

92,40.52 ^{92,81} 28,198 92,724

7e 4B526

(20)

90,18.24 ^{306,77} 93,497 306,755

42

41

• 19
3/4 11/12

1/5

4
26

4
41

19

22

423

• 24

• 25

DENNIS CHRISTENSON

Ne 3BS1

SE-SW-35-140-29

90.07.06 4868.48 4868.48

91.53.06 485.47 485.208

90.10.08 1561.97 1561.963

Ne 4BS3

5 59.48

Ne 5BS3

2 88.53.23

Ne 6BS7

93.38.06 51.27 15.617

91.00.24 120.677

Ne 7BS6

8

Ne 8BS7

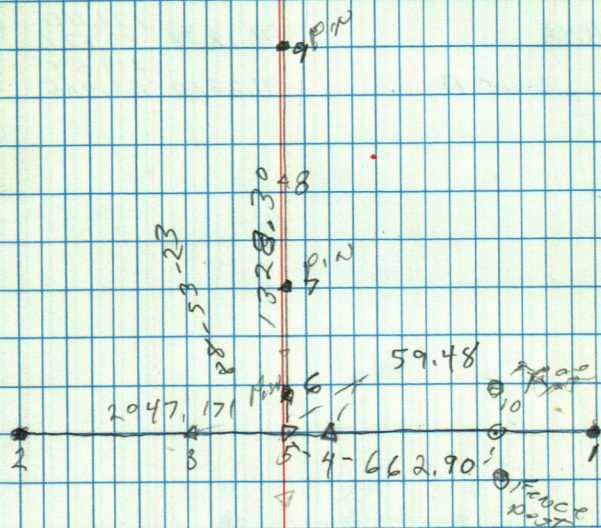
26756.06 103.96 56.069

90.00.06 621.15

Ne 5BS1

90.00.01 662.90

10



1561.963

485.208

2047.171

59.48

1488.691

Te 4BS11

27.

Te 27BS11

(28) 9533.18

92,29.42 142.73 43.506 142.597

90,24.00 210.74 64.234 210.734

(29) 274.11.48

91,18.18 171.00 52.126 170.963

SWAMP

91,28.00 214.59 65.405 214.515

28

11 27 4

29

(28)

LYNN ORTH

$\pi @ 2 BS 1$

139,22.54

90.38.00

483.09
197,249

483.064

③ 278,45.30 139-22-45

91,43,48

113,55
85,219

115,496

$\pi @ 4 BS 3$

159,10.54

5 318,21.54 159-10-57

$\pi @ 5 BS 4$

198,54,24

198-54-30

88.00.00

548,71
167,265

548.403

② 37,49.00

90,39.06

245,82
74,925

245,802

$\pi @ 6 BS 5$

E 135-00

2 • $\frac{1}{4}$ BROKEN
CI MON

1 • $\frac{1}{16}$

Ac 2351

64.09.42 64-09-39

③ 128.19.18

④ 232.11

⑤ 229.50.11

Ac 3352

197-30-06 197-30-0

6 35-00-00

Ac 4353

228.33.48 228-33-42

③ 97.07.24

3928.80 626.61 190.993 626.585

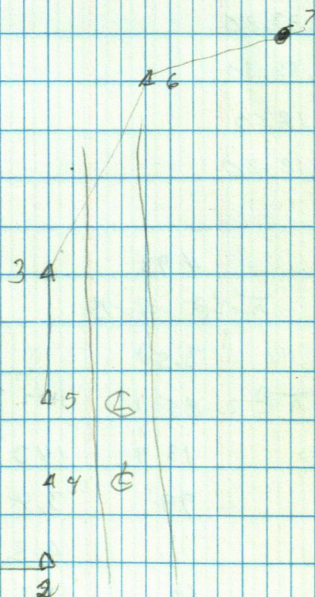
88.45.36 1448.96 441.642 1448.613

90.11.00 247.13 25.313 247.107

89.00.06 422.61 128.820 422.558

89.56.30 1234.88 376.393 1234.876

92.17.30 167.82 51.154 167.689



1				
Te	2851			
3		89,47.00	269.97 82,287	269.967
		269,40.12	133.92 40,847	133.963

271.00.00

Te 4851

		89,37.12	181.12 35,206	181.116
5	246.42.18	91,09.54	74.19	
6	263.02.24	90,47.06	134.44	
7	309.30.00	90,43.12	119.53	
8	323.37.30	90,15.12	191.25	
9	358.52.30	91,02.30	92.38	
10	311.18.00	93,18.30	29.29	
11	274.13.30	90,03.24	241.99	

