

108

Remer

1

Levels

J. M. Greene

☆1145

3.90 C-50  
2.42

6.32

3.35 C-100  
2.47

6.32

3.80 C-150  
2.52

6.32

4.40 C-200  
1.92

6.32

3.50 C-250  
2.82

6.32

3.60 C-300  
2.72

3.00 C-350  
2.32

3.29 C-400  
2.03

6.32

3.500

4.47 C-450  
1.83

6.32 C-500  
4.00

4.32





$$\frac{4}{10} = \frac{x}{12} \quad 4.8 \quad \frac{3}{10} = \frac{x}{12}$$

# Preliminary Levels

+ S H.I. - S Elev. Obj

100.00 B.M. X

3.05 103.05

2.73 100.320 Iron Mon.

3.04 100.01 Big Granite

0.12 100.13

3.54 96.59

~~2.54 97.59~~ X on E. side

3.34 96.79 Water Table

3'10" 3.88 9 99.59

101.42

~~5.7~~  
3.8 1/2 95.7

5.75 95.67

5.35 96.07

~~5.42~~  
101.45 5.35 96.1 A + 1

~~4.10~~  
4.9 96.5 B + A<sub>1</sub> + 2

~~4.6~~  
4.5 96.9 C + B<sub>1</sub> + A<sub>2</sub> + 3

~~4.12~~  
4.1 97.3 D + B<sub>2</sub> + A<sub>3</sub> + 4

$$\frac{5}{70} = \frac{x}{72}$$

$$\frac{10}{12} = \frac{x}{10}$$

$$\frac{1}{10} = \frac{x}{12}$$

10x

for Streets

Cross on stone step of Bank.

rock on Main St. T.P.

school house steps - Top.



2

B.M. #1 - First State Bank

B.M. #2 - Remer School

B.M. Rock in Ravine

+S	H.I	-S	Elev.	Object
		5.75	91.08	#2
5.28	97.61 96.83		92.33	
	97.78		91.55	T.P. #1
		6.6	91.01	#1-S
			90.23	
		4.77	91.55	#1 Ground
		4.77	91.55	T.P. #2 from #1
3.62	95. 96.32		92.70	B.M. Rock
		5.03	91.29	#3 Spike flush

Base #2 + #3  $\angle R \Delta 2$ 

+S	H.I	-S	Elev.	Dis.	$\angle s$
Upper	Lower	Middle	95.32		
1.5	0.1	0.8	95.52	140'	69°35'
1.71	.32	1.02	95.30	139'	107°30'
5.25	4.025	4.64	91.68	123'	185°18'
4.14	3.19	3.66	92.66	95'	266°55'
5.19	3.88	4.54	91.78	121'	330°14'
6.09	4.01	5.04	91.28	208'	#3

Base #3 + #4  $\Delta 3$ 

3.66	96.36	3.66	92.70	B.M. Rock
4.18	2.82	3.5	92.86	136' 32°24'
3.19	1.32	2.25	94.11	187' 64°
4.22	3.06	3.64	92.72	116' 109°40'
4.75	3.30	4.02	92.34	145' 121°30' $\angle$ to I.M
				36°45'



= 100"

2

97.59

91.70

92.70

+S. H.I. - S. Elev. Object

Base #4 + #5 - #4

92.90

B.M.

95.42

91.70

372 96.42

Dis Ls

H L M 91.15

4.9 3.65 4.27 92.15 125' 70°31' L

4.31 2.3 3.3 93.12 101' 33°40' L

5.5 4.17 4.84 91.58 1133' 27°30' R

5.2 91.22 #4 Flush?

4.37 96.42

92.05

#5 Top of stake

Baseline #4 + #5 - #5

4.46 96.61

90.72

5.19 4.39 4.79 91.82 80 127°55' R

5.89 4.12 5.0 91.61 177 154°10' L

6.12 4.26 5.2 91.41 186 180°00'

2.6 0.88 1.74 94.87 172 81°15' L

2.47 1.38 1.92 94.69 109 33°22' R

5.96 98.01

92.05

7.15 4.8 5.8 92.71 235.5 #6

at N.E. Cor. of Townsite



100.35  
4.17  
96.18

set up + 06 sight back to 5

92.05  
8.3  
100.35

3

#6 + #7 - A #6

+S H.I. -S Elev. Obj.

98.01 #5

98.01  
92.01  
92

2.18 0.71 1.44 96.57 147' 42° R

3.06 1.49 2.28 95.73 157' 72° 30' R

3.95 1.54 2.74 95.27 241' 137° 13' L

2.75 0.91 1.83 96.18 184' 79° 45'

2.72 1.3 96.71 06 285' Δ 7

8.3 10.37 8.3 96.71 07 240.6

5.36 2.97 4.17 97.20 08 241' 154° 37'

#7 + #6 sighting back

4.57 3.4 4.0 130° 30'

4.91 3.3 4.1 91.20 181° 25'

6.5 5.35 5.93 On line 268

4.55 3.28 3.92 101.57 238° 10'

5.22 4.26 4.74 100.01 290° 50'

8.3 6.64 7.47 338° 05'

7.83 97.18 On Ice

2.66 96.37

5.84 8.3

3.49 101.67



B. M = nail in J. Pine stump

+S H.I. -S Elev. Dis Obj.

5.32 106.24 100.92

H. L. M.

10.6 52 7.9 98.34 540'

5.15 101.09 #9 on Hub.

11.0 7.1 9.04 97.20 391.2' #8 " Hub.

#8 5.45 #7

929 7.88 8.59 93.52 141 On ice

4.91 102.11 97.20 #8

5.45 5.45 96.66 #7

2.10 102.9 100.92

97.7 5.2

96.54 6.4"

97.46 6.36

96.82 5.44

6.1

6.08

Cor. Blk 7 - N.E. = 100.92'

N.E. Cor. Blk. 7 - - #9 978.4'

N.E. Cor. Blk 7 + Sta. 9

Sta. 9 + #8 - 12042' E



N.W.I.M to N.E.I.M.

Mag.  
Bearing Distance

N.E.I.M - 0 #1

A. 308.9

0#2 - 0#1

156

0 #3-02 N. 7° E.

210'

0 #4 N. 16° W.

0 #5 N. 25° W

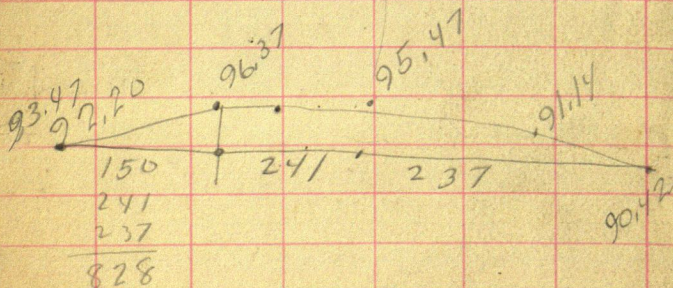
0#1-5 S. 52° E

" 6" - 02 N. 30° W.

① 1-S S.22°E

01 - 02 - 03 N. 69° W.

07 - 08 N. 60° W.



29003





## Hubs

#8 Hub 3"

#7 " 6"

#6 " 6"

#5 " 7"

#4 Spike Flush

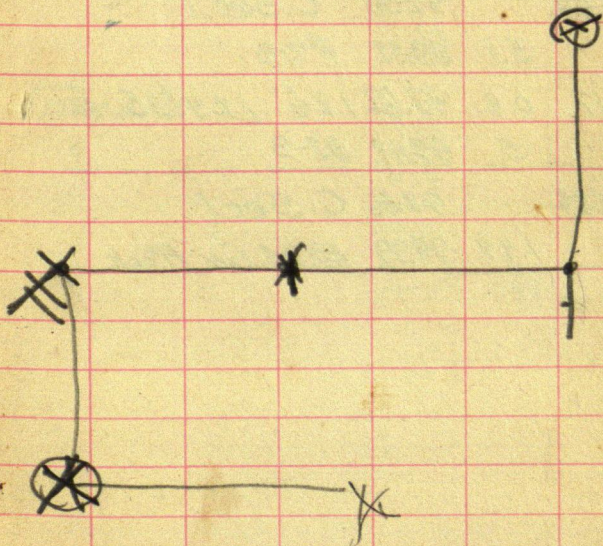
#3 " "

