

333

E	L	A	N

Field Book

E 64-8x4



# Projects

- 1 ROY STROMQUIST 2-8-140-31
- 2 SHARON READ BUCKUS
- 3 REMER APARTMENT BUILD.
- 4 REMER CEMT.
- 5 HARTGILL 2-21-139-29
- 6 SHARON READ BUCKUS
- 7 TOM STAGSNAK 4-5-140-27
- 8 ED SCHIEBE 2-26-140-29
- 9 JIM DEWERDT 1-2-24-142-28
- 11 LEONARD BABINSKI
- 12 FRANCES PLUMB E LINE 28-139-28
- 13 CRAIG WADZINK 2-2-140-30
- 14 BIA-GP BEEBE
- 22 GEO. GAGOLA
- 23 HENRI FORD
- 24 BIA GP
- 29 JOHN ZACKER McKenna
- 31 BIA-GP
- 33 BILL HANSEN 11-20-142-27
- 34 SAM FARR
- 35 BIA-GP
- 42 GEO. GAGOLA



Publishing Co., Inc.

Meredith, N.H. 03253



## Projects (continued) .....

43 AL FOWLEY ..... LOT 17 HAINING ADD

44 BIA-GP

50 WARREN BAKER . . . ISLAND LIK . . 6-3-139-29

51 Jim KESSLER..... L. LAKE.....

52 B/A-GP.....

57 WORICK 2-30-140-29

58 BIA-6P

64 STEVEN BAILEY 1-12-140-31

65 BIA-6P .....

66 AKF-L66Y CEMETERY

67 B/A-GP



ROY STROMQUIST

N @ 1 BS 2

0-0-40

276-15.17

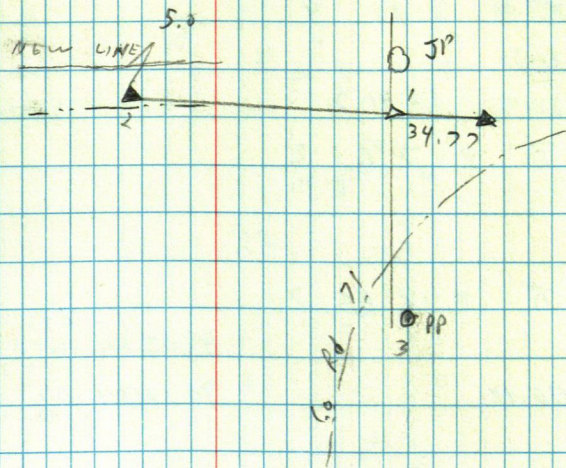
20° CLOD

E. CURR

B. CURR

1

11-22-92









1344.66





[illegible]

Hand-drawn graph on blue grid paper. The x-axis is labeled from 1 to 10, and the y-axis is labeled from 10 to 170. A red vertical line is drawn at x=5. Data points are plotted as circles and triangles, connected by a line. The points are approximately: (1, 170), (2, 140), (3, 150), (4, 140), (5, 130), (6, 120), (7, 110), (8, 100), (9, 90), (10, 80).

70 140 150 140 190 140 110 100 90 80 70 60 50 40 30 20 10

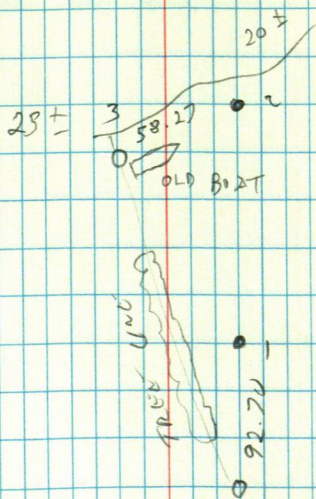


HARTEL

T @ 2 BS 1

62-36-36

3 125-13-36





SHARON READ

BACKUS

T C 1

2

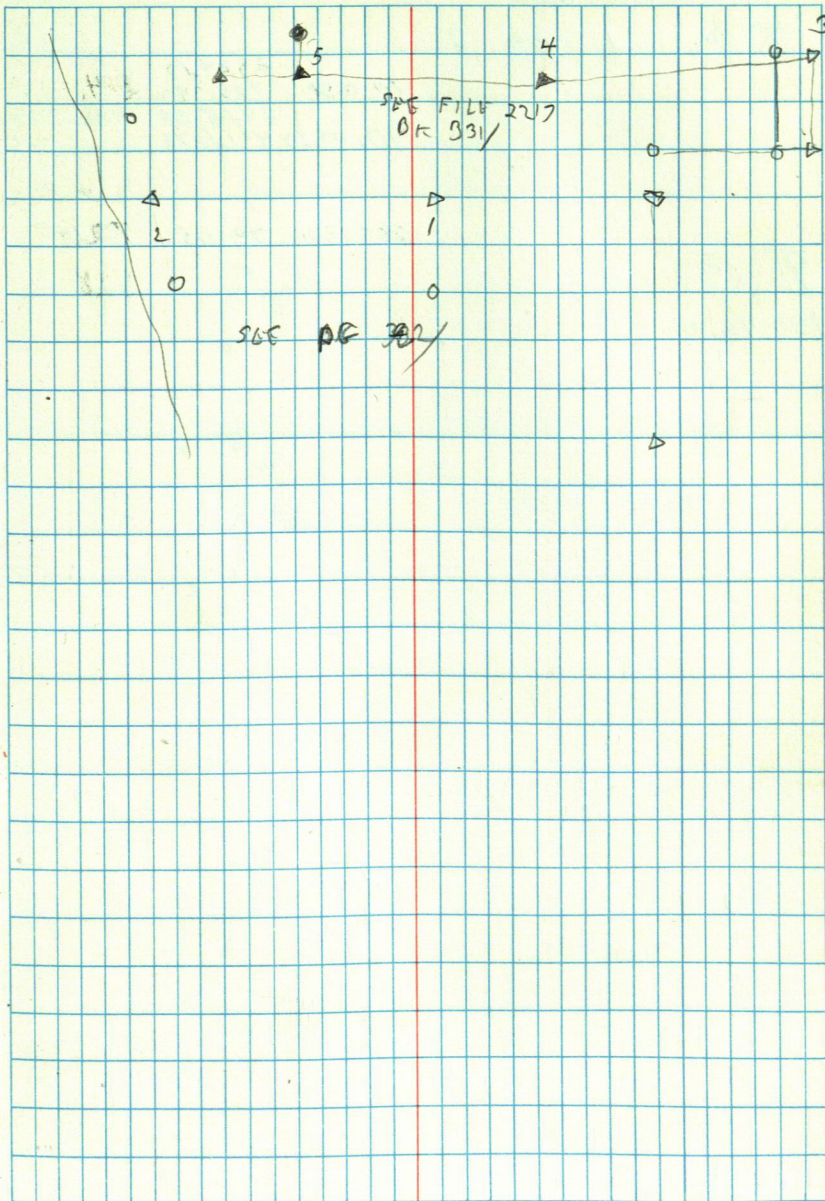
91.08.42 204.29  
62.207 204.247

T C 4 BS 3

182-35.00

89-35.00 192.63  
58.715 192.626

5

90-33-36 528.57  
161.107 528.54



TOM STRUSNAK

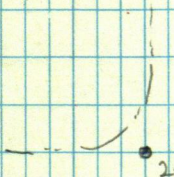
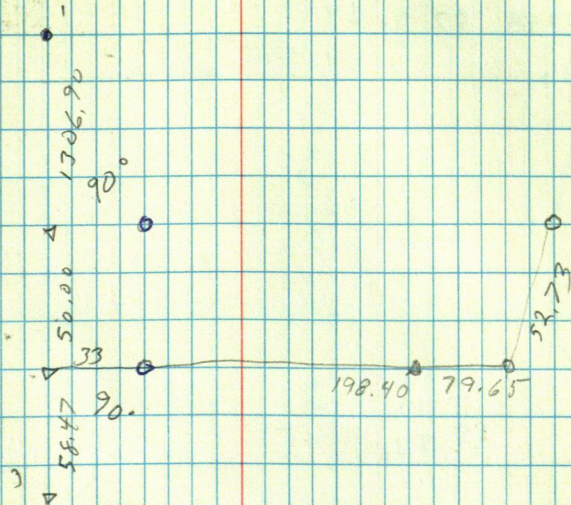
T D 1 BS 2

90.0.54 2524.10  
706.343  
1415.38 1415.369  
90.09.30 431.408

263.18.30 79.65 79.107.

TC

109.43.30

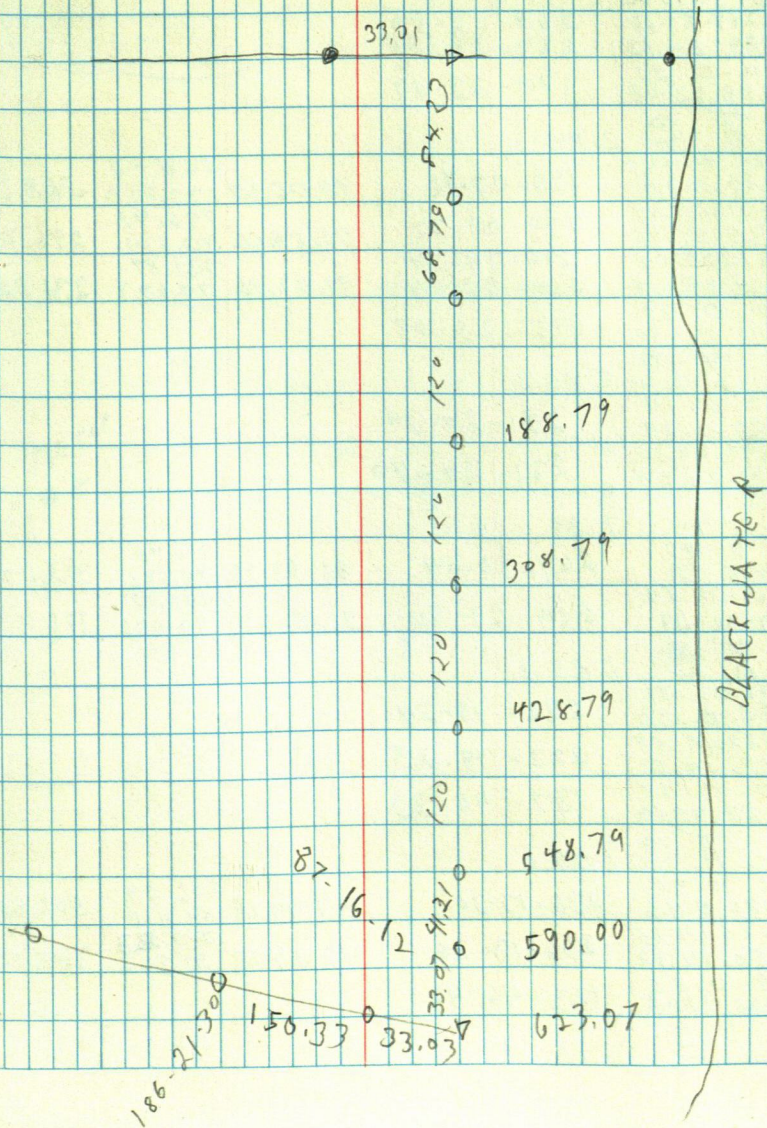




ED SCHIEBE

87, 11.24

174.22.48 87-11-24













LEONARD DABINSKI

TQ 2 B5 1

185.3430

91.35.00

326.08

99.388

325.952

3 191.08.00 185-34

92.36.06

222.26

67.743

222.027

TQ 3 B5 2

175.00.42

95.16.30

286.06

87.212

284.881

4 350.00.36 175.00-18

5 45.39.00

190.40

58.039

6 103.17.00

60.75

18.517

BR CAMP  
MC3  
2

2

5

2

BR CAMP



## FRANCIS PLUMB

TC 2 BS 1

180.36.12

267.42.36

463.56

141.293

463.191

3 8-12-24

271.04.18

1312.58

400.075

1312.346

A 12.10

93.19.00

99.19

30.239

B 9.6

88.56.00

267.411

81.503

C 6.8

88.44.48

563.20

171.676

D 7.90

88.54.12

998.79

304.432

TC 3 BS 2

179.47.00

89.28.42

1246.16

379.827

1246.099

359.35.00

E 10.00

89.59.30

292.23

89.072

F 10.35

89.38.00

643.60

196.169

G 8.95

89.26.12

719.72

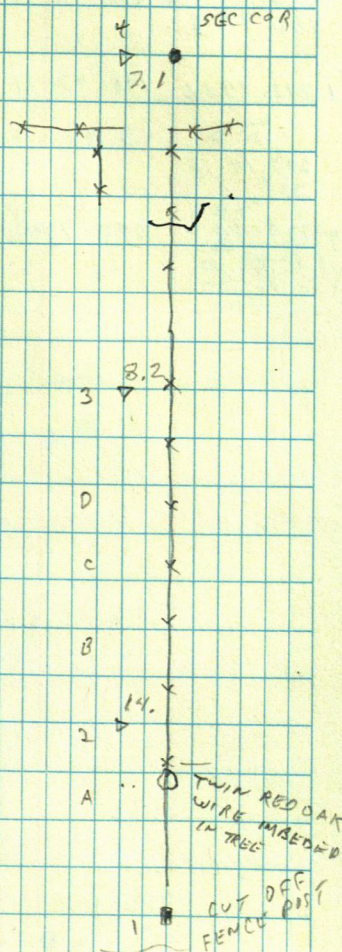
280.330

H

TC

267.23.36 4 BS 3

174.46.00





WADZINK

$\pi @$  2 BS 3  
106.47.18

363.50  
269.35.42 110.790 363.481

1 213.34.36 106-47-18

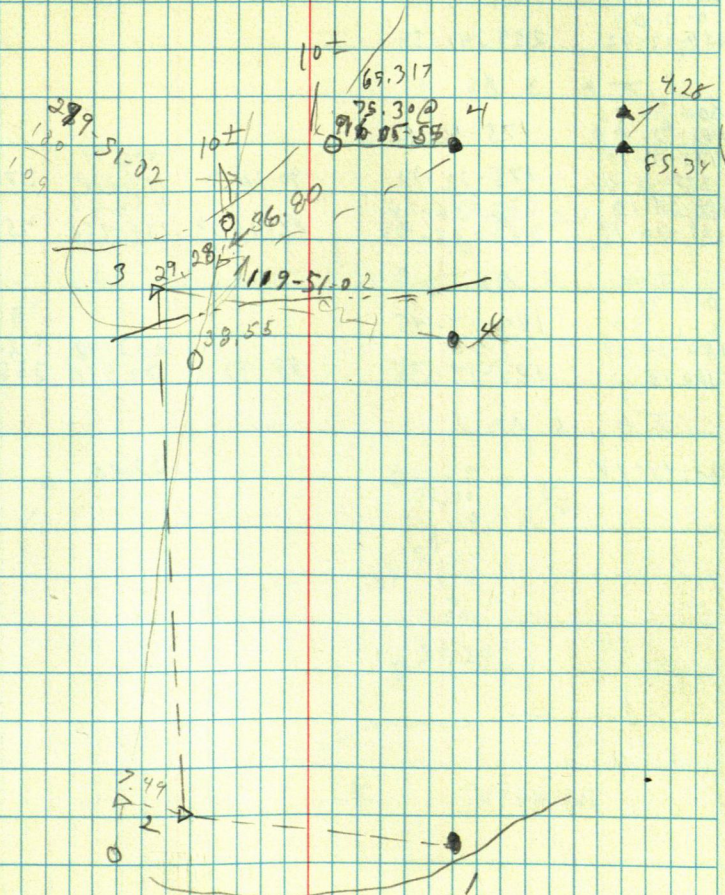
90.32.06 44.396 145.646

$\pi @$  3 BS 2  
245-19-18

4 130.38 245-19-0

87.30-30 202.43  
61.693 202.225

$\pi @$





BEEBE

BIA CR. PORT.

A 2 BS 3

0-0-31			1355.88	
180-0-26	100-18-14	89-54-27	413.124	1355.384
100-18-45			176.19	
1 280-18-44	100-18-18	91-36-59	57.205	176.12
0-0-09				
259-42-02	259-41-53			

A 3 BS 2

000-0-06				
180-0-08	175-12-12			
175-12-18			376.71	
4 355-12-20	175-12-12	90-26-30	114.618	376.692
282-36-10	282-36-04		454.02	
5 102-36-12	282-36-04	86-20-19	138.368	453.096

A 5 BS 3

0-1-35				
0-1-37	180-13-45			
180-15-20			262.38	
6 180-15-12	180-13-35	99-30	79.948	258.704

A 6 BS 7

268-44-48			27.25	
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E. CURD 14

7-21-93

E.B.T.  
2 1/4E.B.T.  
1 X 3 Rnd Hd Bolt

32.01 1/6  
88-57-48  
900  
27.24 1/6

LK SUPERIOR



B/A GA PT,

T @ 2 BS 1

0-0-15			7673.36	
180-0-18	357-16-34	90-11	1119.644	3673.331
257-16-49			1034.25	
3 177-16-55	357-16-37	90-54.08	315.242	1034.102
0-1-42				
2-45-07	2-43-25			

2-

T @ 3 BS 2

0-0-7				
180-0-14	302-19-46			
302-19-53				
4 122-19-53	302-19-39			
0-0-41				
57-41-03	57-40-22			

T @ 4 BS 3

0-1-13			315.13	
180-1-10	210-36-04	87-58-21	96.049	314.921
210-37-17			715.33	
5 30-37-18	210-36-08	89-45-12	218.037	715.528
PI 121-0-20	120-59-07			25'
CF 241-32-12	241-30-59			201.36
W 259-6-30	259-05-17	2		181
0-9-46				
149-33-28	149-23-42			

Hollow Rock  
RHSAT SIGN

RR SPIK

24.3'

FILL

S  
R  
RSEC  
COR  
MC

25

20

40 PA  
100  
100  
100GR RAIL  
POST  
RR SPIK  
4TH  
3' 50" FROM  
NE END

3.5

23.6

3  
125  
GB40 MILE  
POST



	1	2	BS	1	
0-0-12				1559.78	
180-0-2	184-08-	89-32-56	425.428	1559.736	
184-08-72			799.96		
3 4-8-05	184-08-03	92-33-47	248.824	799.15	
0-0-8					
175-51-58	175-51-50				

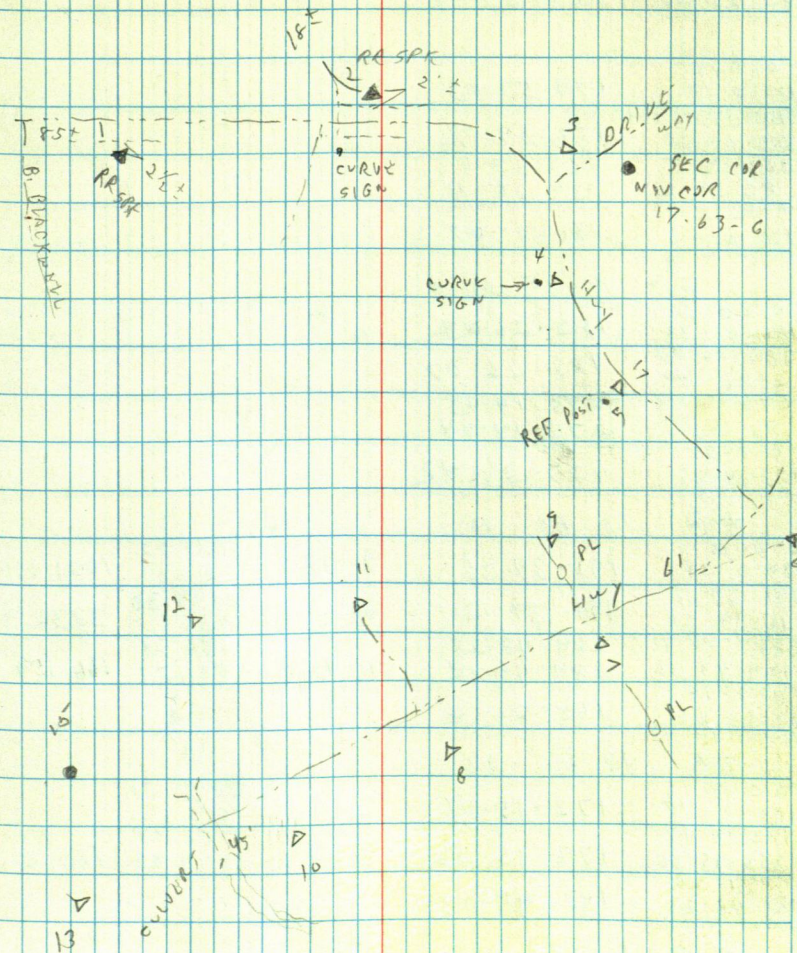
	1	3	BS	2	
0-0-40					
180-0-31	218-22-32				
218-22-12					
4 38-22-58	218-22-27				
0-1-30					
149-39-0	149-37-30				

	1	4	BS	3	
0-0-12				741.90	
180-0-20	169-37-21	86-44-4	226.152	740.154	
169-37-38			979.49		
5 349-37-40	169-37-20	94-36-32	298.534	976.448	
0-0-56					
190-23-38	190-22-42				

	1	5	BS	4	
0-0-11					
180-0-25	152-46-21				
152-46-38					
6 332-46-46	152-46-21				
0-0-12					
207-13-44	207-13-32				

	1	6	BS	5	
9-01-20				2617.22	
180-01-18	307-52-35	86-22-20	797.724	2611.956	
307-53-55			3824.95		
7 127-53-53	307-52-35	91-5-02	952.48	3124.969	
0-0-25					
52-7-39	52-07-14				

	1	7	BS	6	
0-0-10					
180-0-25	180-22-47				
180-22-57					
8 0-23-7	180-22-42				
282-31-52	282-31-42				
9 102-32-03	282-31-38				





T @ 8 BS 7				
0-0-11			564.64	
180-0-12	179-58-47	89-46-38	172.104	564.636
179-58-58			1042.05	
10 359-59-20	179-59-08	90-12-33	317.617	1042.032
263-13-18	263-13-07			
11 83-23-29	263-23-17			

0-0-6				
180-0-18	179-59-03			
179-59-09				
359-59-20	179-59-02			
263-23-23	263-23-11			
83-23-29	263-23-11			
0-0-13				
180-01-0	180-0-47			