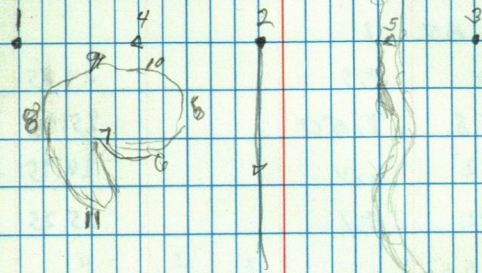
BM 4.93 1235.69 COAR COR MON

Te 4851

BM 3.50 12,43 1228.49 TOP PIPE NW COR

Te 2851 H12 31.99

180	13.4	143'	1218.09	SWMP
180	99'	3.4	28.59	RIDGE
		6.2	25.79	EDGE OF SWMP
270	60	5.0	26.99	
"	125	2.7	29.29	
"	176	4.7	27.29	
11	228	1.20	30.79	



TP	3.86	2.50	29.49
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1 @ 5 BS 1

281-55	74	8.5	24.85
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250,06	68.	7,50	25,85
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274-40	122'	6.4	26.95
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276-30	182	8.1	25, 25
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~~★~~ 6B55

80-34-48 80-34-42

§ 161-09-24

Te 7054

③ 79.03.42	79-03-18	9034.42	843.99 257.256	843.956
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(8) 22.07.00	9035,12	237.72
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⑨ 24.04,48	90.34,30	206.10
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(10) 48.38.24	89.34.36	256.89
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⑪ 198.06.36	90,32,36	921.52 280.879	921.474
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TC 11 B57

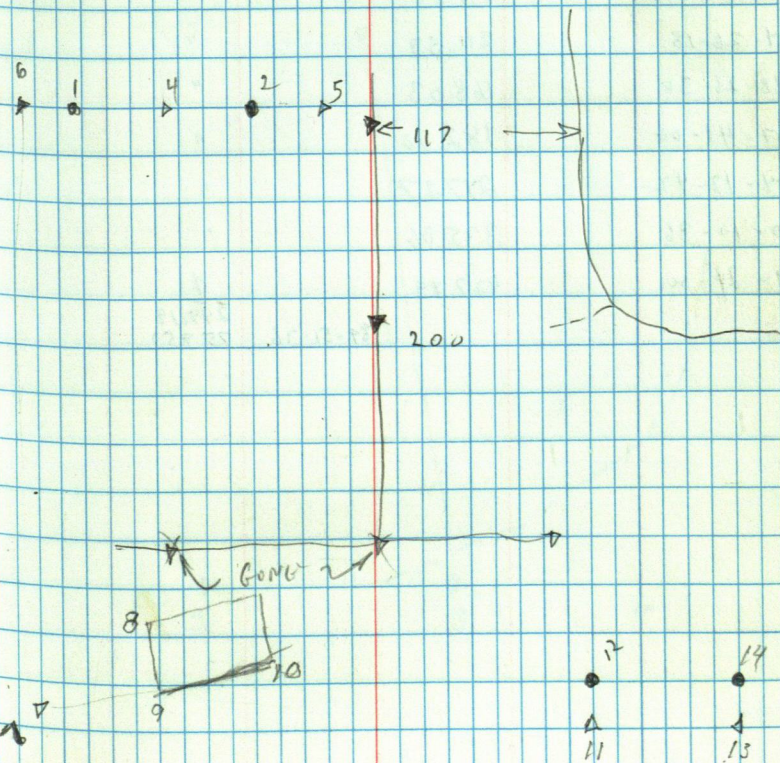
91.15.06 91-15-66

⑫ 82,30,00 18.33

181, 17.36 181-17-27

(13) 02.39.54 101,20

(14) 90, 13, 30 17.58



RAZAR YAGWA

T.C 3 BS 2

179, 25, 18

① 358, 50, 30

A @ 1 B 5 3

369, 49, 24

459.32

2

0.17, 24

370.97

1

03, 28, 42

284.30

4

14-26-18

211.59

1

38-21-30

168.03

"

