

314



LIETZ

SINCE 1882

TRANSIT FIELD BOOK

No. 8152-00

Property of WALTER CURD

Address HACKENSACK N.J. 56452

Telephone 218-675-6697

This Book is manufactured of a High Grade 50% Rag Ledger Paper having a Water Resistant Surface, and is sewed with Nylon Water-proof Thread.

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Dyoke
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- 11 ALICE WILLIAMS
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- 14 R. KEMNITZ LOT 12 BLK 2 LAKE SIAE ADD
MACK.
- 15 USFS REMER COA TIES
- 16 JIM GARRARD E. WESTPHAL NW-NW-4-139-30
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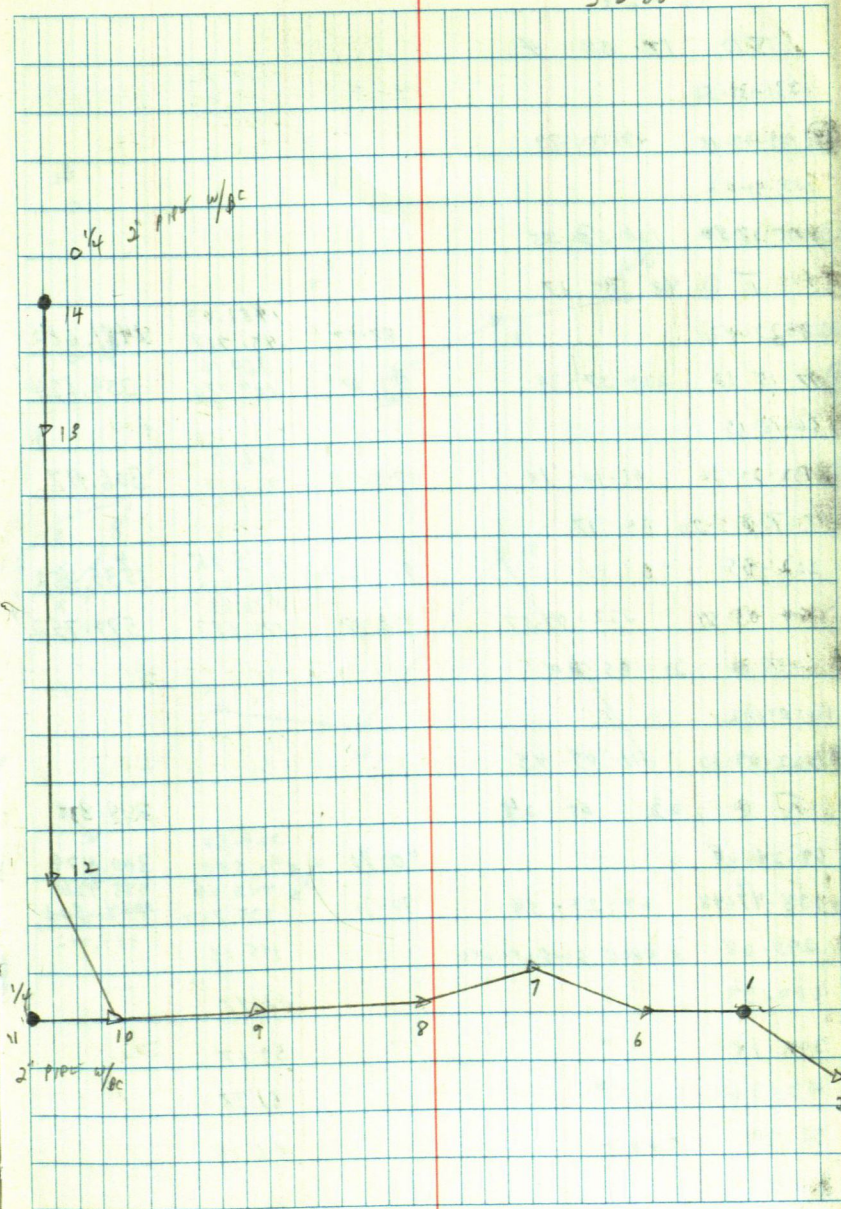
T @ 13 05 12			
180-4348	91-33	2728.23 709.682	2327.48
⑩ 1-26-48 180-43-54	93-50	146.38 44.616	146.051
T @ 12 05 13			
144-38-36			
⑩ 289-17 144-38-32			
T @ 10 05 9	88-05-54	847.69 256.44	847.424
181-30-72			
⑪ 3-20-06 181-30-03	97-05	145.83 44.448	144.714
235-33-50			
⑫ 111-07-54 235-33-57	93-40	247.24 75.361	246.736
T @ 9 05 10			
181-38-06			
181-45-42			
⑧ 3-11-54 181-35-57	3-31-10	181-45-35	
T @ 8 05 9			
172-32-35			
90-28			
⑦ 245-04-57 172-32-28	91-25	583.40 177.827 262.51 80.012	583.389 262.427
T @ 7 05 8			
176-22-40			
352-44-38 176-22-33			
45-03			
T @ 6 05 7			
188-16-06			
16-32-00 188-16-00			
89-09			
⑥	92-33	502.61 153.194 308.33 93.98	502.55 308.025
T @ 1 05 2			
148-06-06 148-06-00			
⑤ 296-12-00			

10° CLR + COLS NW WIND

E. OWA
S. MICK

2

3-6-86



3

T @ 24 BS 25			
179-26-31	89-91	682.72 208.091	682.689
23 254-52-38 179-26-19			
K 246-15-36	N EDGE SWP	78.06	
G 225-14-25	"	95.91	
H 172-01-18	"	84.23	
I 155-20-12	"	145.75	

T @ 25 BS 24			
177-04-30			
23 354-08-12 177-04-21			
T @ 26 BS 27			
104-37-12	90-20	535.66 167.265 320.25	535.642
25 209-14-09	104-37-05	89-28	97.613
T @ 27 BS 26			
162-12-30			
23 324-24-52 162-12-26			

T @ 28 BS 27			
167-31-43	89-03	536.52 163.536	536.452
29 335-03-15	167-31-08	88-49	469.83 143.203
T @ 29 BS 28			
278-30-48			

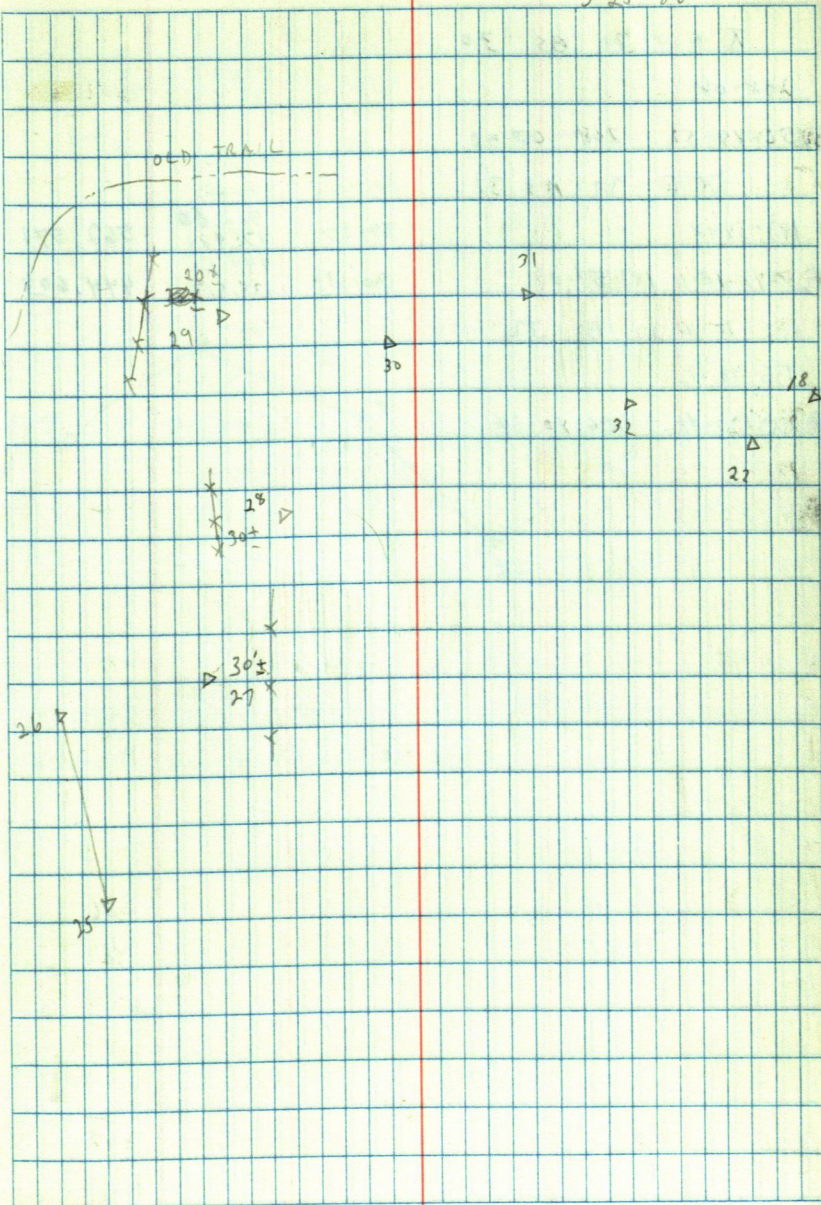
30 192-01-18 278-30-39			
T @ 30 BS 31			
204-52			
29 49-44 204-52			
	92-02	847.055 847.60 258.344	
	91-40	581.09 116.158	
		380.93	

30° CLO/

E. BURD
S. MICK

4

3-25-86



$\pi @ 31 \text{ BS } 30$

208-08

(32) 56-15-52 208-07-56

$\pi @ 32 \text{ BS } 31$

183-54-18

89-27

562.60

171.480

562.571

(32) 7-48-18 183-54-09

90-34

444.60

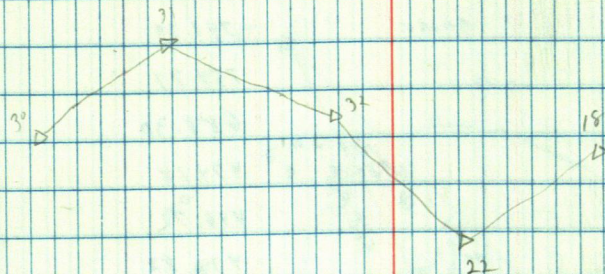
135.512

444.603

$\pi @ 22 \text{ BS } 32$

136-40-42

(18) 273-20-48 136-40-24



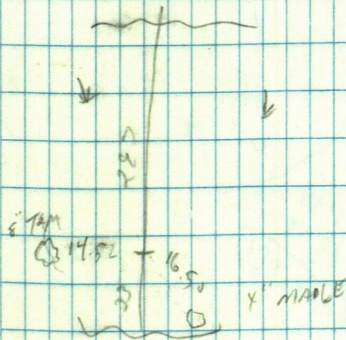
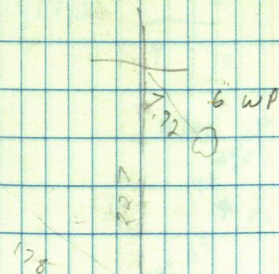
Orig BT's For cor in sec 10

NW Cor

8" BIRCH	S 42 W 8	5.28
6" WP	S 44 E 12	7.92
10" BIRCH	N 72 E 11	7.26
10" BIRCH	N 2 W 28	18.48

W $\frac{1}{4}$

8" TAM	N 89 W 22	14.52
4" MAPLE	S 24 E 25	16.50



$\pi @ 29 \text{ BS } 30$
 $0-00-00$
 $298-0-0$
 $180-00-00$
 $41 \ 117-59-35 \quad 297-59-48$
 477
 $\pi @ 41 \text{ BS } 29$
 $0-10-0$
 $180-10-15$
 $185-38-35$
 $425-32-35 \quad 185-28-28$

$\pi @ 23 \text{ BS } 21$
 $0-18-36$
 $180-17-10$
 $4 \ 234-25-46 \quad 234-07-03$
 $54-26$

$75^\circ \text{ CCR} + \text{windy}$
 1986

E. CUND
 TIM

8

5-21-86

1142
 $4 \ 3$
 $9 \ 10$
 $R26$

11395
 41
 42
 86.09
 141.55
 29
 OLD FENCE
 $N44W$
 7.72
 OLD BURNT PINE STUMP
 WITH OLD AXE MARKS ON
 INSIDE PART OF STUMP FACING NW

30

$140.92 @$
 139.854
 22.03
 23

2.33

595. #2

593,53

667

9

$$\begin{array}{r} 18-20-43 \\ 62-33-19 \\ 80-54-02 \\ 99-05-58 \\ 795960 \end{array}$$

566

233
280

513

616.23

613.00

566

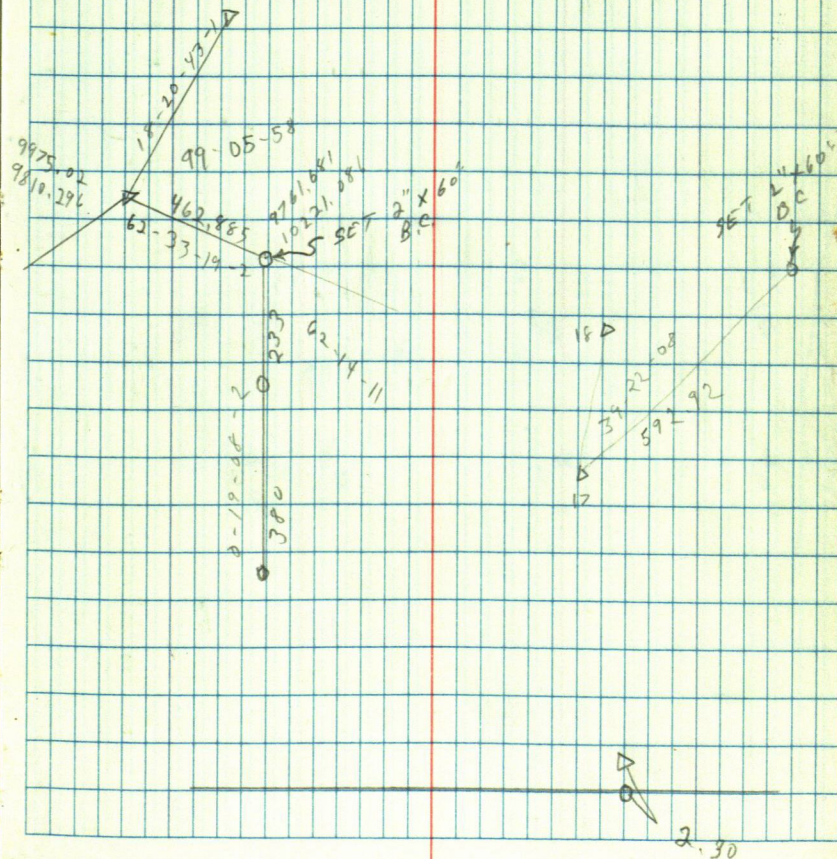
4	2
---	---

3.23

59.