#2 S .3

IS	H.I	- S	Elev.	Obj	Setup
5.28	97.83		91.55	#2	#1
			90.23	02	

3.62	96.32		92.70	0 B.M	02
------	-------	--	-------	-------	----

4.77	91.55		T.P.		
------	-------	--	------	--	--





	H.1			
3.55	<del>95.88</del>		92.33	Ground #1
	<del>95.10</del>		91.55	Top #1
		4.7	91.18	#2 ±
1.16		0.52	95.36	128' 242°34'
3.0	7.63	2.25	93.63	137' 307°
		2.97	92.91	C. Sec. 1
		5.78	90.10	#2-S Top
1.56	94.42		92.86	C. Sec. 1
		5.1	89.32	#2-S
1.43	0.17	0.8	93.62	126' 124°35' E.
		5	89.42	#3-S
8.4	101.26		92.86	C. Sec. 1
		1.27	99.99	B.M. Gr. Rock

101.28  
8.4  
92.88

$$\begin{array}{r}
 93.21 \\
 8.3 \\
 \hline
 102.51 \\
 4.17 \\
 \hline
 98.34
 \end{array}$$

7

4.22 101.42 97.20 #8

4.8 96.62 #7

8.35 93.07 #6

3.4 96.47 #

4.48 91.99 #5 92.05

from #1-5 1-5

$$\begin{array}{r}
 90^{\circ}23' \\
 35 \\
 \hline
 93.78
 \end{array}$$

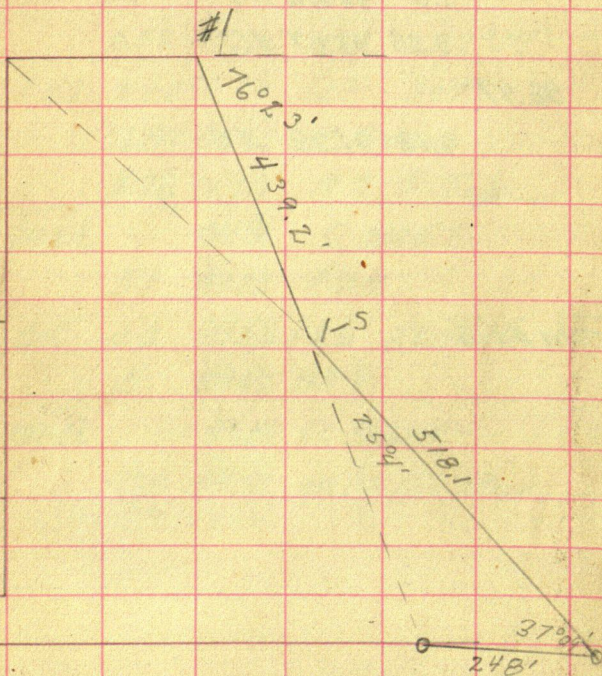
$$\begin{array}{r}
 90.23 \\
 4.7 \\
 \hline
 94.93 \\
 2.97 \\
 \hline
 91.96 \\
 8.4 \\
 \hline
 100.36 \\
 8.4 \\
 \hline
 91.96
 \end{array}$$



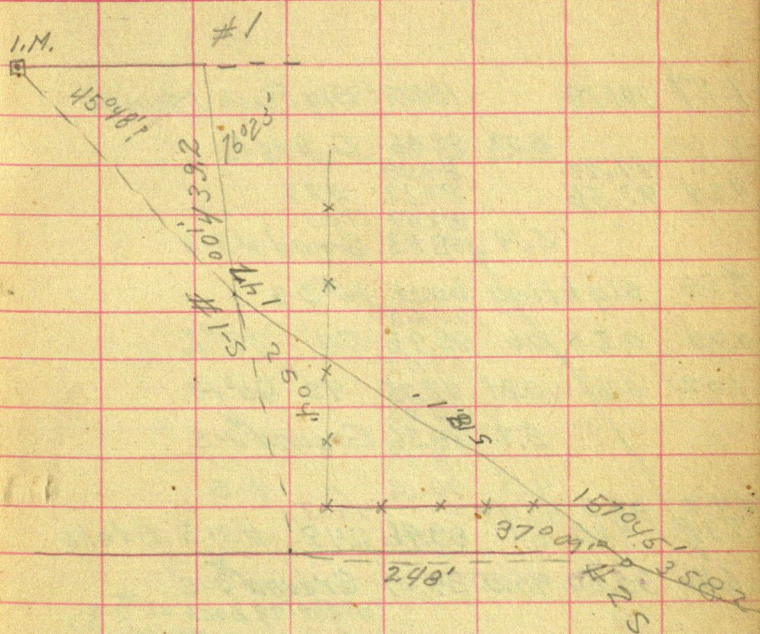
#1 439.2 #1-S

#1-S

#2-S



#2-S

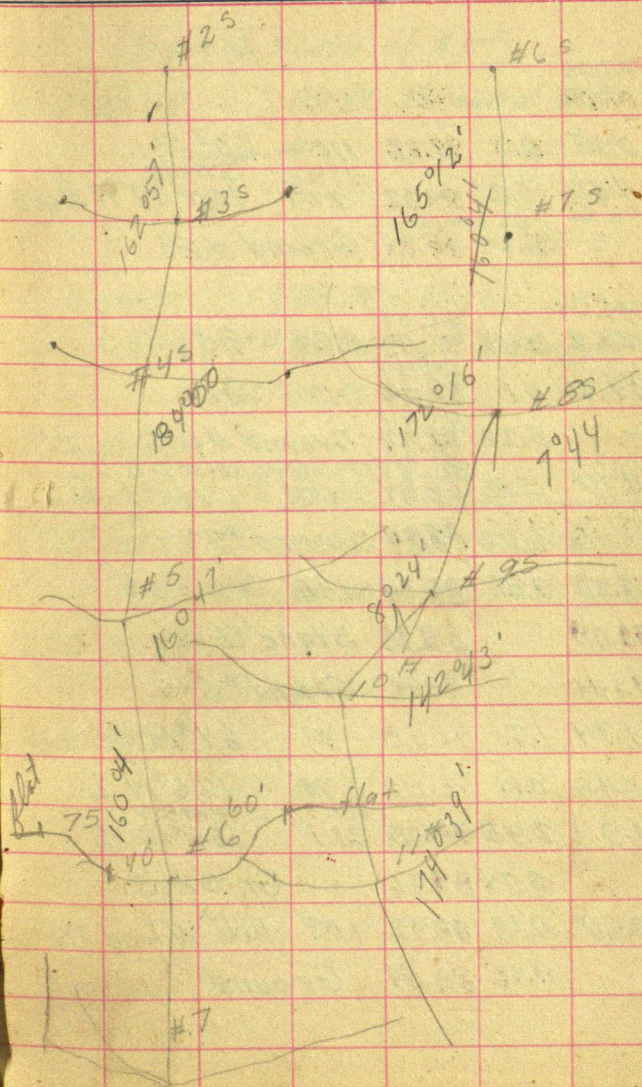




T.P. Hub C. sec. 1 running S.E.

1.17	101.18	100.01	Big Rock Main St.
---	8.32	92.86	C. Sec. 1
4.24	<del>99.23</del> 93.56	<del>89.99</del> 89.32	#2 S
	5.14	<del>89.09</del> 88.42	check Ground #3-S
#3-S	sighting	back to #2-S	
0.95	0.25	0.6	70' 72° L
1.02	0.6	0.81	42' 90° R
	5.2	<del>89.03</del> 88.36	Ground #3-S
	4.15	<del>90.08</del> 90.08	" 4-S
#4-S	95.5	95.56	250.2'
7.34	4.85	6.1	89.46 249' #3-S Stake
6.41	<del>95.60</del> 95.50	<del>89.09</del> 89.09	Ground #3-S sighting back to #3-S forward to #55/184° L
1.00	0.44	0.72	94.78 56' 51° L
1.95	1.07	1.52	93.98 88' 110° R
	5.17	<del>90.33</del> 89.73	Stake #5-S
	5.42	<del>90.08</del> 90.08	Ground #4-S
6.05	2.77	4.42	329.5' 328' #4-S Stake
5.00	<del>95.08</del> 95.08	<del>90.08</del> 90.08	Ground #4-S
	5.18	<del>89.90</del> 89.90	" #5-S
#5-S			sighting back to #4-S 160° 47' R.