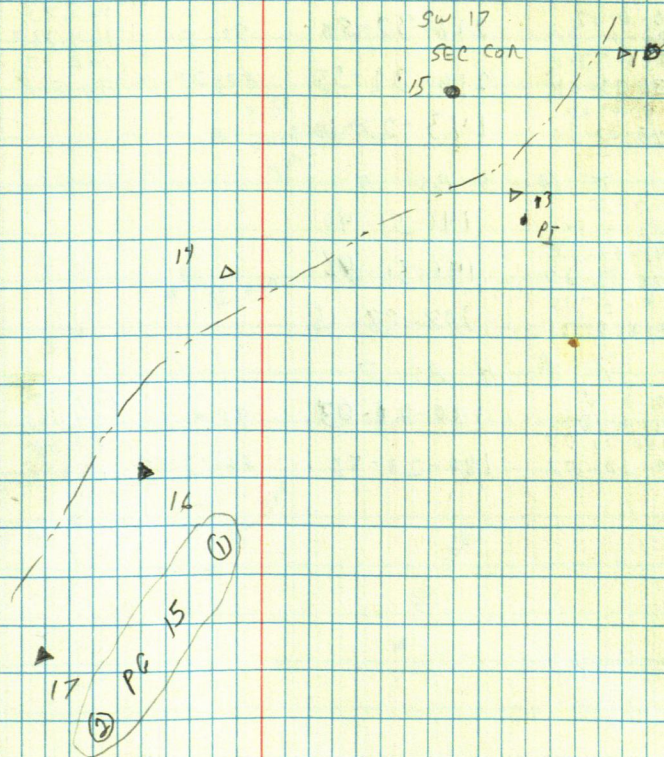
A C 10 BS 8				
0-00-30				
180-0-33	182-26-13			
182-26-43				
13 2-26-40	182-26-07			
275-15-13	275-14-43			
12 95-15-17	275-14-44			
0-0-20				
177-34-02	177-33-42			

T @ 13 BS 10				
0-0-15			1021.93	
180-0-38	191-39-35	90-34-20	311.481	1021.869
191-39-50			3232.30	
14 11-39-50	191-39-12	90-2-17	985.218	3232.306
284-48-40	284-48-25		166.24	
15 104-48-56	284-48-18	91-46-45	50.672	166.159
0-1-12				
168-21-50	168-20-38			

T @ 14 BS 13				
0-0-41			3232.30	
180-0-47	172-15-06		985.206	
172-15-47			786.85	
16 352-15-50	172-15-06	89-35-47	239.83	786.823
0-1-20				
187-46-23	187-45-03			

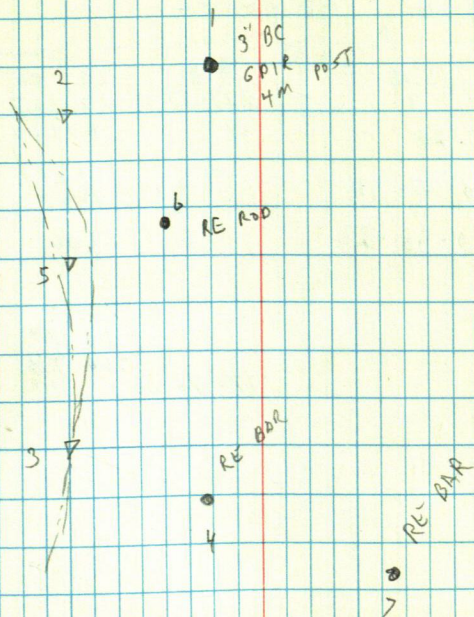
T @ 16 BS 14				
0-0-15				
180-0-14	177-45-30			
177-45-45				
17 357-45-48	177-45-34			

0-1-04  
182-15-33 182-14-29





BA	HAT PT			
$\pi @$	2	BS	3	
0-0-13				875.07
180-0-12	268-	19-01	90-46-50	257.578
268-19-14				844.989
88-19-13	268-	18-56	85-05-45	175.29
0-0-33				57.427
91-41-23	91-	40-50		174.645
$\pi @$	5	BS		
0-0-12				425.73
180-0-09	216-	32-50	90-51	129.768
216-33-02				425.69
36-33-04	216-	32-55	80-28-50	100.13
0-0-20				30.518
143-27-30	143-	27-10		98.748
$\pi @$	3	BS	5	
0-0-55				
180-0-34	141-	51-40		
141-52-38				
321-52-20	141-	51-46		
0-0-20				
218-8-35	208-	08-15		
$\pi @$	4	BS	7	
0-0-4				129.57
180-0-07	180-21-03		91-3-20	29.492
180-21-07				80.89
0-20-57	180-20-50		88-13-55	24.657
				80.854





	$\pi$	@	9	B	7		
	0-0-20						
	180-0-12	87-13-07			92-5-16	392,19 119,538	391,926
	87-13-27					140,09	
1	267-13-27	87-13-15			89-25-50	42,697	140,072
2	115-57-33	115-57-15				86'	
3	166-20-30	166-20-10				44'	
	268-52-56	268-52-36				60,09	
4	88-53-0	268-52-48			91-6-30	18,314	60,076

[illegible]



WITCH TRUCK

A @ 3 BS 2

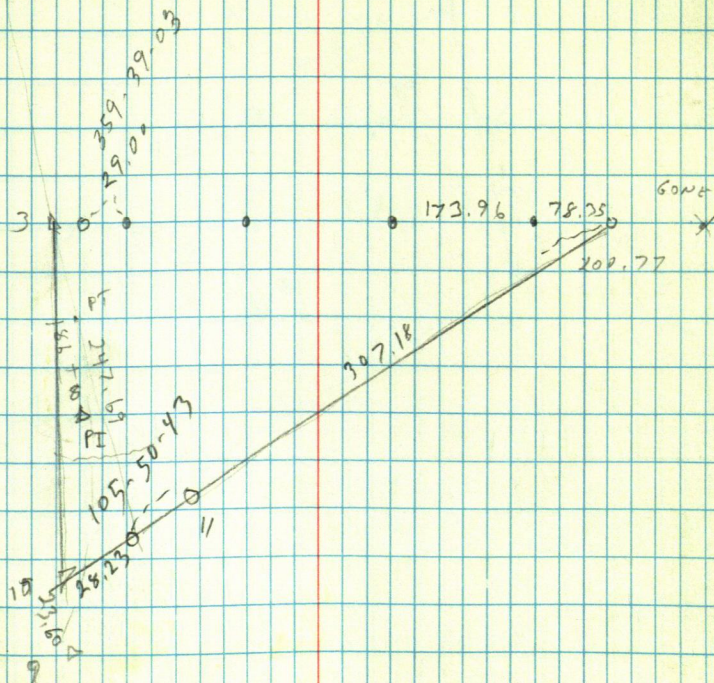
0-0-35			145.53	
180-0-22			44.358	145.365
182-17-26	182-16-51	92-43-50	262.82	
185-54-24	185-53-49	91-16-42	80.107	262.753
9 5-54-24	185-54-02			

A @ 9 BS 3

11 105-50-43	95-09	62.28	18.783
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2

$$\begin{array}{r} 3.55 \\ 28.23 \\ \hline 3.32 \end{array}$$

$$\begin{array}{r} 247 \\ 181 \\ \hline 61 \end{array}$$




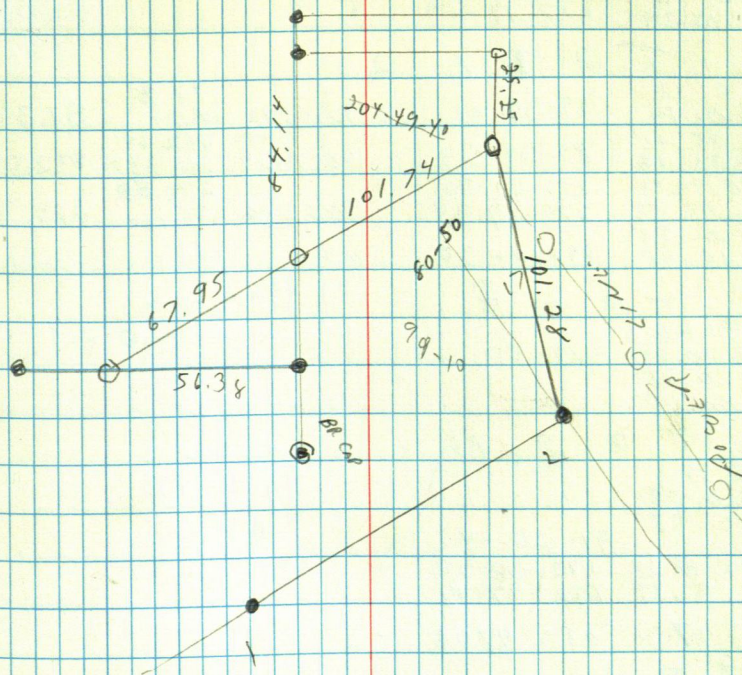
GED CAGOLA

TC 2 BS 1

0 0 10  
180.0 14  
269.14.32  
89.14.29

89-07-57

99-10





HENRI FORD

2 B5

0.005	
180.006	89-47-25

389,47,30	89-47-36
212,42,42	

269,47.42  
0.0, 10  
277,12,39

1 @ B3 2

0.0.15				197.45	
180.0.19	89-35-01		92.07.13	60.184	197.316

89.35.16	89-34-59	90.50.07	802.68	802.591
4269.35.18			244.657	

270.49.53	270-49.38	279.38	
90.49.53	270-49.34	90.23.40	85.160 279.38

0. 0. 25	89-10-20
89. 10. 45	

7 9 4 5 1

0.0, 26  
6279, 50.29      279-50

180.0.25  
.99 50.35

π	Ⓢ	5	BG	1
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0-0-15		
180,0,08		
91-20-57	91-20	-42

192-38-23 192-38-08

8 12, 37, 57 192 - 37 - 49

9 262-47-31      262-47-16

TC 8B55

0.0 r30	202-18.46	85.49.37	105.93	105.653
180.0.20			32,290	

202.19.16	202-18.50	100.52.05	117.47	35.810	115.371
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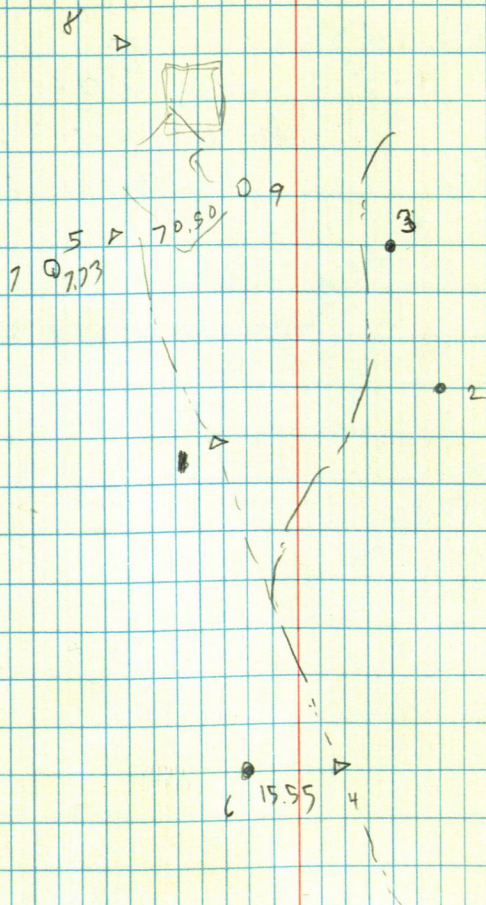
TC 10B58

180.0.01 100-16-27

106-16,27	106-16-27	89,44,46	157,39 47,949	157.372
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[illegible]

GIRL LAKE





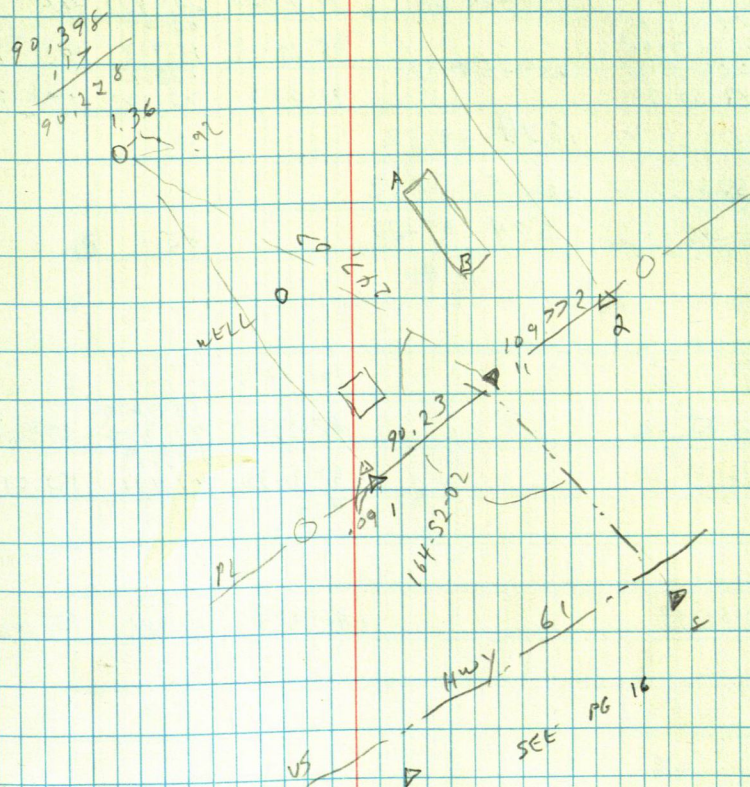
GP

DUANE SPRY

TI @	11 BS &			
0.0-37			409.52	
180-0-42	96-20-46	92-17-20	124.793	409.147
96-21-23			90.45	
1 226-21-18	96-20-36	91-57-50	27.57	90.398
276-17-57	276-17-20		109.78	
2 96-17-53	276-17-11	89-38-26	33.458	109.772
A 196-19	196-18		135'	
B 203-52	203-51-23		70'	
WELL 160-08-48			64	136'
165-10-57		274-23-53	246.87	246.14
			247.64	246.89

274-30-45 233.54 232.816

24





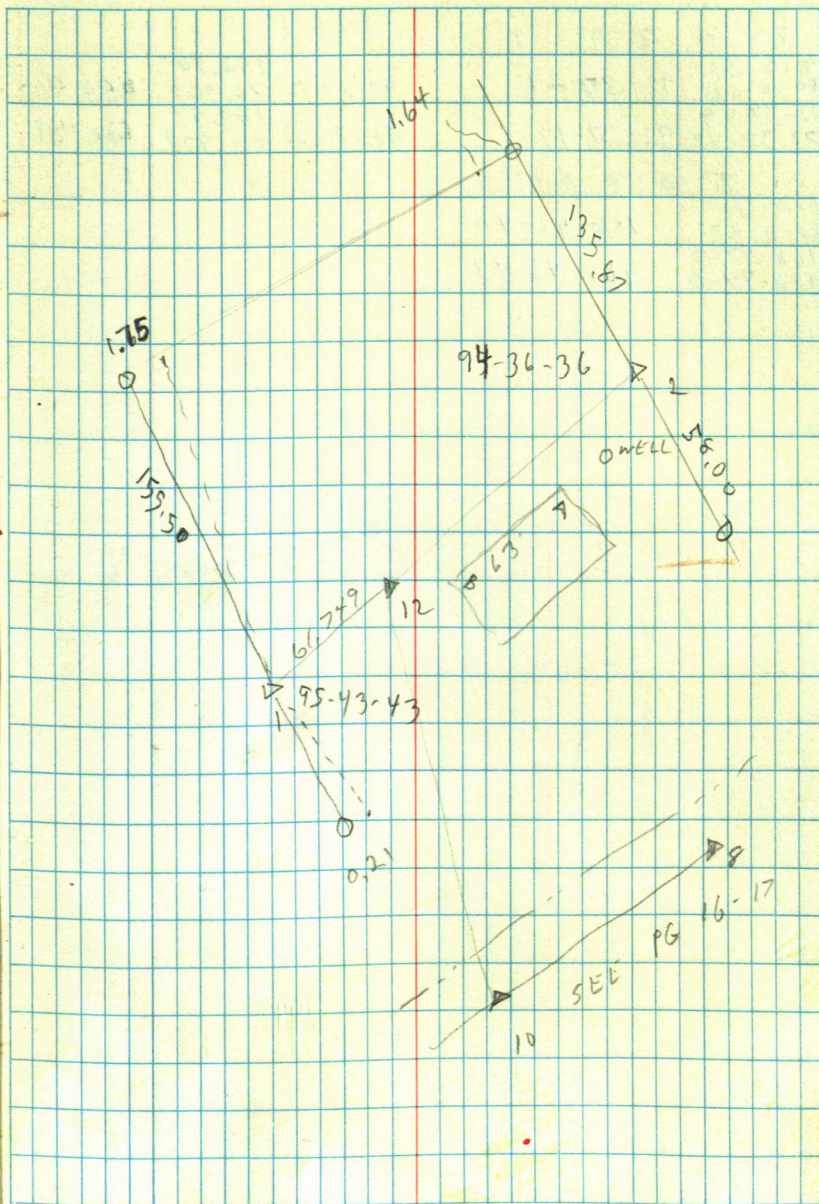
# MICKEL SPRY

70 12 BS 10

0-0-15			673.97	
180-0-12	79-22-56	95-47-20	205.427	670.482
79-23-11			62.02	
1259-23-00		95-20-15	18.703	61.749
259-50-12	259-50-03		138.13	
279-50-23		91-08-31	42.103	138.104
A 274-29-47	274-29-32		71	
B 325-37-27	325-37-12		14.5	
well 274-05-35	274-05-20		80.5	

95-31-55	101-12-12	63.31	62.104
		19.292	
276-23-22	87-55-27	144.21	144.11
		43.952	
276-22-30		155.66	
	87-31-39	47.446	155.516

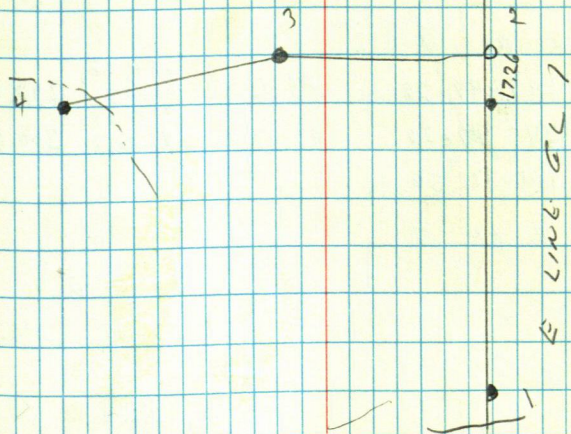
93-54-54	86-42-25	136.11	135.884
		41.486	





$\pi$	@	2	BS	1		
0-0-32					252.50	
180-0-26	92-37-29			90-57-40	76.962	252.468
92-37-49					160.53	
3 272-37-43	92-37-17			88-17-52	42.929	160.458

$\pi$	@	3	BS	2
0-0-30				
180-0-27	168-46-40			
168-47-10				
4 342-47-10	168-46-43			





50 ANN LHO TKA

TA 2 BS 1

0-0-25			1195.75	
180-0-26	125-35-07	90-45-15	364.467	1195.645
125-35-32			367.68	
305-35-25	125-34-59	89-54-20	112.071	367.681
0-0-36				
3 234-25-30	234-24-54			
			86.26	
4		86-32-20	26.292	85.698

TA 3 BS 2

0-01-25				
160-01-28	47-01-38			
47-03-03				
5 227-03-02	47-01-34			
0-0-13				
312-58-38	312-58-25			
45-42-20	45-40-55			

POWER LINE

TA 5 BS 3

0-0-15			298.08	
180-0-25	245-47-28	89-16-42	90.851	298.049
245-47-43			300.69	
6 65-47-45	245-47-20	89-43-45	91.650	300.684
0-01-17				
114-12-53	114-12-36			