67-41-00

182.90

"

84-12-42

242.27

"

90-10-36

335.06

"

91-24-00

427.49

2

3

89-51-36

249.19
75.952

2

3

4

ONLY MOSSEMAN

TC 2 BS 1

197,40.54 90-34-30 191.12 58,253 191,109

35,21.18 197-40-39

TC 4 BS 2

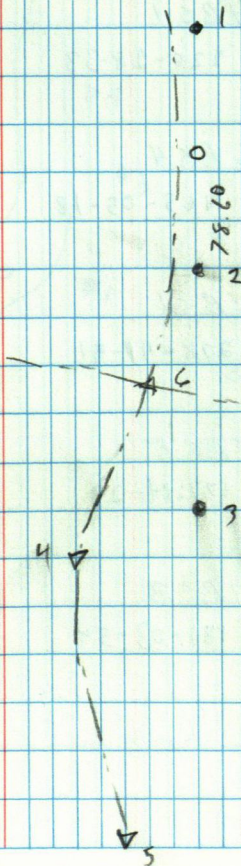
④ 166,16.12 90,20.54 211.54 64.477 211,543

⑤ 382,31.42 166-15-51 89,39.30 367.17 367,125

⑥ 269,21.54 47,816 156,86 156,858

TC 2 BS 3

89-25-54 199.93 60,939 199,92



EARLING

Te 1B52

130,42.48	130-42-51	90,23.00	99,83 30,429	99,829
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(3) 261,25.48		91,40.18	131,72 40,146	131,66
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122,42.00	122-41-54	90,16.54	204,38 92,776	304,377
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(4) 245,23.78

(5) 209,33.36 209-33-33

59,07.04

Te 4B51

220,28.48 220-28-33

(6) 80,57.00

Te 6B54

165,05.24	165-05-18	95,25.54	213,62 66,111	212,659
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(7) 330,10.36		94,12.00	164,12 49,999	163,638
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Te 5B51

278,42.00	278-41-51	94,01.12	160,70 48,980	160,302
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(8) 197,23.42		85,41.30	429,91 131,036	428,692
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Te 8B55

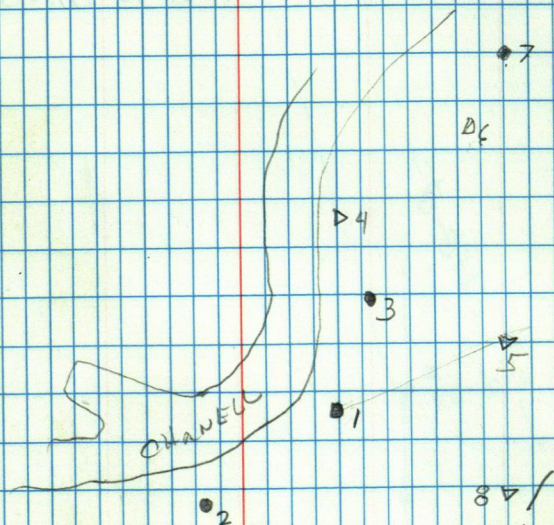
177,14.24 177-14-24

(9) 354,28.48

Te 9B58

181,03.54	181-03-54	89,47.24	820,01 249,940	820,00
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(10) 02,07.48		90,53.30	683,76 268,411	683,676
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CLEAN WITH EM