#5-S

95.08

94.38

1.25 0.15 0.7 94.38 110' 60° R  
 6.94 4.65 5.8 89.28 228.8. Stake  
 229 160° 47' R #6-S  
 6.24 88.84 Ground #65

#6-S

94.06

90.21

89.90

4.87

2.62

3.75

90.31

225

Stake 5

94.00

4.1

91.33

89.90

G.5

5.22

88.84

Ground #6-S

5.87

4.37

5.12

88.74

150.2

Stake #7-S

150'

160° 4' L

#7-S

6.02

88.04

Ground #7

4.55

3.07

3.81

88.84

148'

Stake 6

3.81

93.09

89.28

Stake #6-S

4.26

93.10

88.84

Ground #6-S

2.05

1.34

1.7

91.40

71"

64° R

1.16

0.46

0.81

92.29

70'

126° 14' L

4.01

1.9

2.95

90.15

213.5

Stake 8-S

211'

165° 12' L

3.74

89.36

Gr. #8-S

4.71

3.64

4.18

88.92

107'

Hub<sup>x</sup> w. line Patton's

4.56

88.54

Ground



# Setup South of #6-S

10.3 98.44 88.84 Ground #6-S

6.6 91.84 60'N

5 93.44 115N-S

1.1 97.34 same for #5-S - South 75'S

11.0 99.94 88.94 Hub<sup>x</sup>

5.00 94.94 at setup 400±N

0.42 99.52

5.06 104.58

11.72 92.86 C. Sec. 1.

4.24 104.25 100.01 B.M. Granite Rock

4.9 99.35

2.42 101.77

11.8 89.97

4.05 94.02

5.25 88.77

92.86  
92.14  
72  
88.97  
88.72  
171  
80

.63



88.75 = Mean of 2 levels run to B.M.

Sta 8-5.

94.59

94.43

88.92 Hub<sup>x</sup>

6.2 5.16 5.67 104' Hub<sup>x</sup>

5.65 88.94 #7-S stake

6.55 88.04 Ground

5.27 89.32 Ground #8-5

2.85 2.1 2.48 92.11 75' 124° L

4.27 3.63 3.95 90.64 64' 87° R

8.13 6.1 7.11 87.48 204.6' Stake 172° 16' L #9-5

#9-5 7.7 86.89 Ground #9-5

2.15 92.39 90.99 90.15 Hub #8-5

2.93 92.39 90.87 89.32 Ground #8-5

5.42 86.88 Ground #9-5

1.6 1.08 1.34 87.26 52' 53° 30' R

4.26 3.55 3.9 71' 120° 30' L

6.35 4.67 5.5 86.80 172.1 188° 24' R

168' Stake 10-5

6.03 86.27 Ground -10-5

#10-5 91.52 4.9 3.2 4.04 87.48 70' Hub #9

91.52 4.64 86.88 Ground #9

2.65 1.97 2.31 68' 67° 30' R

5.3 86.22 Ground -10-5



$8945 \quad 8866 \quad 12$   
 $215 \quad 293$   
 $9160 \quad 9159$   
 $8328$

$91.52$

$807$   
 $22$   
 $53$

$9056$

1.66

38'

124°31' L

7.23 4.75 6 85.52 <sup>248.6</sup> 248 Stake 142°43' R-#11-5

6.59 84.93

Ground #11-5

#11-5 90.70

4.55 1.05 3.3 86.80 350 Stake #10-5

90.10 3.84 86.26

Ground #10-5

1.48 1.0 1.24 48' 112°30' R

5.22 84.88

Ground #11-5

11 0.43 0.76 67' 100°47'

5.28 2.48 3.88 86.22 <sup>281.6</sup> 280 Stake #12-5

4.66 85.44

Ground #12-5

#12-5

90.53

3.78

6.6 3.78 5.2 85.52

282 Stake #11-5

90.88 5.8 84.88

Ground #11-5

6' Rise 5.28 85.29

0.87 0.49 0.68 38' 86°30' R

2.6 2.22 2.41 38' 110°15' L

7.75 5.45 6.6 84.12 <sup>231</sup> 230 165°24' L #13-5

#13-5 88.62 7.32 <sup>83.40</sup> 83.24 <sup>81.50</sup> 83.40 Ground #13-5

88.46 2.4 4.6 <sup>86.22</sup> 84.12 Stake #12-5

88.64 3.2 85.44 Gr. #12-5



88.64

5.24 4.89 5.06

35' 18°30' R

5.28 82.36

53°13' R

50'S

90.

6.0 4.32 5.16 83.48

<sup>168.2'</sup>  
168' 160° #14-S

#14-S 88.11 5.64 83.00

4.9 88.16 3.2 4.04 84.12

170' stake  
#13-S

88.18 4.78 83.40

Gr. #13-S

5.17 82.99

Gr. #14-S

6.1 5.4 5.75 82.41

<sup>71.4'</sup>  
70' 149°44' L  
Stake #15-S

#15-S 87.20 5.8 82.36

Gr. #15-S

4.07 3.37 3.72 83.48

70' stake  
#14-S

87.20 4.21 82.99

Gr. #14-S

96.2 10.9 76.30

<sup>252.8'</sup>  
150°52' R #16-S

11.78 10.55 11.78 75.42

<sup>123'</sup>  
246' Gr. #16-S

---

14

to stake on S. fence Pattens



11.42 100.34 88.92 Hub<sup>x</sup>

2.02 98.32

6.05 104.37

5.21 99.16 1/16 Cor.

8.44 95.93

3.34 99.27

7.83 91.44

1.67 93.11

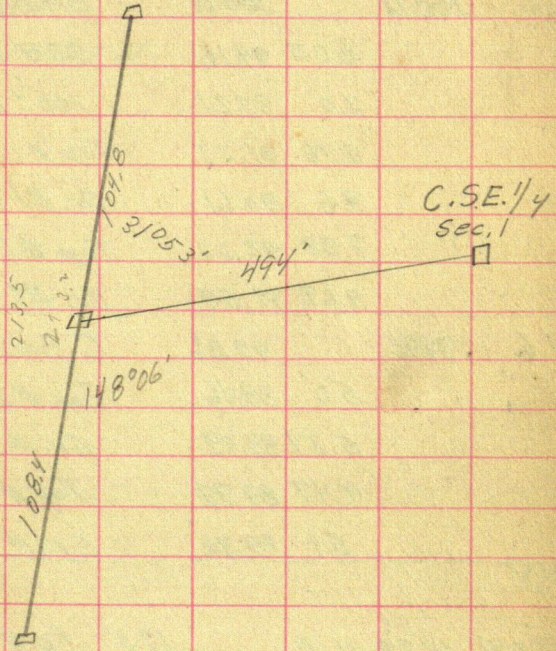
11.1 82.01

2.16 84.17

1.81 82.36 #15-S stake

7.91 76.26 #16-S "

11.15 73.02 Water level





0.2	100.21	100.01	Granite Rock
	6.05	94.16	335' E of
	3.0	97.21	100' E ..
	8.98	91.23	Top #1-S
	9.6	90.61	Gr. #1-S
	7.88	92.33	Top #1
	8.62	91.59	Gr. #1

1.6	94.46	92.86	C. Sec. 1
	5.0	89.46	Top #3-S
	5.37	89.09	Gr. #3-S
	4.47	89.99	Top #2-S
	5.1	89.36	Gr. #2-S

at Y	84.41	11.15	173
12.02	10.29	11.15	173' to #13-S
11.53	8.6		
12.02	10.29	11.15	
95.56	5.0	90.56	Y

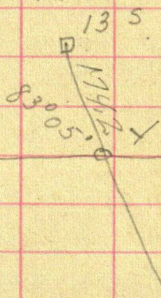
8.4	6.47	7.44	88.12	Top of Rock, South
	7.95	87.61		Marsh

N. side 1st Alley N.

.. ..

