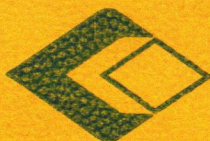


300 B



LIETZ

ECONOMY FIELD BOOK

No. 8152-05

INDEX

1	USFS	TOWN LINE LK	
5	USFS	CLR LK	
6	USFS	GADBOLDT	
7			
8	USFS	TOWN LN	
9	USFS	10 mi. (GADBOLDT)	
10	USFS	CLR. LK	
12	LONNIE	JOHNS	33-139-30
13	USFS	CLR LK	
14	USFS	TEN MILE	
17	USFS	CLR LK	

STA

0+00 \neq PHELOW LK RD

0+? SHOULDER PHELOW LK RD

0+? ~~DI~~ PHELOW LK RD

0+? TOP OF BACK SLOPE

1+00

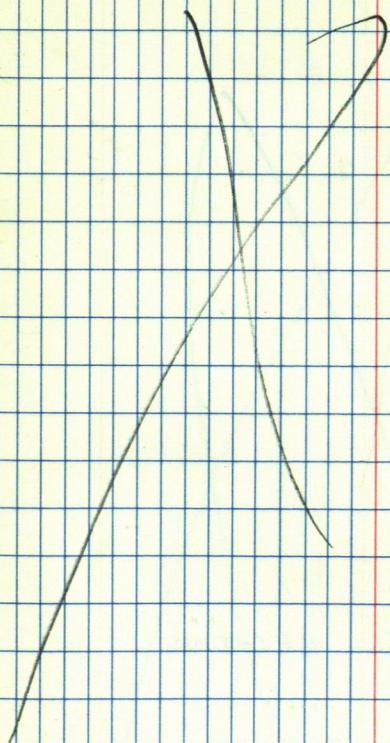
1+20

2+00

2+38 PC

2+50 POC

APPRO 45-48



3+00 POC

EXT

3+50 POC

3+96.95 PT

4+30 WHERE ^{BLV}HILL BEGINS

5+00

5+25 SHOWS HOWE RT & BEGINNING
OF BREAK RT.

5+84 PC

6+00 POC

6+50 POC

6+84 EXT

7+00 POC

7+50 POC

7+79⁸⁶ PT

8+00

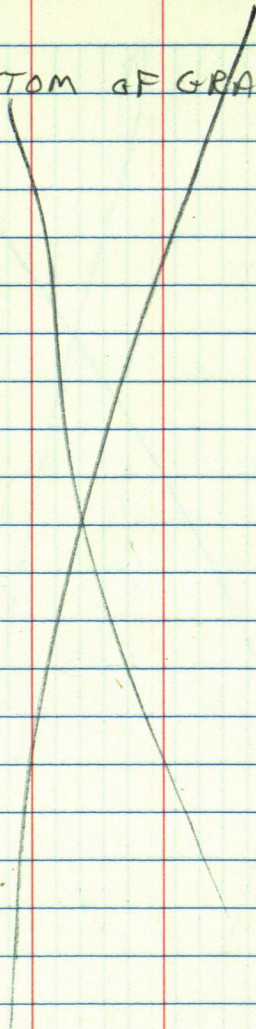
8+50 TOP OF GRADE

9+00

9+50

BOTTOM OF GRADE

10+00



STARTING @ 45+00 XSECTION EVERY
100' DO CURVE TO SHOW
ROUGH TERRAIN

ALIGNMENT BOOKS

SEND XSECTIONS ABOUT WED

LA + H @ 30' NO HUB.

76 2 851

TUN LINE

272-01-06

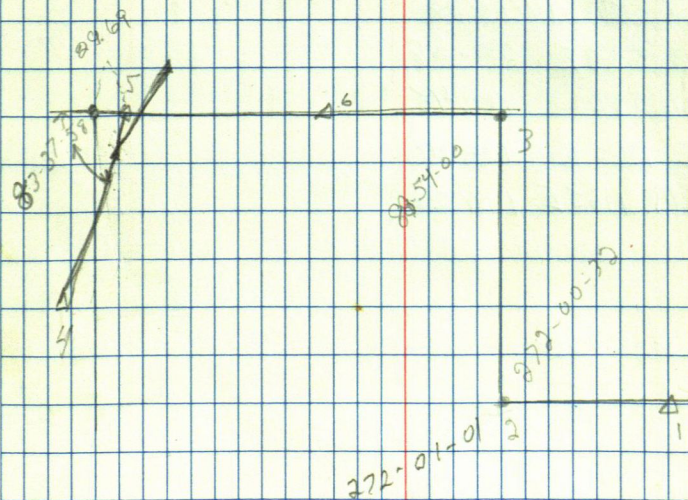
3 84-02-03 272-01-01 90-07-00 1375.06 419.131 1375.072