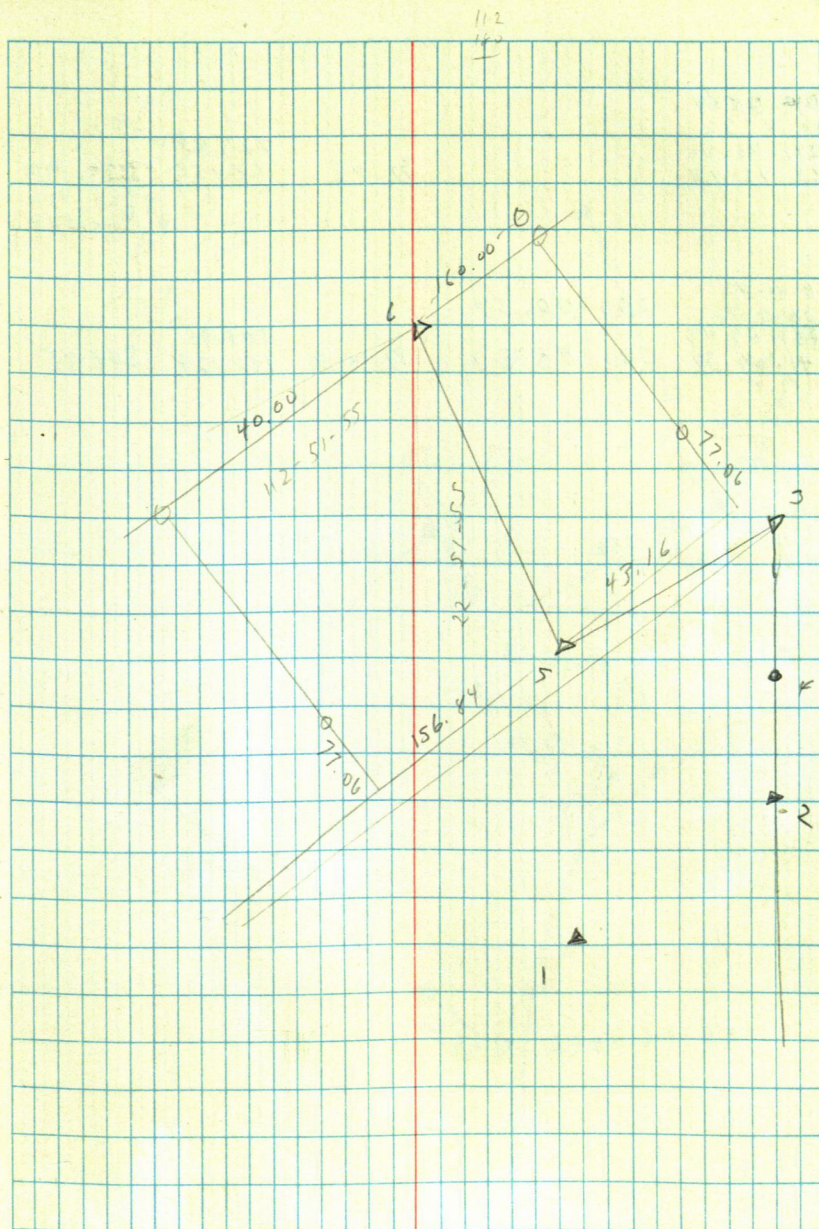
TA 6 BS 5

292-14-50			160.000	
338-21			97.82	WELL

TA 5 BS 3

128-39-19			47.725	
			156.57	

89.48





242-0004  
180-0-32  
242-46-44  
62-46-48

80 - 0 - 32

242-46-44

62-46-48

92-42

223.45

68.108

223.199

221, 724

1.474

0-0-46

180.0-40

221-09-43

41-09-37

221-08-57

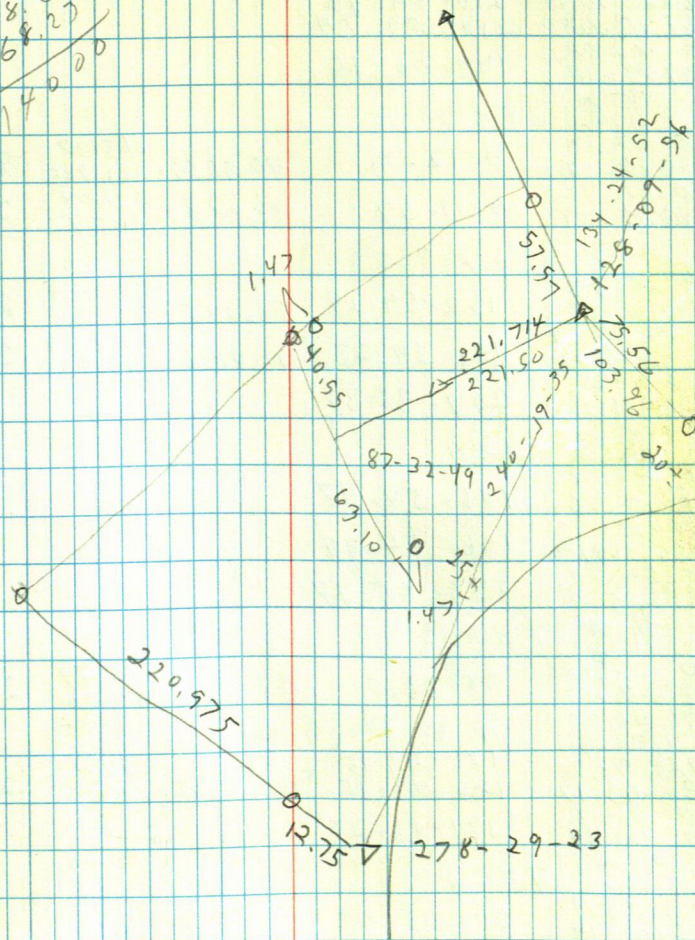
221-08-57

91-35-55

508.95

155,128

508.75

$$\begin{array}{r} 20.97 \\ 2 \overline{) 12.75} \\ \underline{40} \phantom{00} \\ 208 \phantom{00} \\ 2 \overline{) 208.27} \\ \underline{400} \phantom{00} \\ 20827 \\ 2 \overline{) 20827} \\ \underline{40000} \phantom{00} \\ 14000 \end{array}$$




JOHN ZACKER

M. K. TOWN LK

TC 2 BS 1

0.0.19	158-58-26
180.0.31	
158.58.45	
338.58.50	158-58-19
211.0.04	210-59-45
31.0.05	210-59-34
0.0.02	
149.0.18	149-00-16

TC 3 BS 2

0.0.10	0-12-01	90.38.59	865.17	865.113
180.0.12			263.725	
0.12.11	0-11-57	93.04.27	201.04	200.749
180.12.09			61.277	

TC 4 BS 2

0.0.35	152-24-24	88.09.34	299.09	298.93
180.0.38			91.160	
152.24.59	152-24-23	91.48.01	357.02	356.851
5 332.25.01			108.822	
0.0.35	207-35-37			
207.36.12				

TC 5 BS 4

0.0.25	106-54-47
180.0.26	
106.55.12	106-54-44
286.55.19	
0.0.21	253-05-17
253.05.38	

TC 6 BS 5

0.0.10	91-36-0	93.18.25	275.79	275.328
180.0.02			84.060	
91.36.10	91-33-30			
271.33.32	188-43-15		237.47	
188.43.25	188-43-15	89.31.01	72.375	237.451
8.43.17				
0.0.17	171-16-27			
171.16.44				

TC 7 BS 6

0.0.11	219-05-05
180.0.14	
219.05.16	219-05-03
929.05.17	
293.16.37	293-16-26
113.16.53	293-16-39
0.0.14	
66.43.81	66-43-17

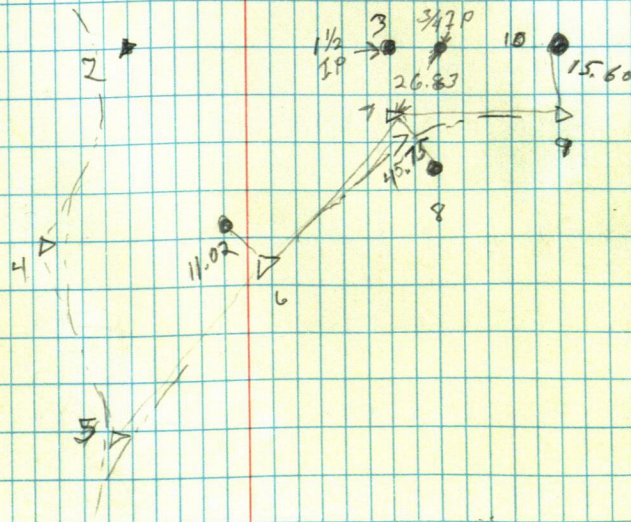
E. CURR

B. CURR

29

8-21-93

NORWAY RIDGE





0.0.28	70-39-21	275.05.56	215.92 65.806	215-054
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$\pi e$	7856
0.0,01	164-22-24
164,22,35	





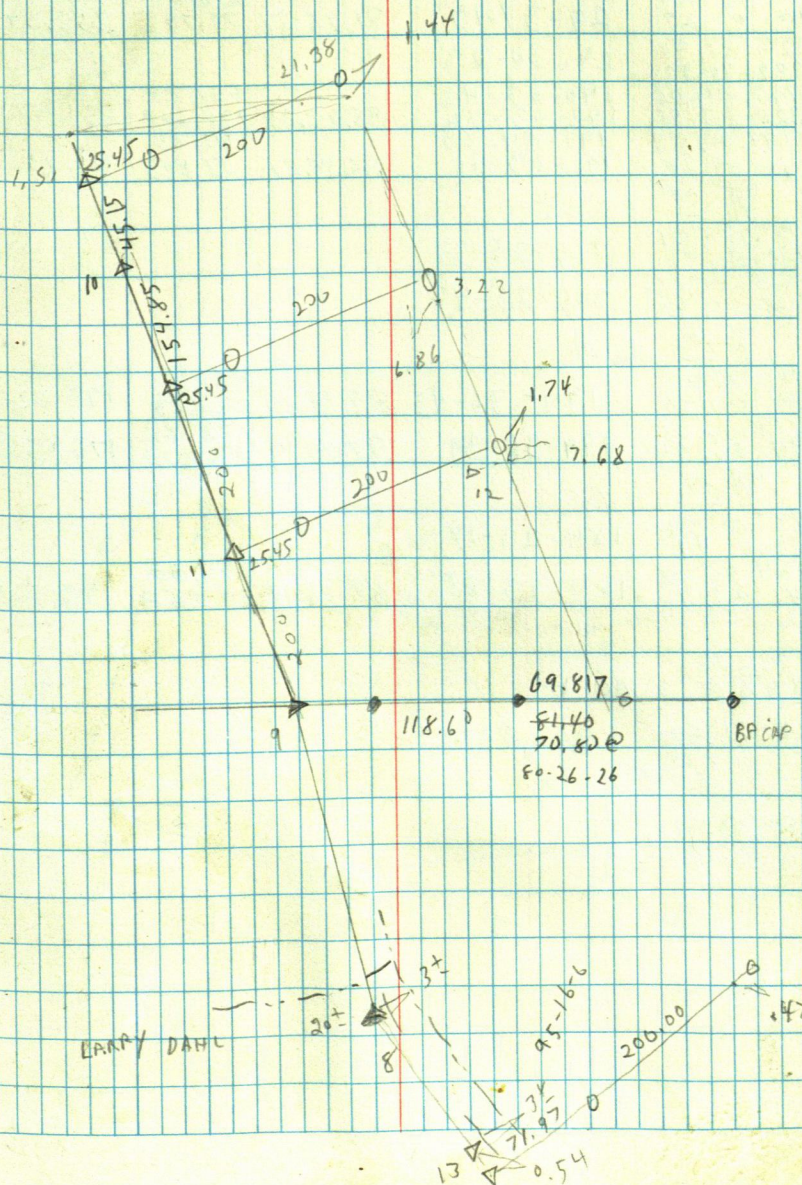


	$\bar{A} @$	BS	IO			
12	0-0-10 90-26-40			78-55-58	221.89 67.63	217.763

90-49-15			73-46-30	227.66 69.39	218.59
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270-45-01			73-02-20	213.39 65.02	204.074
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	$\bar{A} @$	BS	IO			
0-0-16 180-0-0 171-09-30						
1371-9-11		171-09-14		89-37-0	220.93 67.340	220.923
				88-57-55	271.55 82.76	271.50





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PT 6L 11-20-142-27

T @ 2 BS 1				
0 0 29	29-31-17	91,26.27	238.82 72,793	238.744
3 29-31-41	29-30-23			
4 140-04-06	140-03-42	88,23.32	651.74 198,649	651.478
5 191-04-29	191-03-26		111.05	
11-04-10	191-03-41	88,44.51	23,845	111,018

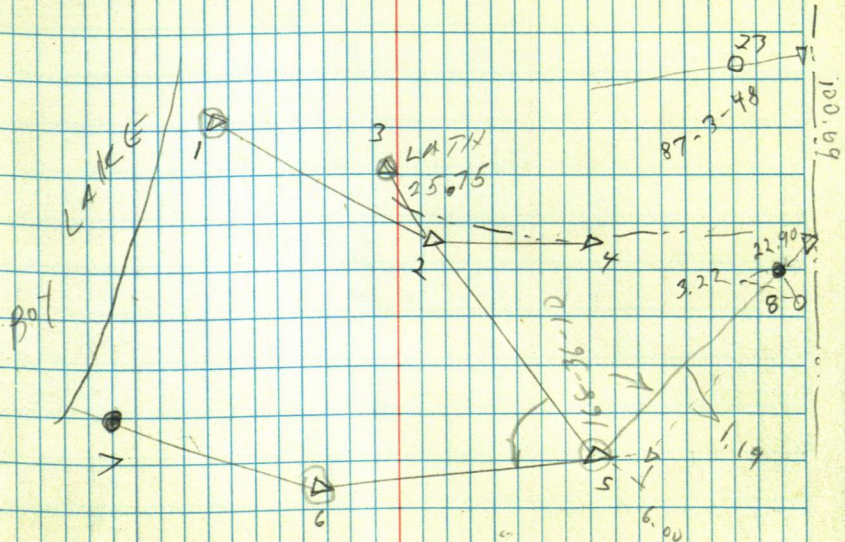
T @ 5 BS 2				
0 0 01	315-25-55			
180-0-02	315-25-43			
315,25.56				
135,25.45				

T @ 6 BS 5				
0 0 13	194-36-43	89,18.10	199.06 60,659	199.021
180-0-05	194-36-39	92,44.19	176.62 53,879	176.426
194,36.58				
14,36.44				

T @ 4 BS 2				
0 0 21	184-23-17			
180-0-41	184-23-05	89-06-14	199.80 60,868	199.728
184,23.38				
4-23-46				

T @ 2 BS 5				
18-26-57	25.75			

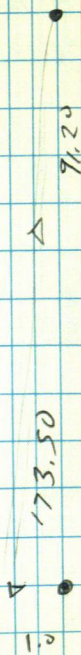
84-40-51





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TEN MILE LK





A @ old ⑥ BS old ⑦  
 0-0-36  
 180-0-27 167-07-04  
 167-07-40  
 1 347-07-33 167-07-06  
 0-0-23  
 192-53-10 192-52-47

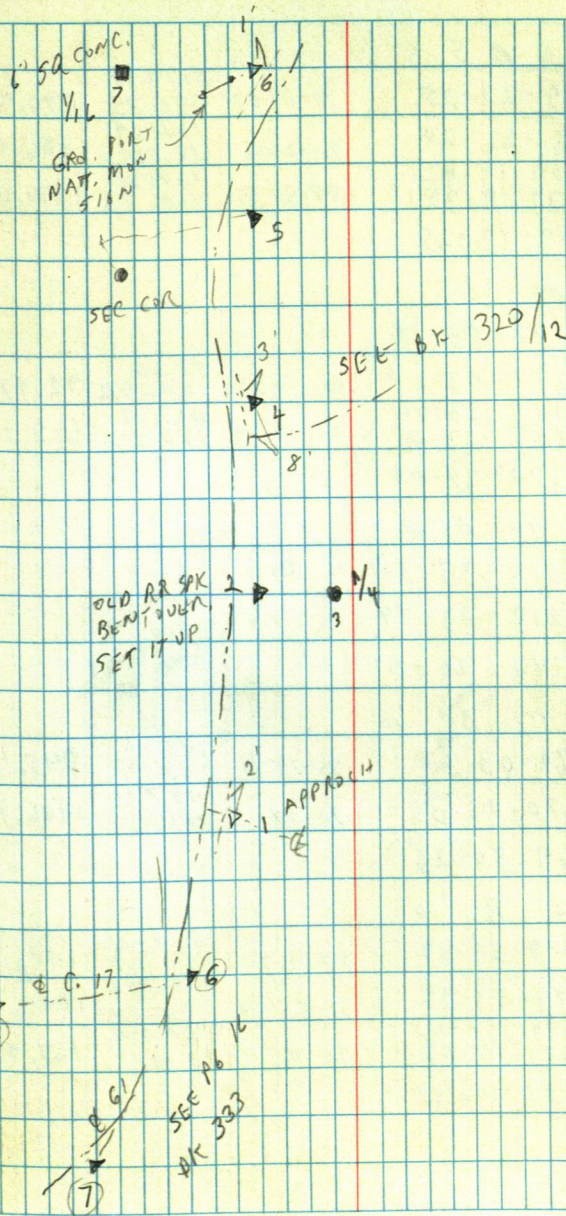
A @ 1 BS ⑥  
 0-0-31  
 180-01- 165-51-19 90-40-30 753.94 753.888  
 165-51-50 165-51 90-40-30 3246.67  
 2 345-52 194-08-28 990.207 3248.648  
 0-1-07  
 194-09-35

A @ 2 BS 1  
 0-0-15  
 180-0-05 177-41-40  
 177-41-55  
 352-41-50 177-41-45  
 0-0-27  
 4 182-18-42 182-18-15

A @ 4 BS 2  
 0-0-07  
 180-0-32 168-47-42  
 168-47-49  
 5 348-47-52 168-47-20

0-0-45  
 180-0-58 168-47-36 92-22-44 1485.96 1484.68  
 168-48-21 1260.13  
 348-48-18 168-47-20 89-07-31 387.057 1259.977  
 0-0-58  
 191-13-22 191-12-44

A @ 5 BS 4  
 0-0-12  
 180-0-24 176-48-09  
 176-48-27  
 6 356-48-27 176-48-03  
 0-0-0  
 183-12-01 183-12-01





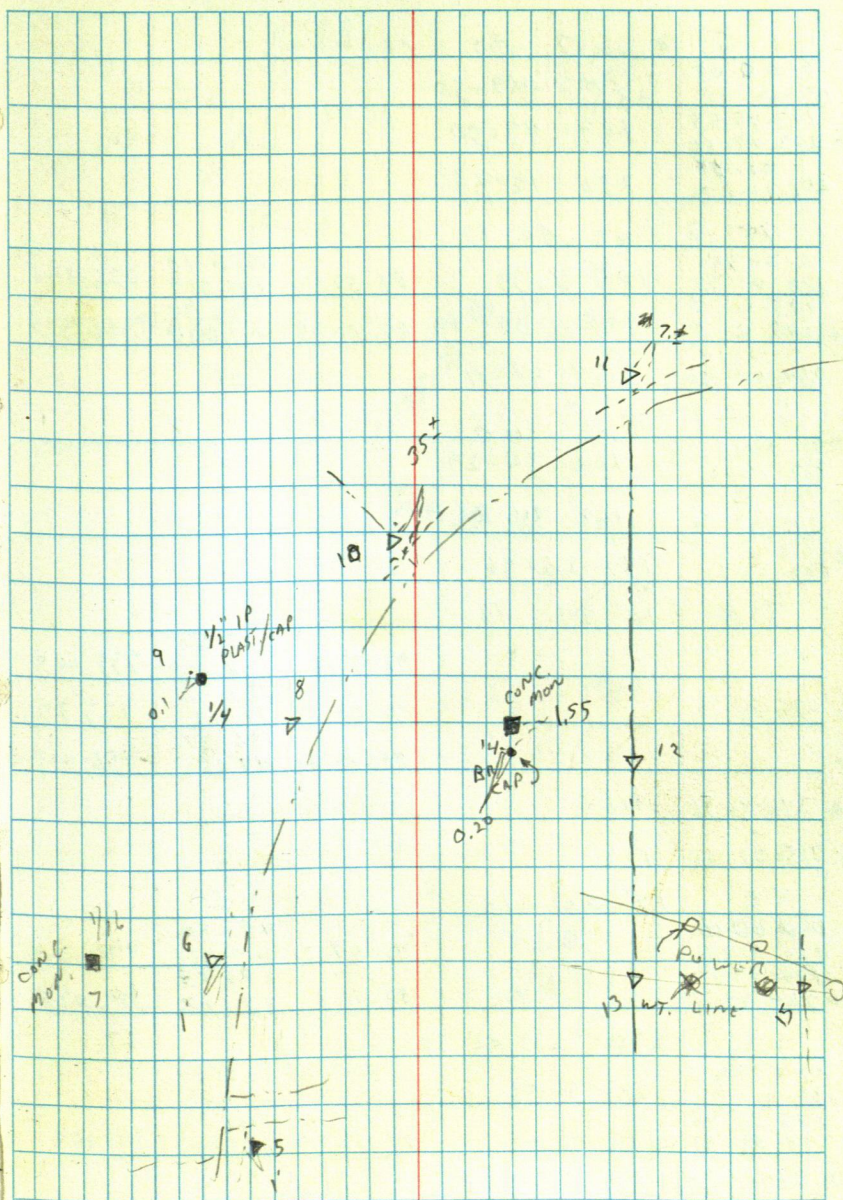
$\pi @ 6 BS 5$			
0-0-26	115-22-25	90-20-03	1170.44
180-0-31			356.25
115-22-51			1170.414
295-22-51	115-22-20	91-12-06	186.09
179-20-08	179-19-42		56.721
359-20-06	179-19-35	89-55-55	1371.42
0-0-17			418.012
180-40-42	180-40-25		1371.418

$\pi @ 8 BS 6$			
0-0-05	107-03-18		
180-0-04			
107-03-23	107-03-20	86-03-53	92.66
287-03-24			28.242
189-23-07	189-23-04		92.475
9-23-09	169-23-05	90-01-23	613.12
0-0-02			186.878
170-37-08	170-37-06		613.116

$\pi @ 10 BS 8$			
0-0-29	215-33-38		
180-0-24			
215-34-07	215-33-44		
35-34-08			
0-0-08	144-26-11		
144-26-19			

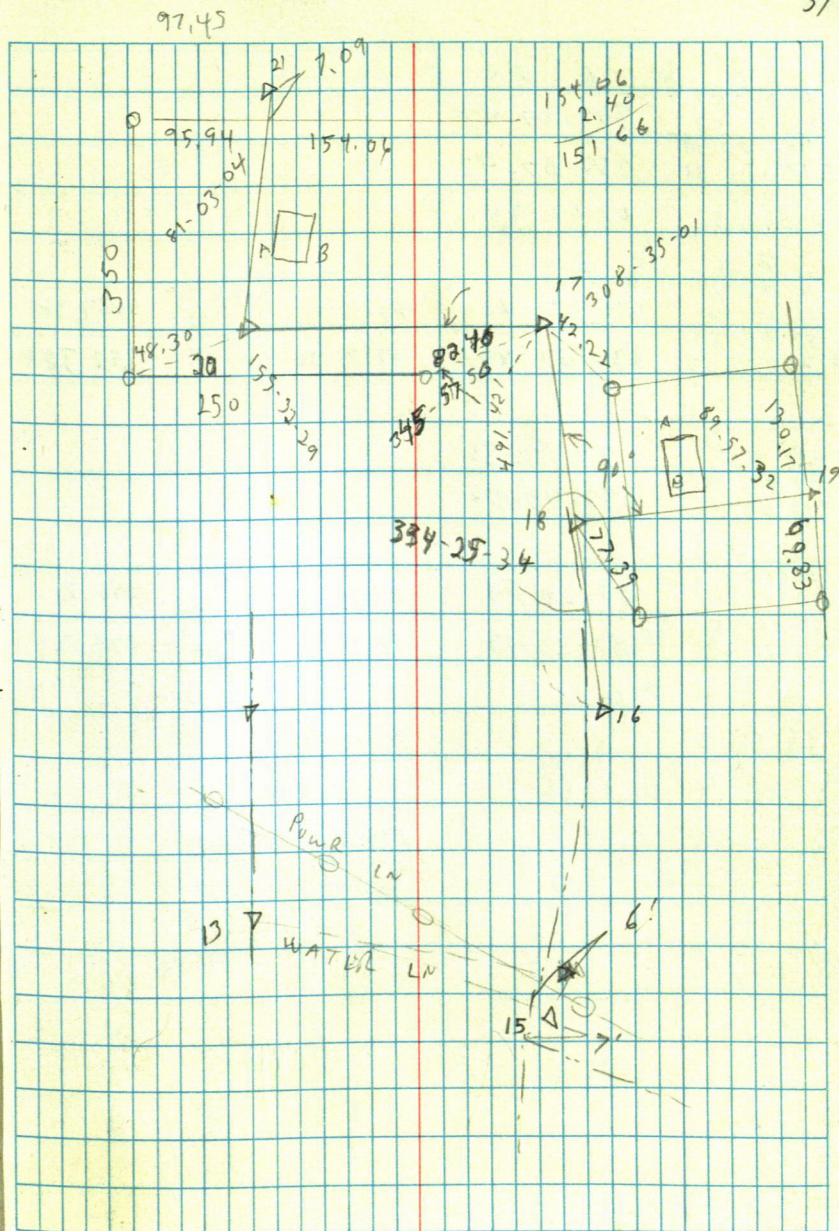
$\pi @ 11 BS 10$			
0-0-13	290-03-37	90-13-15	945.46
180-0-15			288.127
290-03-50			1487.91
110-3-50	290-03-35	92-04	453.85
0-1-06			1486.936
69-57-31	69-56-25		