1/16 Cor 423.2

on E line 500 ft



end of marsh

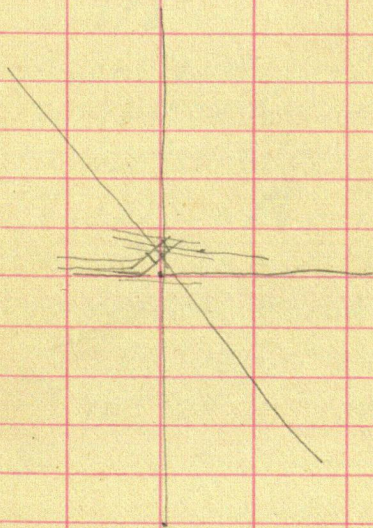


Tops

424 94.23

89.99

#25



4.24 94.23

89.99

Tan

358.2	#2	157°45' R	22°15'	.40911
250.2	3	162°57' L	17°03'	.30669
329.5	4	176° L	4°	.06993
228.8	5	160°47' R	19°13'	.34856
150.2	6	160°04' L	19°56'	.36265
213.5	7	165°12' L	14°48'	.26421
204.6	8	172°16' R	7°44'	.13580
172.1	9	171°36' L	8°24'	.14767
248.6	10	142°43' R	37°17'	.76134
281.6	11	174°39' R	5°21'	.09365
231'	12	165°24' L	14°36'	.26048

13



B.M. Rock. Hote / Cor.

- S H.I. + S. 100.12

6.39 106.51

5.31 101.20 Soo Grade by depot

5.72 100.79 T.P.

2.34 103.13

2.52 100.61 Road <sup>by track</sup> at turn A

9.3 93.83 Low place in road

10.44 92.69 Ice in Bog

7.4 95.73 Rock Cor. Steven's

4.31 100.04

5.37 94.67  $\frac{1}{4}$  line \ Steven's

4.91 95.13 120' E

6.74 93.30 360' E

6.04 94.00 275' S

5.8 94.24

5.94 94.10

6.00 94.04 500' N

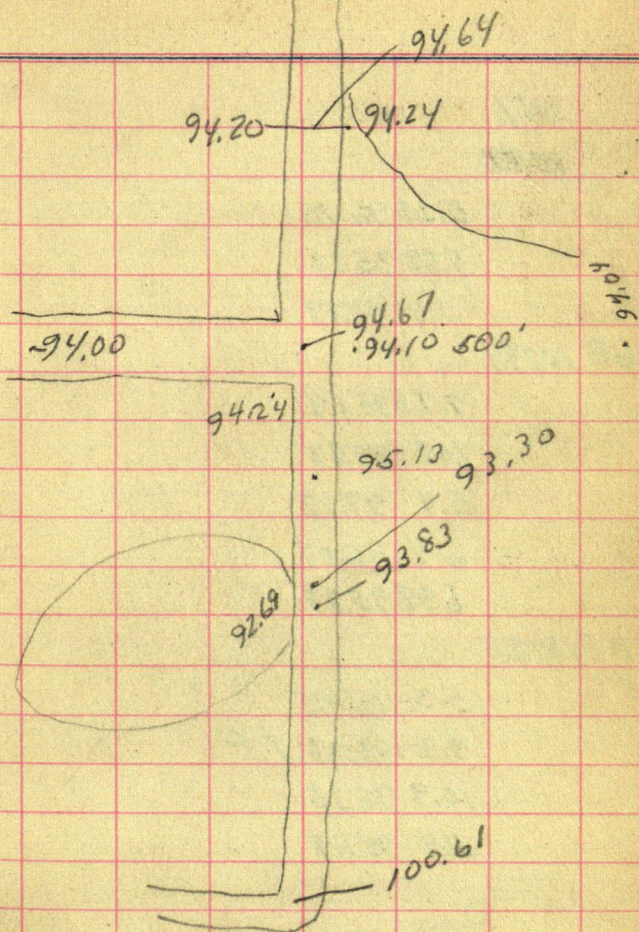
5.8 94.24

5.85 94.20

5.4 94.64  $\frac{1}{4}$  Road 600' W.

6.76 101.40

18





H.I.

101.40

5.25 96.15

5.57 95.83

5.61 95.79

6.68 102.37

7.25 95.12

7.05 95.42

5.4 97.07

6.4 96.07

6.92 95.45

11.8 101.725

5.3 101.95

9.3 97.95 T.P

10.9 96.35

11.4 95.85

95.87

96.37 19

500'

97.97

200'

101.97

95.47 250'

2.50

97.

96.

200'

116

95.32

95.79

95.14

600' 91.64 200' 300'

96.13

95.83



104.55  
~~105.38~~

Elev

97.95

7.43 5.8 6.6 97.79 163' T.P.

5.15 99.40 1st set up

11.73 7.45 9.64 94.91 428' T.P.

4.17 1.83 3.02 234'

97.93

5.00 92.93

5.20 92.73 2nd Set up

6.92 4.58 5.74 92.19 234'

7.25 4.41 5.82 285'

98.01

5.21 <sup>92.80</sup>  
~~92.80~~ 3rd

11.05 6.93 8.97 89.04 412'

11.75 105.79 94.04

94.04 10.45 95.34

11.7 4.32 101.47

105.7 10.34 95.45

37 99.15 10.45 95.34

5.8 93.35

10.34 95.45

$$\begin{array}{r}
 90.08 \\
 + 8.82 \\
 \hline
 99.70 \\
 - 53.72 \\
 \hline
 95.98 \\
 + 9.08 \\
 \hline
 104.06 \\
 - 5.35 \\
 \hline
 98.71
 \end{array}$$

$$\begin{array}{r}
 +s \quad -s \quad 89.84 \\
 + 8.82 \\
 \hline
 97.86 \\
 - 3.72 \\
 \hline
 94.14 \\
 + 9.08 \\
 \hline
 103.22 \\
 - 5.35 \\
 \hline
 97.87 \\
 + 7.5 \\
 \hline
 105.37
 \end{array}$$

$$\begin{array}{r}
 105.37 \\
 + 3.66 \\
 \hline
 109.03 \\
 - 3.56 \\
 \hline
 105.47
 \end{array}$$

Rock Stevens 95.82  
Cor.

$$\begin{array}{r}
 105.47 \\
 - 10.81 \\
 \hline
 94.66
 \end{array}$$

$$\begin{array}{r}
 95.45 \\
 3.7 \\
 \hline
 99.15 \\
 5.8 \\
 \hline
 105.03
 \end{array}$$



5.72 102.19

96.47 I.M. north W. Cor

46.6 97.53 135 paces N on Road

8.2 93.99 175 " N

8.67 93.52 E of Road

6.66 95.53

May 8, 1914

Leo Penn

J. M. Greene

1st Set up S.E. Cor. of N.W. 1/4 - N.W. 1/4 - Sec.

-S H.I. +S Elev Dis 100.92 B.M.

2.65

103.57

Lower

5.54 6.43 97.14 178

W. on S. Line

6.27 2.24 4.25 99.32 403

W. " " "

5.1 98.47

Cor 1st S.U.

3.43 100.14

T.P. Big Rock

3.03 103.17 5.2 97.97

T.P.

3.03 103.17 5.2 97.97

3.3 101.27

#8 { 4.45 96.82 Hub

4.9 96.37 Gr.

#7 { 4.93 96.34 H.

5.58 95.69 Gr.

5.59 95.68 Hub driven down.

100.14

3.03 103.17 5.2 97.97 Big Rock S.E. Cor Marsh

101.09 Old Reading

1.91 101.26 #9 Hub

6.2 96.97 #8 Hub



61  
27  
24

Free's House

50'± on E. 95'± line, Rock 50'± N. of 1st Set

97.20  
26.82  
—  
.42

26.34  
42  
26.76

100.14  
3.3  
—  
103.44  
97

4.15  
—  
99

.16

		97.97	B.M. Rock on Edge Marsh
3.4	101.37	4.56 96.81	Sta. 8 Hub
		5.00 96.37	" 7 Ground
		79 93.47	Surface of Marsh water
3.8	<del>75.0</del> 100.61		
		5.14 95.47	Hub and Gr. 7
		7.85 92.76	Hub 6.
		8.47 91.14	Gr. 6
2.86	95.62	<del>2.86</del>	
		4.02 91.60	Top Hub
		5.20 90.42	bottom
		4.6 91	water
		3.95 91.67	
9.06	100.73		



Average depth on E. side 1.2 with holes  
up to 2' deep.