469.42

1 2 3



89-35-18

318.93

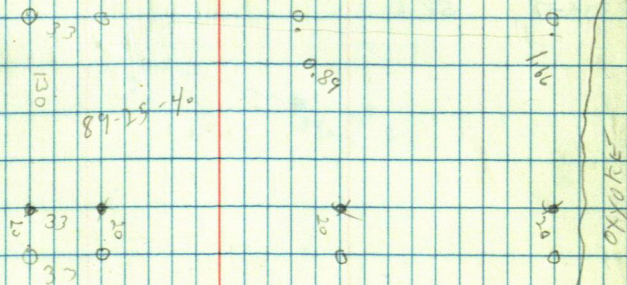
593.55

K. C. R. D.

T/M

5-26-86

(0



ALICE WILLIAMS

π @ 2 BS 1

25.35-21

159-39-18

319-18-36 159-39-18

π @ 4 BS 2

80-00-44

89-34

301.22

301.211

91.612

188.33

57.402

188.252

5 160-17-24 80-08-42

91-38

π @ 5 BS 4

1365-00

6.1

2316-45

10.0

3321-28

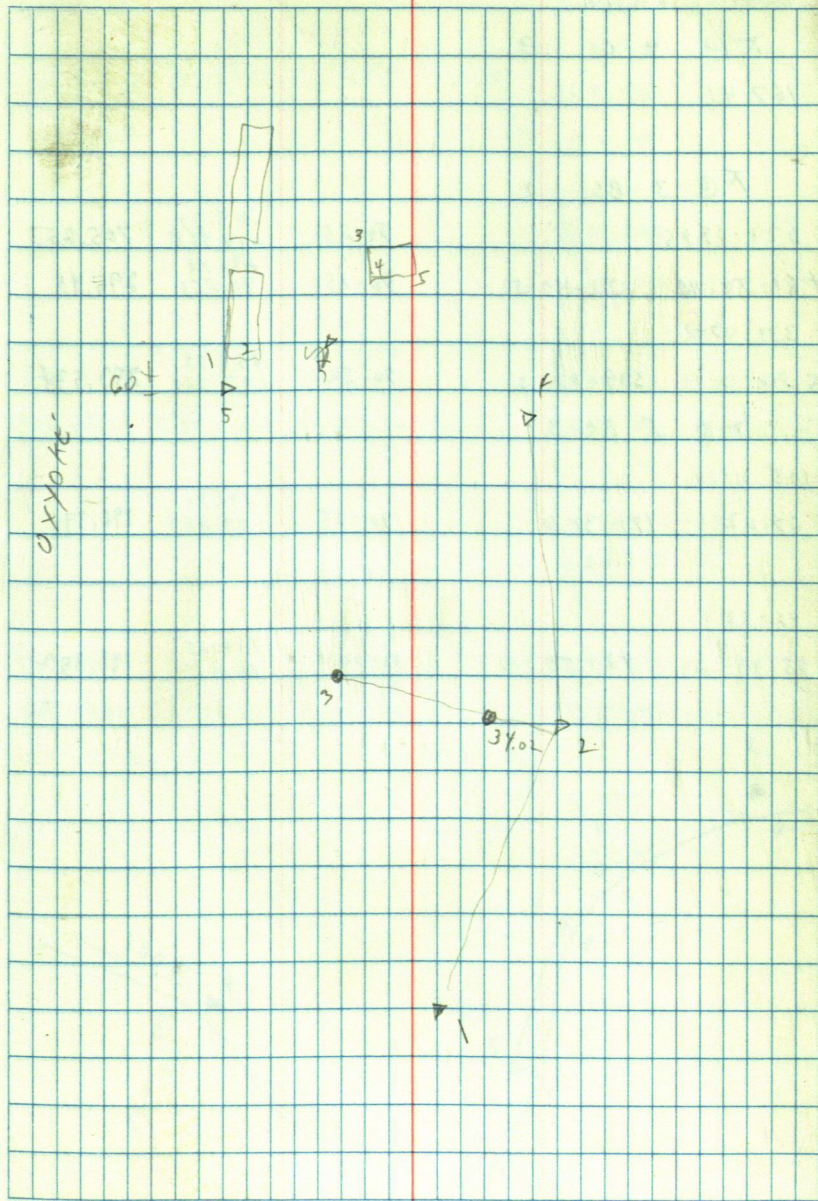
49.0

4330-05

45.4

5335-17

58.6



CHARLY MAYER

К @ 4 05 3

167-41

T	@	3	BS	2
---	---	---	----	---

222-59-K5

90-25

705.27

214,968

705,253

485-59-42

222-59-51

90-15

295.45

90.058

295.45

339-07-20

5 318.14-42

339-07-21

90-32

357.55

107.76

353,534

٥ ٦ ٣

193-31-24

6 27.02.20

193. 31.10

90-25

196.40

59, 86

196.395

42-58

85-49-20

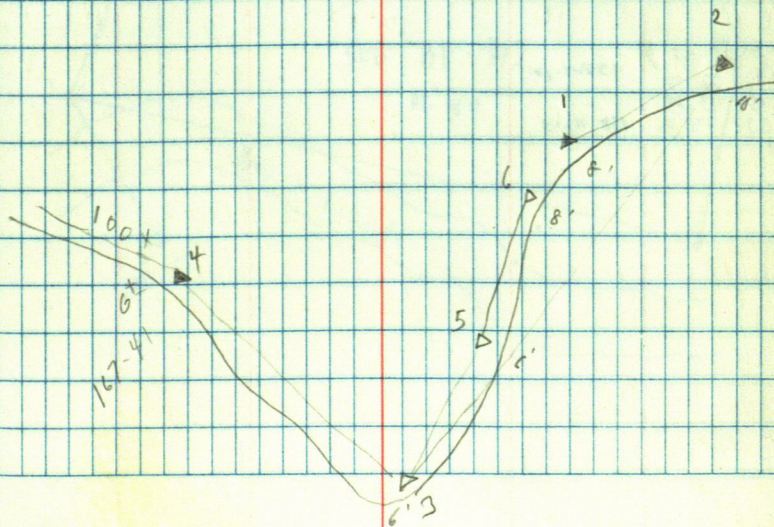
42-58-10

90-02

198,85

60.611

198.852



USFS

19-1X3-27

$\bar{\lambda} @$ 1 BS 3				
0-01-00		209-59-05	8507.54	
180-01-14	104-24-22	90-01-20	2617.784	8587.511
104-25-22		89-25-25	1144.51	
284-25-25	104-24-11	270-34-36	346.846	1144.446
$\bar{\lambda} @$ 1 BS 8				
0-11-05				
120-11-03	255-35-48			
255-46-53				
75-46-59	255-35-56			
$\bar{\lambda} @$ 8 BS 1				
0-26-32		90-39-17	1144.55	
180-26-15	149-12-53	269-20-50	348.84	1144.472
149-39-25		89-24-30	1126.15	
229-39-12	149-12-57	270-36-00	347.250	1126.083
$\bar{\lambda} @$ 8 BS 9				
0-04-40				
180-04-35	210-47-07			
210-51-46				
30-51-41	210-47-06			
$\bar{\lambda} @$ 9 BS 8				
0-27-00		90-40-10	1126.13	
180-26-40	201-48-54	269-19-45	243.248	1126.054
202-15-54		89-52-30	1685.98	
22-15-35	201-48-55	270-07-50	517.891	1685.976
$\bar{\lambda} @$ 9 BS 8				
0-01-55				
130-02-00	158-11-10			
158-13-05				
338-13-05	158-11-05			

CLDY LT WIND

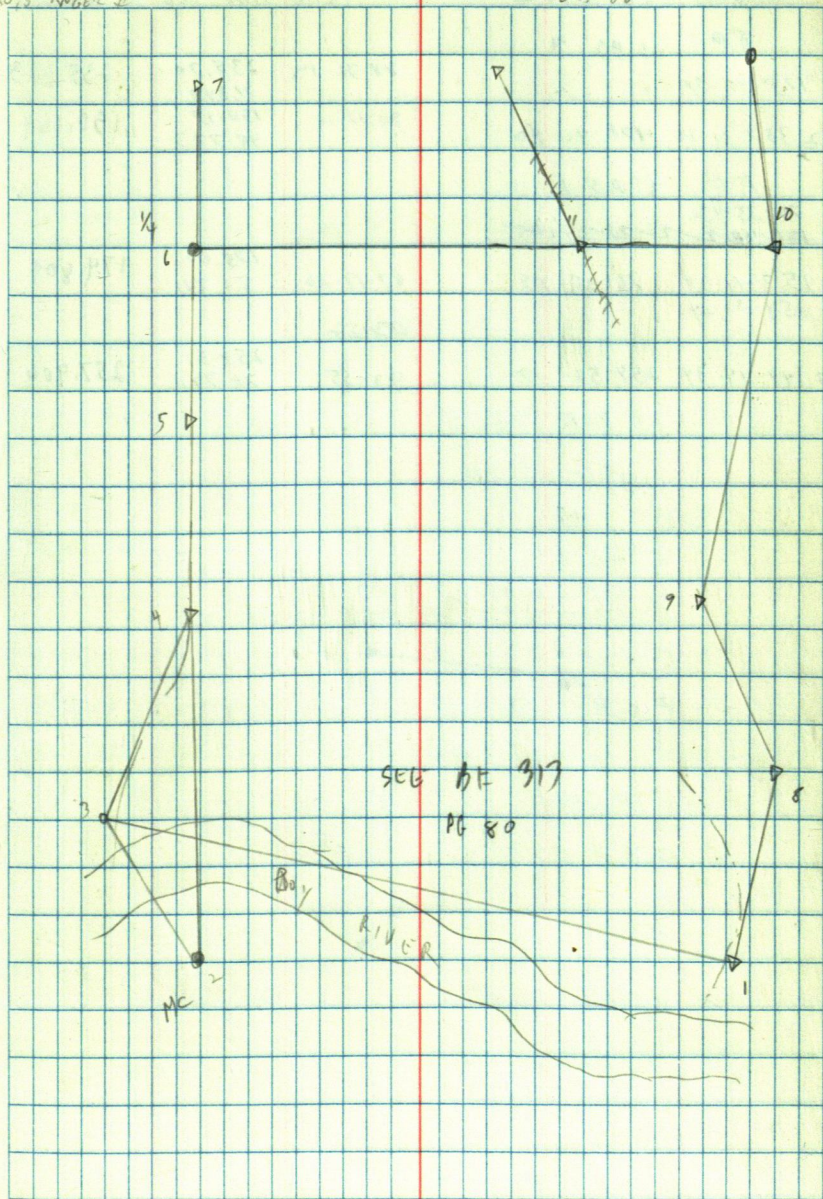
70°

E. CARD
TIM

13

TOMA DIOA
AUTO RANGER II

6-5-66



ROBERT KEMNITZ

LAKE SIDE ADD TO HOCK

TP 1 85 3

178-40-54

88-32-17

235.20

235.623

21.847

2 357-21-20 178-40-40

90-12-18

150.17

150.169

45.773

TP 3 85 1

76-35-42

~~150-40-20~~ 76-25-45

153-11-30

76-35-45

87-19-20

175.00

174.809

53.341

254-52-24

~~87-55~~

258.51

257.906

76.791

5 149-44-34 254-52-17

97-55

5

3

1

20

2

4

USFS

REMEA

142-26

BTS

• N $\frac{1}{4}$ SEC 35

4" NO N 2 W

52.06

W SIDE 1'

ABOVE GRAD

PP N 50 W

81.83

SW 2'

ABOVE GRAD

TEL BOX GUARD POST S 45 W

64.73

SE SIDE 1'

ABOVE GRAD

• E-W $\frac{1}{64}$ COR SEC 35

PP N 12 E

37.92

E SIDE 2'

UP

7" POP S 62 E

58.02

NW 1' UP

6" ASH S 50 W

60.45

SE 1' UP

• NW COR 35

6" W O N 40 W

98.26

SW 1'

6" W O N 20 E 88.94

NW 1'

~~6" MAPLE (TANK) N 52 E 78.15~~

8" POP S 62 W

127.60

S SIDE 1'

9" W O S 27 E

163.37

E 1' KITT

• PROP. COR W LINE S 1/4 OF RR

11" NP S 48 W

55.89

N 5 1' 00

10" NP S 88 W

40.72

N 5 1' 00

• PROP. COR. N OF RR

9" POP N 70 E

83.50

N SIDE 1'

9" NP N 65 W

95.36

N SIDE 1'

• W $\frac{1}{4}$ SEC 35

28" WP N 30 W

80.00

E 5 1'

14" WP N 50 E

70.65

N 1'

6" WP EAST

69.58

N 1'

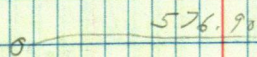
15

6-17-86

BIN GARRETT

$$\begin{array}{r} 579.74 \\ 570.90 \\ \hline 1.84 \end{array}$$

239.39



576.90



92-07-35

90-59-3

AHLEY

π @ 1 BS 2

109-19-54

③ 218-39-48 109-19-54

π @ 3 BS 4

105-28-48 89-40 1504.56 458.325 1504.474

1 210-52-20 105-28-40 90-11 358.74 358.732

π @ 4 BS 3

90-29-50

5 180-59-42 90-29-51 90-41 417.93 127.383 417.89

168-43-18

6 327-26-18 167-43-09 90-20 404.56 127.308 404.548

π @ 6 BS 4

119-14-36

7 238-29 119-14-30 90-12 191.88 58.406 191.88

190-56-54

8 21-53-48 190-56-54 90-54 394.11 120.124 394.059

π @ 8 BS 6

102-30-48

9 205-01-15 102-30-27 94-17 205.00 62.483 204.424

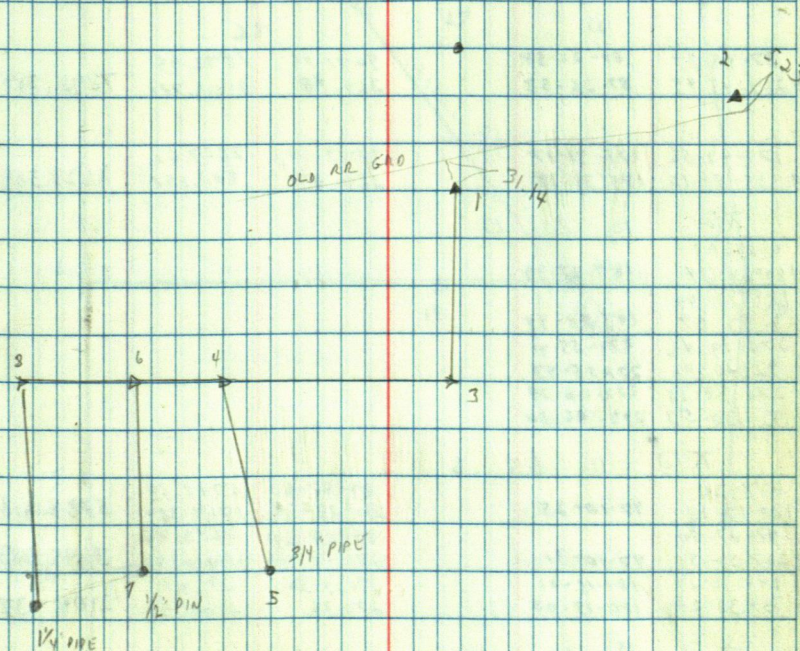
137-39 SE COR H 295.73

140-52 NW " 278.91

147-02 NW " 315.76

E. COR

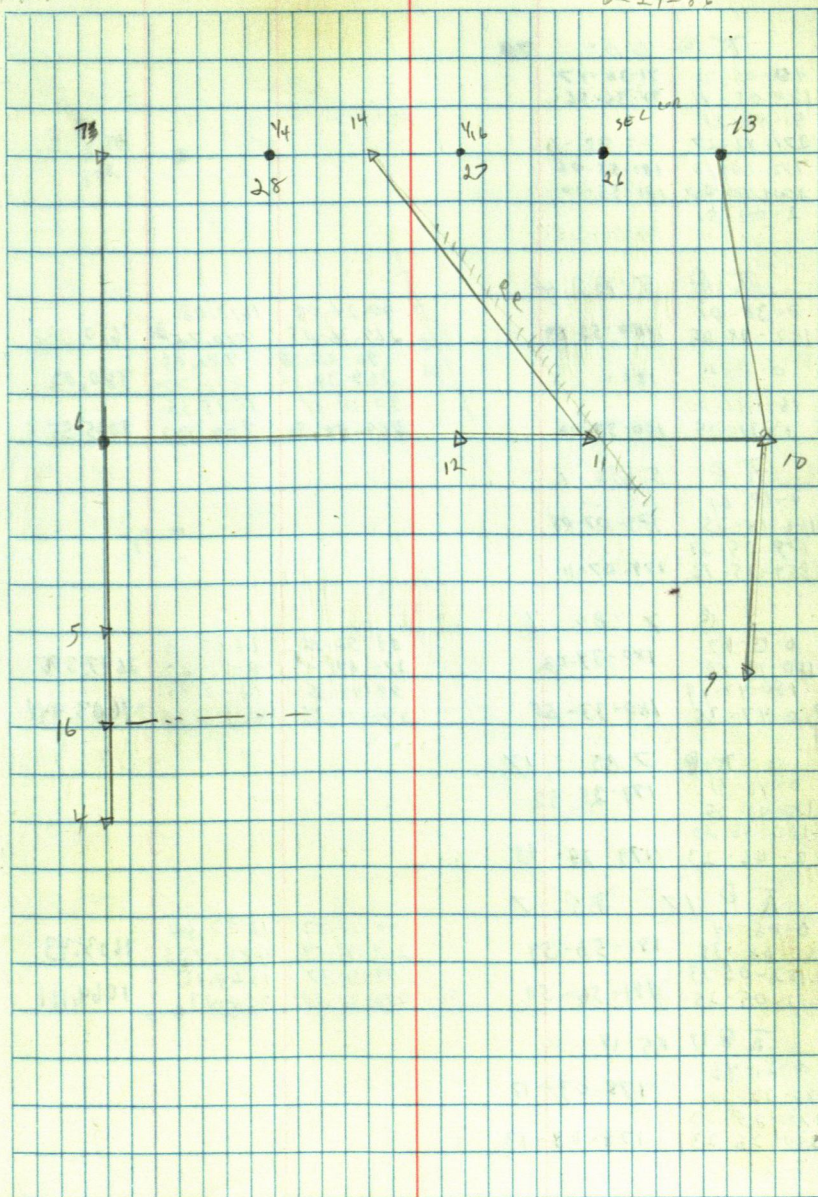
17



USFS

BOY RIVER

T @ 10 AS 9				
0-18-39		90-11-26	1685.96	
180-18-52	82-37-42	269-48-50	513.877	1685.938
87-56-21		90-38-57	2104.56	
11 267-56-35	87-37-43	269-23	641.17	2104.423
87-45-37	82-26-58	90-11-45	7892.95	
6 267-45-45	82-26-53	269-48	2409.781	7892.885
175-47-56	175-31-17	90-14-01	2627.62	
13 355-50-10	175-31-18	269-47	800.898	2627.569
T @ 10 BS 13				
0-24-05				
180-24-34	184-28-39			
184-52-44				
9 4-55-07	184-28-44			
272-19-46	271-55-41			
6 92-20-06	271-55-43			
272-30-39	272-06-34			
11 92-30-53	272-06-30			
T @ 11 BS 6				
0-17-21		89-57-50	5788.64	
180-17-20	47-10-25	270-02-20	1764.380	5788.618
47-27-51		89-57-21	3645.82	
14 227-27-51	47-10-31	270-03	1111.234	3645.783
180-32-27	180-15-01	89-24-35	641.17	
0 6-30-28	180-15-08	270-36	2104.56	2104.437
T @ 11 BS 14				
0-09-17				
180-09-25	133-04-24			
133-13-41				
10 313-17-44	133-04-19			
312-58-55	312-49-38			
6 132-58-59	312-49-34			
T @ 6 BS 12				
0-11-58		90-05-02	5788.65	
180-12-06	90-18-18	269-55-08	1764.384	5788.625
90-30-16		90-28-52	1015.52	
5 270-30-30	90-18-24	269-51-20	307.531	1015.513
268-35-12	268-23-14	90-11-10	2647.40	
7 88-35-30	268-23-24	269-48-40	806.929	2647.377