705854

863-37-46

89-46-48 898.50 273.765 898.493

6 167-15-18 263-37-39 90-50-54 660.18 201.226 660.111



BT'S Town Line

T141NR28W 1/4

15" NRwe N23E 108.95

18" W oak N78E 72.90

5.94" Post 3'4". NE72°

22" UPine S32W 156.40

T141NR28W Sec 8 21/12

20" UPine N64E 187.55

24" Post S43E 61.20

30" W. Pine S55E 103.00

41 53/55

12" W oak W3W 34.30

10" Post S31E 7.20

29" Post S35W 68.70

15" W oak S63W 56.56

Sec 8 21/12 T141NR28

18" W oak S33E 70.06

8" W oak S22W 60.45

6" Post N62W 108.40

30" W. oak N65E 194.26

BTs Town & NE 1/4

(25)

C-E NE 1/4

15" W Oak S 01 W 36.30 S.P. 3'

BASS. 10" S 87 W 63.40

6" ash S 79 W 31.70

C-E E 1/4

(26)

18" W Pine S 15 E 26.75

18" R. Oak S 16 W 13.35 S Post 3'

10" R. Oak N 32 W 12.50

10" Birch N 60 E 13.55

(27)

C-W E 1/4

8" R. Oak N 7 E 6.68

12" R. Oak N 79 E 49.19

10" R. Oak S 35 W ~~6.68~~ 15.55

Sign Post 3 FT ~~15.55~~

(28)

C-W SE 1/4

20" R. Oak S 10 E 14.00

10" Bass. N 12 E 19.00

12" R. Oak S 78 W 16.20

Sign Post 2.50 N 4.08 W

(29)

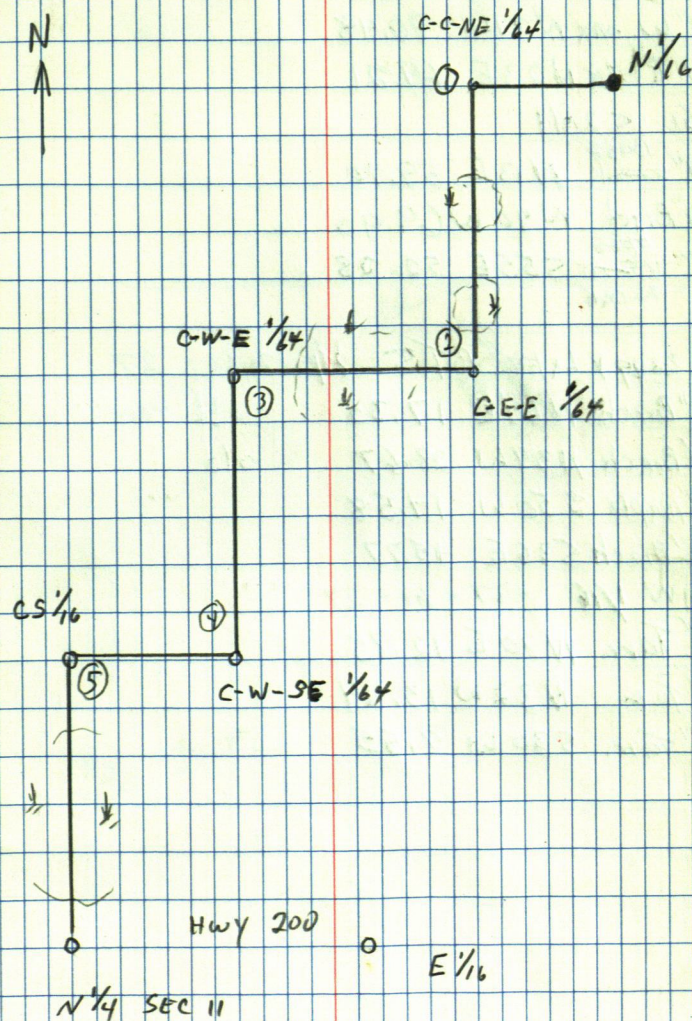
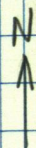
CS 1/6 S 2