33.47

91

2.50

92.05

91.60

.45

8.7		91	water
		91.60	Top stake T.P.
100.30		90.4	lower marsh -
	7.05	93.25	water surface upper M
		92.05	Aver bottom - - -



$$\begin{array}{r} 92.05 \\ 90.4 \\ \hline 1.65 \end{array}$$

$$\begin{array}{r} 221 \\ 4 \overline{) 884} \end{array}$$

1st 221 -

2nd 442 -

3rd 663 -

4th 884 -

$$4 \overline{) 5357.3}$$

$$1339.3$$

$$1339.3$$

$$2678.6$$

$$1339.3$$

$$4017.9$$

$$1339.3$$

$$5357.2$$

$$\begin{array}{r} 250 \\ 269.5 \\ \hline 519.5 \end{array} \sqrt{271000} \begin{array}{r} .006 \\ 21570 \end{array}$$

$$\begin{array}{r} 99.25 \\ 96.54 \\ \hline 2.71 \end{array}$$

$$\begin{array}{r} 250 \\ 269.5 \\ \hline 519.5 \end{array}$$

$$\begin{array}{r} 99.25 \\ 96.61 \end{array}$$

$$\begin{array}{r} 519.5 \\ \hline 271000 \\ 25975 \\ \hline 11250 \\ 10390 \end{array}$$

$$\begin{array}{r} 99 \\ 1.3 \\ \hline 97.7 \\ 1.4 \\ \hline 96.3 \end{array}$$

$$\begin{array}{r} .0052 \\ 250 \\ \hline 260 \\ 104 \\ \hline 1.3000 \end{array}$$

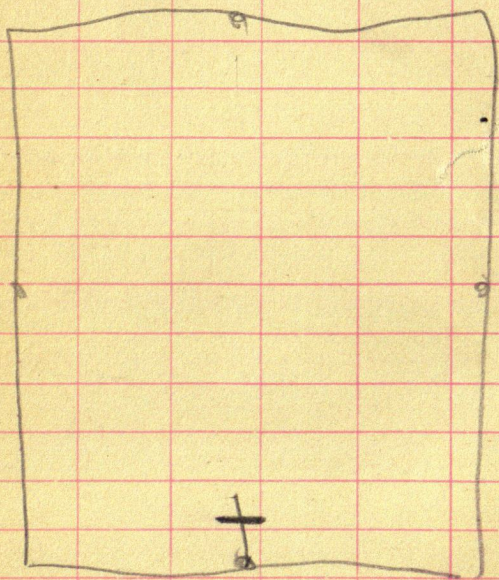
$$\begin{array}{r} 269.5 \\ .0052 \\ \hline 5390 \\ 13475 \\ \hline 140140 \end{array}$$

$$1.3475$$

$$\begin{array}{r} 1.25 \\ 1.35 \\ \hline 2.60 \end{array}$$









May 16 ~~Village of~~ Town of Reimer

Leo Penn

Fred Lincoln

J. M. Greene

21.25

850

600

200

3

4075



May 16 Town of Slater

Leo Penn 2.00

hunch 35.

J. M. Greene 5.00

John Murchie 2.00

May 15 Remer Town - Ditch

Leo Penn 2.25

John Greene 1 day and 1/4 6.25

Team 1/2 day \$2.00

12 Edgar Riey  
John Greene - 1/4 on ditch  
Leo Penn

13 " and Charley Anderson

14 " " " 1/2 day

1/4-11 Leo Penn  
John Greene

" 11 1/4 Village of Remer Penn  
Greene

1/4 for John Greene

#69 1/2 day Village of Remer.

26 1 Village of Remer.

Leo Penn

Fred Lincoln

John Greene

7 1/2

May 26, 1918

Extension of 1st Ave. No

Running North

Sta 0 = + 1st Ave & Main St.

" 2693 = + with North sec. Line.

Running west.

Sta 3161' 1/16 Cor.

4501.8 Sec Cor

Center Sec N. to 1/4 Cor

26873161

4501.8  
2693

1808.8

3 26 93

9 04

35 97

26 + 93

91 044

35, 97.4

20,09275

20,09275

67.17 20  
1343.4 0  
1349.6 3  
2693941 064925  
12055650  
13496300175



Leo Penn } Chain  
 Fred Lincoln }  
 J. M. Greene - Transit  
 660

3161  
 2693  
 ———  
 468

1340  
 468  
 ———  
 872

4501.8  
 2693  
 ———  
 808.8

4501.8  
 3161  
 ———  
 1340.8

X

40.09275

40.09275 | 269300000 67.17  
 1

24055650

28743500

28064925

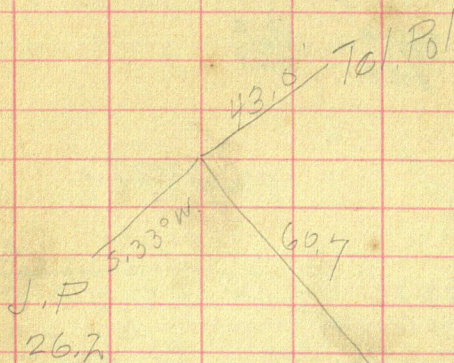
6785750

4009275

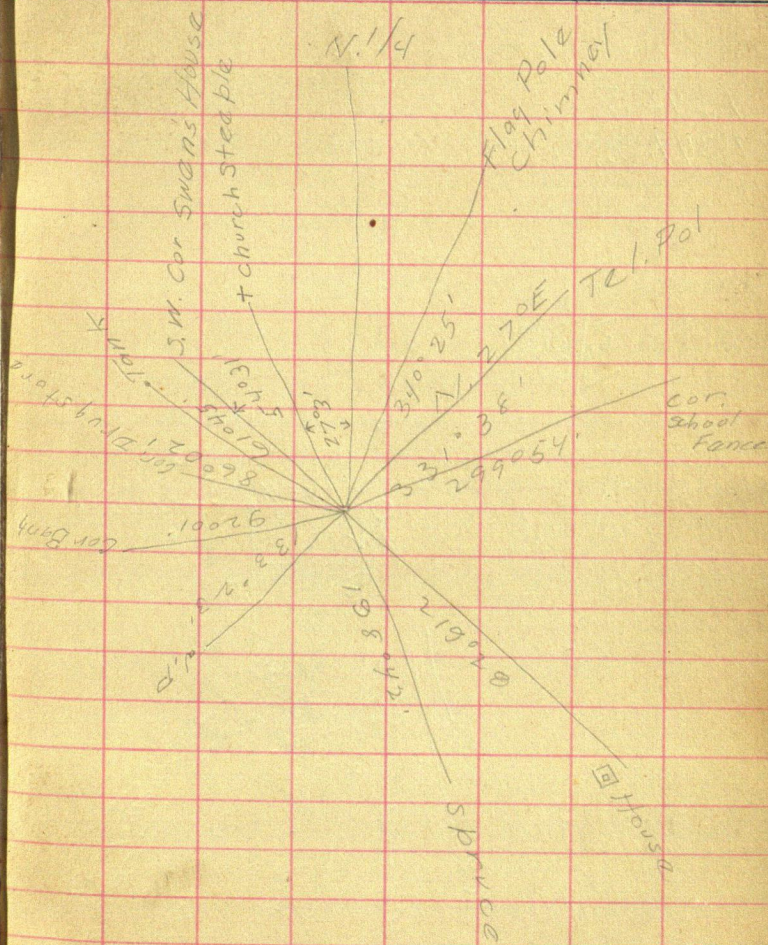
27754750

3161  
 2693  
 ———  
 468

40.14

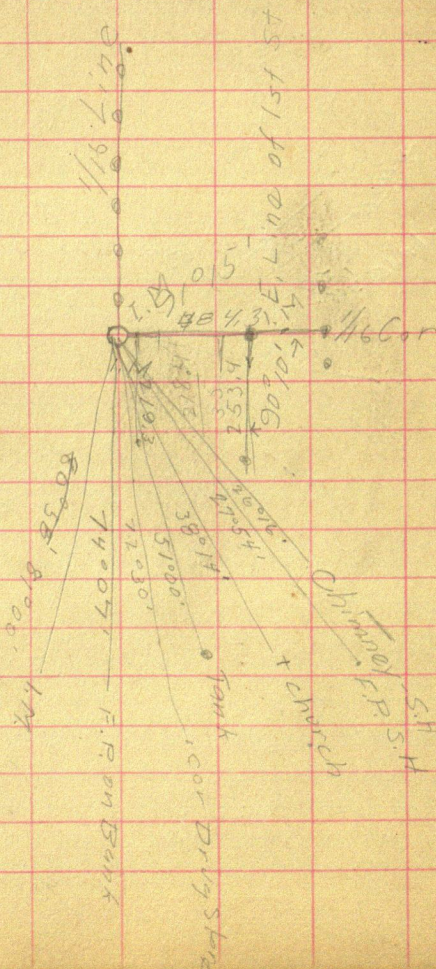






1345.8

1341. 2.