1407 75°
IENA
AUTO RNGRB. CARD
T. VOLCKE 18
6-24-86

T @ 6 B 3 72

40-05-34 71-36-47
 180-05-41 71-36-46
 91-42-21
 11 271-42-27
 182-00-40 181-55-06
 5 ~~200-00-51~~ 181-55-10
 2-00-51

T @ 5 B 5 4

0-38-01 180-52-59
 180-38-05 180-52-59
 16 0-0-0 180-
 181-31-00
 6 1-31-05 180-53-00
 90-24-05 1610.08
 269-36-05 440.754 1610.037
 90-25-48 980.05
 269-34-20 276.720 980.02
 90-01-14 1015.55
 269-58-30 309.543 1015.55

T @ 5 B 5 6

0-18-01
 180-18-05 179-07-08
 179-25-09
 4 359-25-16 179-07-11

T @ 7 B 5 6

0-13-47 180-34-02
 180-13-40
 180-47-49
 17 0-47-35 180-33-55
 89-52-15 2647.379
 270-09 806.927 2647.375
 89-49-35 1603.43
 270-10-35 488.735 1603.441

T @ 7 B 5 17

0-40-31 179-25-52
 180-40-25
 180-06-23
 6 0-06-23 179-25-48

T @ 17 B 5 7

0-08-14 181-56-59
 180-08-35 181-56-59
 182-05-13
 18 2-05-25 181-56-50
 90-14-33 1603.44
 269-45-54 488.735 1603.43
 89-51-37 1064.12
 270-08-50 324.343 1064.111

T @ 17 B 5 14

0-21-46
 180-22-10 178-03-17
 178-25-03
 7 358-25-23 178-03-13

500
col

20

18

19

17

1

K @ 18 BS 17				
0-09-25		20-12-40	1064.09	
190-09-15	269-52-10	269-47-30	324.738	1064.084
370-01-35		89-46-17	729.51	
1990-01-34	269-52-19	270-18-15	283.316	929.498

K @ 18 BS 19				
0-09-31				
170-04-48	90-07-54			
170-10-45				
220-12-48	90-08			

K @ 19 BS 18				
00-12-33		90-24-06	929.52	
181-12-33	46-13-30	269-36-10	283.721	929.499
46-26-03		89-58-44	10812.77	
25 226-26-05	46-13-32	270-01-0	3295.236	10812.725
119-54-28	119-41-55	89-46-55	3082.78	
20 299-54-25	119-41-52	270-13-10	734.631	3082.744
226-13-25	226-00-52	90-15-10	3604.25	
44 46-13-30	226-00-57	269-46	1098.574	3604.198

K @ 19 BS 25				
0-12-47				
180-11-37	73-28-54			
73-41-23				
20 253-41-30	73-28-43			
120-00-05	179-47-36			
14 0-0-20	179-47-43			
313-59-08	213-46-39			
18 103-54-23	313-46-46			

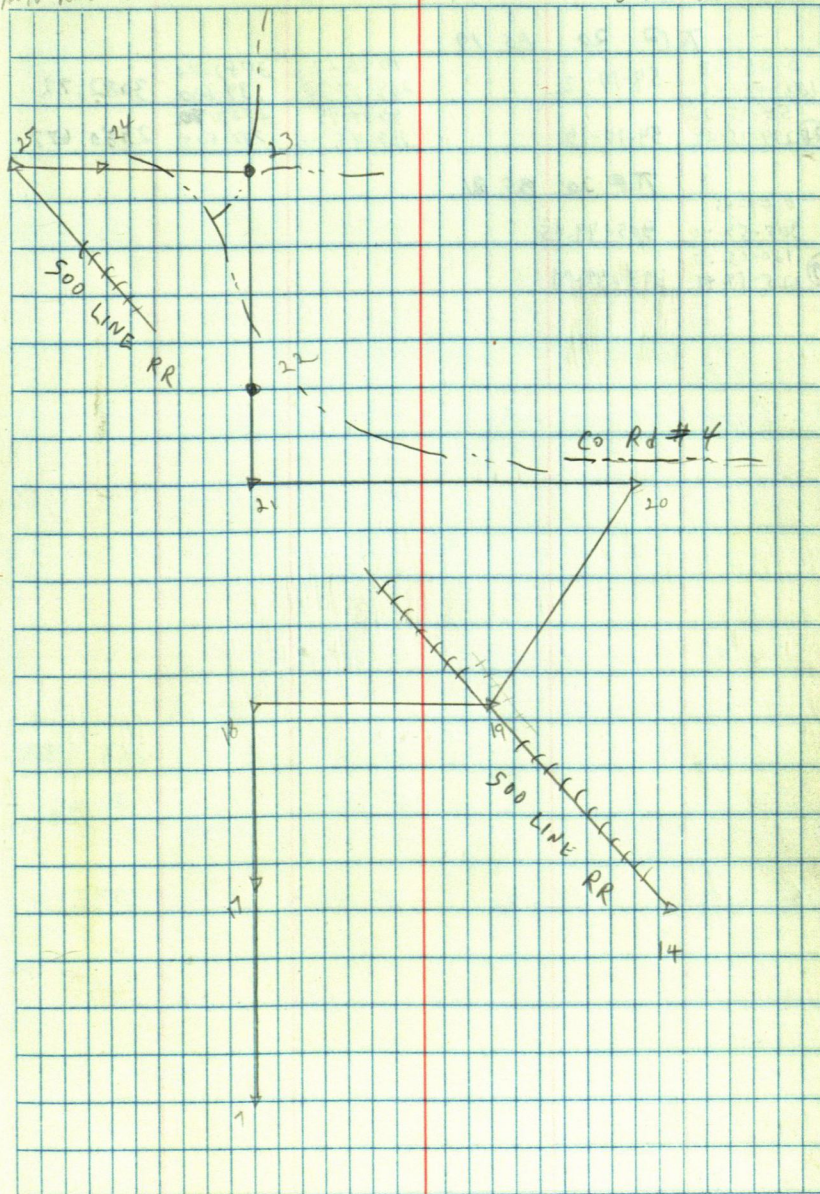
K @ 14 BS 11				
0-16-47		90-04-40	3645.77	
120-17-00	179-37-27	269-55	111.234	3645.756
179-54-14		89-52-30	3604.25	
19 359-54-25	179-37-25	270-07-40	1098.576	3604.227

K @ 14 BS 19				
6-15-00				
180-15-18	180-22-40			
180-37-40				
110-37-53	180-22-35			

HOT 80°
 TENA
 AUTO RMBL

B. CURT
 T. JONES 20

6-28-86



$\pi @ 20 \quad BS 19$

0-05-08	54-10-12	90-16-22	3082.76	
180-05-06		264-17-30	939.630	3082.72
54-15-20		90-14-45	2560.70	
(20) 234-15-22	54-10-16	264-15-05	780.509	2560.677

 $\pi @ 20 \quad BS 21$

0-04-55	
305-54-40	305-49-45
(19) 180-05-00	
125-54-41	305-49-41

BOB NIELSEN

LOTS 15-16-17 WOODK No. SHORE

T @ 1 BS 2

150-04-43

89-30

206.76

63.02

206.752

2 300-09-30

150-04-45

90-49

113.09

34.422

113.081

T @ 1 BS 4

70-49-06

89-10

196.51

59.896

196.488

2 181-37-45

90-48-53

T @ 2 BS 1

193-02-43

5 26-05-18

193-02-39

T @ 5 BS 6

2 171-37-30

171-37-45

T @ 4 BS 1

191-15-40

7 22-30-44

191-15-22

T @ 7 BS 8

89-40

255.64

77.919

255.569

9 180

88-22

130.06

39.62

189.970

4 80-17-50

4 180-35-48

80-17-54

100-20

190.67

58.127

187.597

94-42-48

187-24-40

94-49-36

184-38-30

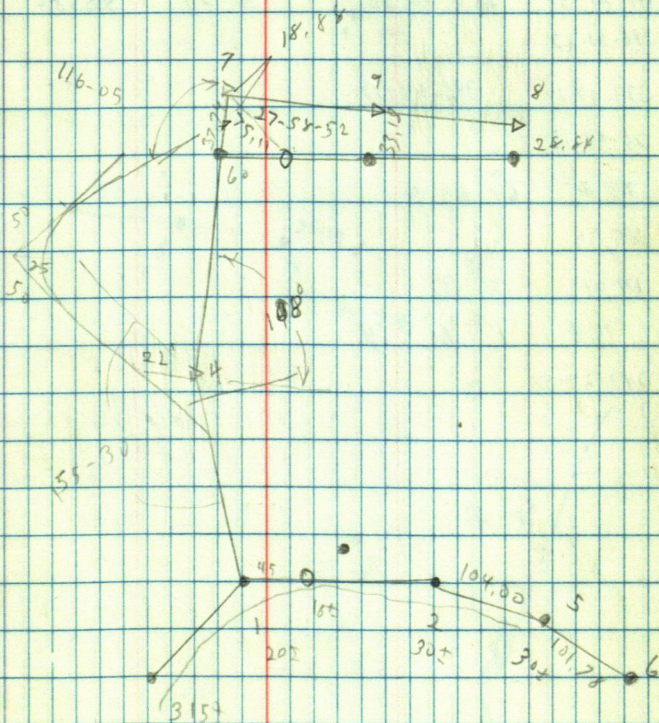
75° WARM

E. CURD

T. VOL 16

22

6-26-86



STAN DUFF

LOTS 1 & 2 KINNY CAMP

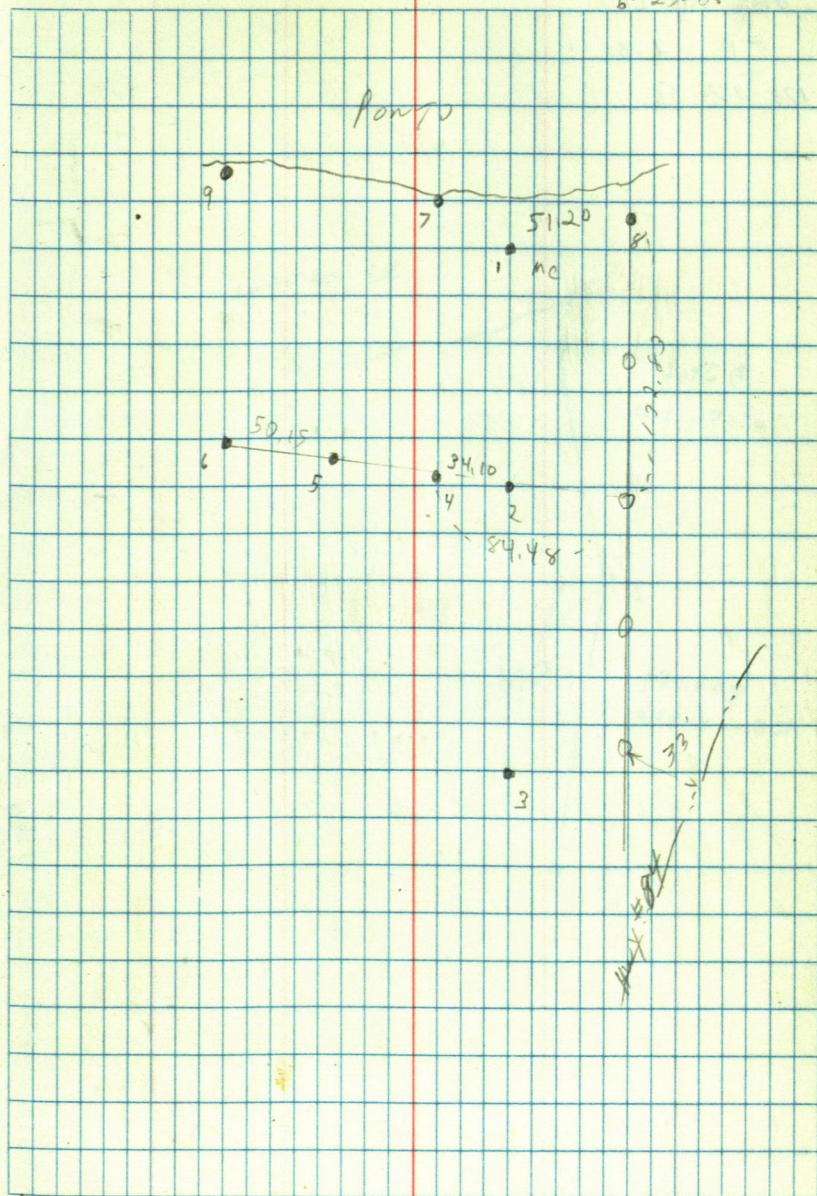
T @ 4 BS 1				
152-15-06		99-03	133.51 40.694	133.488
3 304-30	152-15-00	89-28	149.83 45.67	149.824
250-10-36				
6 141-20-50	250-40-25	90-29	100.36 30.586	100.356
346-40-27				
7 333-20-20	346-40-10			
2 75-50-12				
4 T @ 6 BS 9				
85-32				
4 171-04	85-32			
T @ 1 BS 4				
217-25-57				

75° WARM

E. CURR
T. 10 LK

23

6-27-81



JAY REEFLES

PA 2 BS 1

3 128-47-05

24

WOMAN LK

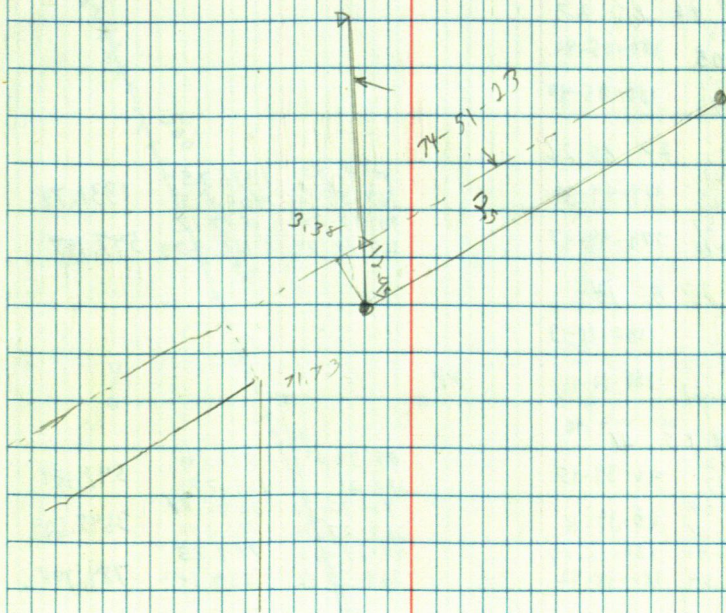
92,96 @

102-27-10

141.80 @

264-40-30

Akeley

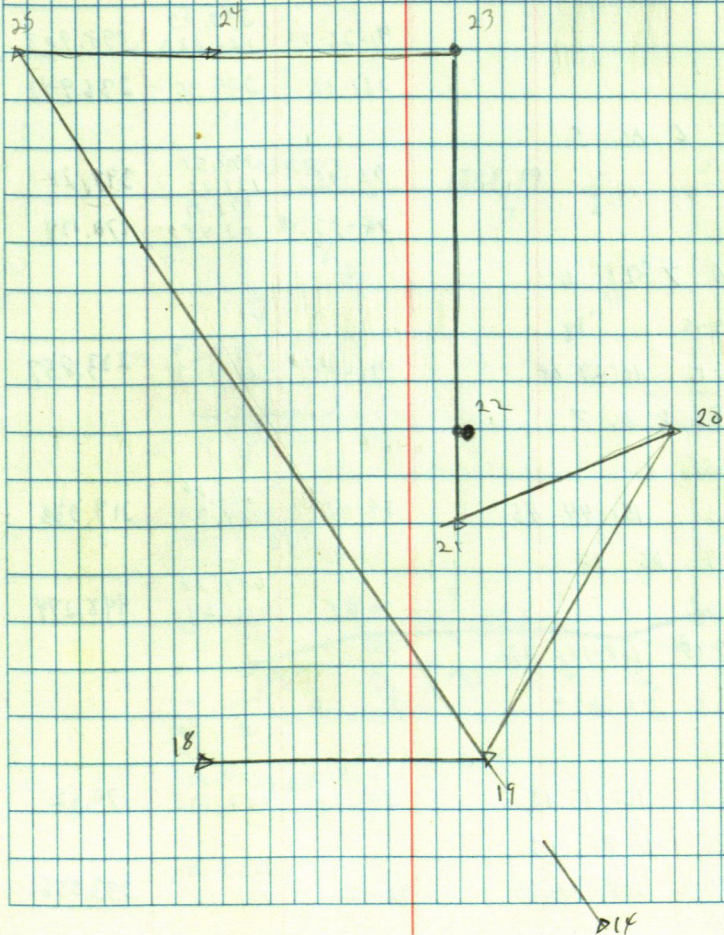


uses

BOY RIVER

T @ 21 BS 20			
0-04-06		88-47-47	2560.74
180-04-25	275-53-02	270-12-32	780.511
275-52-08		89-50-00	5515.03
28 95-52-20	275-52-55	270-06-44	1680.983
277-24-56	277-20-50	91-57-74	229.68
28 97-25-10	277-20-45	268-06-31	70.009
			229.562
T @ 21 BS 23			
0-45-10	1-27-47		
180-45-22			
2-12-57			
22 161-12-10	1-27-48		
84-52-10	84-07-00		
20 264-52-30	84-07-08		
T @ 23 BS 21			
0-03-10	88-52-40	90-14-35	5515.03
180-03-25		269-45	1680.788
88-55-50		90-05-14	5145.26
24 265-56-05	88-52-40	269-54	1568.268
			5514.976
			5145.254
T @ 23 BS 24			
0-21-35			
180-21-30	271-07-20		
271-28-55			
21 91-29-10	271-07-37		