TC 2 BS 1

181.47.18 181-47-12

③ 03.34.24

TC 3 BS 2

280-56-18

90-21-30 954.76
291.013 954.74

Row
man

3
371

2
RR SH

3

TERRY DOWD

K @ 2 B 5 1

96-09-42

3 192-18-44

96-09-24

90-08-36

571,33

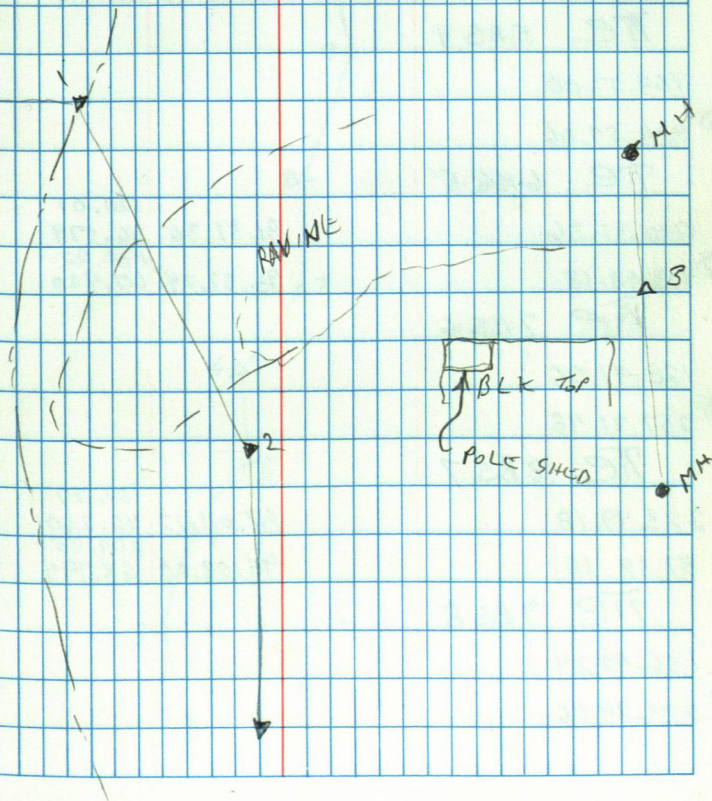
174,142

23,16,30 205,93

19,42,36 123,55

317,24,24 152,28

316,52,54 286,12



<p>TE 2BS1 RPE 100 Road</p> <p>89,22.36</p> <p>③ 178.45.00</p>	<p>89.44.18</p> <p>86.41.42</p>	<p>907.97</p> <p>276.749</p> <p>407.58</p> <p>124.233</p>
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TE 3BS2