$$\begin{array}{r} 33.51 \\ 115.7 \end{array}$$
$$\begin{array}{r} 2193 \\ 1853 \\ \hline 34.3 \end{array}$$




1383  
33.4

40.07 | 268700  
24042  
28280  
28049  
23100  
20035  
30650

469399

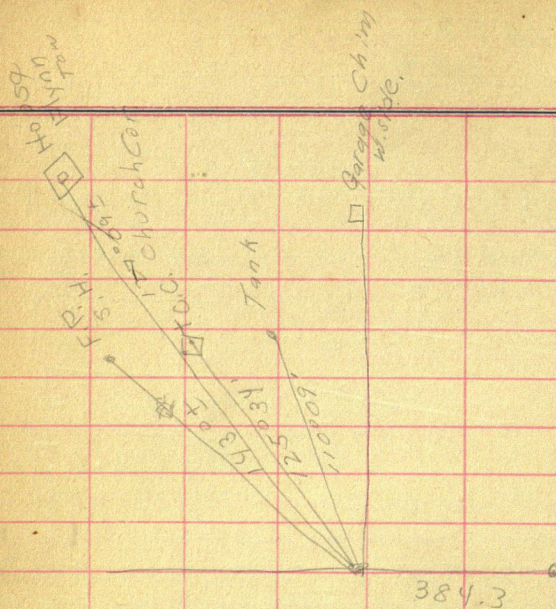
67057  
20  
1341140  
4.69  
1345.83  
2686.97

1343.40

1349.63

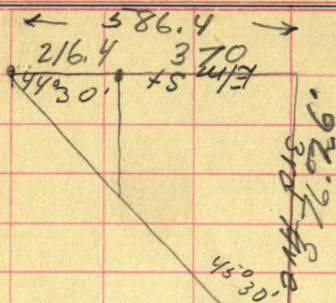
484.3  
380  
104.3  
20.  
34.3

21931

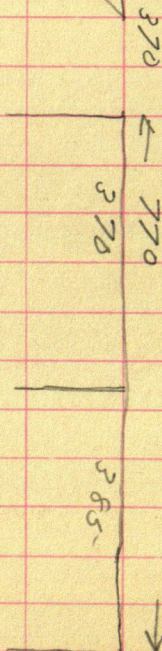




3rd Ave



$$\begin{array}{r}
 370 \\
 770 \\
 \hline
 576.26 \\
 \hline
 1716.26
 \end{array}$$



770

$$\begin{array}{r} 576.26 \\ \hline 134626 \end{array}$$

1486.8.

13 4709  $\frac{1}{2}$



July 20, 1914  
Ditch - Jim Carus  
John Greene

$L 166^{\circ} 28' = 15^{\circ} 32' 6''$

Sta. 0 - 1' - 1' water

1 - 1' - 7' water

Gr 1 + 12' - Edge.

845

water

745

Gr

4.4

4.8

4.8

3.9

4.0

4.5

5.4

5.8

6.2

6.6

8.15

5.3

4

4

4

4

4

4

4

4

4

4

4

4

4

4

4

4

4

4

B.M. 100 - Ground Sta. 0

H.I. = 108.45 Arb. = 95.05 <sup>100.20</sup> 100.10

4.9 95.3 96.3

5.3 94.9 95.9

5.3 94.9 95.9

4.4 95.8 95.8

4.5 95.7 96.7

5. 95.2 96.2

5.9 94.3 95.3

6.3 93.9 94.9

6.7 93.5 94.5

7.1 93.1 94.2

8.65 92.03 to b

96.95

106.16 91.65

90.55

94.36

4

4

4

4

4

Sta. 3

4

5

6

7

8

9

10

11

12

13

13+

14

15

16



$$1st H.l. = 95.85$$

$$\begin{array}{r} 95.85 \\ 7.45 \\ \hline 88.40 \end{array}$$

$$\begin{array}{r} 95.85 \\ 3.82 \\ \hline 92.03 \\ 8.13 \\ \hline 100.18 \end{array}$$

$$\begin{array}{r} 92.73 \\ 1.73 \\ \hline 91.73 \end{array} \quad \begin{array}{r} 92.73 \\ 91.05 \\ \hline 1.68 \end{array}$$

		Gr.	St	Water = 92.73		
				<sup>st</sup>	<sup>gr</sup>	
Sta	0	8.45	6.45	93.73	91.73	21.05
	1	8.15	6.45	<sup>st</sup> 93.73	91.03	21.45
	2	5.4	4.9	<sup>st</sup> 95.28	94.78	<u>89.98</u> 1.83

Bottom of m. road ditch

Beyond #5 <sup>at 5</sup>  $\begin{array}{r} -4.8 \\ 92.05 \\ \hline 96.95 \end{array}$  sta. 1.15 high 90.



91.65

~~90.55~~

94.36 90.05

14

95.85 4.2

~~94.75~~

~~98.56~~

4.24

91.61

91.11

~~90.51~~

~~90.01~~

15

3.9

91.95

91.45

~~90.85~~

~~90.35~~

16

91.45

90.35

~~95.85~~

4.4

~~94.75~~

3.9

91.75

91.25

17

4.1

~~90.65~~

~~90.15~~

4.8

~~91.05~~

~~90.95~~

98.10

5.35

90.50

90

~~97.6~~

T.P.

~~97.0~~

7.6

~~89.40~~

~~88.9~~

88.0

9.1

~~87.9~~

89

9.4

~~88.7~~

88.7

5.14

~~87.6~~

~~87.26~~

Sec. 1

1.3

1.3

~~86.8~~

~~85.7~~

~~93.16~~

5.38

98.54

101.08

2.13

~~98.95~~

1<sup>st</sup> Low,

~~2.13~~

100.08

2.13

100.05

Proq Big

marsh

1

marsh

91.73

88.7

3.03

Ground

1.19

I.M.

Kls ditch.

Cor. ditch-bottom.