12" R. Oak S 45 E 11.45

8" R. Oak S 6 E 18.75

14" R. Oak S 68 W 21.94

20" R. Oak N 60 W 11.55



BTS Turn line

4 52/511 T 141/28

4" R oak S50E 62.40

6" W oak S17W 82.58

14" W oak N31W 70.48

14" R oak N23E 64.21

④ 1/16 S 2611

14" Bass N13E 59.90

10" Birch N40W 69.90

16" W oak S55E 52.28

Boggy Lake BTS 1/4-27-60-27

8" Birch N64E 17.35 old tree

10" Birch N39W 28.67 old "

6" Maple S50W 14.58

12" Birch S36E 15.77

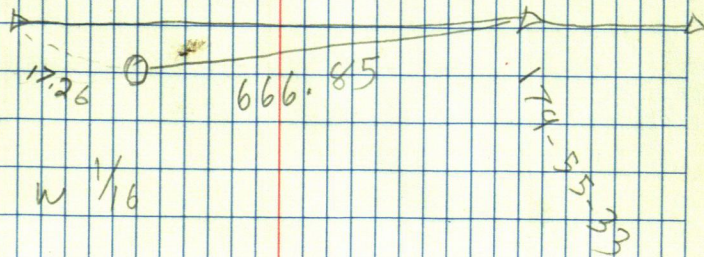
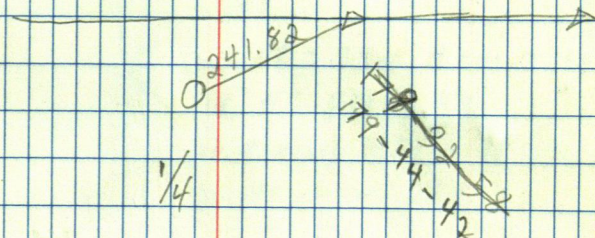
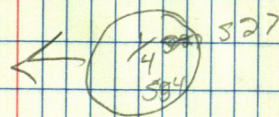
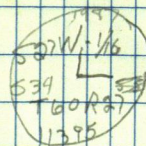
W 1/16 -27-60-27

4" Tam N70E 12.85

12" Tam N32W 13.24

12" Tam S30W 8.55

Sign N $\frac{1}{2}$ E Face
own S $\frac{1}{2}$ W



CLR LX

5

2
66
4
2.67

1/4 14" NP S 39W 4 CTS + LK 2.71m² 1/4
1/4 14" NP SIDE 41.9
25" PINE ST 155E 15'
15" NP NW 28.4

ML

GADADLOT TRLR LOCATION

TC 10 BS BRSS Cup Ely 505'

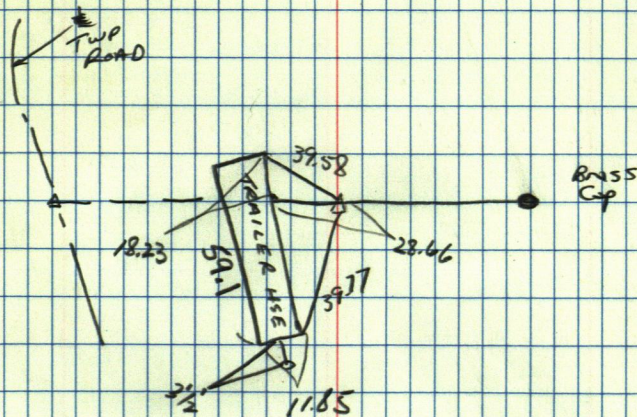
0-0-10

108-55-18 SE COR
 X-108-55-18 ~~SE~~ TRLR HOUSE 39.77
 205-0-38 NE COR
 X-205-0-28 TRLR HOUSE 39.58

Feb. 20, 1988
 Clear -10

Ken
 Tom

6



TUN Line

8

π@2BS1

89-33-04 1409.27
429.547 1409.223
701.69
88-58-30 213.874 701.573

π@4BS3

89-35-46 799.48
243.681 799.456
450.70
93-36-28 137.373 449.804

π@6BS5

8-85-47 268-16-45 91-01-27 153.82
190-05-46 46.883 153.793
268-22-32 335.62
88-22-22 268-16-36 90-51-15 102.298 335.583