 140° 75°
 TEND
 AUTO RUN

 E. CARD
 T. VOLCKE
 6-16-86
 27


DON CORNELL

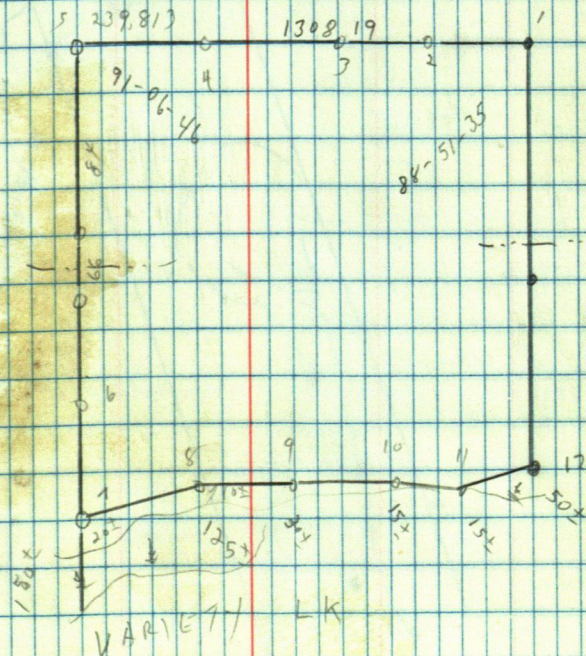
GL 4-33-140-31

7	2	BS	1		
180-00				90-06-78	408.89 124.615 408.860
3				89-03-36	260.62 79.446 260.585
7	4	BS	7		
				91-26-42	399.03 141.623 398.903
5				261-52	239.35 236.942
7	6	BS	5		
				92-15	397.51 121.16 397.20
7				98-53	172.19 52.484 170.124
	7	BS	6		
118-29-15					
8 232-58-15	116-29-08			91-00	223.89 68.243 223.857
7	8	BS	7		
151-44-55					
9 303-29-30	151-44-45			89-47	213.06 64.93 213.038
7	9	BS	10		
168-18-25				90-25	448.28 136.641 448.274
8 336-36-45	168-18-22				
7	10	BS	9		
166-13-25					
11 316-26-36	166-13-18			90-06	170.62 52.026 170.62
7	11	BS	12		
208-07-30	208-07-33			90-12	333.05 101.58 333.056
56-15-06					

E. CORNELL
T VOLKE

28

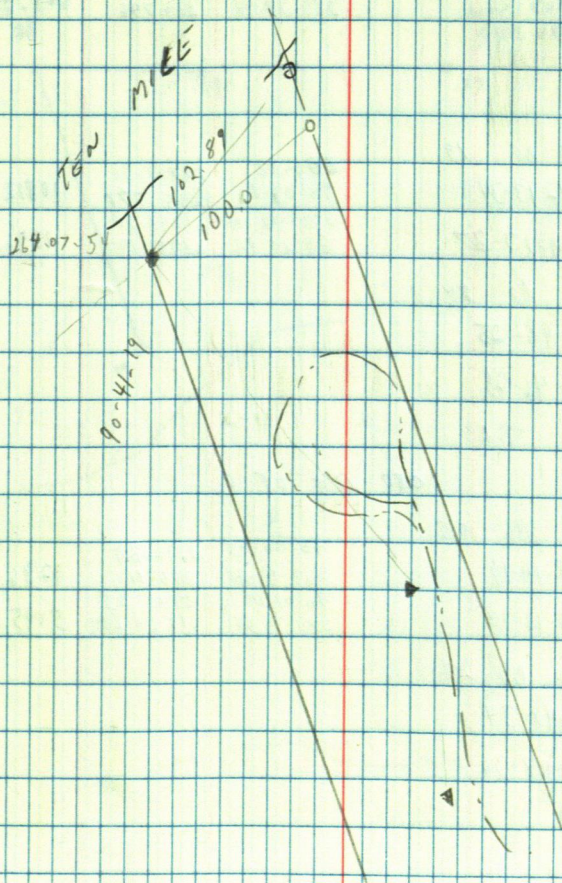
7-8-86



Don Willis

29

7-8-86



VSFS

Boy RIVER

T @ 4 BS 3

350-03-30

340-06-42 350-03-21

46.96'

T @ 11 BS 6

11A 180-0-0

70-21-00	666.46	
269-39-16	207.746	668.444

T @ 25 BS 19

0-05-32	314-13-34	267-56	10812.90	
180-15-48		70-03-46	3295.778	10812.845
314-19-06		270-32-05	1296.28	
24 134-19-25	314-17-37	89-28-02	395.109	1296.223

T @ 25 BS 24

0-15-00	45-46-25
180-15-15	
46-01-25	45-46-25
226-01-40	

RR TRKS

45-44.36 0.80 NE OF E

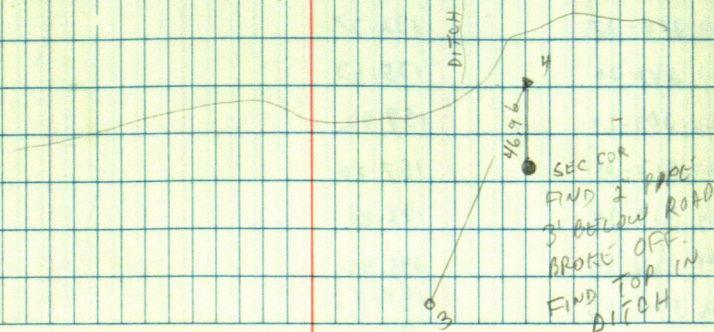
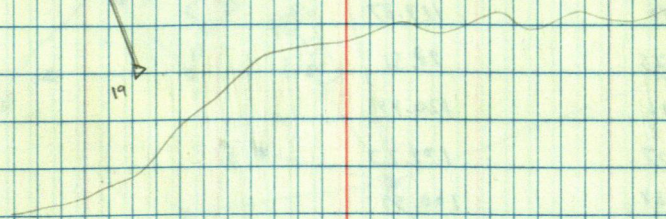
T @ 24 BS 25

0-03-10	178-11-19	70-00-25	1296.89	
180-03-10		269-59-25	395.110	1296.245
178-14-29		90-01-05	5145.25	
27358-14-28	178-11-18	270-0-55	1566.265	5145.248

T @ 24 BS 27

0-21-56	181-48-34
180-22-00	
182-10-30	181-48-30
25 2-10-36	

30



π @ 7 BS 2

68-23-54

3 9 136-47-14 68-23-39 92-32 79.88 30.442 99.78

70-43-06

5 10 141-26 70-43-00 91-27 134.98 46.153 134.954

62-33-36

6 11 125-07 62-33-70 91-27 138.74 42.146 138.397

240-07-42

7 8 120-14-50 240-07-25 81.24 27.762 90-10-0 81.239

12 π @ 2 BS 1

13 309.23

14 28 254-46-15 309-23-07 100.78

15

16

17

18

19

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22

23

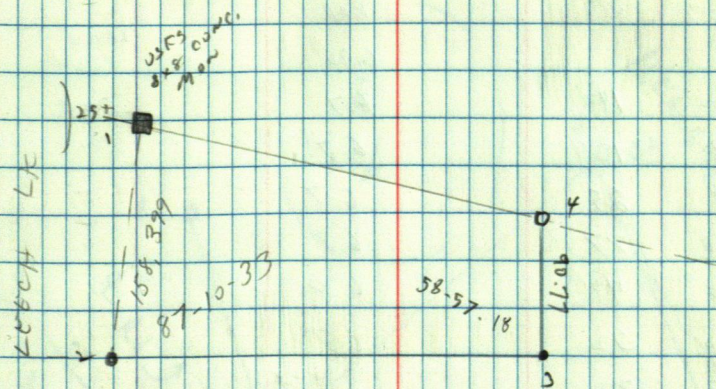
24

25

26

27

54 308 178.177



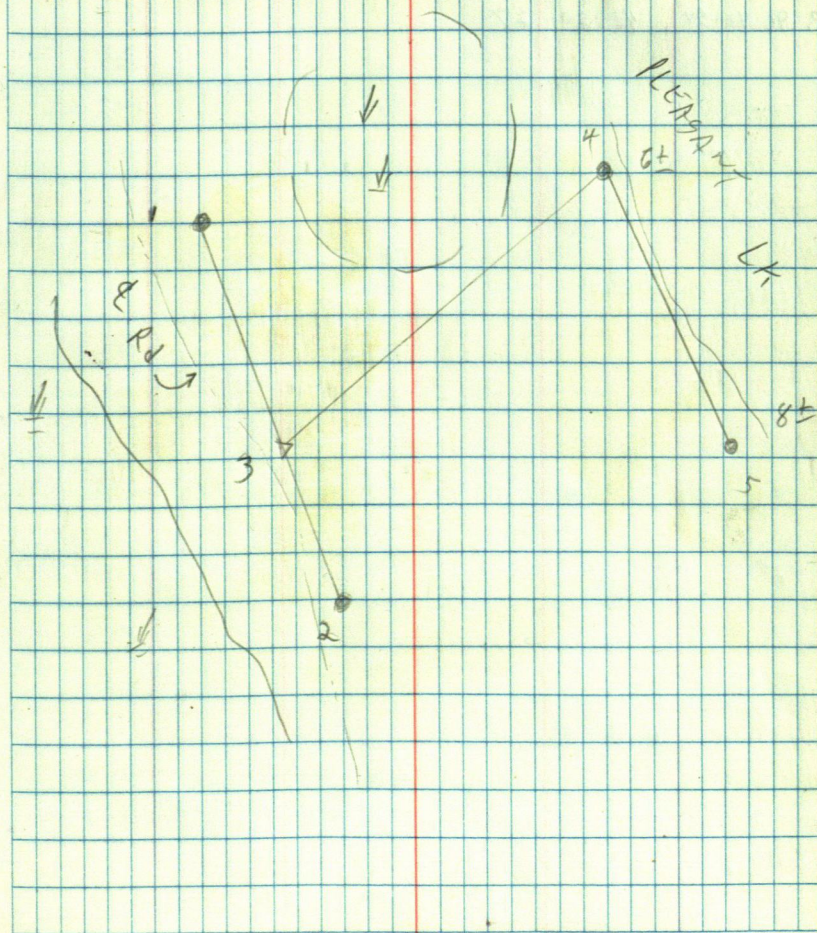
AMITA ROSIERE
PAT SCHONEBAUM

GL 2 - 28-140-30

T D 3 BS 1

		88.53	79.91 26.605	93.894
2		86.37	44.24 13.486	44.165
	93-29-45		26.602 160.57	
4	186.59	93-29-30	89-37	48.943
	50A		160.57	160.568
			48.943	
		ROD		
		6.90		
1	80-30	140	6.7	LAKE 6.66V
2	90-30	109	6.7	SUP.
3	93-48	85	6.7	
4	95-10	77	6.8	
5	91-40	48	6.8	
6	70-40	32	6.7	
7	57-37	32		
8	42-05	39		
9	34-00	47		
10	34-10	62		
11	35-10	70		
12	34-50	80		
13	46-10	99		
14	50-35	118	4.4	102.5 CON GAR
15	355-60	74	3.2	103.7
16	350-	37	4.3	102.6
17	23-35	37	4.2	102.7 BNL
18	57-15	21	4.0	102.9