$\pi @ 12 BS 11$			
0-0-0	179-53-33	87-44-13	1487.82
180-0-0			453.467
179-53-33			1004.76
359-53-34	179-53-34	91-58-40	306.248
304-18-04	304-18-04		167.97
14-12-17-52	304-17-52	90-43-30	51.197
0-0-0			167.955
180-06-15	180-06-15		





T @ 13 BS 12			
0-0-05	103-49-50		
180-0-05	103-49-50		
103-49-55	103-49-50		
15 283-49-55	256-10-13		
-01-04			
256-11-27			
T @ 15 BS 13			
0-0-35	105-11-35	88-52-10	625.19
180-0-35			190.559
105-12-10			366.59
16 285-12-5	105-11-30	87-49-35	111.734
0-0-19			366.320
254-48-50	254-48-31		
T @ 16 BS 15			
0-1-10	162-34-29		
180-1-10			
162-35-39	162-34-28		
17 342-35-38			
0-0-45	197-25-36		
197-26-21			
T @ 18 BS 16			
		92-9-10	335.33
			102.209
			233.32
20 270-02-28		91-04-0	71.116
			156.37
17		88-40-40	47.662
			156.328
A 246-46-56	116		
B 265-02-36	103		
T @ 17 BS 16			
00-00-00			491.55
186-0-02		91-59-21	149.826
104-43-17			286.03
20 284-43-22		89-51-0	87.182
			286.028
T @ 20 BS 17			
0-0-12			286.04
180-0-0	278-56-56		87.185
278-57-08			347.16
21 98-56-53	278-56-53	89-56-40	103.986
			341.159
A 284-21-20	36		
B 315-43-40	46		





	$\wedge$	(2)	6	B5	5
	0-0-55				
	18-0-53		359-07-43		
	359-08-38				
25	179-08-35		359-07-42		
	0-0-0				
	0-52-25		0-52-25		

$\pi a$	25 B5 6			
0-0-11				
180-0-08	83-22-40	89-50-17	1084.39 330.522	1084.381
83-22-51			352.39	
26 267-22-57	83-22-49	89-46-50	107.41	352.388

0-0-10	
180-0-00	139-42-55
139-43-05	
319-43-02	139-42-54

0-1-23			446.77	
180-1-10	87-20-09	89-10-24	136.175	446.721
87-21-35			279.85	
267-21-23	87-20-13	92-36-24	85.304	279.569

89-58-22

91-12-40

89-09-40 235.05

$$\begin{array}{r} 233.09 \\ 232.26 \\ \hline .79 \end{array}$$

7  $\frac{1}{16}$

6

23

11

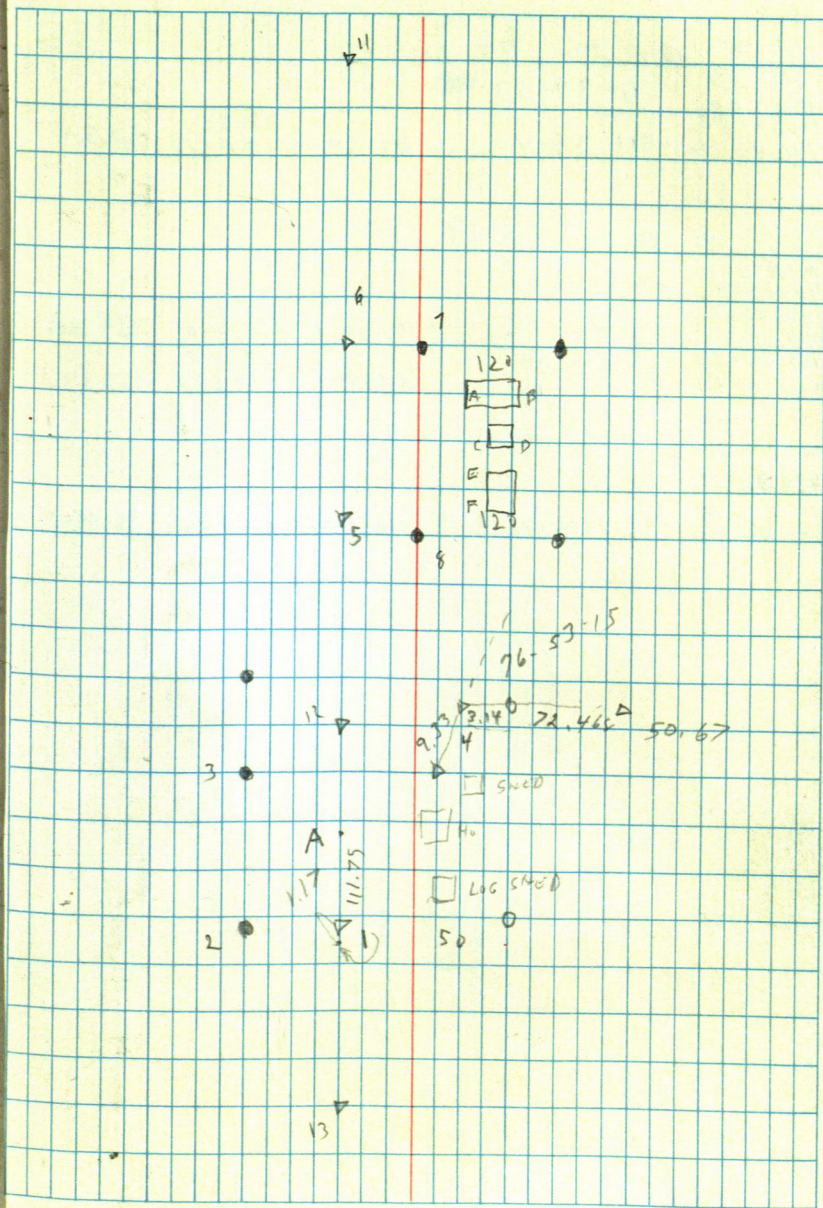
5  
RR SPK

Hand-drawn diagram of a triangle with vertices labeled 26, 27, and 28. Side lengths are given as 200, 254.05, and 291.6. An angle of 33 degrees is marked at vertex 28. A dashed line connects vertex 26 to the midpoint of the opposite side.

53-54-42 59, 91

87- 20 - 11      39,16





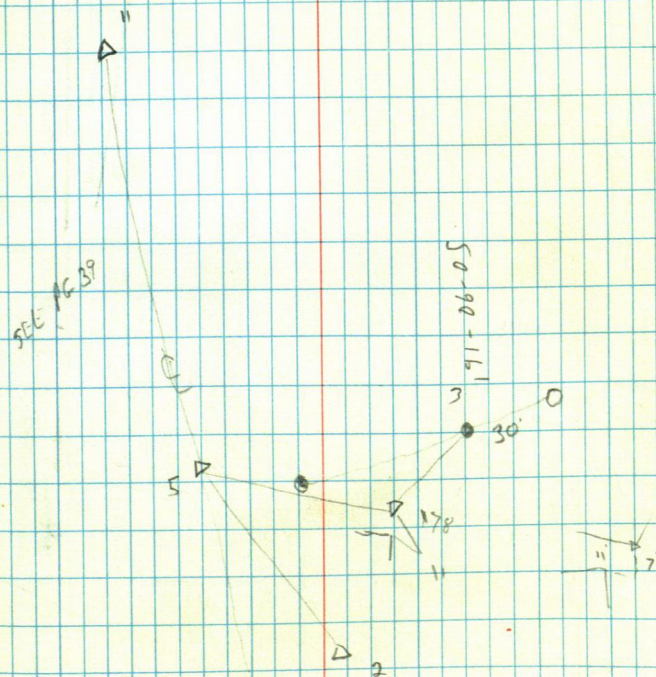


	K	0	19	BS	18
	0-0-35				
	180-0-40		11-39-53		
	11-40-28				
2	191-40-20		11-39-40	89-55-33	57.32 17.466
					57.311

	K	0	5	BS	11
	0-0-11				
	180-0-09		97-04-04		
	97-04-15				
1	277-04-10		97-04-01	91-55-55	135.75 41.373
	161-07-50		161-07-39		155.17
2	341-07-51		161-07-42	94-44-04	47.294 154.637

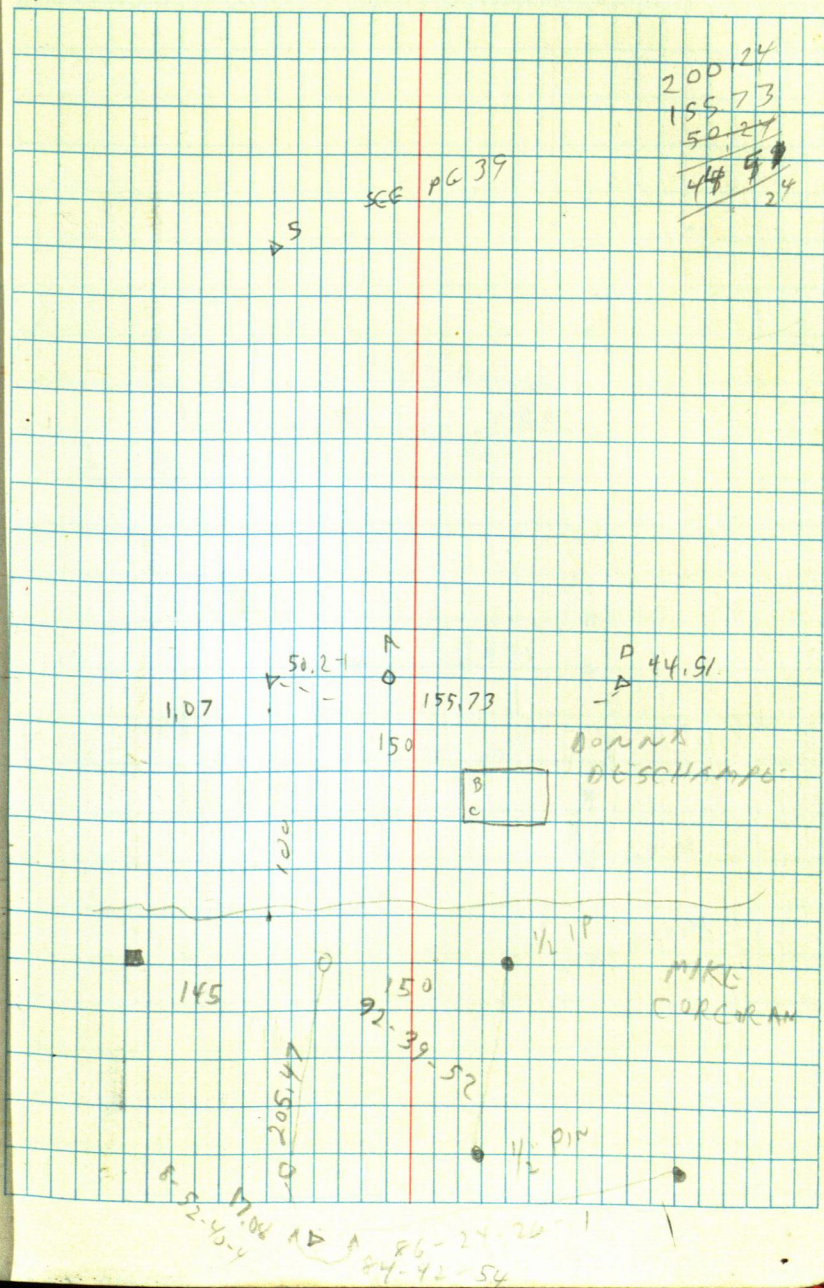
	K	1	BS	5
	0-0-19			
	180-0-15		161-46	
	161-46-19			
3	341-46-10		161-45-55	116-50-45
				40.69 12.465
				36.485

C<sup>1/4</sup>  
 18  
 19  
 SEE PC 37

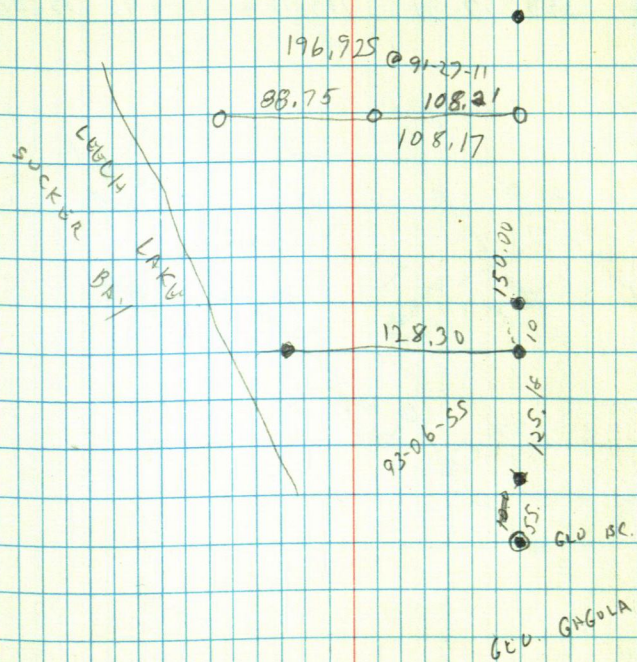




	A	B	C	D
B 30-13	61	88-07	395.93 120.64	395.795
C 54-06	87	91-50-30	155.75 42.477	
		87-00-06	146.91 44.777	
0-0-35		87-36-12	379.75 115.738	379.418 379.40
180-0-32	7-30-15			
7-30-30				
187-30-50	7-30-13			









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11	2	B	S	1
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Q - 5 - 0

180-0

262-36-05

262-36-05

262-36-02

1 2 3 BS 2

0-0-04

80-0-05

171-56-02

91-11-29

397.51

12111

397.35

171-56-06

171-55-54

115-51-58

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45 513

551-55-59  
50 25 20

259-27-2

115-51-58

15, 2/17

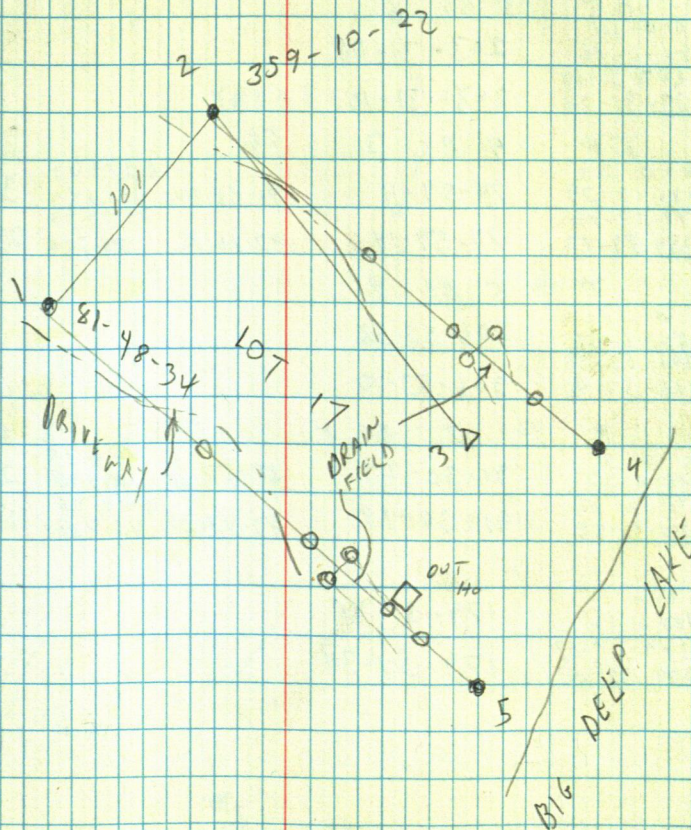
39-27-30  
39-27-34

259-27-2  
159-27-3

103-28-20

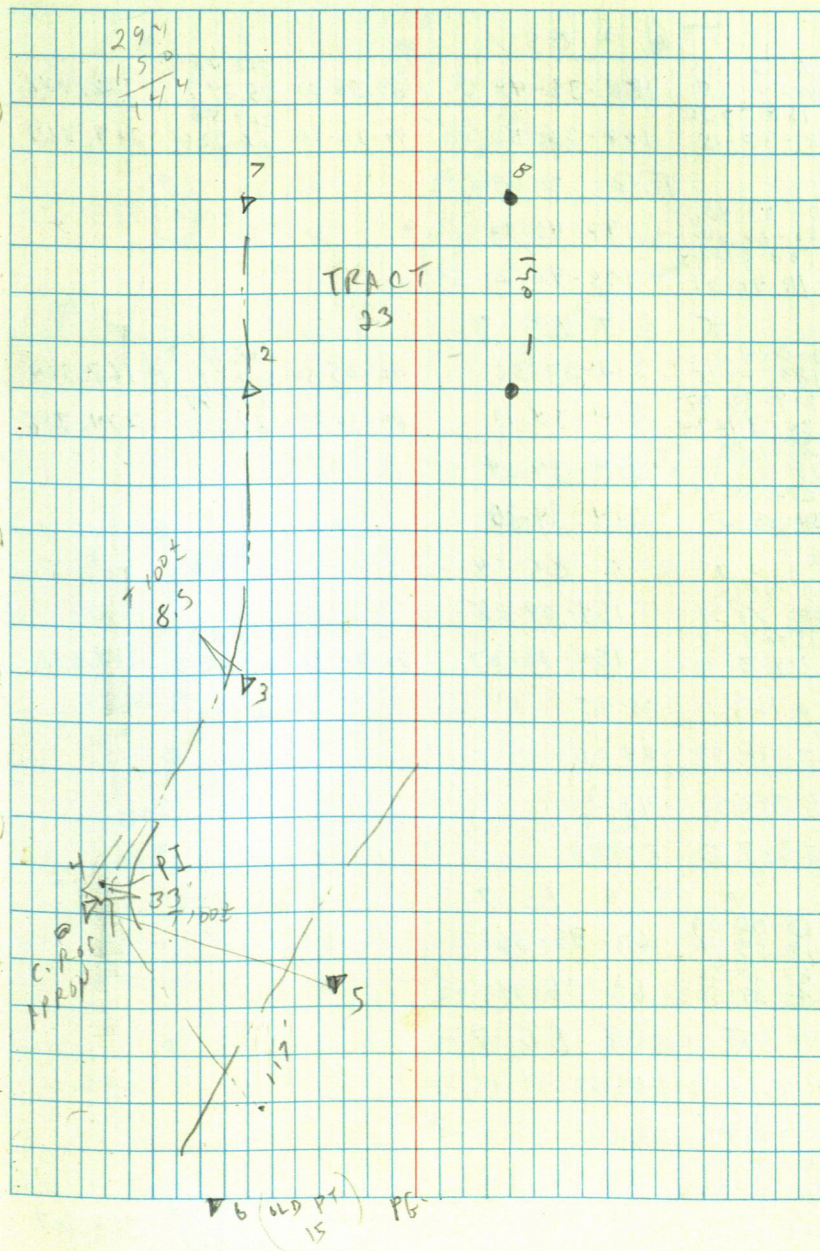
98.58  
20.41

95,865





	RIA	DAN	OLSON			
	$\pi @ 2 BS 1$					
	0-0-00				228.89	
	129-59-49	91-29-49	88-39-39	69.768	228.825	
	91-29-49			277.16		
3	271-29-50	91-30-01	89-55-10	89.659	294.157	
	$\pi @ 3 BS 2$					
	0-0-11					
	180-0-16	203-31-08				
	203-31-19					
4	23-31-26	203-31-10				
	$\pi @ 4 BS 3$					
	0-0-35			379.43	379.381	
	180-0-29	74-59-11	90-52-50	115.649		
	74-59-46			230.36		
5	254-59-43	74-59-14	82-16-12	70.216	230.092	
	$\pi @ 5 BS 4$					
	0-0-37					
	180-0-26	306-52-58				
	306-53-35					
6	126-53-46	306-53-10				
	$\pi @ 7 BS 8$					
	0-0-3			226.38	226.337	
	180-0-27	91-30-29	88-57-20	68.998	226.317	
	91-30-32			149.95		
2	221-30-45	91-30-18	89-47-30	45.706	149.95	
	0-0-12					
	180-0-51	179-57-45				
	179-57-57					
	359-58-25	179-57-34				





π @ 2 BS 1

0-0-32			312.48	
180-0-25	188-36-48	89-58-40	95.242	312.476
188-37-20			219.56	
3 8-37-15	188-36-50	90-20-10	66.928	219.565

π @ 3 BS 7

0-0-45				
180-0-40	198-40-19			
198-41-04				
4 18-41-01	198-40-21			

π @ 4 BS 3

0-0-41			167.51	
180-6-15	214-33-56	90-05-50	51.654	167.504
214-34-37			274.89	
5 34-34-34	214-34-19	89-50-25	83.633	274.386
0-0-59				
180-0-10	214-34-24			
214-35-23				
34-35-21	214-34-20			