π@6BS7

8-01-36
180-01-38 91-43-19
91-44-55
5 271-44-53 91-43-15

π@8BS7

948.25
90-01-19 289.045 948.276
127.89
94-10-14 39.983 127.554

π@10BS9

257.94
89-00-32 78.619 257.899

π@11BS10

659.54
90-17-59 201.045 659.581
503.61
90-59-11 153.498 503.516

π@13BS12

457.09
92-11-48 139.323 456.755
275.91
90-10-26 84.099 275.91

12 13 14

11

10

6 7

8

9

5

4

2

3

1

Ten mile

112 11.15-50

9

T@ 86B585			
0-00-00	180-0-13	87.47-41	713.13
180-00-02		272-12-39	217.364
180-00-13		88-05-59	570.27
87 0-00-07	180-0-05	271-55-20	173.818
			569.948

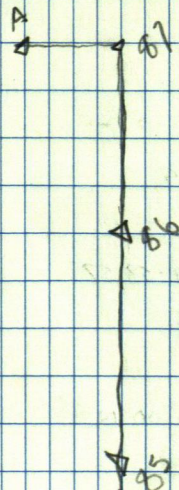
T@ 86B587			
0-00-05	179-59-53		
180-00-07			
179-59-58			
85 0-00-03	179-59-56		

T@ 87B586			
0-00-12		92-03-39	
180-00-04	85-03-53	267-57-01	
85-04-05		100-22-13	
A 265-03-51	85-03-47	259-38-34	

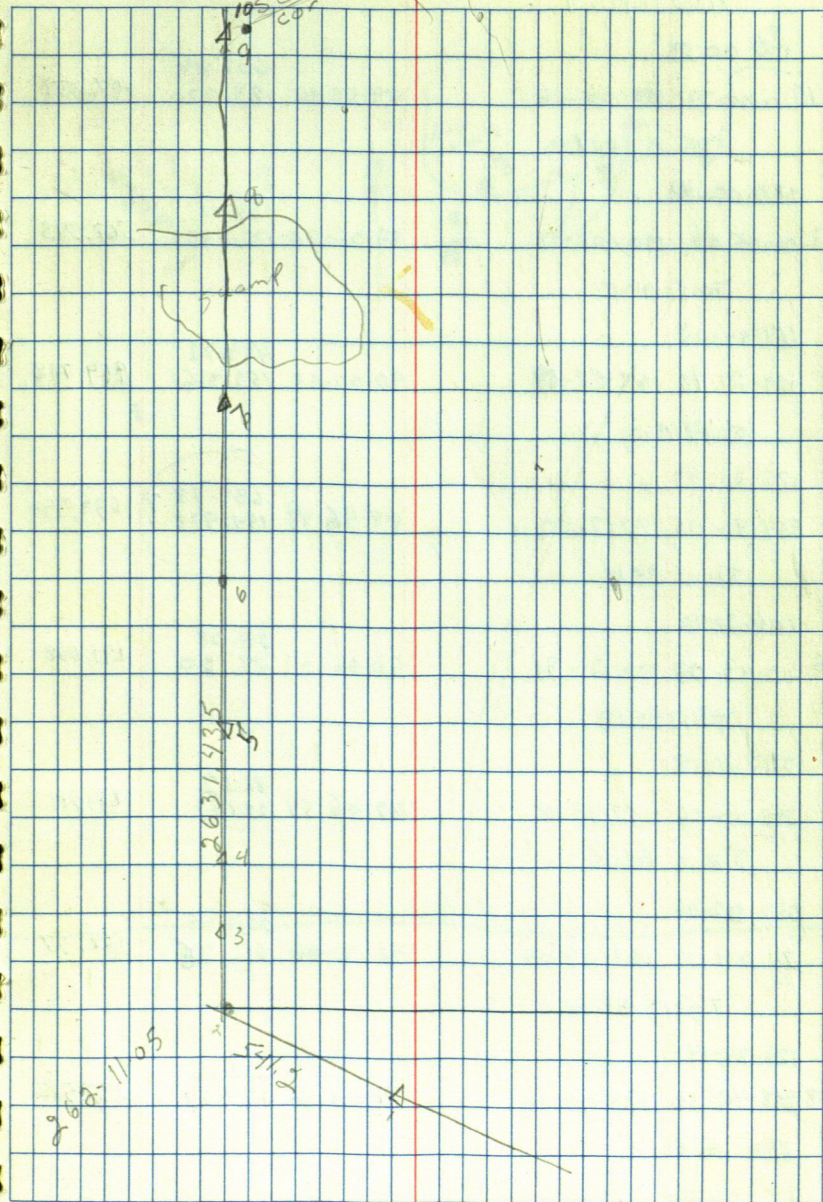
T@ 87B5A			
0-00-13		48.90	
180-00-21	274-56-45	14.907	48.105
274-56-58		570.42	
86 94-56-59	274-56-38	173.863	590.049