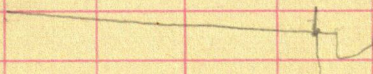
bottom Culvert



2.43

1.75

4.18

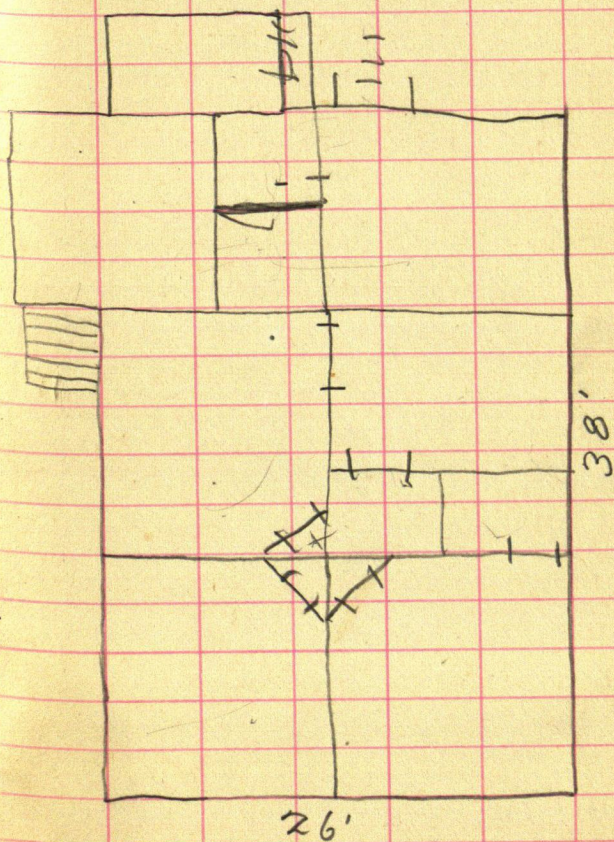


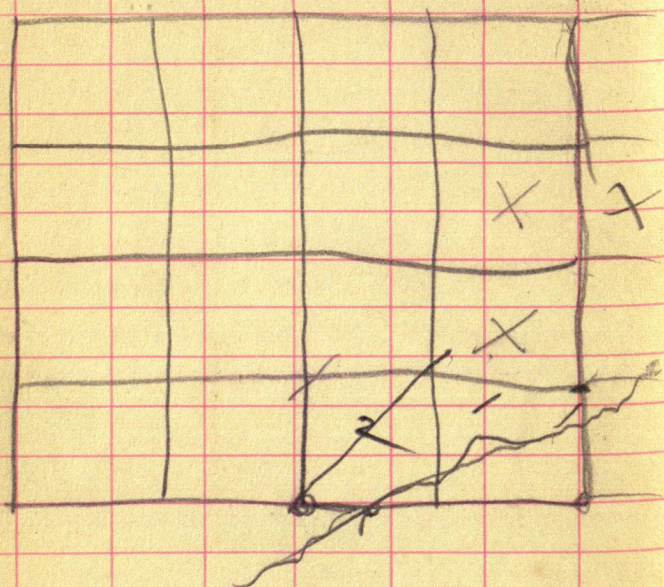




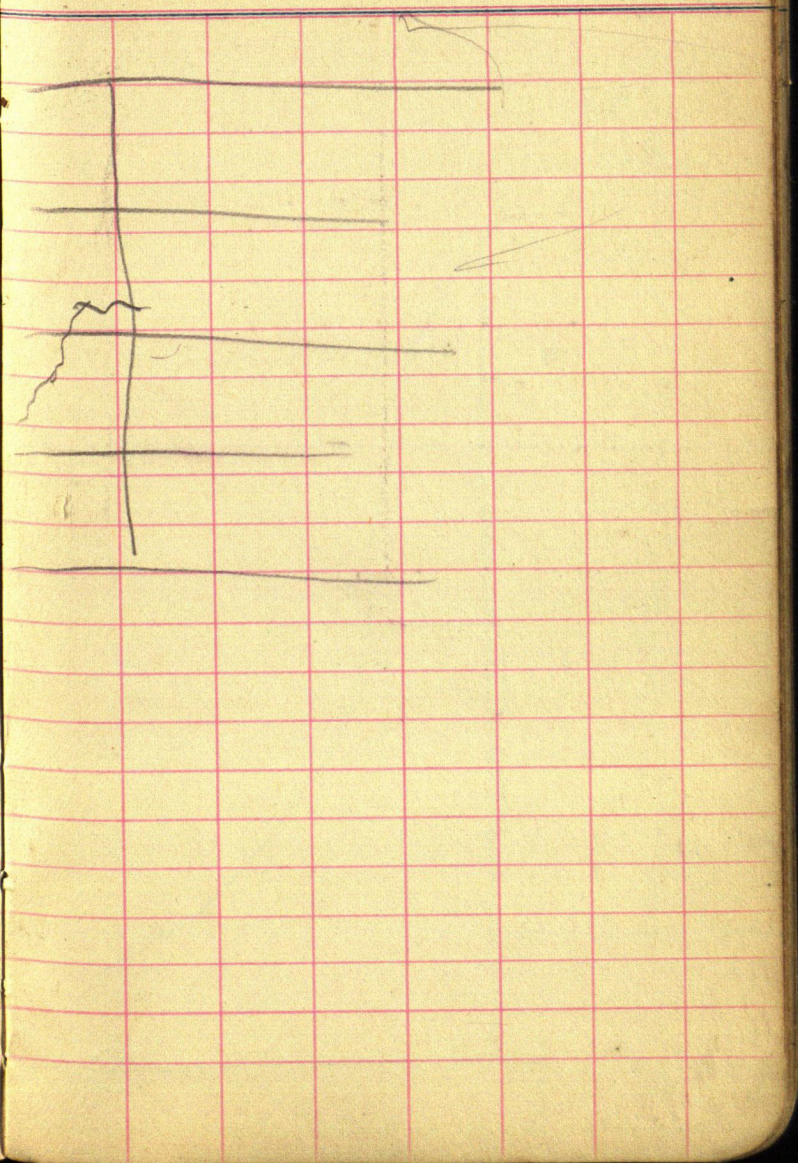
4.1  
4.1



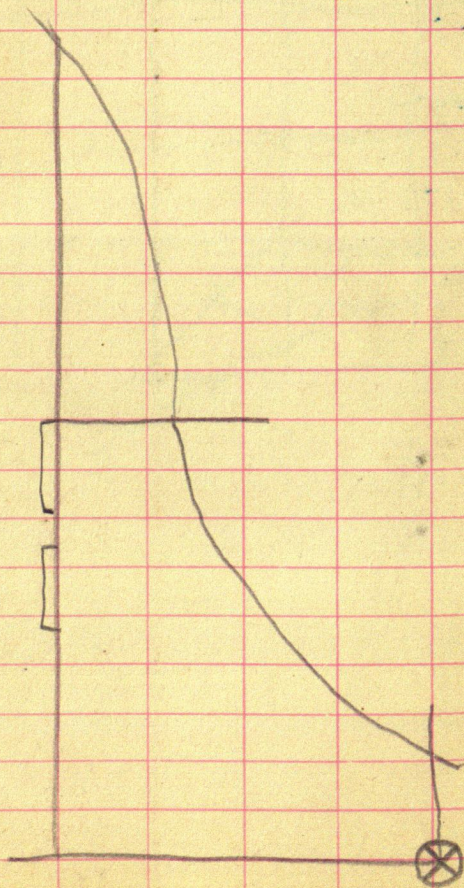








100  
13.2  
13868





$$\begin{array}{r} 1383.4 \\ 33.8 \\ \hline \end{array}$$

$$\begin{array}{r} 1349.6 \\ \hline \end{array}$$

$$\begin{array}{r} 1343 \\ \hline 6.6 \end{array}$$

$$20 \overline{) 1336.4}$$

$$66.8.2$$

$$\begin{array}{r} 20.07 \\ \hline \end{array}$$

$$\begin{array}{r} 46774 \\ \hline \end{array}$$

$$\begin{array}{r} 1336400 \\ \hline \end{array}$$

$$\begin{array}{r} 13410774 \\ \hline \end{array}$$

$$\begin{array}{r} 1336.4 \\ \hline \end{array}$$

$$\begin{array}{r} 2677.4 \\ \hline \end{array}$$

$$1349.6$$

$$67.48-7$$

$$2014-7$$

$$\begin{array}{r} 26992 \\ \hline \end{array}$$

$$6748$$

$$134960$$

$$\begin{array}{r} 13590472 \\ \hline \end{array}$$

$$1349.6$$

$$\begin{array}{r} 2708.64 \\ \hline \end{array}$$

May 12, 1914

Traverse of Road

Note

Sta 172 +30' Dead dry Cedar-Poplar  
 175 +80 Hard Brushing  
 175 +80 Fairly Open  
 178 lots of dead and down  
 178

70°05'

24°20'

17°05' 30

17°14' 30

1°15'

7°30'

1°15'

6°15'

1°15'

27°35'

18°50'

Sta 191 +20

189 +60

187 +25

184 +75

182 +50

178 +00

175 +80

Sta 177 +30'

Running North



# Remer-Bear River

Through section 142-26

J. M. Greene - Transit

L. Fenn } AXE & Chain  
E. Rily }

Crest

N 8 W

21 27

29° 27'

27° 50'

57° 17' 11° 47'

45° 30'

12° 32'

N 8° W  
5.8° E

Edge

Sta. 172

172+30'

steep pitch at start  
gradually leveling.

Sta. 175+80'

Sta. 178+00'

27° 50'

102+50'

184+75'

low place  
in middle

creek 186+3  
sharp grade  
swamp could be  
drained from  
here.