π @ 5 BS 4

0-0-29				
180-0-24	154-09-08			
154-09-37			204.82	
6 334-9-31	154-09-07	90-20-10	62.427	204.812

A 163-10 95.95

B 168-39 64.26

C 308-33 43.21

D 323-35 53.88

π @ 6 BS 7

0-00-00				
129-57-46	63-35-56			
5 63-35-56				
243-35-50	63-36-04			

π @ 8 BS 7

A 93-20 264.50

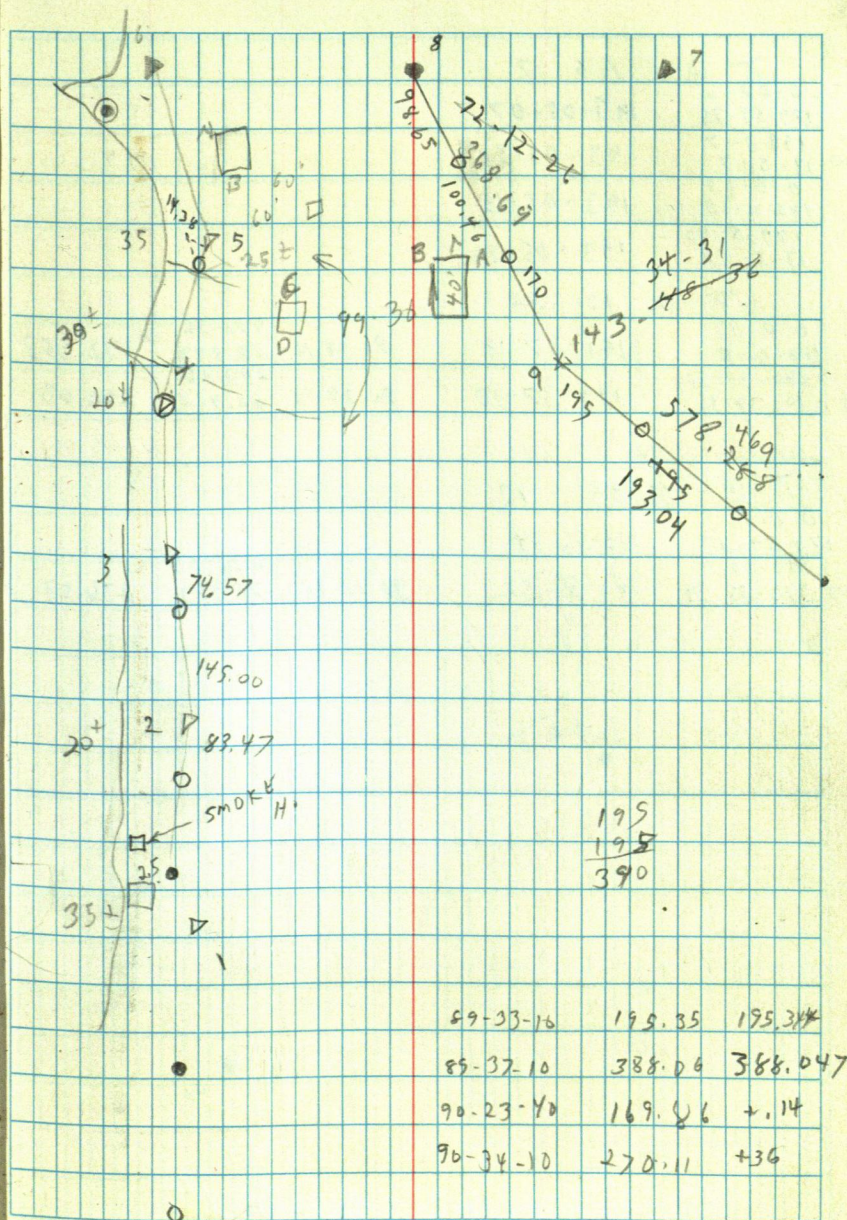
B 98-37 265.01

0-0-16 72.20-44

180-0-12 72.20-43

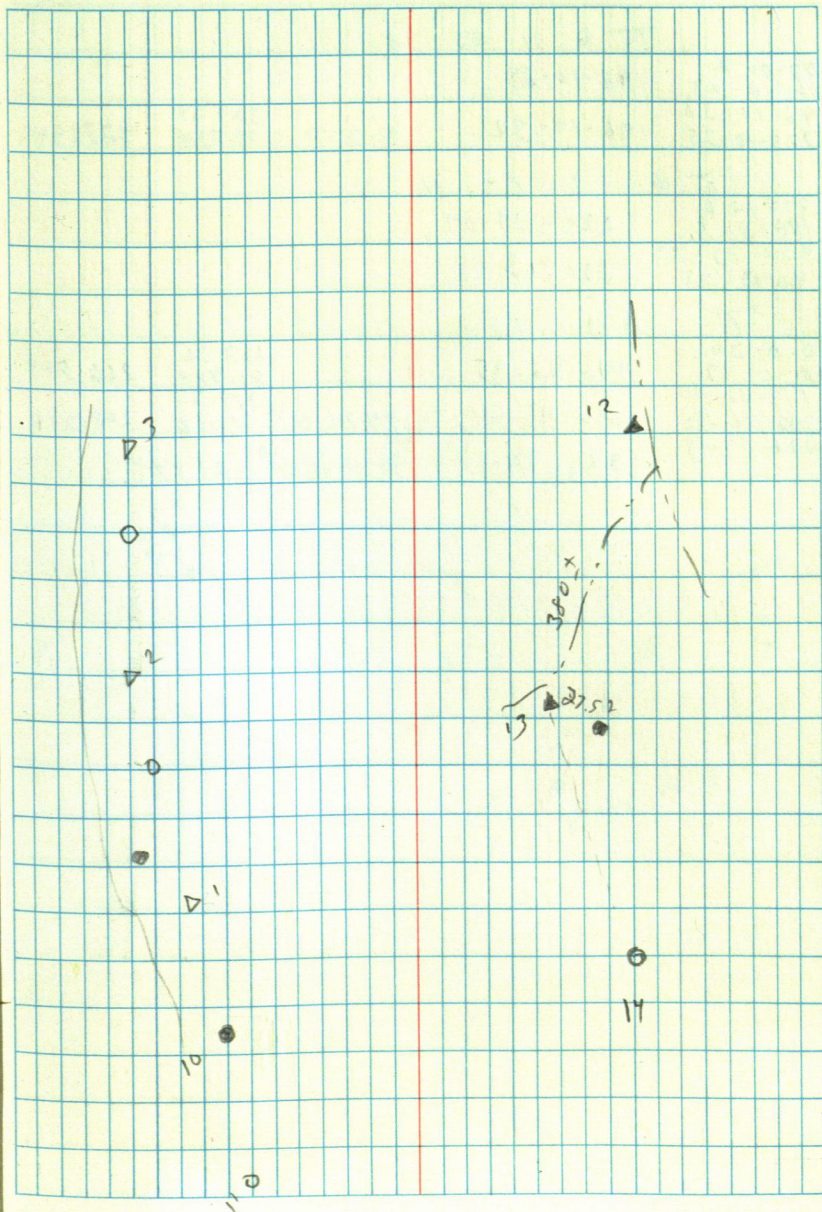
9 252-20-55

89-48 369.82  
112.509 369.117





	$\pi @$	1 BS 2			
	0-00-0				
	129-59-35	193-05-07			
10	193-5-7				
	13-5-7	193-05-32			
	0-0-25				
	180-0-15	193-05-15			
	199-5-40				
	13-5-37	193-05-22			
	$\pi @$	10 BS 1			
	0-0-32			172.56	
	180-0-5	190-37-18	90.39-10	52.599	172.553
	190-37-50			200.05	
11	10-37-35	190-37-30	90.29-10	60.968	200.03
	$\pi @$	13 BS 12			
	0-0-15				
	174-59-47	140-55-54			
	140-56-9			236.08	
14	320-55-39	140-55-52	90-12-20	71.953	236.07

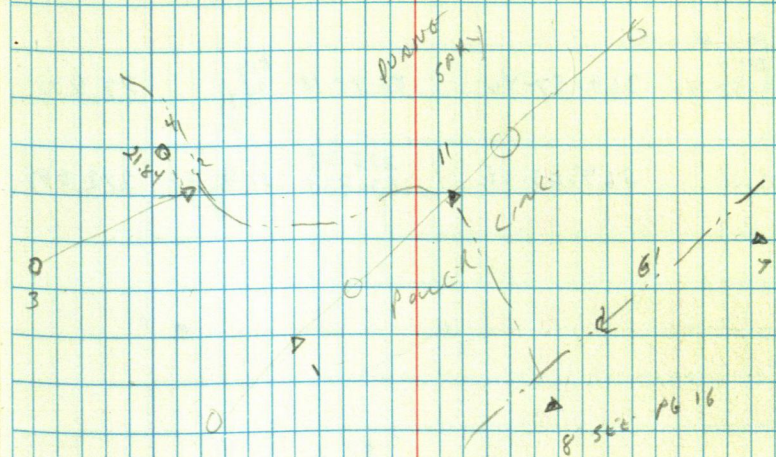




	$\pi$	@	11	BS	8
00-00-2					
140-0-03	96-10-29				
96-10-31					327.21
276-10-35	96-10-32		91-3-10		99.734
					327.154

	$\pi$	@	1	BS	11
0-0-26					
140-0-5	220-13-07				
220-13-33					
2	40-13-33	220-13-28			

	$\pi$	@	2	BS	1
0-0-39					
181-0-39	146-45-35				267.26
146-46-14					81.488
3	386-46-36	146-45-51	94-29-10	200,52	266,514
	226-59-49			61,060	200,304
4		226-59-10	90-48-08	21.84	





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0-0-39  
180-0-28 160-36-46  
160-37-25  
340-37-08 160-36-40

$\pi$  3 8 5 2

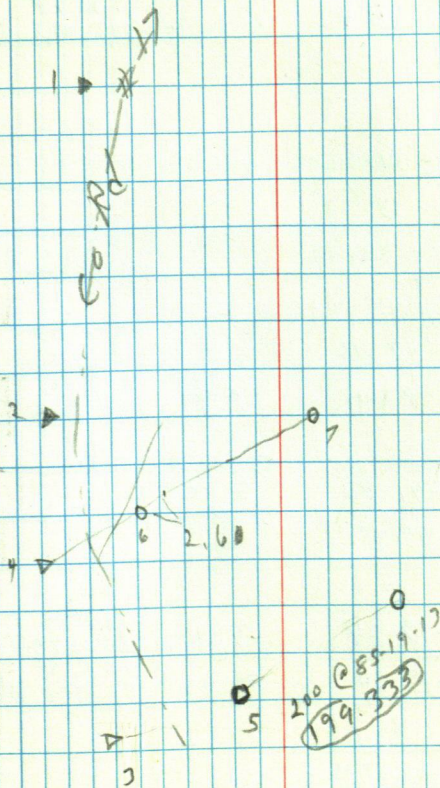
0-0-40			572.70	
180-0-33	89-07-00	92-40-17	174.566	572.087
89-3-40	89-03-03	81-0-16	78.33	
5 269-7-36			27.876	77.368
359-10-55	359-10-15		200.55	
4 179-10-55	359-10-22	93-40-37	61.125	200.132

$\pi$  4 8 5 3

0-0-0			80.11	
4 269-57-40	269-57-40	86-48-18	24.41	79.976

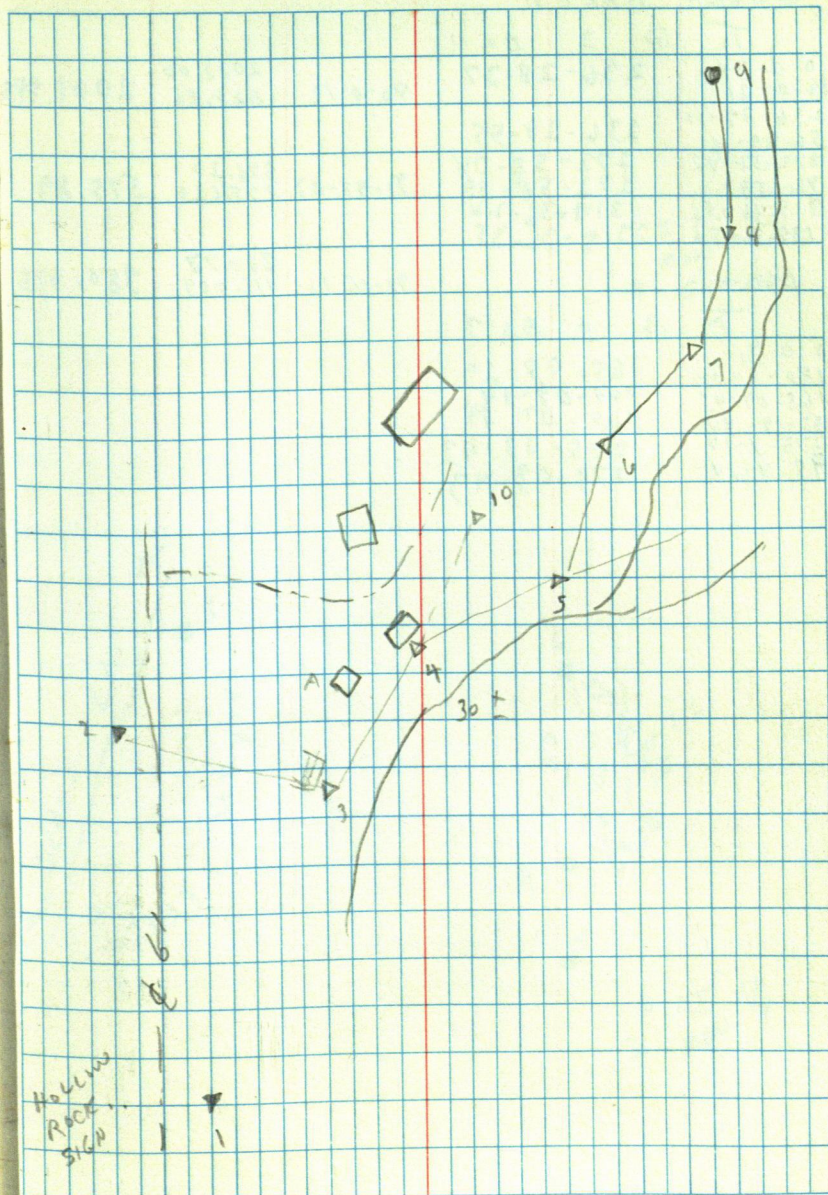
0-0-0

7269-05-06	269-05-06	275.28	81-12-52	272.097
		83.935		





K @ 2 BS 1				
0-0-06	302-27-39			
179-59-54				
302-27-45	302-27-44			
3122-27-38				
K @ 3 BS 2				
0-0-24	107-33-40	86-16-55	339.23	339.105
180-0-18			103.415	
A 92-20 180.83				
107-34-04	107-33-42	90-42-30	335.17	335.131
4 282-34-0			102.153	
K @ 4 BS 3				
0-0-55	200-33-09			
180-0-48				
200-34-04	200-34-22			
5 20-35-10				
0-0-06	200-32-57			
180-0-15				
200-33-03	200-32-55			
20-33-10				
K @ 5 BS 4				
0-0-34	125-47-16	91-42-42	200.08	199.991
180-0-32			60.985	
125-47-50	125-47-11	88-39	213.16	213.094
6 305-47-43			64.968	
K @ 6 BS 5				
0-0-36	190-41-44			
180-0-30				
190-42-20	190-41-45			
7 10-42-15				
K @ 7 BS 6				
0-0-29	146-19-34	89-35-30	228.44	228.434
180-0-20			69.629	
146-20-03	146-19-24	89-04	165.35	165.326
8 326-19-54			50.398	
K @ 8 BS 7				
0-0-18	139-26-33			
180-0-11				
139-26-51	139-26-34	94-38-20	223.04	222.299
9 319-26-45			67.977	

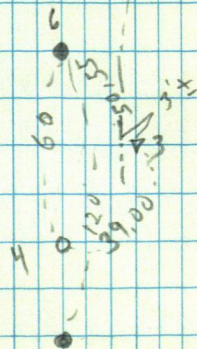
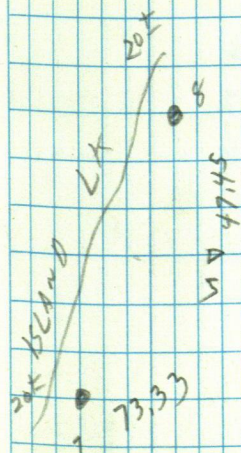




WARRER BAKER

	T	@	3	BS			
	0-0-34		236-28-37		90-0-12	2062.00	2061.995
	180-0-21					628.50	
4	236-29-11		236-28-55				
	56-29-16						
	272-58-42		272-58-08		71-92-02	576.20	575.89
5	72-59		272-58-39			175.625	
	319-36-56		319-36-22				
6	139-36-56		319-36-35				
2	180-				90-16-16	380.77	380.675
						116.059	

	T	@	5	BS	
	0-0-31		165-09-29		
	180-0-30		165-09-14		
7	165-09-45		165-09-44		
	345-9-44				
	275-4-14		275-03-43		
8	95-4-14		275-03-43		



CI  
mon 1/4

CI  
mon  
Sec col



5/11 1255 EL

0-0  
89-24.30

355.36

80-1-20

425.65

79-37.50

452.75

13.6

Top water  
pond

14.25

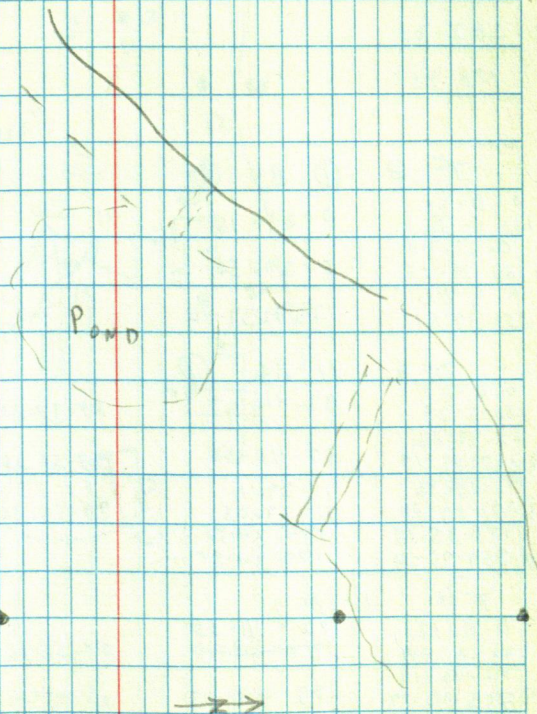
Lake

2.6

2.9

6.4

51





TP 4 BS 5  
0-0-0  
10 306-32-30 76.66

TA 10 BS 4  
A 86-25 76.42  
B 100-51 60

C 147-59-30 82.67

D 262-30

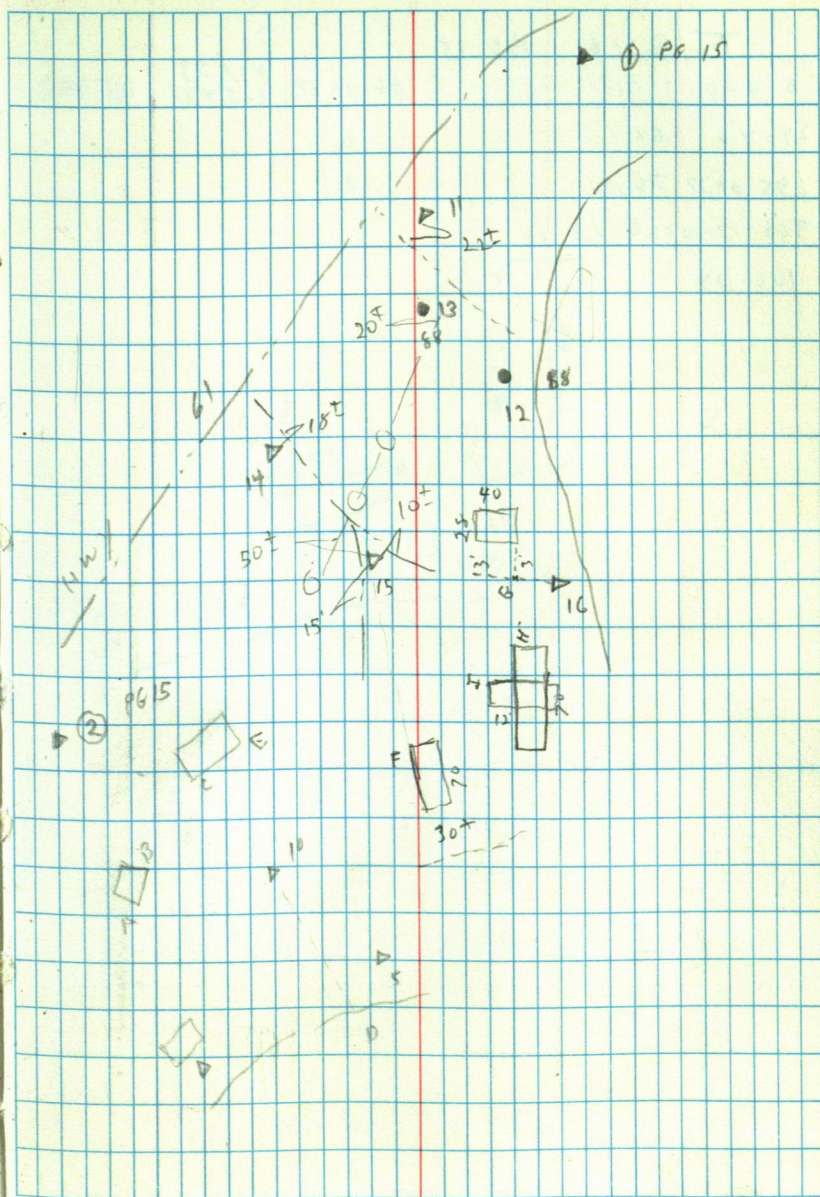
E 126-40

TA ① BS ②  
0-0-25 0-21-15  
180-0-50  
0-21-40  
11 180-21-45 0-20-55  
0-0-41  
359-39-51 359-39-10

TA 11 BS ①  
0-0-25 87-41-57 89-37-20 580.21 580.193  
180-0-29 176.847  
87-42-22 292.55  
12 267-42-19 87-41-50 93-51-50 89.170 291.885  
91-29-36 91-29-11 177.37  
13 271-29-34 91-29-05 99-55-36 54.063 176.714  
179-35-15 179-34-50  
14 359-35-20 179-34-51