T@ A B5 B			
0-00-04	177-08-42	88-07-42	452.46
180-00-04		271-51-41	137.911
177-08-46		81-13-55	48.45
87 357-08-39	177-08-35	278-47-12	14.768
			47.8824

T@ A B5 87			
0-00-03	182-51-05		
179-59-32			
182-51-08			
B 02-51-00	182-51-28		



T@ 2B51			
262-11-05		89-46-54	591.20
164-21-54	267-10-57	88-55-06	408.618
T@ 3B52			
180-00-11		91-16-36	408.648
4 0-00-18		92-50-52	285.676
T@ 4B53			
180-00-01		87-23-36	285.646
5 359-59-54		89-43-30	964.012
T@ 5B54			
179-59-06		90-30-35	964.037
6 359-57-54	179-58-57	89-46-05	973.281
T@ 6B55			
180-00-12		90-19-12	973.307
7 5-00-24	180-00-12	90-16-24	517.659
T@ 7B56			(658)
185-00-00		89-53-18	517.657
8 59-59-40	184-59-50	90-47-36	622.438
T@ 8 B57			(428)
180-00-28		89-20-48	622.419
9 5-00-42	180-00-21	90-02-24	1508.462
T@ 9 B58			(458)
298-29-30		80-01-03	1508.455
10 216-59-23	288-29-41	95-00-30	7.16
T@ 9 B58			
264-59-47		90-01-24	1508.447
11 169-59-02	264-59-31	89-25-30	697.963



USFS
elec lake

TT@ 11 BS 9

180-00-28

12 0-00-33 180-00-16

89-55-36

607.84

185.220

607.832

TT@ 12 BS 11

180-02-48

13 00-05-54 180-02-57

89-36-30

567.41

172.946

567.393

TT@ 13 BS 12

164-44-02

14 229-27-48 164-43-59

90-24-05

499.72

151.316

499.708

TT@ 14 BS 13

177-21-49

15 354-43-05 177-21-32

89-46-48

639.78?

194.975

639.959

TT@ 15 BS 14

106-21-42

16 212-43-08 106-21-31

90-26-12

391.08

88.720

291.068

TT@ 13 BS 12

227-11-18

A 294-22-36 357-11-18

89-06-54

82.52

33.153

82.511

TT@ 16 BS 15

267-02-06

15 174-04-12 267-02-06

90-30-06

200.58

61.135

200.57

TT@ 17 BS 16

129-24-14

18 258-48-32 129-24-16

89-00-20

237.62

72.428

237.586

TT@ 18 BS 17

222-24-42

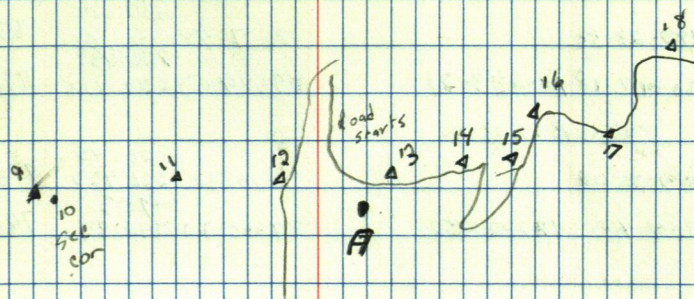
19 84-49-20 222-24-40

87-47-25

348.50

106.226

348.247



8

11

10
5 sec car

8

LONNIE JOHNS

T@ 2 B51

180-23-55	90-27-48	639.60 1941.951	639.578
3 20-47-18 180-23-39	89-49-03	726.43 121.415	726.422