34



17	100-25	20	2.7	TOP ANT
----	--------	----	-----	---------

20	192	43	5.0	101.9	E
----	-----	----	-----	-------	---

6.5	100.40	SUP
-----	--------	-----

TRD 4	BS 5	101.9
-------	------	-------

48-20-30	71-35	79.99 90.447	99.95
----------	-------	-----------------	-------

3	96-40-54	48-20-27
---	----------	----------

MARILYN SYKES

6-11-10-139-30

70 2 BS 1

180-00

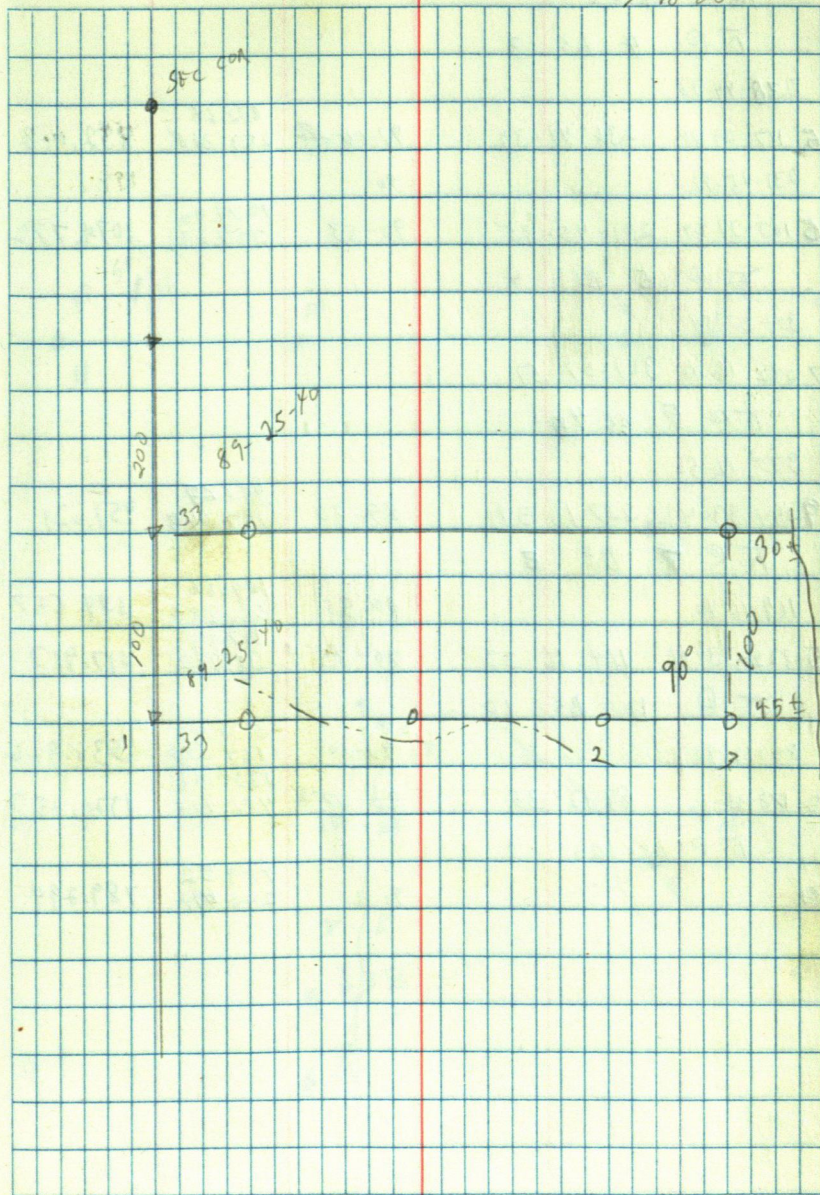
3

70-43	454.81 138.626	454.778
98-44	176.45 59.826	194.168

E. 2-20
T VOLCH

37

7-18-86



ROY HAUGEN

$\pi @ 4 BS 3$

238-44-42

5 117-29-18 238-44-39 91-00 ~~832.65~~ 253.788 832.513

231-45-42

90-

5 103-31-09 231-45-35 90-53 1074.90 227.632 1074.772

$\pi @ 5 BS 4$

301-07-54

7 242-15-42 301-07-51

$\pi @ 5 BS 4$

327-16-50

9 244-33-42 327-16-51 89-30 451.68 137.648 451.621

$\pi @ 7 BS 8$

164-16-42

89-55

184.66

56.283

184.657

5 328-33-06 164-16-33 90-35 117.92 35.942 117.912

$\pi @ 11 BS 10$

89-12-40

90-10

538.97

164.270

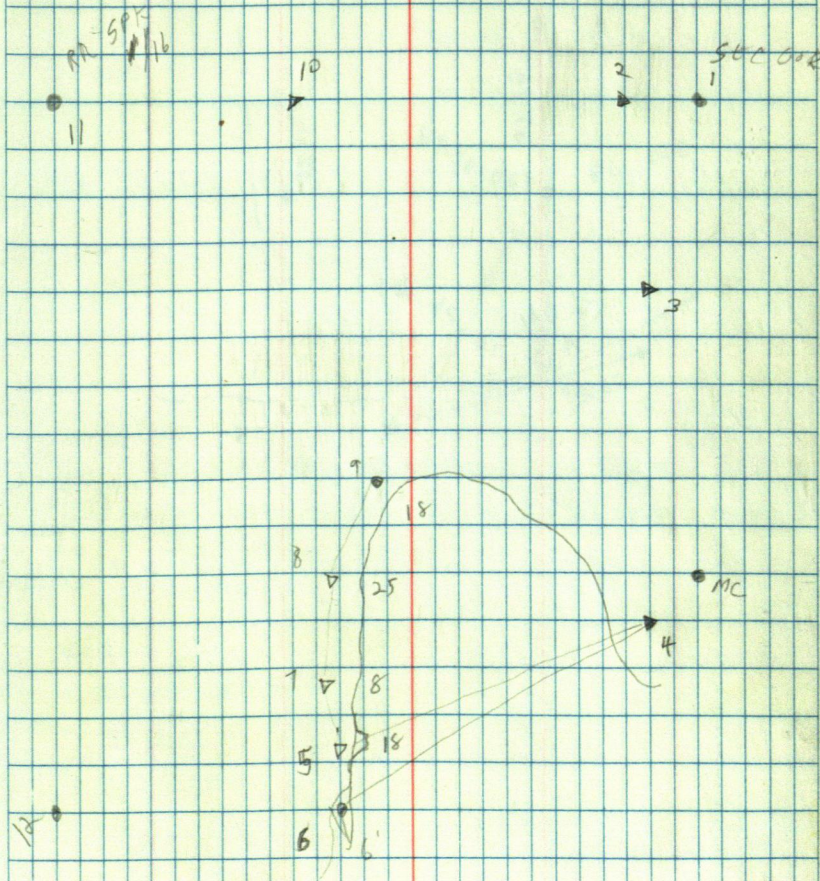
538.966

12 128-25-12 89-12-36 90-07 1320.26 402.416 1320.253

$\pi @ 10 BS -1$

90- 91-21 789.52 240.644 789.294

38

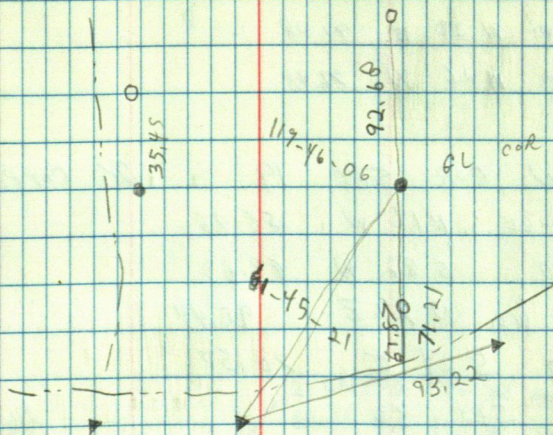


JIM SMITH

157-41-30

87.46 410.28

39



USFS

BT 5

BOY RIVER

NW COR SEC 18

BR CAP IN CONC. MON

24" SPRUCE S 43 E 168.10 OLD BT ^{GOOD} COND

PP S 43 N 50.98

8" ELM N 20 E 91.88

6" ELM N 26 W 76.48

NW COR SEC 19

2 1/2" CAPPED PIPE

18" SPRUCE N 16 W 88.45

5" WD S 82 N 89.67

10" TWIN WD N 73 E 95.44

10" Y WD S 24 E 70.57

NE SEC 30

SIGN

10" WD N 80 W 101.92 102.03

3.26 W

8" ELM N 11 E 66.67 66.91

4.10 S

6" TWIN WD S 50 E 53.24 53.50

5" " WD S 3 N 19.83 19.57

W 1/4 SEC 30

8" WD N 15 E 64.17

6" DALSON S 42 W 86.78

6" MAPLE S 38 E 138.10

PP N 45 W 52.04

NW 31

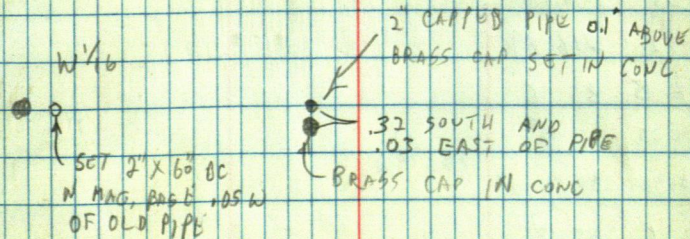
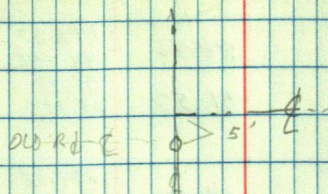
6" DALSON N 15 E 150.46

PP N 80 W 46.72

GUY POLE N 75 E 24.79

40

7-27-86



BT 5

10" WD N 70 W 35.95

7" WD N 17 W 56.56

7" PIPE N 30 E 20.06

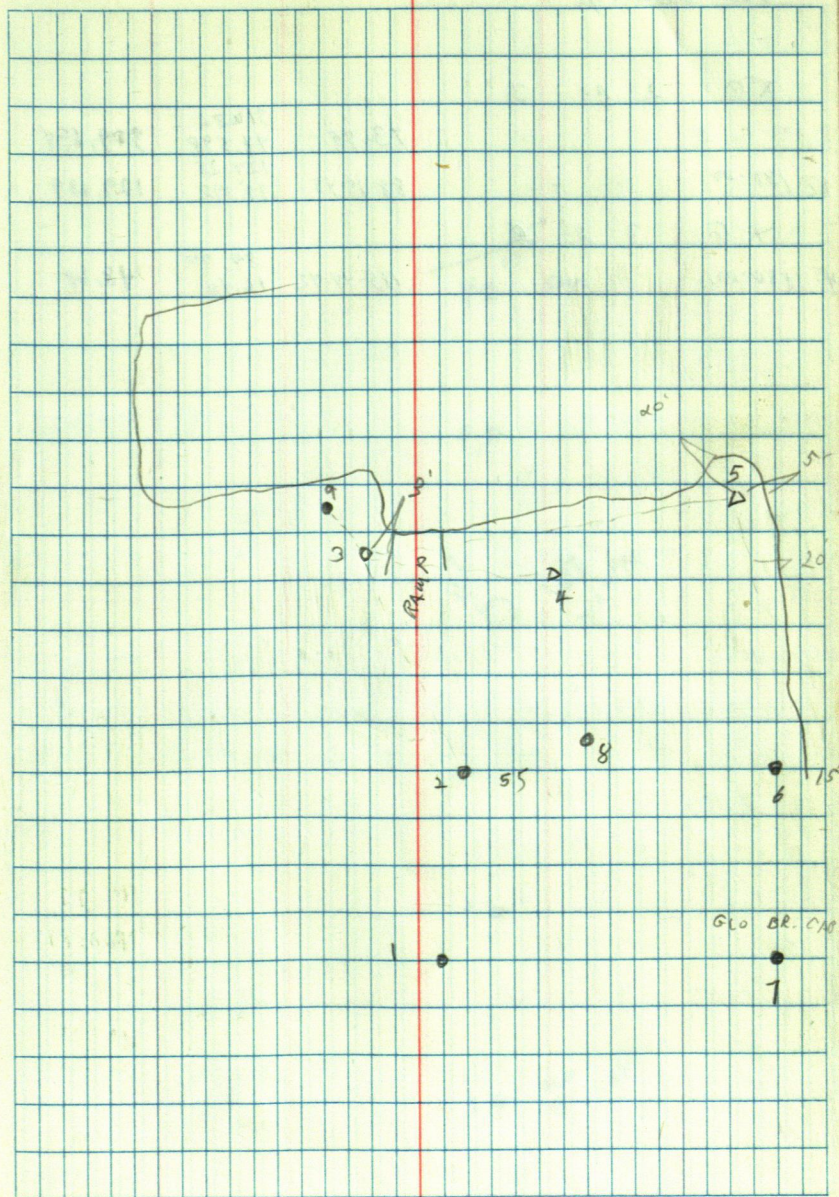
ST. SPR E 2.78

" S 3.22

4' S. OF ϕ OF OLD TRAIL

PEPWORTH

T @ 2 BS 1				
142-52-45		88-46	144.97 44.188	144.938
(3) 285-45-12	142-52-36	91-52	92.48 28.189	92.432
T @ 3 BS 5				
72-06-36		88-55	200.94 61.245	200.901
2 144-12-42	72-06-21			
4 7-30-24	78.68			
9				
(10) 2-51-44	115.60	SHORE OF HARBOR		
11 348.23	17.16			
12 261-33	34.50			
13 193-55	176.46			
14 210-72	216.69			
T @ 5 BS 6				
84-50-25				
3 169-40-36	84-50-18			
T @ 6 BS 7				
87-58-48		92-01	115.31 350.166	115.27
8 175-57-12	87-58-36	89-36	110.26 32.613	110.26
121-00-48				
5 342-01-18	171-00-39	91-01	112.74 34.363	112.722