195.16.48

④ 30.33.24

TE 4BS3

157.47.42

⑤ 315.35.48

TE 5BS4

169.27.00

⑥ 338.54.06

TE 6BS5

246.31.36

⑦ 183.03.18

TE 7BS6

128.41.06

⑧ 257.21.48

TE 8BS7

223.49.18

⑨ 87.38.18

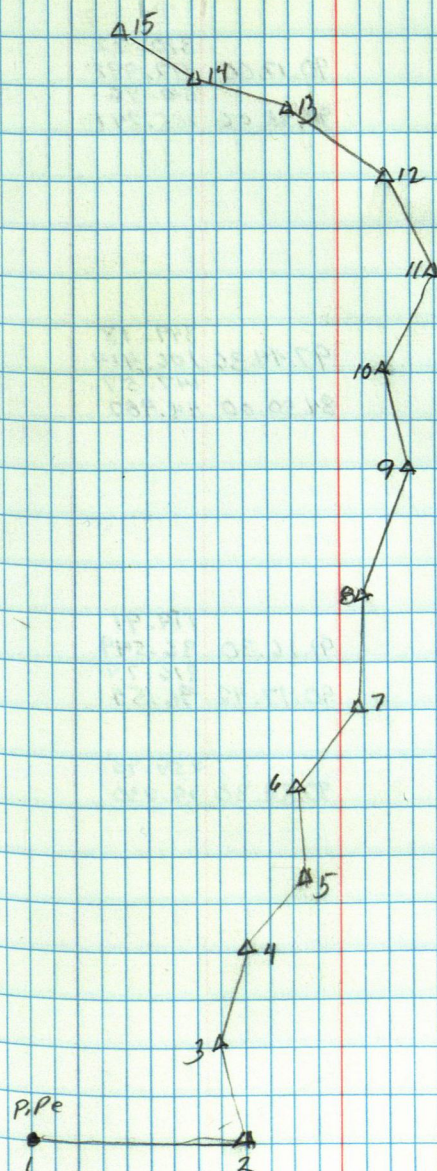
TE 9BS8

136.42.24

⑩ 273.24.06

<p>214.30</p> <p>88.42.00</p> <p>268.49.36</p>	<p>120.01</p> <p>26.579</p> <p>198.22</p> <p>60.420</p>
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<p>91.51.36</p> <p>93.57.24</p>	<p>131.77</p> <p>46.260</p> <p>209.95</p> <p>63.994</p>
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Te 10B59