T@ 3 B52

177-21-00	90-17-38	726.45 221.423	726.439
7 354-41-55 177-20-52	89-05-20	1903 24.084	79.02

BT SEC COR

12" R.O. S75E	37.55	old 53
14" R.O. N85E	30.30	53
10" R.O. S59.0	50.42	54

12

1/4
0-29-02 154.72
499.976

1 2 3 4
sec
cor

π@ 19 B 518

CLR LK

164.54-54

20 329.49-54 164.54-57

89.37-33

472.68

144.071

472.664

π@ 20 B 519

199.58-48

21 39.57-24 199.58-42

90.28-06

372.87

113.650

372.854

π@ 21 B 520

123.45-56

22 267.31-48 123.45-54

89.53-36

540.99

164.895

540.989

π@ 22 B 521

275.14-24

23 190.28-36 275.14-13

87.51-08

278.58

84.915

278.389

π@ 23 B 522

211.30-13

24 63.01-06 211.30-33

89.49-48

838.15

255.482

838.141

π@ 24 B 523

190.49-00

25 21.25-42 190.47-51

90.14-29

883.13

269.178

883.118

π@ 25 B 524

189.29-30

29 18.58-45 189.29-22

90.19-30

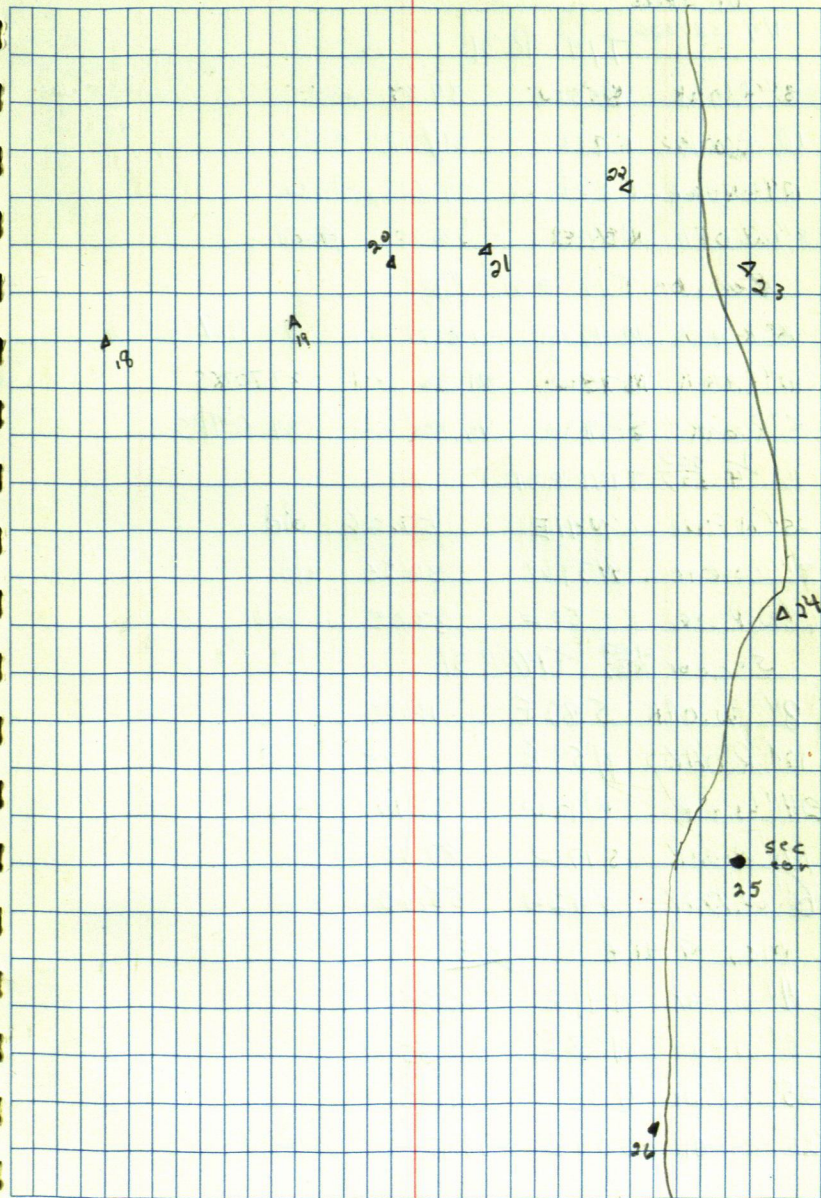
1312.54

400.062

1312.513

4101
Windy 58°

13



BT Trees

1/4 527526

T141 R.31

8" R. Oak S53W 34.89 old
 10 R. Oak N85W 34.40 old
 12" W. Oak N03E 39.60 New
 8" W. Oak N39E 10.70 Dead

Sec cor T141-R31 $\frac{89.83}{87.50}$

12" R. Oak N46E 18.71 old 10.907KS
 12" R. Oak N75W 21.38 old 33.707KS
 8" R. Oak S39W 14.50 old 34.607KS

1/4 527

T141 R31W

25" N. Pine N41E 57.26 old
 8" W. Oak N39W 36.25 old
 6" N. Pine S50E 33.05 old

Sec cor $\frac{21.22}{20.27}$

T141 R31

8" W. Oak S82E 16.05 old
 12" R. Oak N59E 21.95 old
 24" W. Oak N12W 32.10 old
 14" W. Oak S17W 87.90 old
 16" W. Oak S42W 55.60 old

mc, T141 R31 $\frac{28.27}{28.27}$

14" W. Oak N41E 65.25
 25" W. Pine N28E 32.65
 25" W. Pine N35W 12.85
 25" W. Oak S54E 18.90

Section ⁸²¹²⁷₂₁₂₄ T141 R31