TED DEWEY

KO 2 03 3

73-45 310.36 309.694
 88-15-45 94.598 129.25
 37.395 129.189

* 2 3 03 4

4 180-00 115-44-42 54.00 48.64
 16.46

E. CORD
 T. VOLCKE

42

6-24-86

4 15x SMC

3 1/2

11 50 PTC
 121X

2

1 20 BR CAP

VSE3

BOY RIVER

143-27

K@ 32 BS 6

88-59-54

④ 177-59-48 88-59-54

89-37-18	1206.57
270-26-35	367.762
	1206.528

K@ 32 BS 40

271-00-15

④ 182-0-12 271-0-06

K@ 40 BS 32

179-56-54

90-31-02	1206.57
269-28-54	367.763
270-20-20	738.831

359-53-42 179-56-51

89-50-40	228.192
	738.831

K@ 40 BS 41

180-03-09

④ 0-06-18 180-03-09

K@ 41 BS 40

179-49-36

90-19-05	738.91
269-41-52	225.222
	738.89

42 359-38-48 179-49-24

269-39-36	633.65
90-20-20	173.137
	633.637

K@ 41 BS 42

180-10-40

40 0-21-12 180-10-36

K@ 42 BS 41

243-0-30

89-48-42	633.65
270-12	193.126
	633.647

43 126-0-57 243-0-28

LN VCL	18.17
--------	-------

K@ 32 BS 6

46

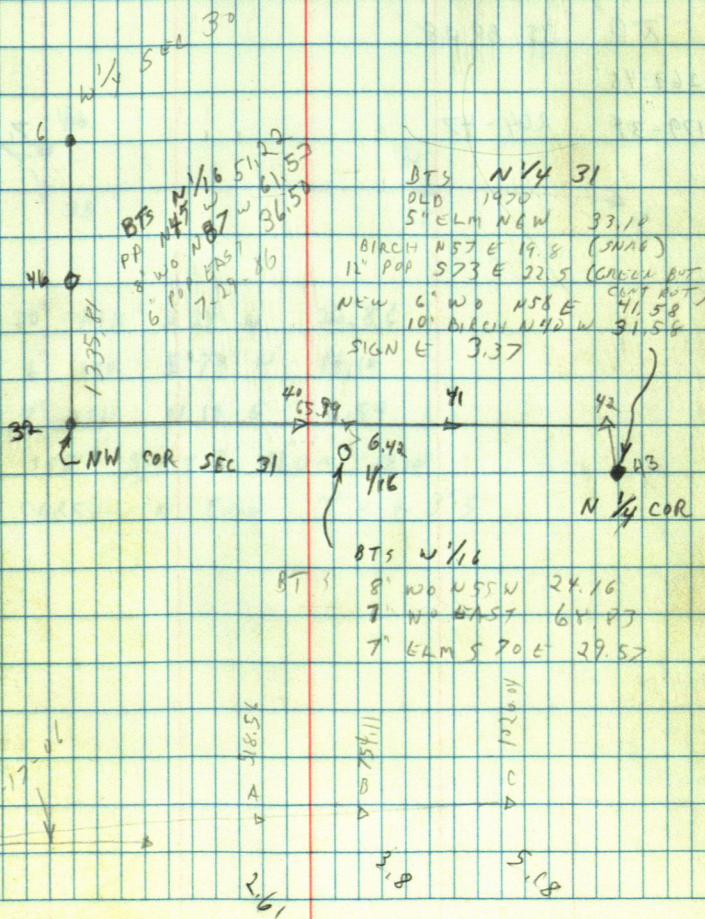
89-47	1335.83
89-41	2671.56
	814.29

HOT + HUMID

T1
AUTO RANGERE. C. VAO
T. VOLCKE

43

7-27-86



TIE To W $\frac{1}{16}$ N LWB SOC 19-143-27

$\pi @$ 28 05 14

178-19-08

89-44-06

784.64

784.629

270-16-05

237.159

90-11-24

1351.32

269-48-35

411.884

1351.309

35 357-37-50 178-18-55

$\pi @$ 28 05 35

181-41-10

14 3-22-0 181-41-00

$\pi @$ 35 05 28

269-48

179-34 269-47

7.39

HOT & HUMID

BEURO
T. VOLKE

44

T
AUTO-RODOL

7-28-86



10" ASH S 24 W 22.86

6" ASH S 74 W 14.10

7" ASH N 10 E 6.54

SET 5/8 X 5' ALUM. MIN

CARSONITE SIGN 3' N & 3' S

W $\frac{1}{4}$
SEC 19

24.13
16-12-29

6" ELM N50 E 35.64
6" POP N18 W 20.90
6" MAPLE N60 W 88.00

17

NW cor SEC 19
SEC 19

15.8

7

33-45-35

BT 5

8" SPR N58 E 30.83
8" SPR S85E 27.71
7" SPR S50 E 39.87

TC 3 BS 1

49

90-04

1281.26

50

90-01-30 3877.52

TC 51 BS 6

89-39-43

269-05-18

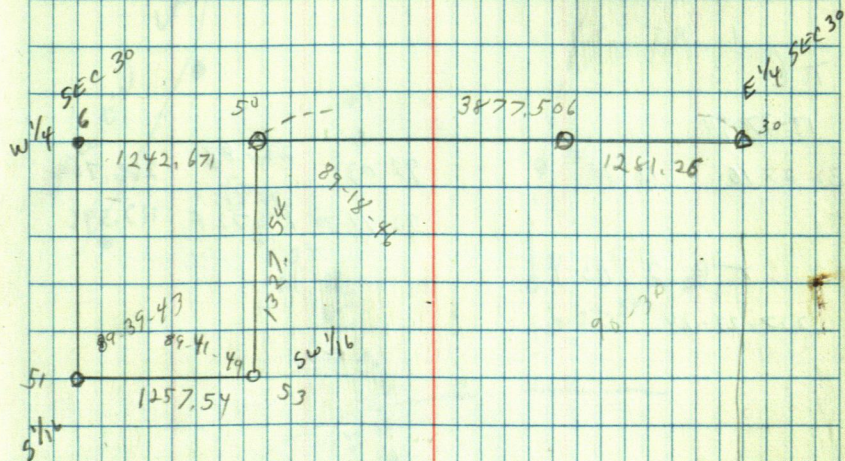
196.23

212.204

179-29-20

90-01

5681



BT 5 SW 1/4

6' MAPLE S 80 W 20.00

7' " N 5 E 52.02

6' PDP EAST 30.59

SIGN N 9.68 FIB. GLS

W 3.60

$\pi @ 2 BS 1$

279-05

29 118-10-12 279-05-06 265-28 $\frac{129.17}{39.380}$ 128.79

337-16-06

30 314-32 337-16-03 89-54 $\frac{147.66}{45.008}$ 147.661

1 BS 2

$\pi @$

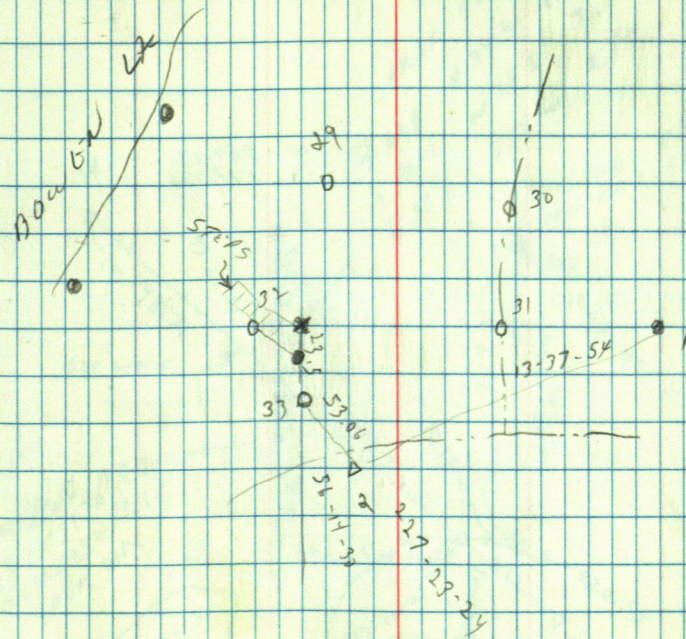
13-37-54

32 27-16- 13-38 92-03 $\frac{266.88}{34.661}$ 266.709

31 92-44-30 $\frac{113.72 F}{113.596}$

$\pi @ 2 BS 1$

227-23-24



USF9

143-27

* a cw $\frac{1}{16}$ BS cc $\frac{1}{16}$

89-18-56

89-54-10	1327.57
	404.647

89-03-20	580.47
	177.076

678.98

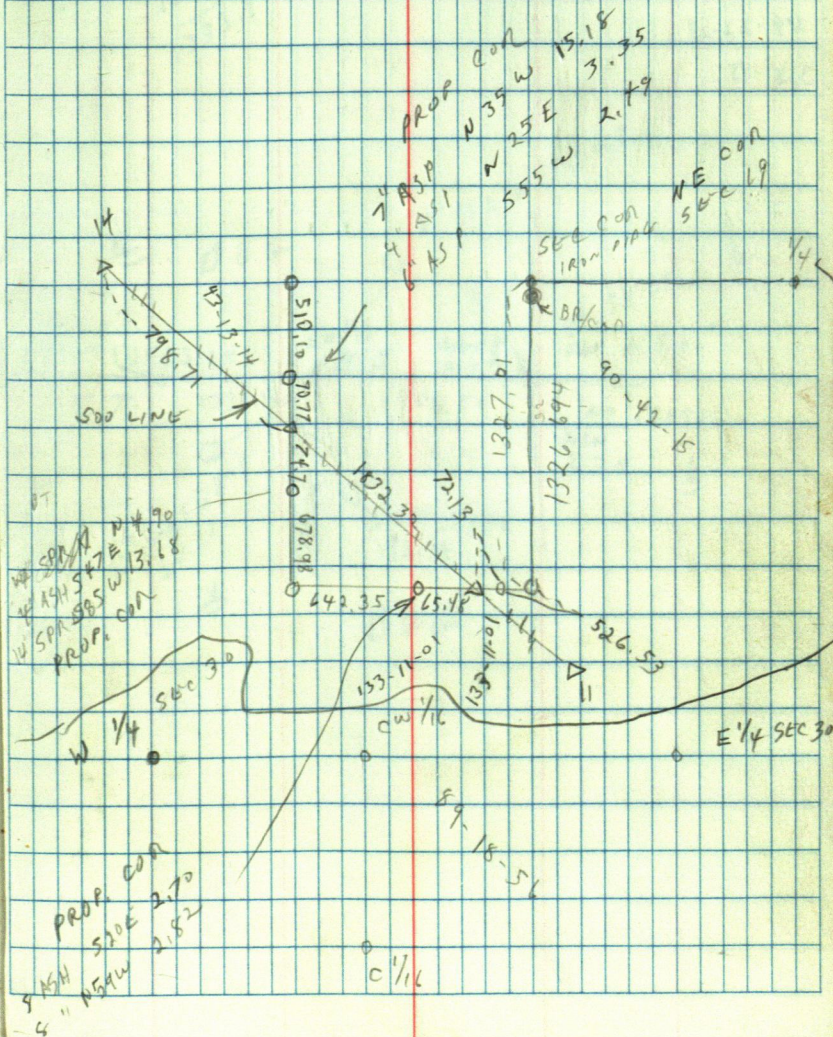
74.72

7	5	3	.	6	8
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757

753.68

7.32



VSFS

143-27

64-58-24
179-56-54

89-58-27

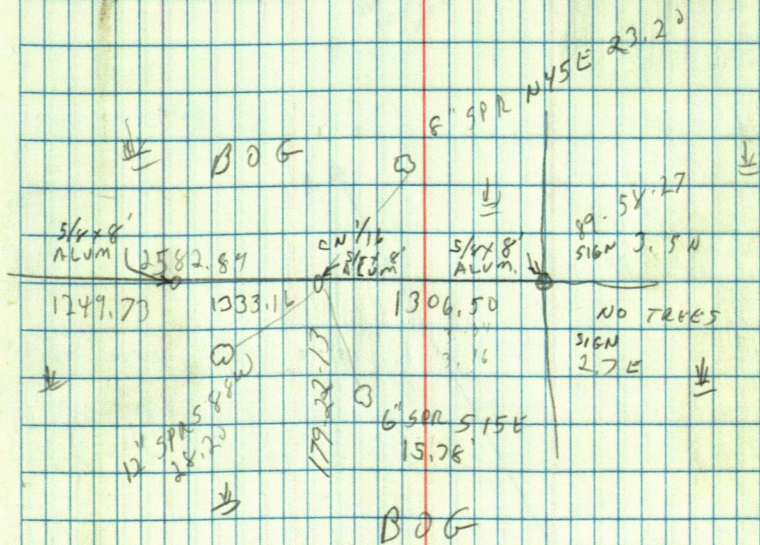
179-22-13

358-45

49

$$\begin{array}{r} 2582.84 \\ 1249.73 \\ \hline 1333.11 \end{array}$$

$$\begin{array}{r} 27.62 \\ 33.16 \\ \hline 4.46 \end{array}$$

$$\begin{array}{r} 22 \\ 6 \\ \hline 16 \end{array}$$


BOB JOHNSON

T @ A BS B

191-28-07	27-22-11	89-54-52	2722.94	2722.923
11-28-23			829.951	
218-50-18			1280.73	
5/4 38-50-32	27-22-09	89-57-40	390.370	1280.728

30

OLD SPK
SEE SURVEY FOR
CHUCK SHEATH

A D

5 1/4

10' B E 371

BOY RIVER

(22)

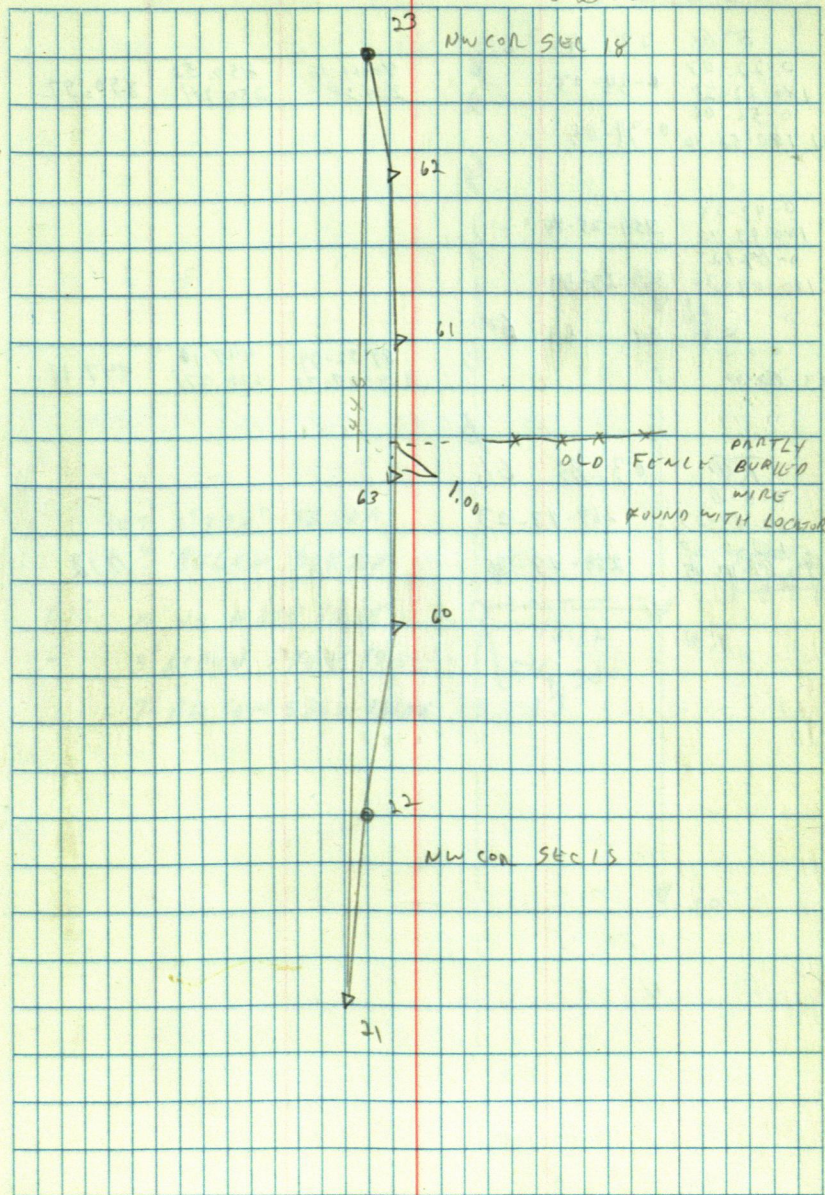
T @		NW COR	SEC 19	AS 31		
0-0-20	178-42-30		84-22-30	229.74		
160-0-45			271-36-45	20.027	229.65	
178-50-50	178-42-25		90-06-50	743.35		
60 358-51-10			269-53-0	226.574	743.347	
T @ 22 BS 60						
40-20-56	181-17-26		90-0-36	743.31		
180-01-01			269-59-30	226.567		
181-38-22	181-17-29		89-55-30	2345.97		
21 1-38-40			270-04-40	715.09		
T @ 60 BS 61						
0-0-08	180-15-48		90-0-36	743.31		
180-0-12			269-59-30	226.567	743.316	
180-15-56	180-15-53		89-55-30	2345.910		
22 0-15-05			270-04-40	715.07	2345.892	
T @ 60 BS 22						
0-0-10	179-44-10					
186-0-12						
179-44-20	179-44-16					
61 359-44-28						
T @ 61 BS 60						
0-0-33	0-22-33	180-15-03	90-18-50	2345.95		
180-34-32	180-22-40		264-41	715.045	2345.903	
180-44-18	180-32-36		89-09-13	2345.96		
61 0-44-10	0-32-50	180-15-10	270-00-35	410.349	1346.123	
				1346.26		
T @ 61 BS 62						
0-29-41	179-44-56					
180-22-43						
180-14-35	179-44-48					
60 0-07-37						
T @ 62 BS 61						
0-09-26	179-15-54		90-54-55	1346.30		
180-04-26			264-05	410.36	1346.134	
179-25-20	179-15-57		90-00-55	850.54		
20 359-25-22			269-59-10	259.242	850.516	
T @ 62 BS 23						
0-25-45	180-44					
180-25-42						
181-09-45	"					
61 1-09-44	180-44-02					

CLL 78° 27 wind

Fig. 0000

51

8-23-88



VSFS

SET E 1/4 SEC 13 147-28

T @	23	BS	62
0-22-03			
180-22-25	0-34-03		
0-56-06			
21 180-56-30	0-34-05		

0-43-23			
180-43-40	359-25-49		
0-09-12			
180-09-30	359-25-50		

T @	61	BS	60
0-0-0			
63 180-00			
	89-52-39	447.16	
	269-07-30	136.278	447.14

T @	63	BS	61
0-0-0			
269-43-23	269-43-23		
180-0-20			
64 89-43-45	269-43-25		16.12

E. COLE
T. VOLKE

52

8-29-86

SET 2" X 24" BR CAN

1" BELOW OLR TOP

DT'S 10" WD N 80 E 94.65
 - 5" ASPEN 570 E 69.62
 7" BAL 50 M S 36 W 121.06

COUNTRY Rd

64

16.12

E 1/4 SEC

13

FENCE

63

60

BTS

REMER

142-26

C-E $\frac{1}{16}$

S 35 142-26

6" WD NSE 44.94

8" WD N40W 26.18

6" WD S80W 32.96

SGN 3' N 3' E

CN $\frac{1}{16}$

4" SPR N 5 W 5.53

6" " N 88 W 31.65

8" " S 35 W 13.47

SIGN 3' W, 3' S

C $\frac{1}{4}$

6" POP N 10 W 44.81

6" WD N 85 W 41.25

10" POP S 50 W 21.58

S 3.75 W 53.95 N

S $\frac{1}{4}$ SEC 27

ASH S 75 W 78.52

ASDEN S 60 E 48.66

PP N 70 N 81.64

5' N OF ϕ

BOY RIVER

143-27

CW $\frac{1}{16}$ - 30 - 143-27

7" POP S 18 E 30.27

5" ASH N 12 E 75.66

9" SPR S 40 W 40.25

6' S ϕ

BOY RIVER

E. 25-26

E $\frac{1}{4}$ SEC 30 143-27

PP N 15 W 36.44

STL. SIGN POST N E

N W

3' E OF CULVERT (NEWER ONE)

3' S ϕ N $\frac{1}{16}$ SEC 30 - 29

10" WD N 89 W 28.85

6" DALSON N 88 E 8.51

12" DALSON S 2 W 23.35

VSFS

BOY RIVER

D

TQ 1 05 3

19-08-10
27-37-3627-37-36 27-37-36
207-37-07 27-37-42

33

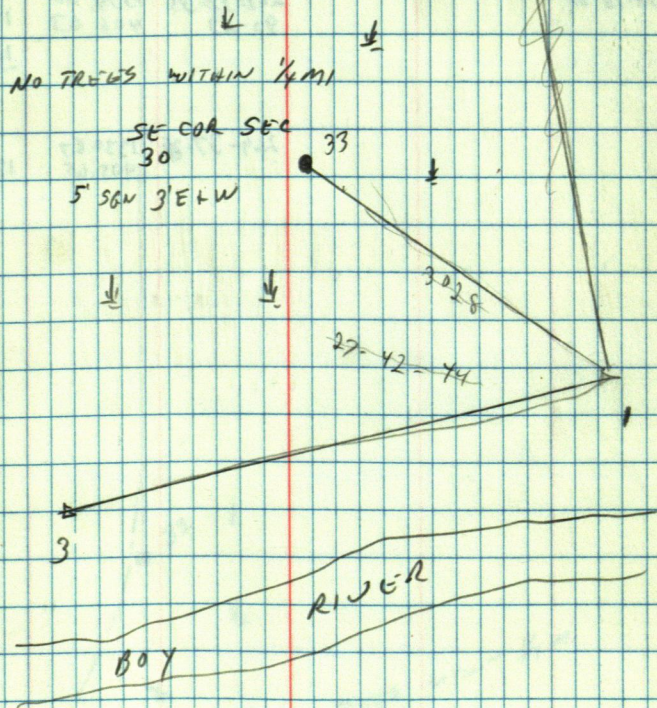
TQ 1 05 33

0-00-00
179-59-35332-22-20 332-22-20
152-21-50 332-22-15

3

90-02-15 3026.72
269-57-50 722.544 3026.706CLOY 65°
RAIN IN PME. C. URO
T. FREEMAN
9-8-66

54



USFS

BOY RIVER

X @ 32 BS 6

0-0-00

180-0-15

WC 179-19-31

359-19-50

90-01-05 1469.70

X @ 6 BS 32

0-0-0

178-16-08

269-37-35 1334.08

90-23 406.63

1334.048

1330.80

3.248

269-37-25 1330.87

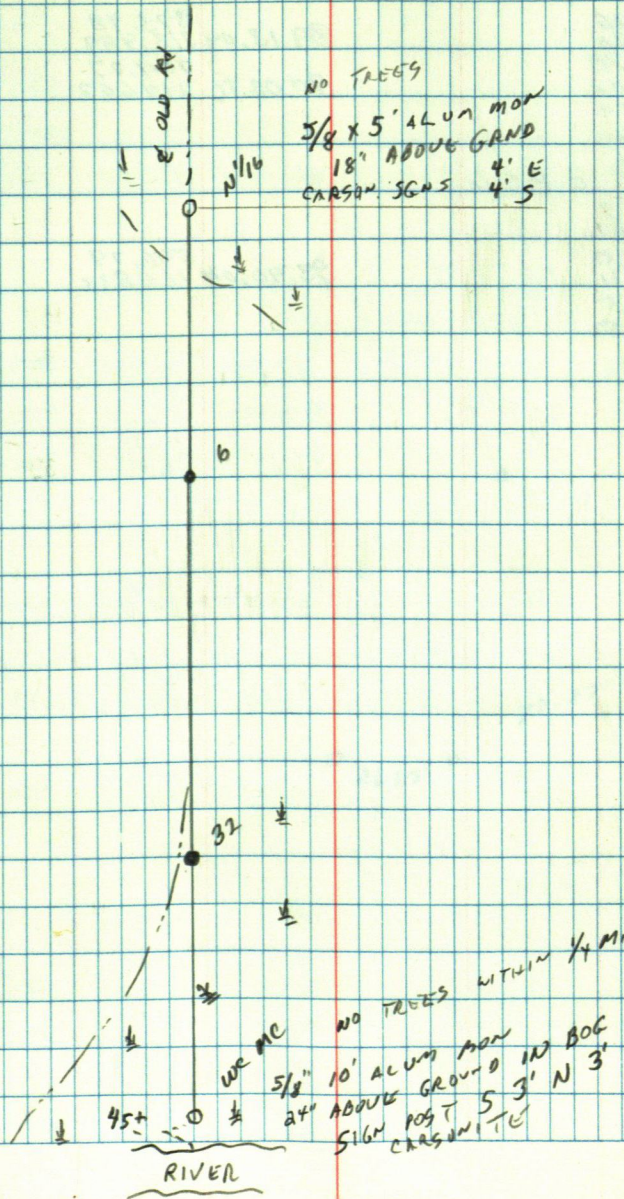
405.65

1330.834

E. COAD
T. FREEMAN

55

9-10-86



T C 6 B 5 5

0,0,26

180,0,25

204,85,00

24,35,02

0,0,14

155,25,48

39,13,09

373,98

113,989

704,27

90,03,16

214,662

T C 8 B 5 6

0,0,17

180,0,17

174,34,12

354,34,11

0,0,15

185,25,50

93,40,04

540,79

164,833

26.63

70.27-50

SUE ANDERSON

⌈ @ 2 BS 1

335-02-12

84.01

4

96-24-30

87.31

83.78

A 42-14

105-10

37.95

36.63

B 112-27-12

106-42-16

54.28

52.56

150-43-06

301-25-48 150-42-54

⌈ @ 6 BS 11

130-20-33

87-54

307.74

93.798

307.543

2 260-41

130-20-30

95-07-40

87.49

26.666

87.138

12

87-53-20

316.57

96.491

316.355

⌈ @ 7 BS 12

303-27-54

4 246-56

303-28

92-33

126.53

38.523

126.415

310-15-50

9 266-31-50

313-15-55

91-46

237.84

72.489

237.718

315-19-36

10 270-39-06

315-19-37

91-32-30

338.63

103.211

338.500

⌈ @ 12 BS 6

318-04-30

14 276-08-12

318-04-03

93-41

90.50

27.595

90.33

13 242-35-48

90-12

30.17

9.197

30.172

15 315-00

92-38

134.46

40.956

134.322

16 323-06-10

94-26

118.56

36.14

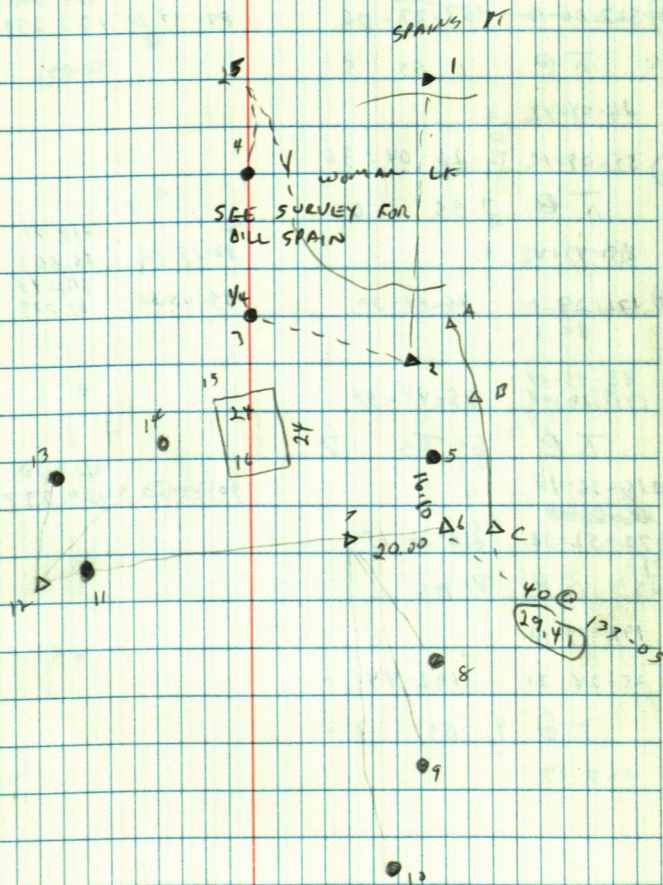
118.21

E. C. L. =

T. M.

9-20-86

57



USED

T @ 42 05 41

408.04
124.368

182-09-24

4-18-36

182-09-18

90-21-24
269-38-30

408.04
124.368

408.026

T @ A 05 42

73 180-0-0

86-74-42

201.10
61.287

200.76

T @ 73 05 A

178-29-00

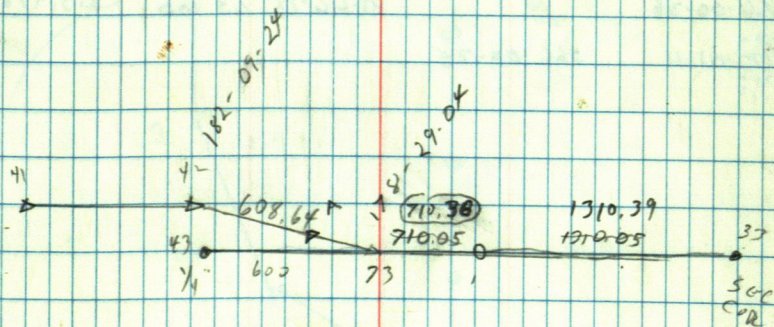
56-57-53

178-24-57

2020.77

90-07-41

615.939
2020.77



600
2020.77
2620.77
1210.38
1310.39

CHAS LOUPPEX

π @ 2 BS 3

145-16-12

89-42-55
~~89-42-55~~

70.773
232.16

232.174

1 190-32-08

145-16-04

89-07-34

244.52
74.528

244.484

π @ 3 BS 4

137-14-00

2 274-28-06

137-14-03

π @ 4 BS 5

131-35-43

91-05-24

162.29
47.466

162.26

3 303-11-00

131-35-30

89-51-42

178.83
54.525

178.824

π @ 5 BS 6

266-00-26

91-46-13

213.58
65.100

213.478

4 172-01-11

266-00-35

162.26
81.97
~~81.97~~
80.29

10 MILES

1" PIPE
IN CONC.