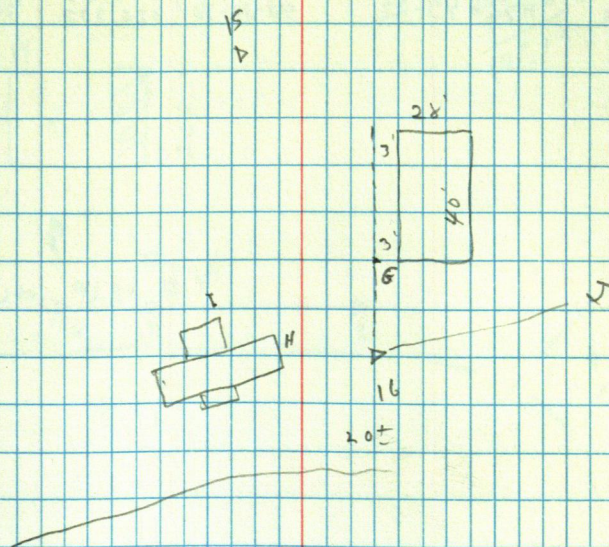
TA 14 BS 11  
0-0-12 72-41-58 556.10  
180-0-14 148-40-10 89-56-16 169.50 556.100  
72-42-10 261.49  
15 252-42-19 72-42-05 90-56-10 79.689 261.407

TA 15 BS 14  
0-0-30 148-40-10  
180-0-17  
148-40-46 148-40-29  
16 328-40-46  
212-35-55 212-35-25





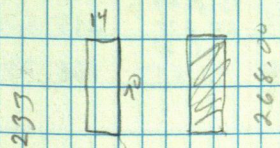
	K	Q 16	BS 15		
	0-0-0			86-31-47	411.53 125.437 411.397
G	24-40	61			
H	295-0-37	76.41			
I	306-17-20	120.43			
J	100-04				





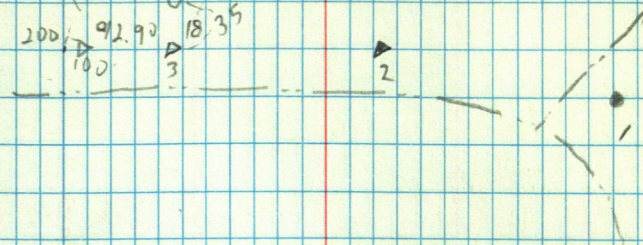
	2	BS 1			
2-0-55	176-43-27				
181-1-38					
176-44-22			414.36		
3 356-45	176-43-22	90-26-40	126.297	414.346	

0 107.10 92.90



200  
92.90  
107.10

0 35 200 92.90 18.35 100 3 2





T @ 3 BS 2				
0-0-47	144-17-05	92-20-30	75.22 22.928	75.158
5 144-17-52		86-12-22	215.97 65.835 166.87	215.508
4 142-2-55	182-02-08	65-39-50	50.833	166.299

T @ 2 BS 1			
0-0-42	305-37-23		
180-0-21			
305-38-05			
3 125-38	305-37-39		

0  
5  
CURTIS  
GRENOR

04

D3

D2

D1



A @

4 BS 5

0.0.10  
180.0.08 5-25-49  
05.25.59  
183.25.50 5-25-49  
0.0.30  
354.24.57 354.34-21

A @

6 BS 4

0.0.27	170-10-20	91.09.31	507.19	507.098
180.0.23			154.608	
170.10.47	170-10-33	92.36.42	376.08	375.692
350.10.56			114.632	
171.40.39	171-40-12			
220.19.45	220-19-13	94.32.51	581.17	579.274
240.19.38	220-19-15		177.143	
0.0.27	<del>220-19-16</del>			
180.0.21	217-11-41			
212.12.08	<del>217-11-51</del>		331.63	
932.12.02	217-11-59	97.06.35	101.080	329.077

A @

8 BS 6

0.0.0	267-14-56	90.52.42	643.04	642.897
267.14.56		91.22.19	195.999	
			189.39	189.27
			57.705	

A @

2 BS 6

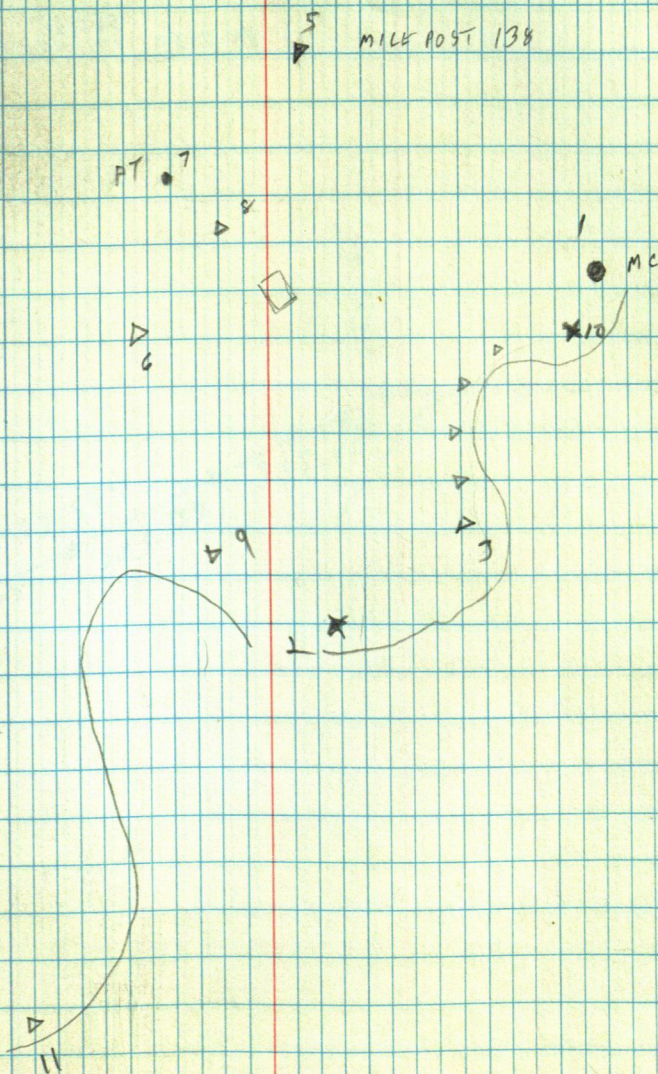
0.0.24  
180.0.22 137-09-20  
137.09.44  
10317.09.44 137-09-22  
0.0.15  
222.50.43 222-50-24

A @

10 BS 2

0.0.0	0-55-06	91.17.35	10415.09	1044.734
180.0.0			318.492	
0.55.0	0-54-53	91.17.31	883.34	883.108
180.54.53			269.240	
0.0.9				
9.49.0	9-48-51	90.59.39	634.41	634.279
22.25.42	22-25-33	90.23.12	193.348	
26.22.26	26-22-27	91.06.05	583.53	583.376
0.0.22	194-12-54		177.866	
194.13.26		92.47.52	407.14	407.034
			124.079	
			106.45	106.366
			92.47.52	

A. 93.13.24 A B  
38.20 B 109.55  
48.70

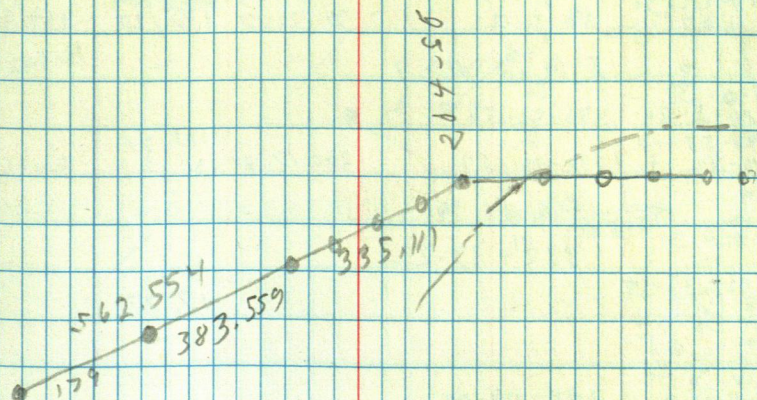




work

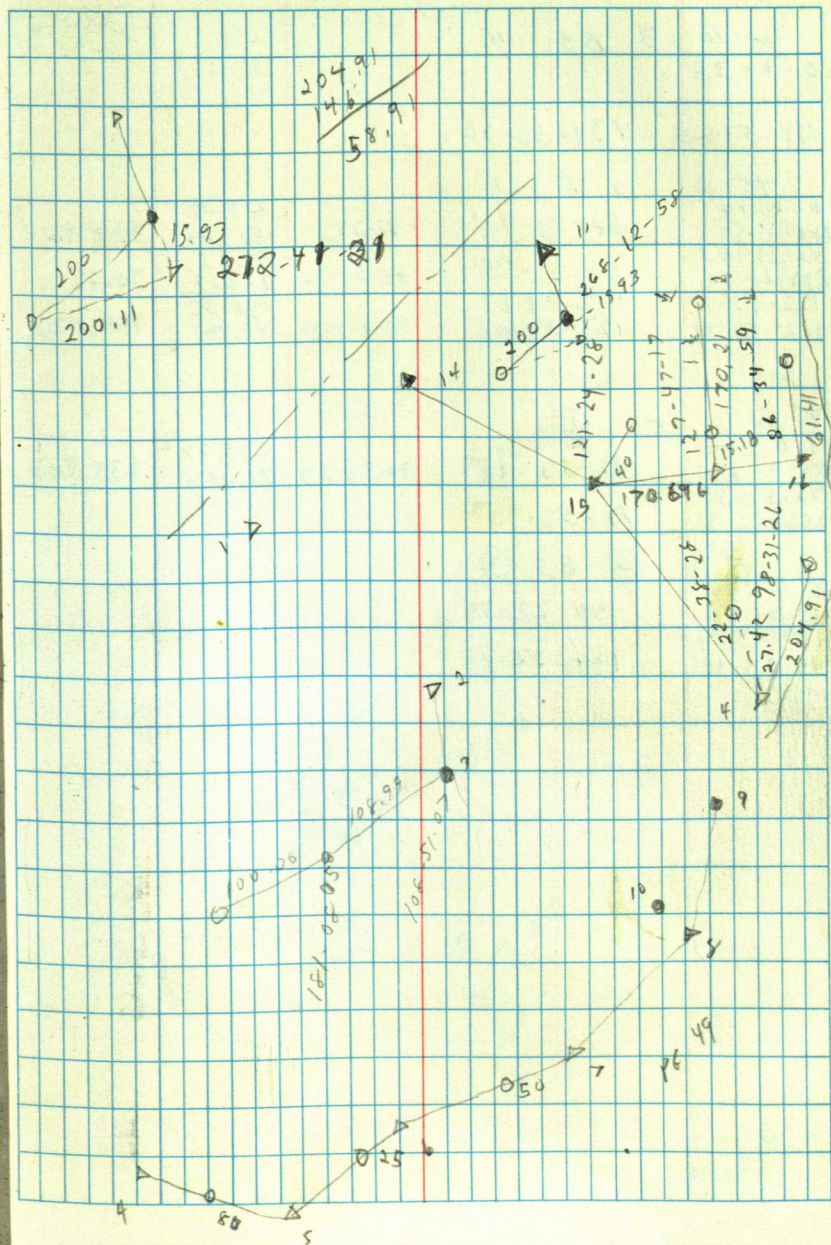
89.7-50    562.67  
171.475    562.559

57





$\pi$	$\Theta$	$14$	$BS$	$11$
0-0-32				
180-0-28		180-02-41		
180-03-13				
10-3-13		180-02-45		





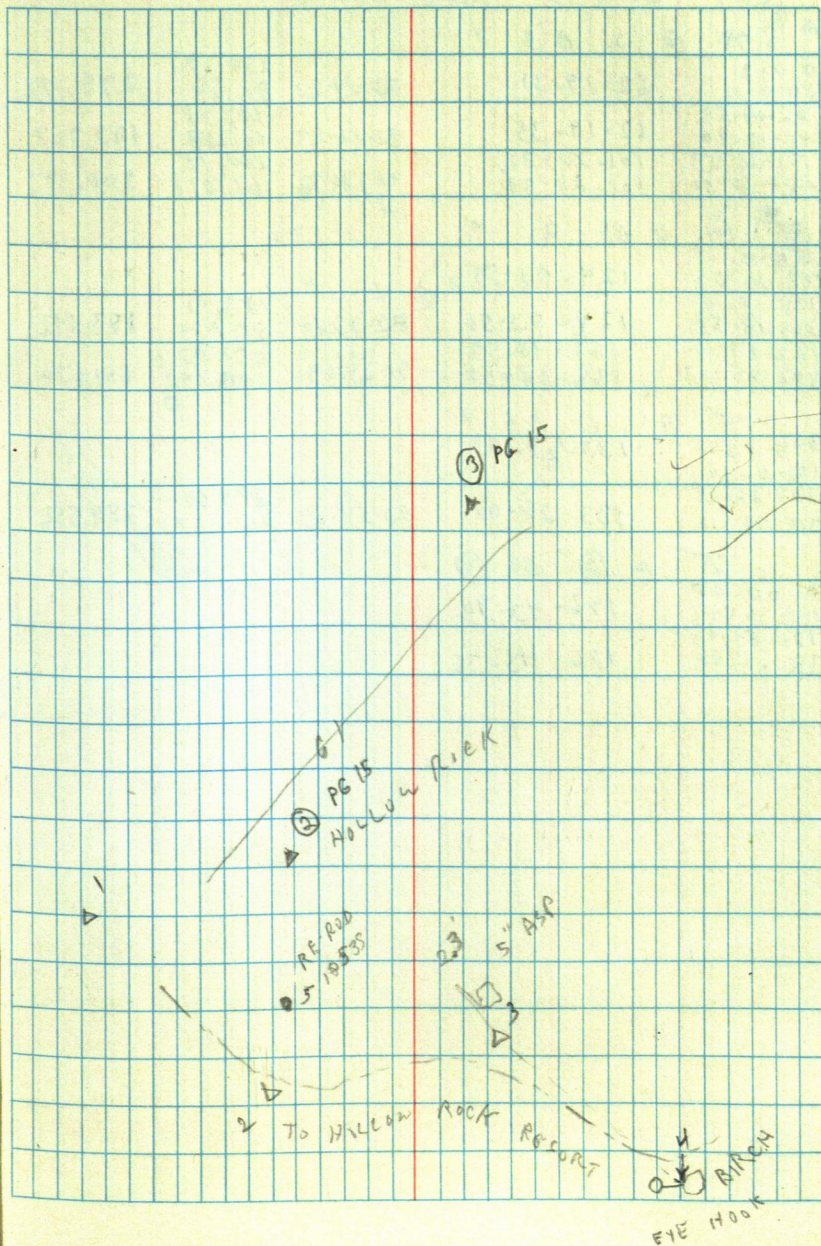
$\pi @ 3 BS 4$   
0-0-35

2 134-57-25 134-56-50

	$\pi @$	2 BS 1			
0-0-14			91-22	329.02	
180-0-15		58-21-26		100.266	328.901
58-21-45				90.75	
5 238-21-50		58-21-35	88-29-26	27.662	90.72
122-54-21		122-54-01		158.52	
4 302-54-21		122-54-06	91-52-26	48.31	158.423

	$\pi @ 1$	BS ②			
0-0-20			90-54-30	235.77	
180-0-21		72-52-31		71.864	235.742
72-52-53					
2 252-52-51		72-52-30			

	$\pi @$	② BS ③
0-0-47		
180-0-46		194-22-49
194-23-36		
1 14-23-34		194-22-48





# RAT JOHNSON TRACT BIA SP

T @ 2 BS 1

0-0-21	62-19-31	90-01-23	299.17	299.172
180-0-11			91.189	
62-19-52	62-19-35	91-18-23	197.78	197.727
242-19-46			60.283	
101-28-53	101-28-32	91-18-36	200.18	200.197
3 281-28-50	101-28-39		61.018	

T @ 4 BS 2

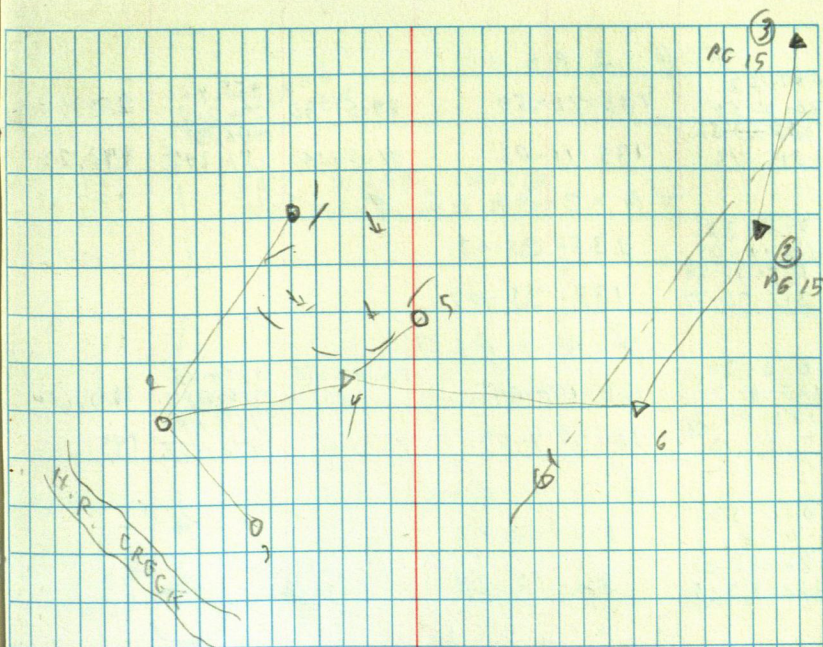
0-10-11	124-03-59			
5 180-10-05				
124-14-10	124-03-50	89-33-10	183.21	183.192
45 304-13-55			55.839	
162-29-10	162-18-59	91-24-03	651.87	651.676
6 342-29-13	162-18-58		198.692	

T @ 6 BS 4

0-0-12	135-28-03			
180-0-10				
135-28-15	135-28-08	90-54-03	384.60	384.552
23 315-28-14			117.227	

T @ 2 BS 3

0-00-07	176-43-30			
180-0-04				
176-43-37	176-43-36			
1 356-43-40				





A @ 2 BS 1				
0-01-02	135-10-59	89-56-30	955.40	955.402
180-0-54			291.210	
135-12-01			496.37	
3 315-12	135-11-06	91-5-15	151.294	496.271

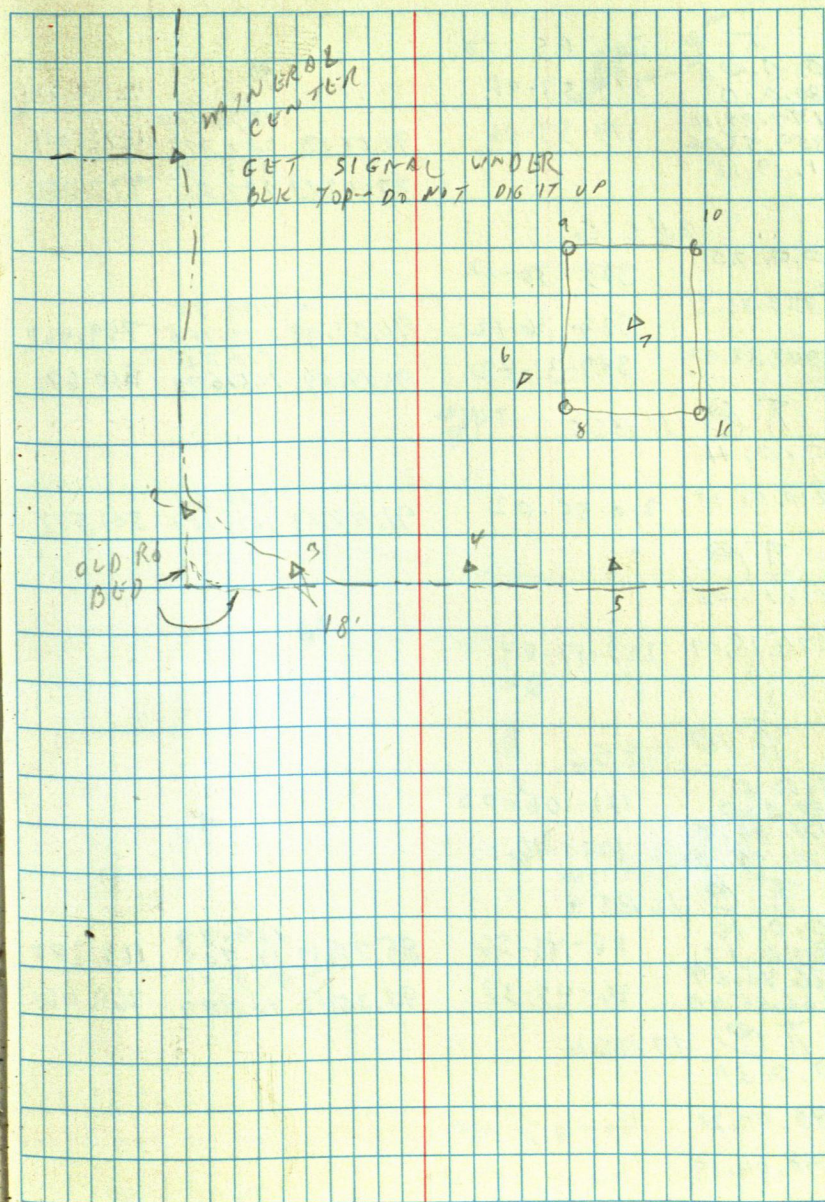
A @ 3 BS 2				
0-0-37	135-35-03			
180-0-05				
4 135-35-40	135-35-02			
315-35-77				

A @ 4 BS 3				
0-0-30	180-04-09	91-42-07	1216.15	
180-0-30			320.683	1215.609
180-04-39			1454.84	
5 0-4-40	180-04-09	92-56	443.437	1452.93