6" W. oak S 38 W 45.15
 25" N. Pine N 34 W 35.20
 12" R. oak N 27 E 41.15
 10" R. oak S 59 E 33.23

1/4 ⁸⁷₃₄ T141 R31.

10" W. oak S 34 W 34.85
 8" W. oak N 53 W 36.54
 14" W. oak N 14 W 45.22

Section ²²⁸⁵₄₅₅ T141 R31

118" N. Pine N 43 W 76.46
 12" W. oak N 55 E 51.90
 20" N. Pine S 24 E 83.19
 10" R. oak S 25 W 49.40

TO A B S G

C 236-12-46

89-28-42 391.44
119.357

16

4A

4B

4C

Clear 19K4

T@2BS1

156-51-04

90-09-06

272.15

272.146

③ 313-42-09 156-51-04

90-07-36

278.469

913.603

T@2BS2

4

90-03-06

492.14

492.144

T@5BS4

91-08-17

90-04-24

1350.02

1350.016

6 192-16-42 91-08-21

90-03-18

587.95

587.952

T@6BS5

7

90-05-06

587.96

587.956

90-06-48

691.45

691.451

T@7BS6

8

89-59-36

691.47

691.47

90-59-00

345.40

345.348

T@8BS7

9

89-12-30

345.36

345.32

90-43-30

373.16

373.127

T@9BS8

10

89-30-06

373.15

373.136

89-52-18

109.44

109.437

T@9BS8

195-46-11

⑦ 31-32-06 195-46-03

90-55-18

131.89

131.872

410

411

A9

A8

A7

A6

578

578

557

557

44

$\pi @ 11859$

131 17-49-46

83.40

12 32-05-07

39.64

14 52-15-24

28.25

15 99-15-24

41.50

18 152-43-00

63.81

16 154-49-12

55.75

17 162-42-09

58.50

 $\pi @ 11859$

147-15-36

89-42-09

131.86

40.192

131.859

123.39

19 294-31-12 147-15-36

95-59-59

37.610

122.715

 $\pi @ 198511$

123-28-37

84-38-10

123.19

37.547

122.648

20 246-56-53

123-28-27

89-57-59

1378.34

420.121

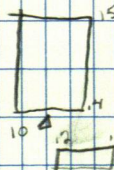
1378.339

10

19ke

19

16 17



19

Gerald Davidson

22

391.66

89-28-42

119,379

698
821
170529

667.40¹⁰
666.85
25

517.60
62.51

1140.12

1111
408.55
285.94
964.03
1659.72