6

81.97

5

14.26-57

4

3

2

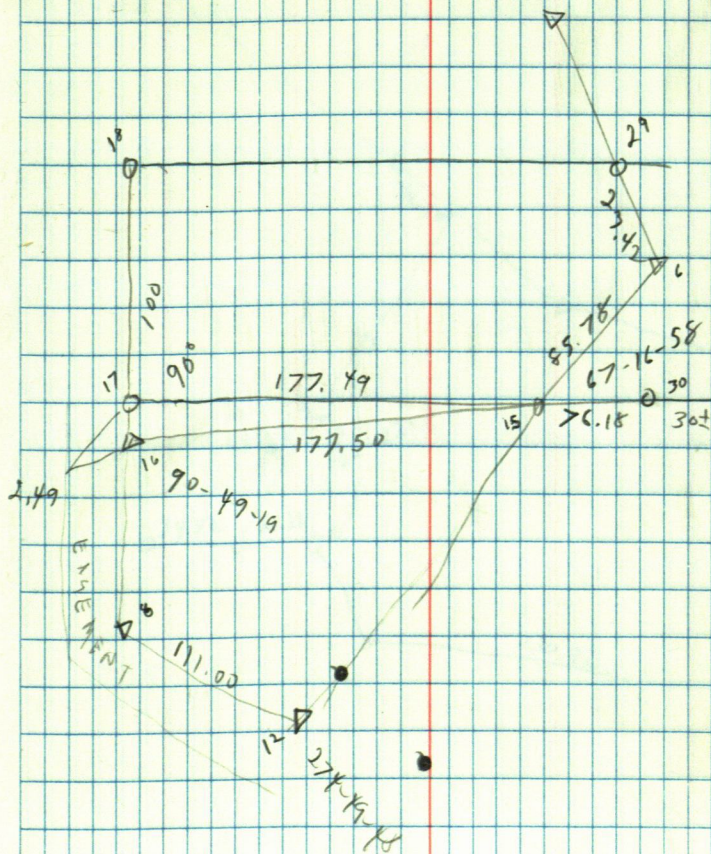
SW 1/16

1" PIPE IN CONC.
SEE BK 298/60

SUE ANDERSON

66-27-48

61

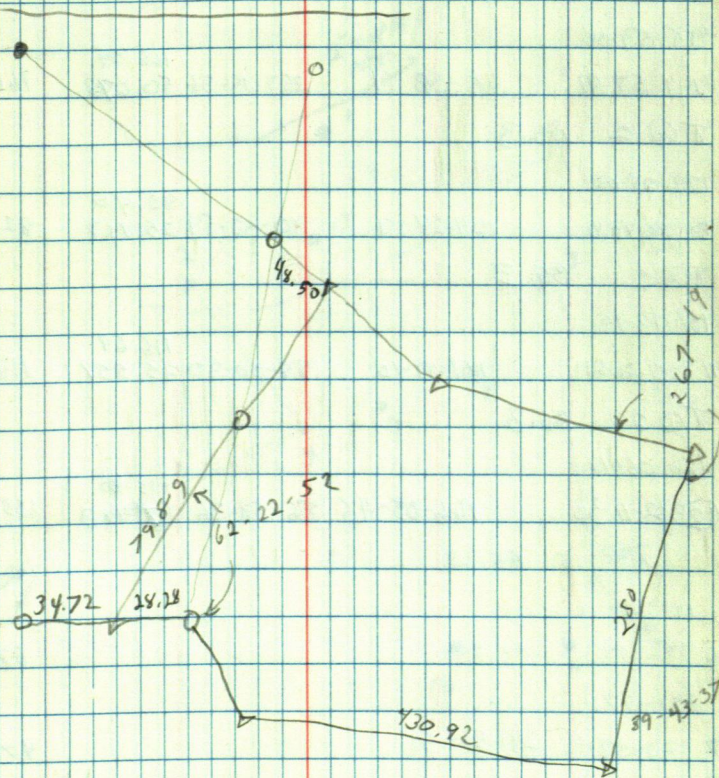


PITTENGER

231.28
18.79
250.00

62

34.72
28.28
63.00



B. VANDER-BRANDEN

T @ 2 BS 1

64-30-06

95-46-18

240.39

239.177

5129-00-00

64-30-00

268-47-18

288.08

288.013

T @ 2 BS 1

95-59-00

4191-57-41

95-58-57

267-19-36

166.24

166.063

T @ 2 BS 3

124-25-06

10248-49-41

124-24-51

90-62-54

82.40

82.402

T @ 2 BS 3

151-13-18

11302-26-21

151-13-10

88-20-30

116.64

116.589

T @ 2 BS 3

166-05-48

12332-11-30

166-05-45

86-58-36

155.80

155.574

T @ 5 BS 3

141-29

6382-58

141-29

87.75

241-57

7123-53-42

241-56-51

47.90

265-50-18

16171-40-72

265-50-21

105.45

T @ 3 BS 5

110-41-12

2221-21-54

110-40-57

93-24-18

128.32

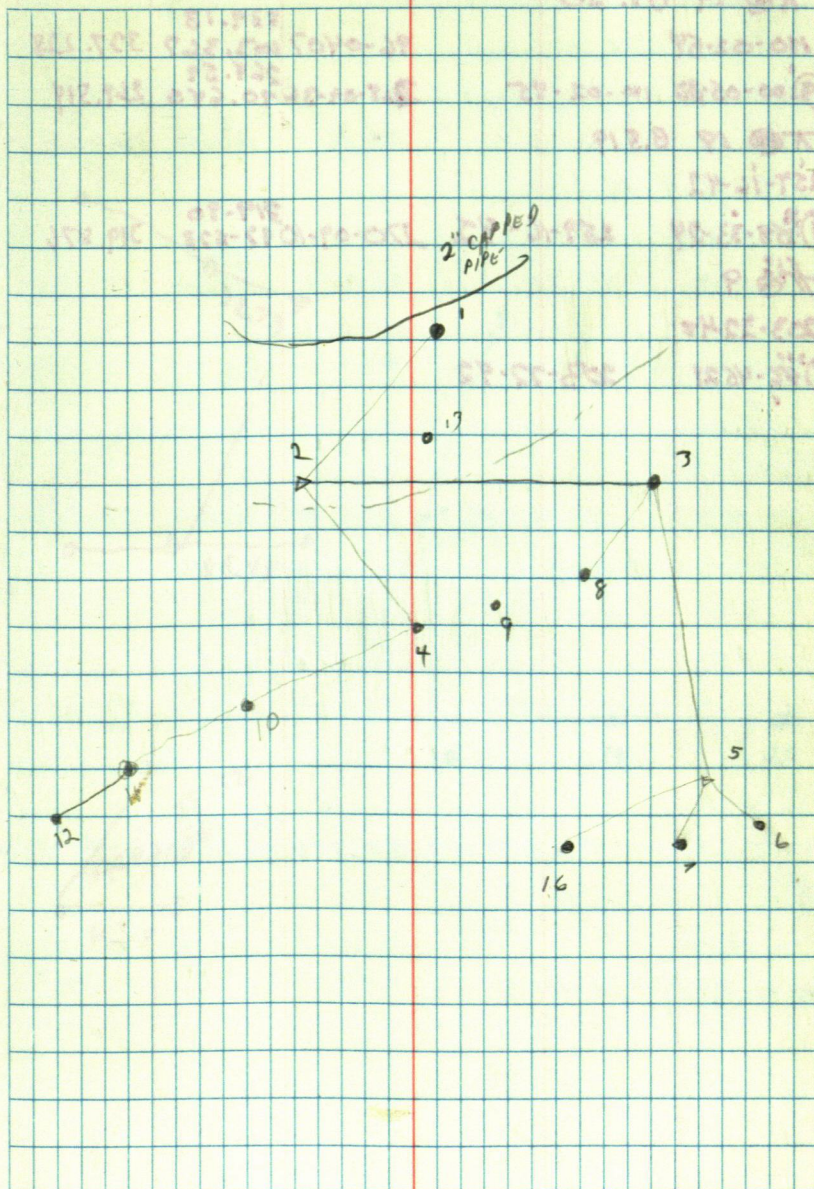
128.104

77-11-20

8146-22-42

73-11-21

61.03



PYTHAGORAS

$\pi @ 19 \text{ BS. } 20$

110-02-54

96-0407

339.13

103.367

337.224

6 19100-0530 100-02-45

247-09-36

264.52

90.645

264.514

31 $\pi @ 19 \text{ BS. } 19$

257-16-42

319-90

9 1157-33-24

259-16-42

270-09-10

97-523

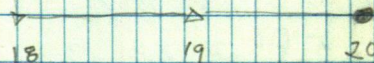
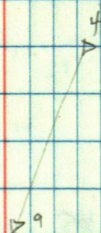
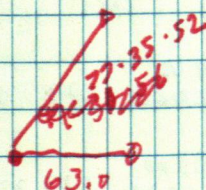
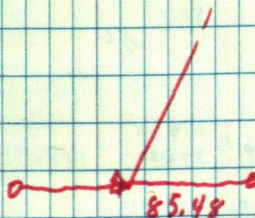
319.876

415 fig 9

π 203-2248

12 1176-4521

203-22-92



ROBERT VAN DEN-BRANDEN

T @ 14 BS 4

180.00

13 249-49-42 50.66 47.55

T @ 4 BS 2

44-17-42

14 84-35-14 44-17-39 84-36 101.18
30.840 101.15

9 121-19 50.1

219.06-30

1578-13-30 219.06-45 96-32-42 109.64
3424 334.3 108.916

K @ 5 BS 17

145-45-50

291-31-30 145-45-45 90-00 904.69
275.75 904.68

T @ 2 BS 3

36-30-12

1973-00-30 36-30-15 267-12-54 129.46
39.460 129.307

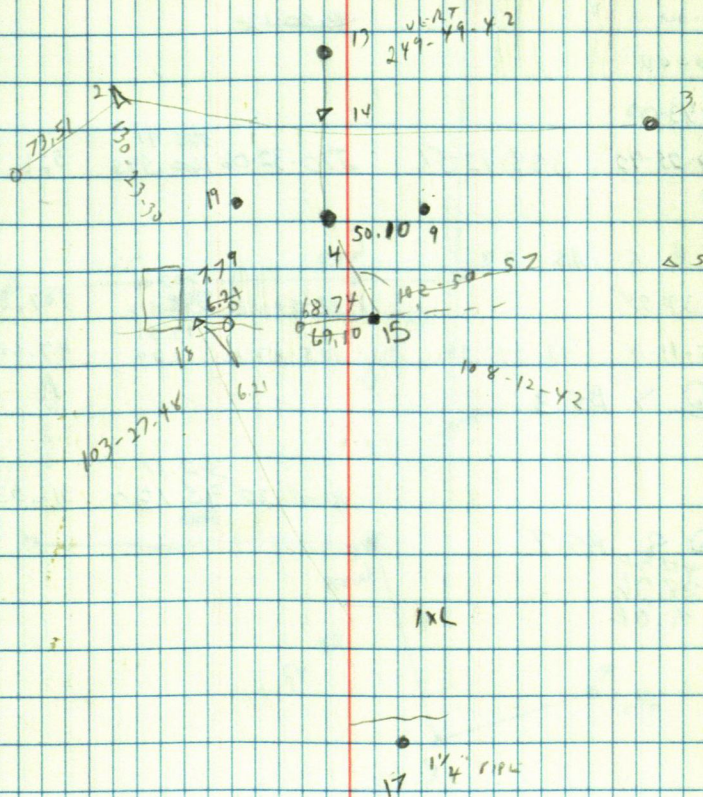
T @ 17 BS 18

26-18-48

90-29-24 823.40
250.956 823.339

5 52-37-42 26-18-51

68-19-48



HERB WILSON

T @ 2 BS 3

302-13-42

90-05-20

1441.90

439.490

1441.889

① 214-27-30

302-13-45

272-47-36

204.48

62.307

204.176

T @ 3 BS 2

86-37-06

④ 173-14-06

86-37-03

266-44-48

152.48

46.460

152.207

⑤ 0-0-00

~~99-50-12~~

⑥ 0-0-00

354-43-00

⑦ 349-25-42

354-42-51

270-32-06

526.91

160.598

526.878

T @ 5 BS 2

92-39-54

89-50-12

707.06

215.514

707.057

6 185-19-14

92-39-39

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49.51

15.09

47.618

T @ 7 BS 3

91-11-30

312.11

95.130

312.039

T @ 8 BS 7

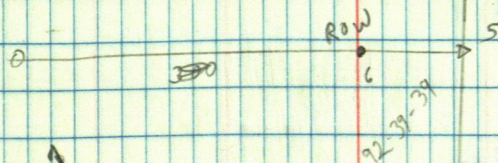
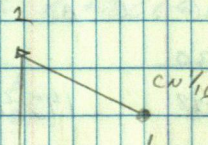
47.38.26

9.01

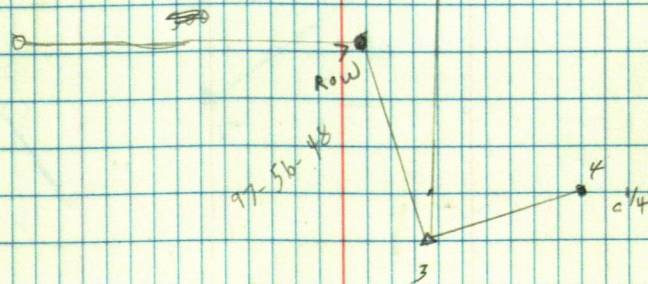
10-2-86

66

1442
707
735



104.6



BILL LUND

24-139-30

$\overline{A} \cap B = 10$

139-4242

C277-24.48

138-42-24

89-44-54

88:36

26.931

88.357

π	@	C	DS	A
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172-46-30

B 285-32-48

145-46-24

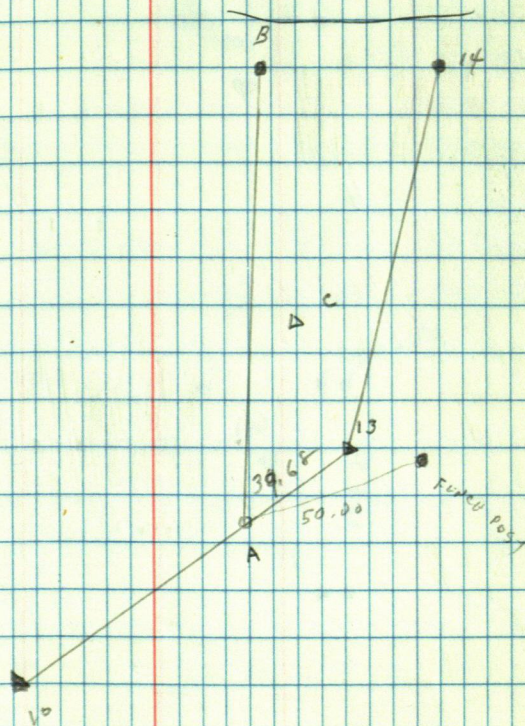
90-34-54

169.31

51.605

169, 299

BIG PORTAGE LN



D. ENGLER

7-23-189-26

68

ROOSEVELT

105.89

20.48-20.40

109-11-40

100

90°

.50

100

90°

132.29

DAVE WILLIAMS

SW-SW-7-140-30

A @ 2 BS 1

113-33-42	88-32-16	709.56 216.280	709.336
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4227-06-54	113-33-27	90-38-18	324.53 98.917	324.509
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39023-36

80-16-44 90-23-24

A @ 4 B.S. 2

276-29-36

5192-48-54	276-29-27	141.09 42.976
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A @ 5 B.S. 4

86-57-54

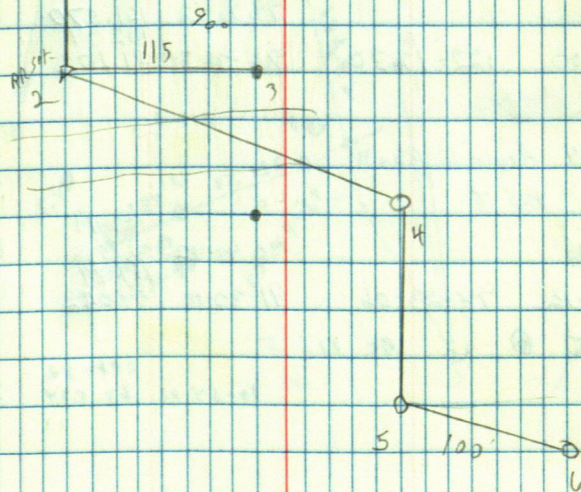
87-20-36

140.857

6173-55-42

86-57-51

2" PIPE
1/16" 1" TRIPPLE



PLESEN

T@ 3 B.S. 4

142-14-06

89-10-54

5-18-170-30

573.31

174.795

573.249

① 244-28-06

142-14-07

88-04-54

368.79

112.215

367.967

T@ 3 B.S. 1

242-14-00

② 124-27-36

242-13-48

88-07-18

725.97

221.273

725.572

241-02-54

③ 152-05-21

241-02-40

89-22-44

698.60

212.934

698.352

T@ 4 B.S. 3

184-58-24

④ 29-56-18

184-58-09

T@ 7 B.S. 4

122-15-36

89-46-12

398.79

121.570

398.816

8 244-35-00

122-17-30

86-36-30

102.64

31.102

101.861

3-49-24 Angle for P.P.