A @ 5 BS 4				
0-0-50	88-52-43			
180-0-48				
6 88-53-33	88-52-37			
268-53-28				

A @ 6 BS 5				
0-0-51	217-01-29	97-5-32	344.77	
180-0-59			105.086	342.111
217-01-20			146.74	
7 37-2-20	217-01-41	86-39-20	160.15	159.838
8 312-21-30	312-20-39		19.79	

A @ 7 BS 6				
0-0-15	6	96-28-10		
9 65-49-03				
149-32-05	65-48-44	96-28-10	177.33	176.204
10 149-32-05	149-31-50	90-44-07	113.35	113.339
11 264-57-20	264-57-08	89-51-20	122.92	122.92





0.0.0.5	2 05 10		
180.0.0	179-53-06		
179.53.11	179-53-06	91.17.13	1272.94
1359.53.06			287.993
1.19.15		271.07.13	977.25
			297.861
			977.051

2BS 4

0.0.20	323-36-12		
323.36.32	323-36-12	91.31.08	799.75
14349.32.02	349-31-42	91.19.59	243.765
			510.82
			155.673
			510.671

70

11BS2

0.0.11			
210.55.13	210-55-02	91.42.51	501.81
			152.951
			501.582

70

0.1.05

225.18.09 225-17-04

70 4BS6

0.0.0	121-06-00
180.0.0	
121.06.0	121-06-00
16201.06.0	

70

16BS4

0.0.16	86-45-38	85.28.12	169.79	169.287
180.0.17			57.769	
1786.45.44	86-45-23	93.35.54	160.37	160.067
266.45.40			48.889	

70

17BS16

0.0.31

90.04.20 90-03-49

190.04.19 190-03-48

77

77PT

60

40

160

418

417

Apr 175.00

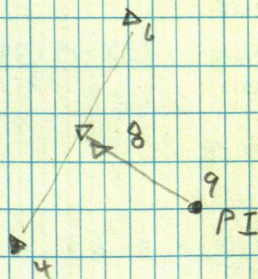


$\pi$	0	1	BS	6		
0, 0, 17					1234.76	
180-0-6				91-25-42	376.354	1239.644
359-30-19					859.25	
179-30-22				92-14-18	261.896	858.963

$\pi$	0	4	BS	6		
0, 0, 13						
180-0-14				203-17-01		
203-17-14					627.17	
2 23, 17-16				203-17-02	92.04.12	196.151
						626.749

$\pi$	0	5	BS	4		
0-0-23					136.48	
180-0-37				280-07-10	71.09.26	41.60
1 280-07-39					91.65	136.453
9 100-07-30				280-07-0	101-43-59	27.937
						89.739

2  
PC





STEVEN BAILEY

1-12-140-31

TC 1 BS 2

181.07.54

(3) 02.15.48 181-07-54

TC 3 BS 2

(4) 16.22.21

2 352.44.42 176-22-21

TC 4 BS 3

(5) 139.20.24 139-20-24

278.40.48

TC 5 BS 4

138.19.36

(6) 276.39.18 138-19-39

TC 6 BS 5

200.44.06

(7)

TC 5 BS 6

0-0-10

0-0

0-10-51

0-10-41

8

359-42-55

9

359-42-45

90-02-50

90-42-55

775.34

236.322

425.29

129.63

775.333

425.256

TC 3 BS 4

4A 0-0-0

4B

274-15-35

92.54.42

575.81

575.067

31.56

575.81  $\frac{7}{2}$ 

50

B. CRO

ROGER

64

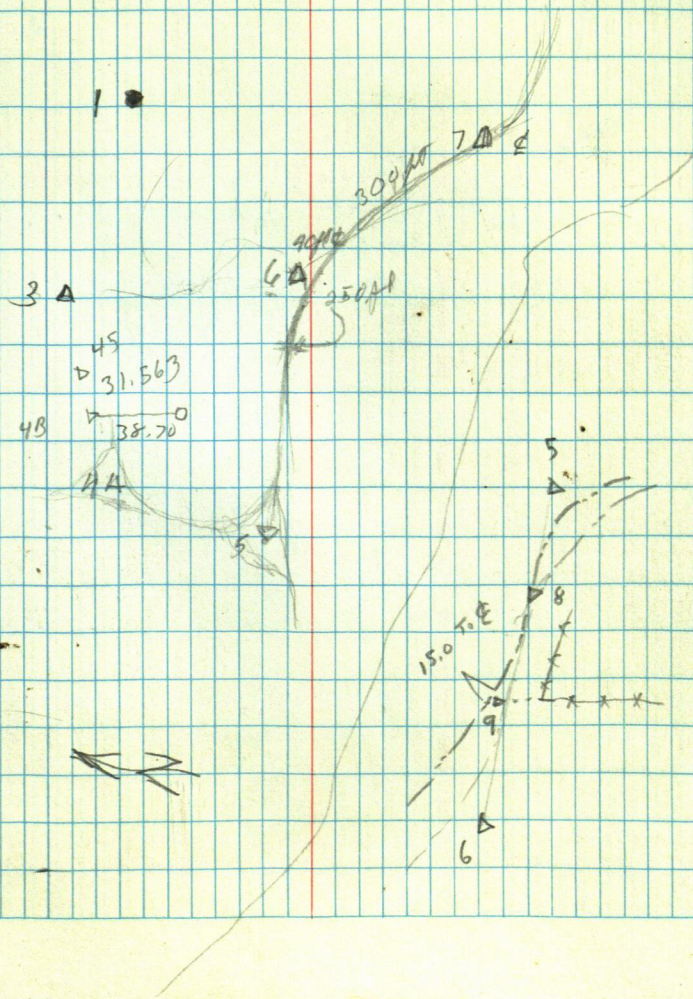
11-8-93

50  
11.30  
38.70

977.124

575.067

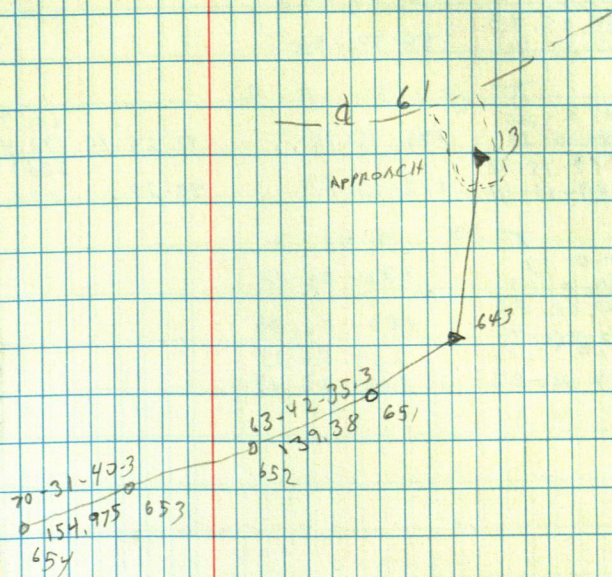
402.057





DIA GP

65





# ARABLEY CEMETERY

① 2 BS 1

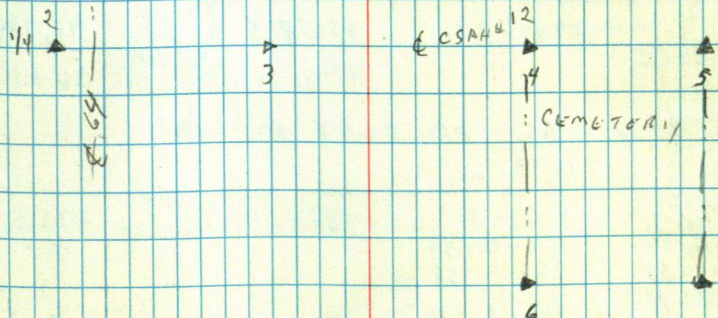
0-0-23 88-23-07  
180-0-34  
88-23-30  
3 264-23-40 88-23-06

② 3 B 2

0-0-20 631.33  
180-0-19 179-15-18 91-26-12 192.423 631.119  
179-15-38 2869.91  
4 359-15-41 179-15-22 90-29-11 874.75 2869.796

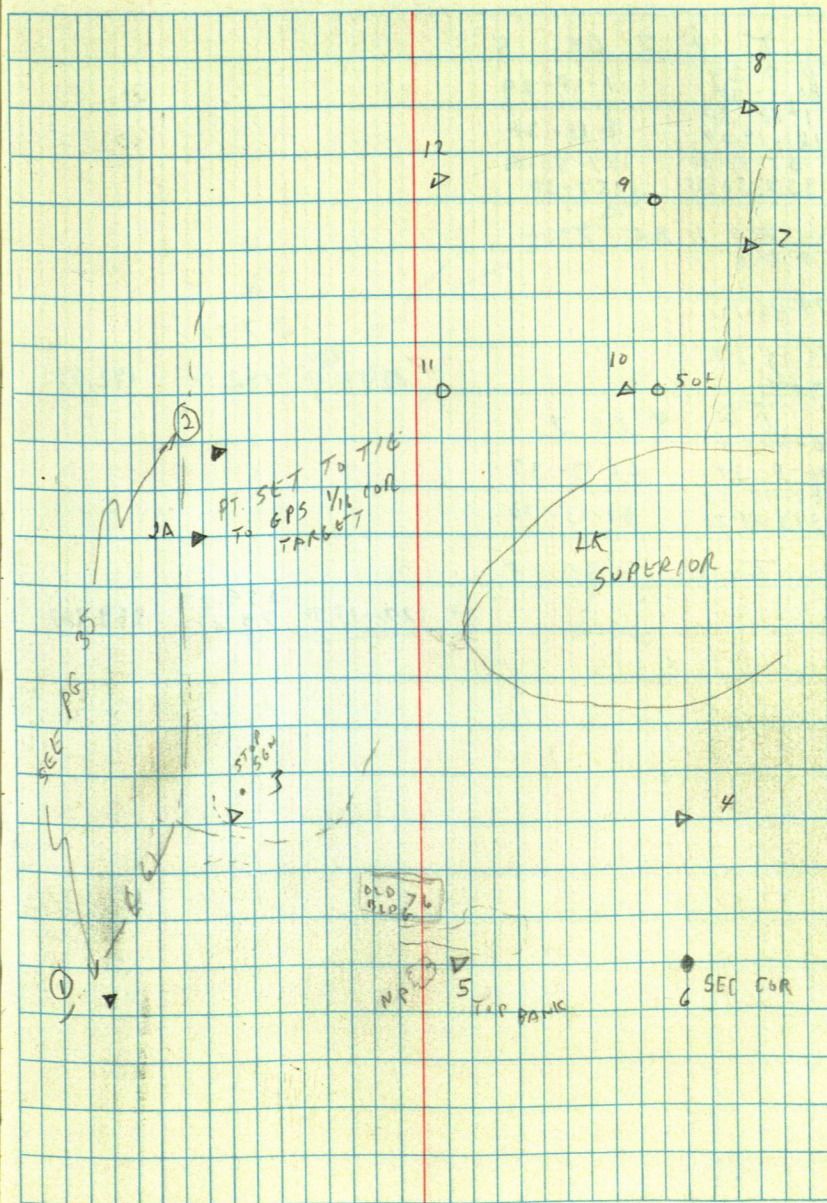
③ 4 BS 3

0-0-17 180-06-17  
180-0-10  
180-06-30  
5 0-06-40 180-06-30  
269-26-26 269-26-13  
6 89-26-22 269-26-12





T @ 1 BS 2A				
0-0-04	3-23-59	90-17-40	3172.24	3172.191
180-0			966.903	
3-24-03			1034.78	
3 183-24-04	3-24-04	91-24-04	315.364	1034.397
T @ 3 BS 1				
0-0-35	283-50-59			
180-0-0				
283-51-34				
4 103-51-03	283-51-03			
314-13-48	314-13-13			
5 134-13-18	314-13-18			
T @ 4 BS 3				
0-0-16	230-58-11	89-19-4	760.96	760.903
179-59-55			231.941	
230-58-27			87.10	
6 50-58-30	230-58-35	91-22-30	26.547	87.07
T @ 5 BS 3				
0-0-31	57-30-24	90-08-04	381.28	381.279
180-0-23			116.215	
57-30-55			10787.61	
7 232-30-50	57-30-27	89-5-5	3288.072	10786.20
T @ 7 BS 8				
0-0-21	286-27-11	85-59-5	99.23	98.989
286-27-32			30.247	
9		87-31-24	56.68	56.63
T @ 7 BS AM. FLAG ON LODGE				
0-0-10	1-39-26			
180-0				
1 39-36	1-39-31	96-0-40	223.75	222.518
10 181-39-31			68.199	
158-11-09	158-10-59			
8 338-10-58	158-10-58			
165-02-40	165-02-30			
T @ 8 BS 7				
0-0-30				
12 68-7-47	68-07-17			





$\pi @ 7 BS 5$   
 0-0-29  
 185-0-35 1-18-29  
 1-18-58  
 10 181-19-09 1-18-34  
 157-50-30 157-50-01  
 8 337-50-35 157-50

$\pi @ 11 BS 7$   
 0-0-0

74-40-12

7.22

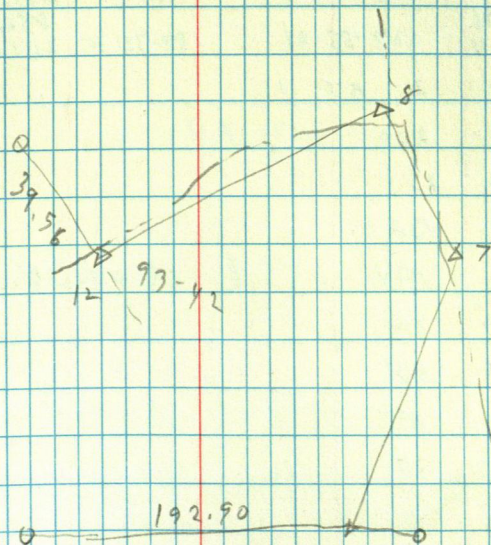
73-43-23  
 2180

85-10-10 192.90 192.21

$\pi @ 8 BS 7$   
 0-0-55  
 180-0-58 68-13-33  
 68-14-30  
 12 248-14-28 68-13-30

$\pi @ 12 BS 8$

271-13-30 259.23  
 79.012 259.167



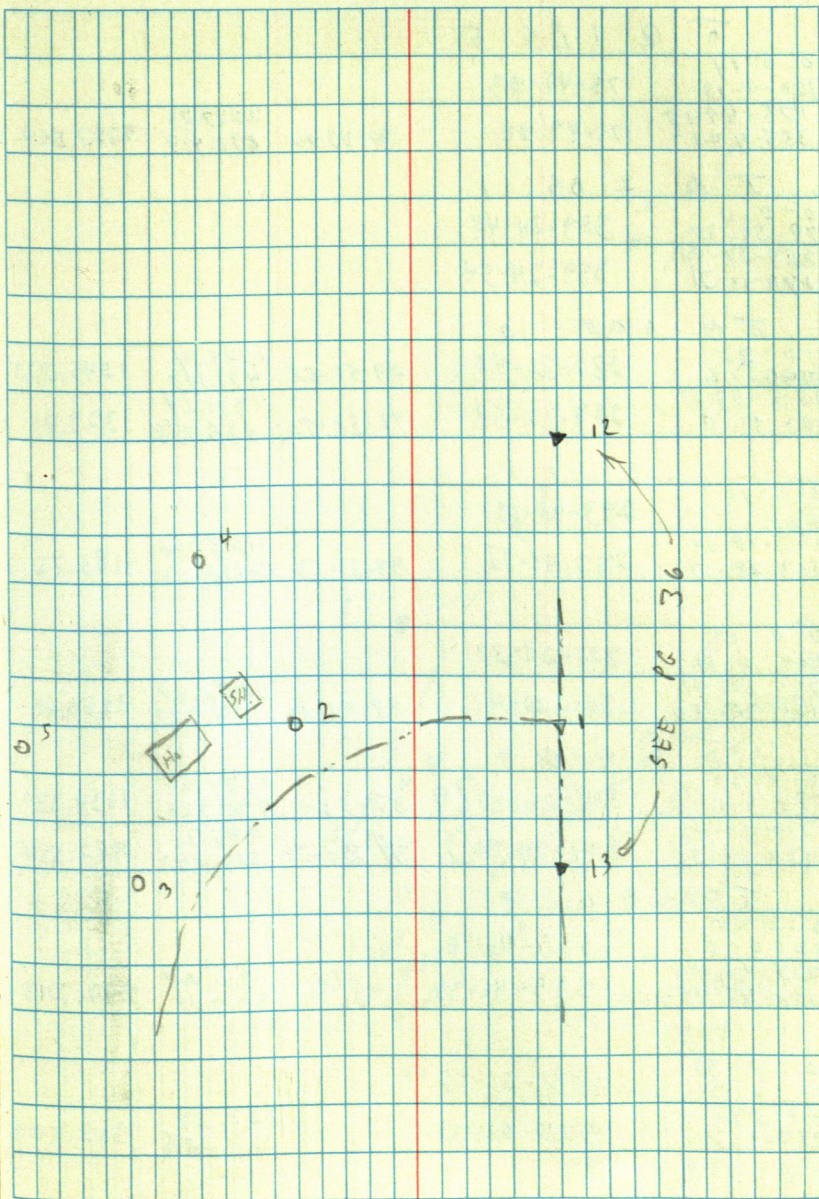


T @ 1 BS 13				
0-0-19	269.55-07	88-07	804.14	803.701
180-0-16			245.101	
269-55-26			856.31	
2 89-55-17	269.55-01	87-32-30	261.002	855.516

T @ 2 BS 1				
0-0	200	PQ		
8-46-30	175			
3-11-50	138			
9-37-25	104	e CURVE		
25-19-18	72			
56-1-46	58			
91-13	69			
108-24-50	97			
115-42	134			
118-36-50	173	PT		
120-48-20	240	PC		
177-58	100	COR 110		
192-53	71			
204-0	90			

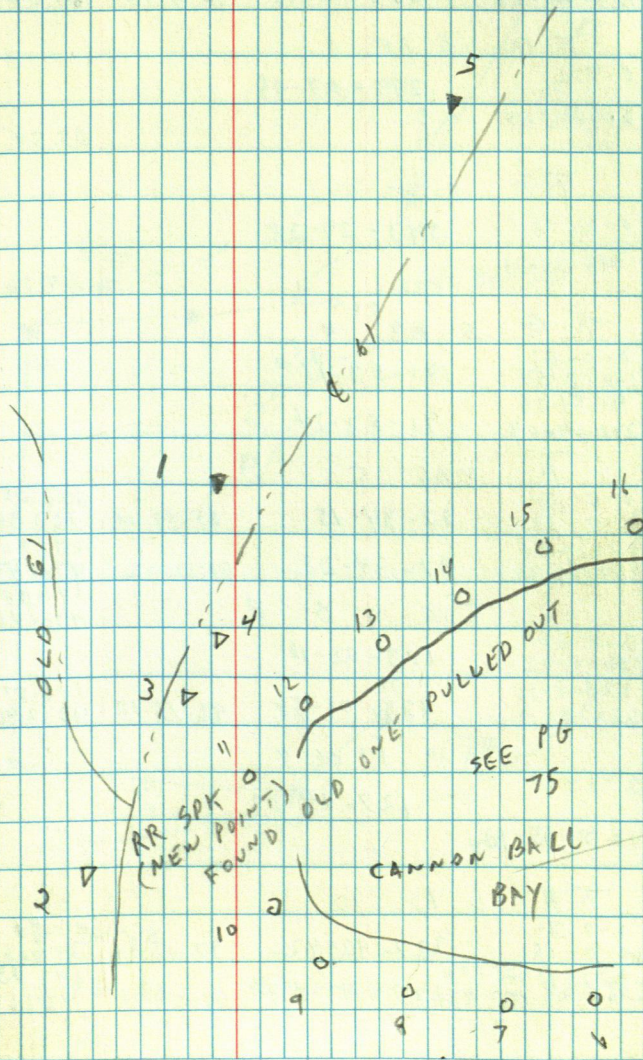
T @ 2 BS 1				
0-6-43	136-24-01			
180-0-41				
136-24-48	136-24-09	88-43-50	200.29	200.233
3 316-24-50			61.044	
0-0-51	255-59-54	85-16-50	199.82	199.201
4 256-0-45			60.923	

T @ 3 BS 2				
0-1-04	283-13-53			
180-1-08				
283-14-57	283-13-52	86-30-51	202.87	202.494
5 103-15			61.835	





0-0-14 180-0-13 175-49-17 2 355-49-13	Q 1 BS 5 175-49-03 175-49-00	90-43-10	2727.75 831.419	2727.524
0-0-0 179-59-27 359-24-48 3 379-24-21	T Q 2 BS 1 359-24-48 359-24-54			
0-0-25 180-0-06 287-33-13 6 107-33-0	T Q 3 BS 2 287-32-48 287-32-54	89-55-55 92-58-52	1545.74 471.145 1321.24 405.748	1545.738 1329.41
0-0-11 180- 293-48-24 7 113-48-17	293-48-13 293-48-17	93-21-13	1185.74 261.423	1183.72
0-0-19 180-0-9 301-28-56 8 121-28-50	301-28-37 301-28-41	92-42-10	1052.69 320.855	1050.48
0-0-25 180-0-25 314-20-48 9 124-20-55	T Q 4 BS 2 314-20-23 304-20-30	89-50- 94-20-50	1634.59 498.226 985.31 300.343	1634.581 982.528
0-0-5 180-0-5 335-46-40 10 155-46-43	T Q 9 BS 4 335-46-35 335-46-38		190.24 57.988	190.243
00-0-35 180-0-35 358-2-30 178-02-30	358-01-55 338-01-55		362.54 110.506	362.544