⑪	183.56.24	90.17.00	370.72
	07.52.30	90.58.06	112.992
			510.96
			155.741

Te 11B510

109.41.30

⑫ 219.23.12

Te 12B511

⑬	169.20.00	97.44.36	349.13
	338.39.00	84.50.00	106.414
			147.57
			44.982

Te 13B512

⑭ 229.39.48

99.19.36

Te 14B513

⑮	108.45.34	91.16.30	119.91
	212.30.30	90.17.42	36.549
			316.74
			96.541

Te 15B514

⑯	191.05.00	90.32.30	259.95
	22.09.24		79.230

Pipe

TC 1852

287.28.48

③ 214.57.47

TC 3851

250.13.12

288.25.48

433.70

132.193

267.99

90.42.54

87.781

④ 140.26.00

TC 4853

292.48.00

⑤ 25.35.48

TC 5854

161.33.12

88.35.48

235.21

71.692

284.63

⑥ 323.05.36

88.42.42

86.765

TC 6857

161.09.36

⑦ 322.18.42

TC 7856

244.53.06

90.31.06

192.43

58.652

130.84

⑧ 129.46.00

90.32.24

39.882

TC 8857

134.04.06

⑨ 268.08.18

TC 9858

213.37.54

87.46.48

209.71

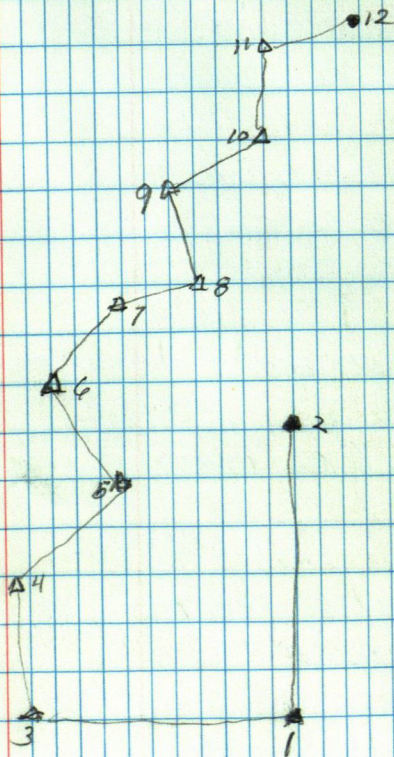
63.920

247.64

⑩ 67.15.42

91.12.00

75.481



AC 10 R59

⑩ 163.27.42

826.55.00

AC 11 R5 10

220.41.18

⑪ 81.22.18 P.P.P

89.03.06

148.76

45.342

108.78

90.35.36

33.152

Q ROND
SE-SW - 17-140-29

TC 1852

③ 180.0648

90.24.12 149.84
45.667 149.829
219.92
90.01.34 67.039 219.923

④ 179.13.12 123.28

⑤ 169.38.24 59.94

⑥ 99.20.06 55.95

⑦ 82.30.30 121.98

⑧ 87.01.00 188.23

⑨ 93.21.00

186.41.30 93-20-45 90.07.18 236.48
72.072 236.467

TC 9851

⑩ 218.04.06 138.34

⑪ 216.59.04 210.20

⑫ 211.06.30

62.13.12 211-06-36 91.05.42 304.01
92.662 303.953

TC 12859

⑬ 146.13.18

292.2634 146-13-18

TC 138512

90.23.06 474.77
144.710 474.757

⑭ 133.05.24 66.95

⑮ 141.58.36 141.74

⑯ 133.11.18 219.68

⑰ 130.34.20 319.26

⑱ 134.16.30 467.57

21A

20A

22A P1P2

419

23 P1P4

418

417

416

415

414

413

412

411

410

9A

408

407

406

405

3

1

2

(19) 130,48.18

266.36.48 130-48-24

90.33.12 ^{481.95}
146.900 481.928

~~Te~~ 19.8513

(20) 143.22.12 75.26

(21) 157.08.48 160.90

(22) 162.06.24

89.25.48 ^{94.85}
28.909 94.843

(23) 324.09.00 162-04-30

288.39.48 288-39-33 92.46.12 ^{64.32}
19.603 64.242

23 217.19.04

π e 2 85 3

150-03-48

91-21-30

584.87

584.706

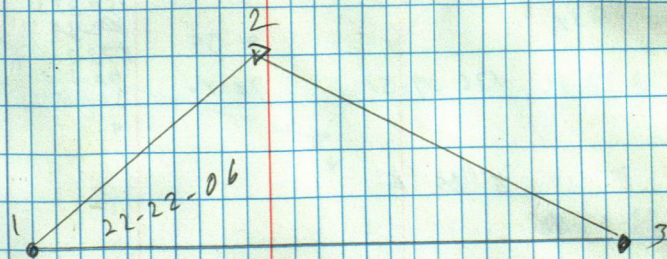
① 300-07-36

150-03-48

90-22-40

202.37

202.363



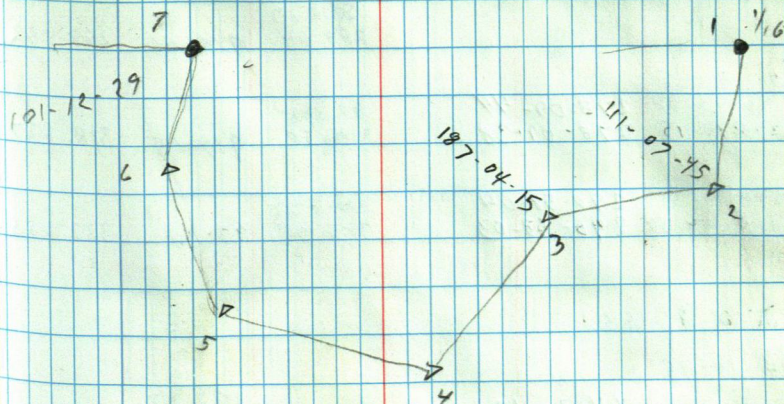
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111.07-36	87-11	24.337	243.89
122.15.30	111-07-45	129.571	423.82
	95-23	725.10	424.545

* @ 3 BS 4	
187-04.18	
2 14.08.30	187-04-15

* @ 4 BS 5			
136-09-54	91-35	150.333	361.532
3 272.19.46	90-40	473.24	493.184
		110.238	
		361.67	

* @ 5 BS 6	
152.03.48	
4 304-07-12	152.07-36

* @ 6 BS 7			
155-19-54	92-12	44.434	145.672
5 310-39-30	87-02	145.78	202.239
		61.786	
		202.51	



$\pi @ 1$ BS 2

180-0-24				
0-0-27	240-39-55	91.865		300.489
60-40-11				
3 240-40-22	240-39-47	301.39	94-26	
80-02-10	260-01-46			
260-02-13	260-01-46			

4		88.279		
		289.64	94-06	288.892

5 2				
98-10-08	278-09-44	92.386		
5 278-10-15	278-09-38	319.50	94-15	318.627

290-58-30	290-58-04	116.672		
5 110-58-28	290-58-03	382.78	93-30	382.065

$\pi @ 2$ BS 1

64-20-18

7 128-40-24	64-20-12	92-30	147.97 452.65	452.221
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3

$\Delta 4$

$\Delta 5$

$\Delta 6$

$\Delta 7$

$\Delta 8$

2