T@ 9 B.S. 8

75-23-06

80-49-42

109.99

33.536

108.596

10 150-46-12

75-23-06

91-32-18

164.89

55.258

164.819

π @ 12 B.S. 11

70-54-01

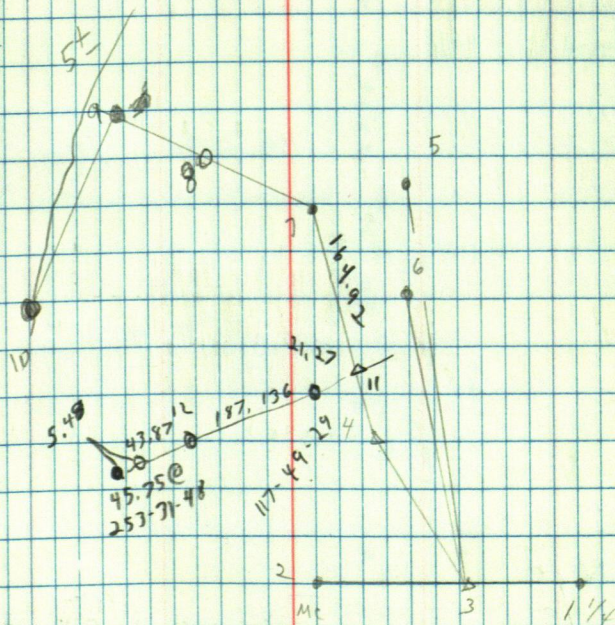
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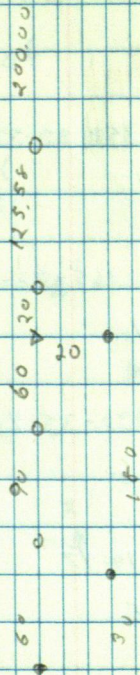
63.534

208.406

E. CURRO
T. VOLLETT 70

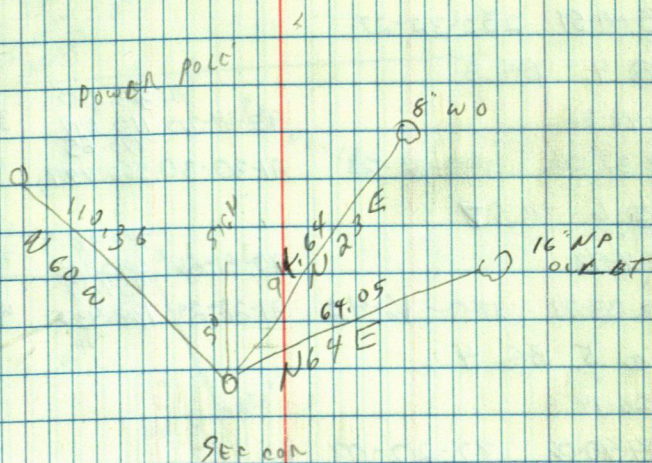
10-8-82





602,895

LK



MARVIN CROSSDIT

T@ 2 BS.1 E 100' OF W 604 GL 1-18-180-31

27-36-18 89-45-18 90-762 297.761

① 175-12-06 87-36-03 90-4454 153.457 503.424

T@ 3 BS.2

252-35-45

① 145-04-54 252-32-27

T@ 4 BS.3

199-48-36 90-48-30 363.00 110.649 362.972

⑤ 39-37-06 199-48-33 91-30-30 266.889 875.328

T@ 6 BS.7

180-16-48 90-51-56 787.98 240.185 787.901

5-00-33-24 180-16-42 91-22-24 138.426 454.029

T@ 5 BS.4

71-28-18

⑥ 174-40-06 87-20-03

T @ A BS B

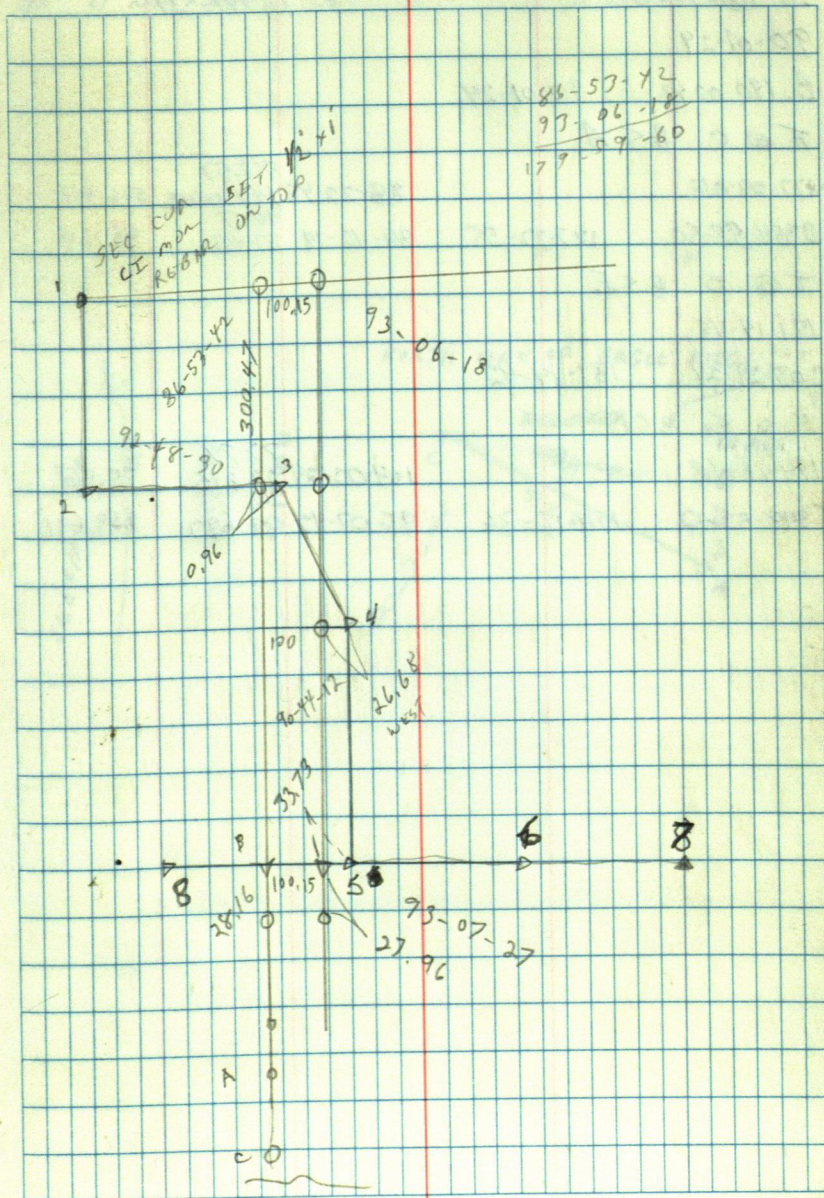
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98-23-24 130.66 37.225 129.261

T @ C BS. A.

92-06-42

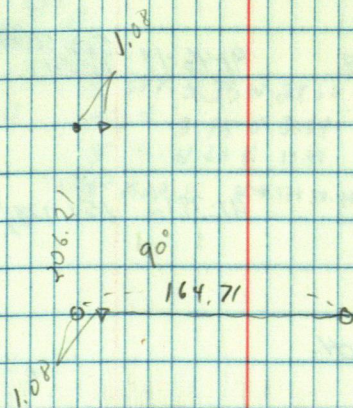
D



LOT 13 SPIDER LA SHORES

164.71
- 1.08
163.63

76



NORM BEBENSEE

732-3024

SUE SCHUOK

π @ 2 BS 1

02-59-18 93-58-48 388.59 387.915

③ 05-58-27 02-59-13 92-04-36 118.436
132.39
40.351 132.30

④ 179-49-36

④ 357-38-37 178-49-18 91-46-18 533.88
162.717 533.607

276-44-42

⑤ 193-24-06 276-44-33 91-34-12 498.61
553 151.978 498.453

π @ 4 BS 2

177-27-18

⑥ 354-54-18 177-27-04

π @ 6 BS 4

181-49-48 93-50-12 293.88
29.373 292.59

⑦ 03-38-48 181-49-24 90-54-27 509.80
553 155.386 509.732

π @ 5 BS 2

83-09-19

8 166-18-42 83-09-21

π @ 8 BS 5

9 70-25-42 571.16
174.026 571.152

10 91-36-24 220.78
67.298 220.699

11 42-24-12 31.13 102.041

12 194-56-30

12 272-52-43 194-56-18 88-25-36 91.47
28.038 91.924

π @ 9 BS 5 21.68

13 268.08-36 19.08

50+ SEC COR
APR 190
70+ BTB

5" SPR 5.35 W 28.80
3" " S 45 E 30.54
3" " N 60 E 19.90
5" MAPLE NORTH 50.49

178-09-59 10

130.53 12

9 13

5 2 5

3

1 84 COR

1 84 COR

$\pi @ 110.5.8.$

107-21-42

115-05-48

⑭ 230-11-18

115-05-39

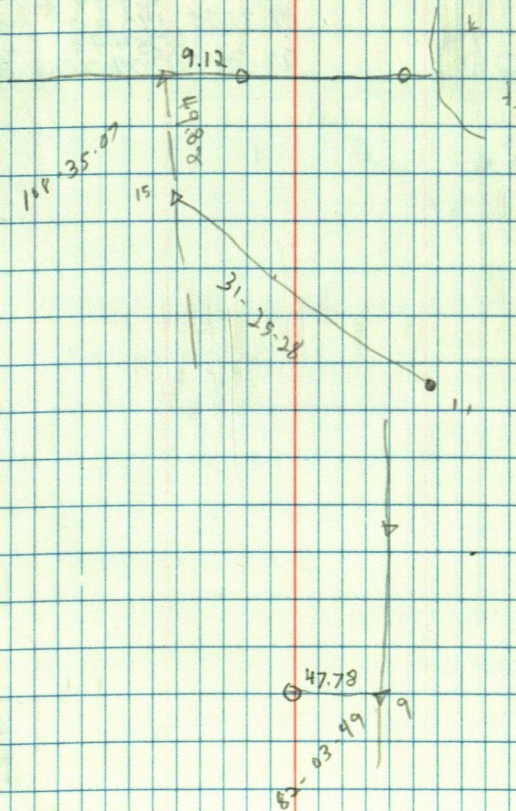
90-02-54

343.92

104.829

343,922

283.75



K6E - N6E - M00 - SH4

T @ B AS A

90-59-06 ^{555.80} 555.721

C 180-68

T @ C B.S. B

B 89.45.54 ^{239.44} 239.441

D 91.31.30 ^{468.84} 468.668

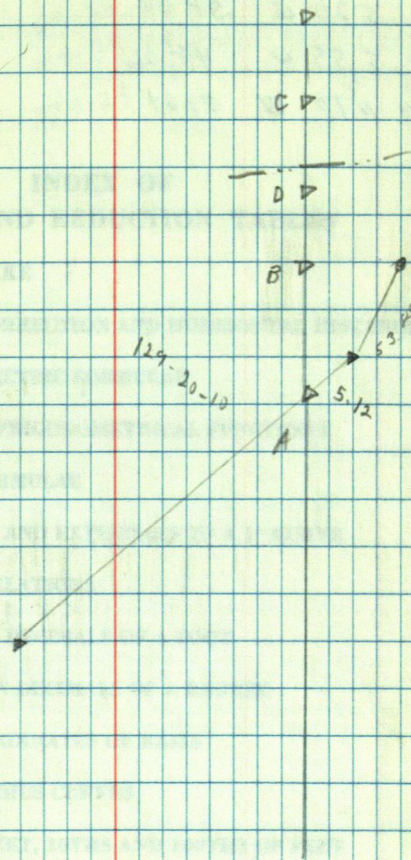
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10' COLD WINDY
BY SNOW

E. CURD
T. VOLCKE

79

11-12-86



BT'S

5 1/4 SEC 23 140-31

6' NO 520 E 58.44

8' NO 555 W 48.06

C 8' ASPEN N 10 ~~E~~ 74.64

5785.64

2104.56

7893.20

7892.95

2405.781

89-39-40

89-39-40

179-29-20

24

5 | 1230
10
23

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Table XI—LINKS IN FEET, 10THS AND 100THS OF FEET



LIETZ

SINCE 1882

FIELD BOOKS

Rain resistant fine quality ledger paper, bound in high visibility chrome yellow imitation leather. Printed in waterproof ink.

Left page: blue horizontal lines; red vertical lines.

Right page: 4 horizontal and 8 vertical blue lines; red vertical center line.

Stock No. 8152-00 Transit Field Book. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Stock No. 8152-05 Economy Field Book. Spiral Bound Paperback. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Left page: blue horizontal lines; red vertical lines.

Right page: 8 x 8 blue lines; red vertical center line.

Stock No. 8152-20 Mining Transit Book. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Left page: blue horizontal lines; red vertical lines.

Right page: 10 x 10 blue lines; red vertical center line. Inch lines heavy.

Stock No. 8152-30 Engineers Field Book. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Both pages: blue horizontal lines; red vertical lines. 6 vertical columns.

Stock No. 8152-50 Level Book. Size $4 \times 6\frac{1}{2}$ inches.

Stock No. 8152-55 Level Book. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Left page: blue horizontal lines; red vertical lines.

Right page: 4 x 4 blue lines; red vertical center line.

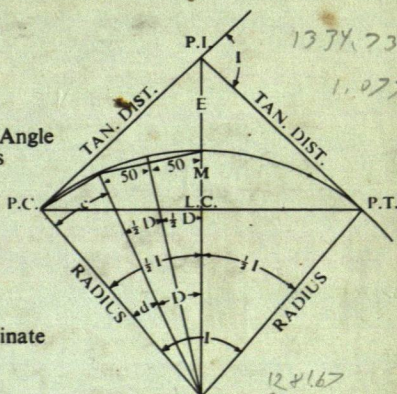
Stock No. 8152-60 Field Book. Size $4\frac{1}{2} \times 7\frac{1}{4}$ inches.

Both pages: 10 x 10 blue lines; inch lines slightly heavier.

Stock No. 8152-75 Cross Section Book. Size $6\frac{1}{2} \times 8\frac{1}{2}$ inches.

CURVE FORMULAE

- D = Degree of Curve
- 1° = 1-Degree of Curve
- 2° = 2-Degree of Curve
- P.C. = Point of Curve
- P.T. = Point of Tangent
- P.I. = Point of Intersection
- I = Intersection of Angle, Angle between Two Tangents
- L = Length of Curve, from P.C. to P.T.
- T = Tangent Distance
- E = External Distance
- R = Radius
- L.C. = Length of Chord
- M = Length of Middle Ordinate
- c = Length of Sub-Chord
- d = Angle of Sub-Chord



$$R = \frac{L.C.}{2 \sin \frac{1}{2} I} \quad T = R \tan \frac{1}{2} I = \frac{L.C.}{2 \cos \frac{1}{2} I}$$

$$\frac{L.C.}{2} = R \sin \frac{I}{2}, D 1^\circ = R = 5730, D 2^\circ = \frac{5730}{2}, D = \frac{5730}{R}$$

$$M = R (1 - \cos \frac{1}{2} I), = R - R \cos \frac{I}{2}$$

$$\frac{E + R}{R} = \sec \frac{I}{2}, \frac{R - M}{R} = \cos \frac{I}{2}$$

$$c = 2 R \sin \frac{1}{2} d, d = \frac{c}{2R}$$

$$L.C. = 2 R \sin \frac{1}{2} I, E = R (\sec \frac{1}{2} I - 1), = R \sec \frac{I}{2} - R$$

Minutes in Decimals of a Degree

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

Inches in Decimals of a Foot

$\frac{1}{16}$	$\frac{3}{32}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{7}{8}$	
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167