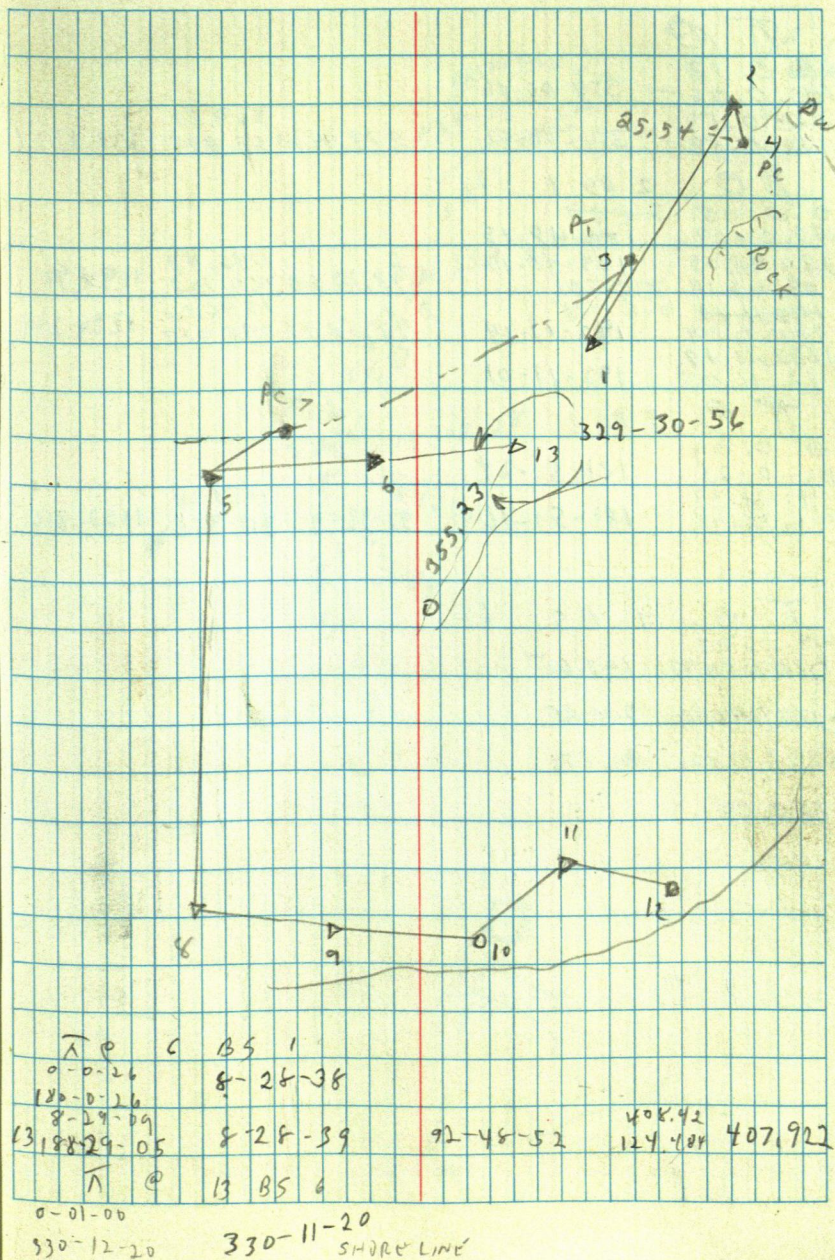




	$\overline{A} @$	1 BS	2		
0-0-11					
180-0-12		353-48-21			
353-48-32			134.64		
3 123-48-28		353-48-16	90-4-13	41.04	134.642
	$\overline{A} @$	2 BS	1		
0-0-6		299-03-05			
4 299-03-05				25.54	
	$\overline{A} @$	5 BS	6		
0-0-10		343-29-28			
7 343-29-38				69.76	
	$\overline{A} @$	5 BS	6		
0-0-52					
180-0-50		91-53-17			
91-54-09					
8 271-54-04		91-53-24			
	$\overline{A}$	8 BS	5		
0-0-30				526.08	
120-0-22		87-34-15	85-52-22	160.35	524.711
87-34-45				141.90	
9 267-34-30		87-34-08	91-51-12	43.253	141.804
				141.88	
				43.246	
	$\overline{A} @$	9 BS	8		
0-0-06					
180-0-02		173-02-10			
173-2-16				188.77	
10 353-02-0		173-01-58	96-16-10	42.296	137.929
	$\overline{A} @$	10 BS	9		
0-1-10		127-14-02			
11 127-15-12					
	$\overline{A} @$	11 BS	10		
0-0-30				94.98	
180-0-15		227-42-42	97-12-50	28.926	94.154
227-43-12				143.85	
12 47-42-54		227-42-43	96-24-30	43.663	142.355

302.42, 92, 177  
348.58

71





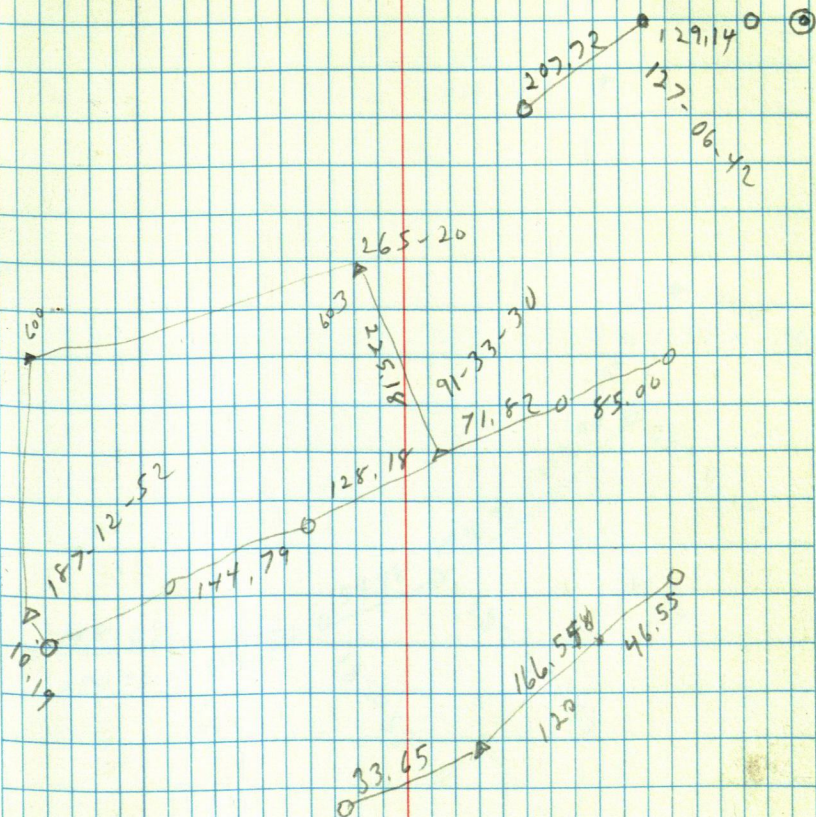




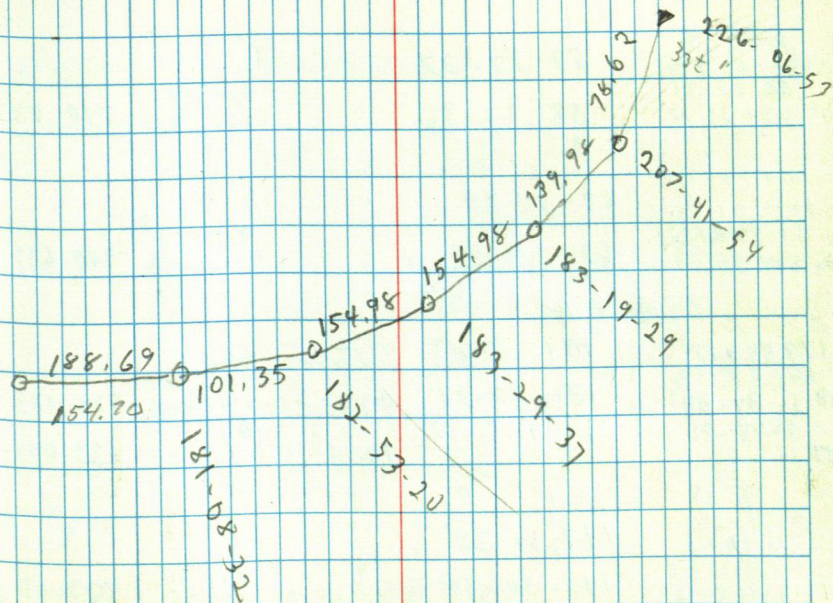
265,20,0

$$\begin{array}{r} 71 \\ 85 \\ \hline 156 \end{array}$$

73

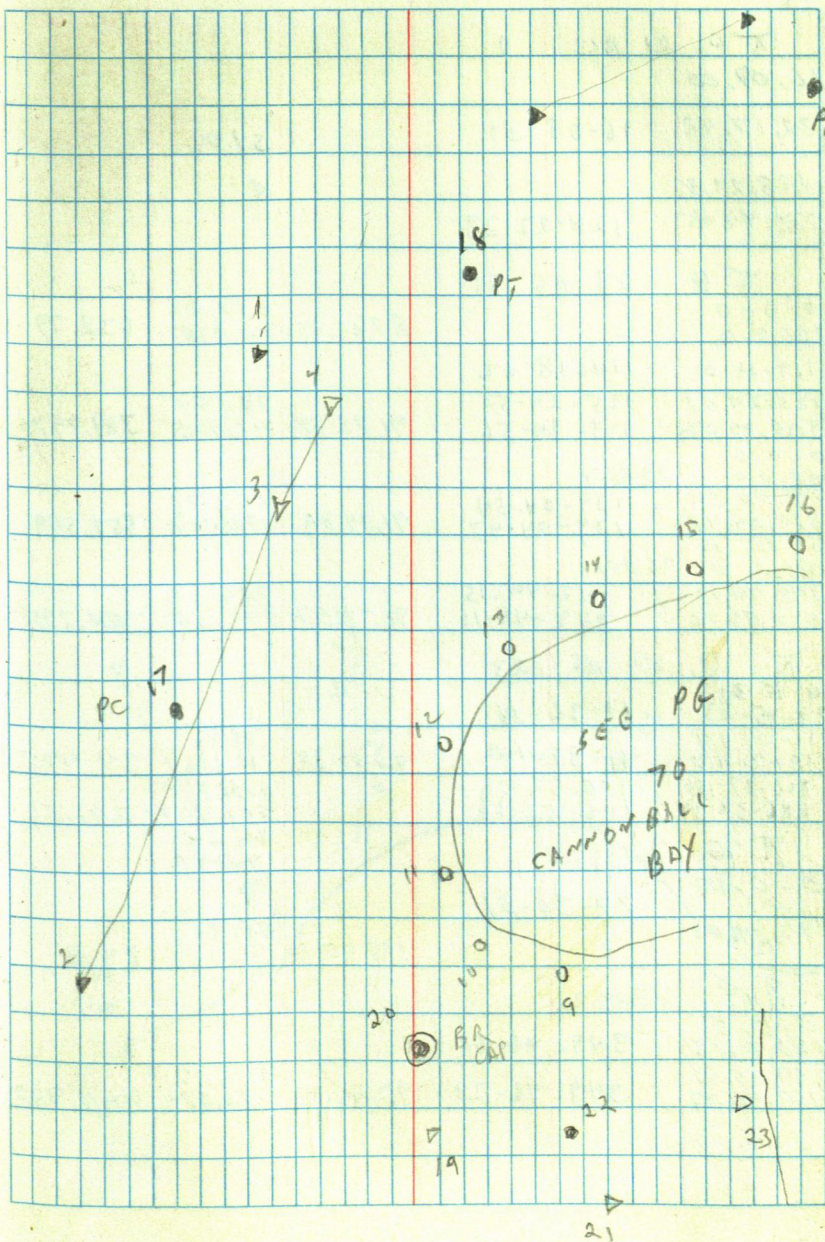








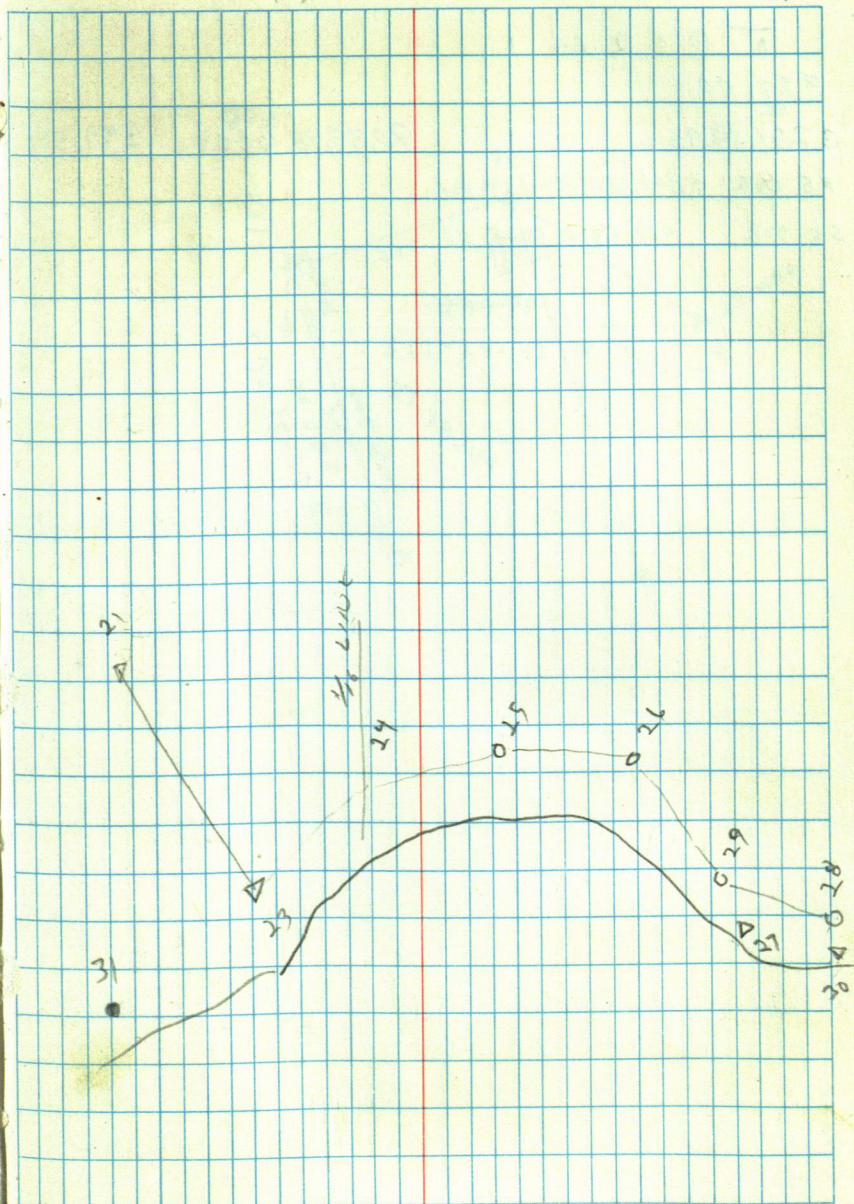
K @ 9 BS 1				
0-0-41				
180-0-39	15-18-0			
15-18-41			512.77	
12-195-18-35	15-17-56		156.307	512.792
0-0-12				
180-0-0	32-11-26			
32-11-38			623.88	
13-212-11-27	32-11-27		192.136	623.820
0-0-09				
180-0-05	46-00-07			
46-0-16			740.89	
14-226-0-88	46-0-13		225.826	740.891
0-0-35				
180-0-35	58-22-37			
58-22-21			840.87	
15-238-23-12	58-22-36		256.283	840.843
0-0-41				
181-0-45	67-54-39			
67-55-20			969.69	
16-247-55-22	67-54-37		295.533	969.639
0-0-0	K @ 4 BS 2			
179-59-17	181-37-33	91.17.05	221	
181-37-33			726.24	
181-37-08	181-37-51	89.25.01	221.348	726.183
1-04-51	1-04-51		634.04	
17		93.14-38	193.269	633.044
0-0-02	K @ 2 BS 1			
179-59-46	147-50-38			
147-50-40			835.19	
19-327-50-25	147-50-39	93.15.40	254.562	833.83
148-08-41	148-03-39		1243.08	
21-328-03-37	148-03-51	92.38.45	378.897	1241.76
51.52.30	K @ 19 BS 2			
103.44.48	51-52-24			





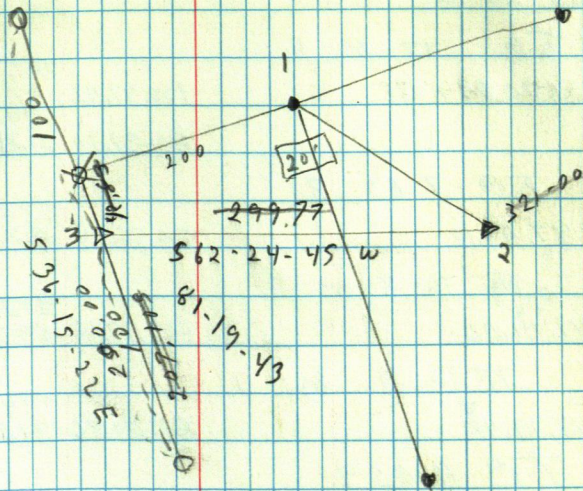
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	16.09.00		
22	32.17.42 16-08-51		58.00
23	128.22.31		5
	256.44.45 128-22-23		
	TC 23 B5 21		
	0-0-0		
	180.0.0	87.06.52	632.87 192.898 632.79
24	114-18-02 114-18-02		
	125.24.57 125-24-57		
25	305.24.56 125-24-56	91.33.58	381.94 116.416 381.797
	0.0.0		
	180.0.0 23 B5 21		
	139.04.54 139-04-54		
26	319.04.47 139-04-47	91.34.09	557.76 170.006 557.549
	0.0.0		
	180.0.0 23 B5 21		
	142.44.15 142-44-15		
27	322.44.16 142-44-16	94.33.57	784.62 239.155 784.328
	TC 27 B5 23		
35	45-30 18-36-14		
	179.45-33		
	11-21-44		
29	191-21-47 11-36-14	98.07.24	34.82 10.616 34.475
	106-37-50 106-52-20	2	
30	286-37-39 106-52-06		614.21 M 201.50 Ft 201.50
	TC 30 B5 27		
	0.0.12		15.55 4.740
	77-30-51		
28	77.31.03	114.40.10	15.55 4.740 14.13
	TC 27 B5 23		
	0.0.0		
	180.0.13 349-46-55		
513	49.46.53 349-46-21	90.44.47	941.02 286.824 940.938
	164.46.39		

76





SE COR	350.55.12	128.00
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TC 6 BS 3

253-20-24

TC 17 BS 6

253.20.24 10

100.47.42 141.45  
43.118 138.953  
84.39.30 104.06  
31.707 103.606

18

TC 7 BS 3

247.49.12

76.35.54 269.09  
82.038 268.647

TC 8 BS 3

241.41.06

80.17.18 212.77  
64.709 204.488

TC 9 BS 11

247.19.48

85.09.36 234.07  
71.345 233.24

TC 11 BS 9

138.58.12

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68.056 222.961

TC 12 BS 9

158.02.16

86.16.29 225.04  
68.591 224.56

TC 10 BS 9

138.56.54

86.49.00 238.66  
72.745 238.131

TC 16 BS 9

108.50.42

85.10.42 249.73  
76.117 248.844

TC 15 BS 9

122.51.24

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73.823 241.661

TC 14 BS 9

138.31.18

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78.106 255.266

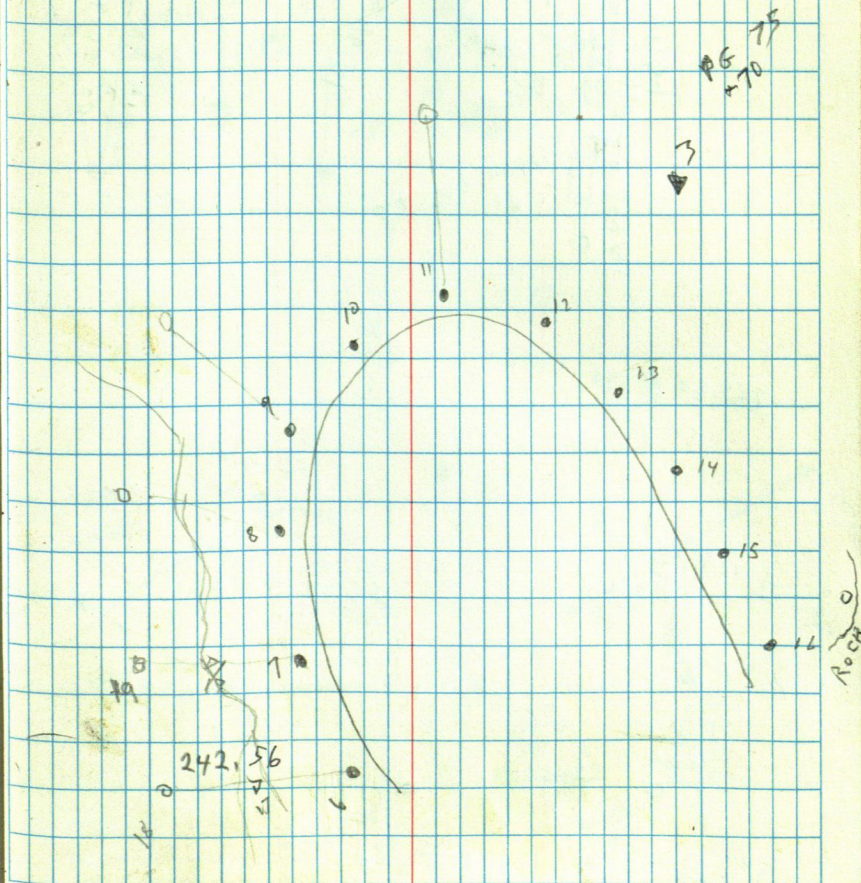
TC 13 BS 9

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85.22.18 228.16  
69.546 227.446

232.31

78









258.05.12

115.24

112.52

2,75

214 09

395 8'4  
374'46  

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21,38

95 84  
392.22  

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3.62

90.09.48

214.09



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 348.23 \\
 355.23 \\
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 348.58 \\
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 6.45
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106.231

$$\begin{array}{r}
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 176.87 \\
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 14.82
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 83 \\
 96-20 \\
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 179
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 75
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 86 \\
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 536
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94, 43, 20

7.83

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 1-20- \\
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 275-15 \\
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 1-20-00
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 4.33
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93, 41, 27, 63-13

83-13

174-45

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 15.19
 \end{array}$$

$$\begin{array}{r}
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 68
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