Sta. 187+25'

N 1° 15' E

191+20'

Sta. 189+60'

27° 35'  
28° 50' E

172 + 30  
350

220

450 N 28° 50' E  
45° 15'

225 16° 25'

250 36° 45'

235 20° 20'

160 33° 30' 53° 30'

1890 73° 50' 6° 26'

67 24 69 56

191 + 20

1 20

214 15.492 + 40

200 + 80 80

199 + 50 193 + 20

198 + 20 2

196 + 70 195 + 20

195 + 20 1 50

193 + 20 196 + 70

192 + 40 1 50

191 + 20 199 20

189 + 60 1 30

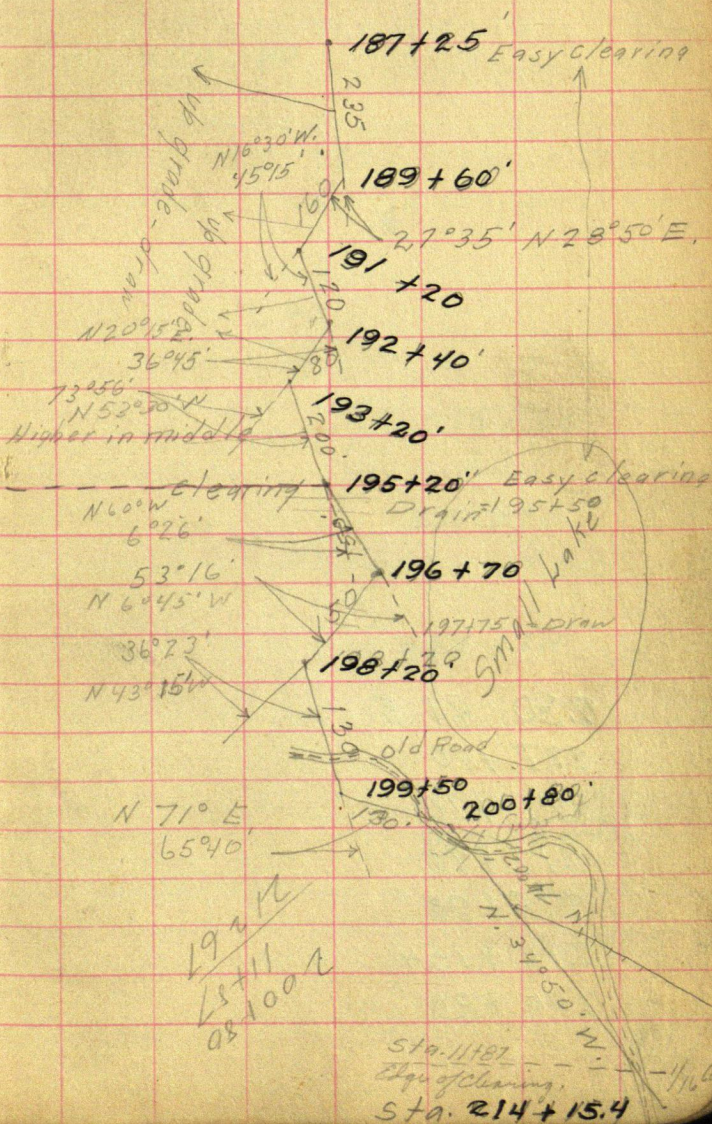
Sta. 187 + 25 199 - 50  
1 - 30

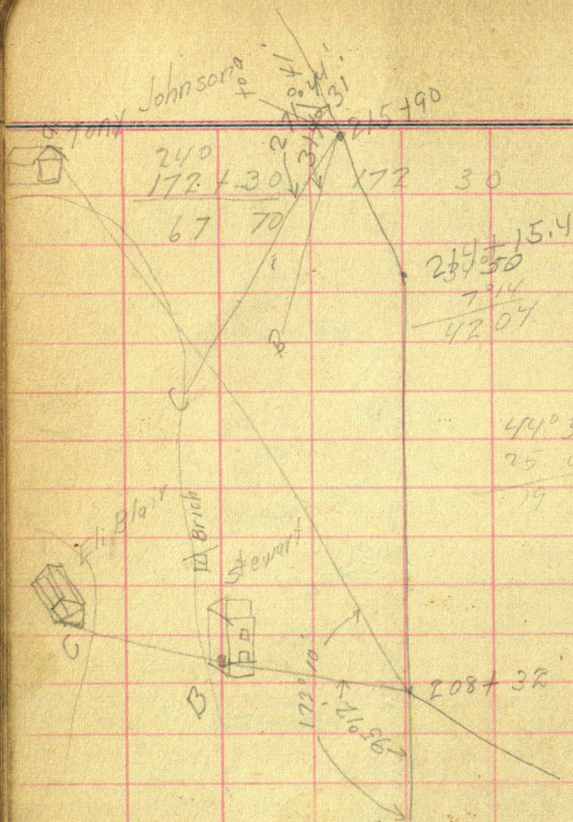
200 - 80

13 35

214 154







230 41.5

227 + 10

222 + 10

217 + 10

215 + 90

214 + 15.4

Sta 200 + 80



$230 + 41.5$   
 $172 \quad 30 \quad 6 \quad 15.4$   
 $580 \quad 11.5 \quad 54.6$   
 $62 \quad 70.0$   
 $230$   
 $172 + 30$

$680 \quad 70$

$214 + 15.4$

$200 + 80$

$201 + 10$

201 in middle of old road.

$2201 + 20$  Draw-Culvert

202 Big log - 202 + 10 instead.

clearing

203 - small draw

$206 + 50$  Draw-Cul

$31050'N$   
 $3.5'$   
 $3.5'$

$214 + 15.4$   
 $1014'$

Edge of hill

Commences to Drop

$42'10"$

$174.6$

$215 + 90'$

$50'17'30"$

$217 + 20'$

N.  $44'30''W$

Draw  $220 + 3'$

$222 + 10'$

$25'09'$

N.  $19'20''W$  10'

$227 + 20'$

$221 + 85'$  drop to river

N.  $27'45''W$

$230 + 41.5$

$13.75$   
 $76'45''$

$240$   
 $214 + 70$   
 $21241$

242

Lots of small brush  
 Not much that cannot be  
 cut with brush hook.

steady dip

May 15, 1914 - Remer Town

Levels for ditch on road

+S	H.I.	= S	Elev		Cut
			100'	= bottom of 1st	
10.65	110.65				
		12	98.65	= " " 2nd	
		12	98.65	= stake in road	
		13.65	97'	= Sta 21 Comp	
		5.43	105.22	Sta 14	7.17
		4.60	106.05	15	8.15
		8	105.15	16	7.75
18.9	5.4	105.25	17	7.65	
	7.05	103.60	18	6.15	
	6.3	104.35	13		
	7.1	103.55	12		
	8.0	102.65	11		
	9.0	101.65	10		
	10.4	100.25	9		
	8.15	102.50	T.P		
9.55	108.20	9.5	98.65		
	12	10.90	97	21	
		11.4	96.80	20	
		10.	98.20	ditch 19	



Greene-level  
Penn - Rod.

by Sam Brockways

			100	grade	Sta
				3.00	1
Culvert,	↑		99.85	2.85	2
	825		99.70	2.70	3
"	↓	0° 6'	99.55	2.55	4
below hill.			99.40	2.40	5
			99.25	2.25	6
			99.10	2.10	7
			98.95	1.95	8
			98.80	1.80	9
			98.65	1.65	10
	12.75		98.50	1.50	11
			98.35	1.35	12
			98.2	1.20	13
			98.05	1.05	14
			97.90	.90	15
			97.75	.75	16
			97.60	.60	17
			97.45	.45	18
			97.30	.30	19
			97.15	.15	20
			97	0	21

ditch about 18"

2100'

+S H.I.	-S Elev		
3.54 106.04	102.50		
7.6 98.4	8	in detail	
7.104 99.10	7	"	
6.54 99.5	6	"	
6.14 99.9	5	"	
5.74 100.3	4	"	
4. 102.	3	"	
3.1 103.	2	"	
4.15 101.90	1	"	



water 1.3

# East side of Road

sta 0	4.15 5.5	H.I. - 5	98.35 101.4	98.35 100	
1	+3.06 2.8 4.35	105.56	stone 101.76 102.50	ditch 101.21 T.P.	bottom of stone
2	1.45 3.0		104.11	102.56	
3	1.74 3.1		103.82	102.46	
4	3.8 5.4		101.76	101.76 100.16	
5	4.2 6.		101.36	99.56	
6	4.6 6.3		100.96	99.26	
7	4.72 6.6		100.84	98.98	
5.2 6.8	4.6 6.3		100.36	98.76	
9	5.5 6.8		100.06	98.76	
10	3.45 5.4		102.11	100.16	
11	2.3 4.4	103.26	103.26	101.16	
6.26 12	5.5 7.5	110.52	105.02	103.02	
13	5.8 6.6		104.7	103.9	
14	3.51 5.44		107.0	105.1	
15	2.9 4.3		107.6	106.2	
16	3.6 5.1		106.9	105.4	
17	4.93 5.6	105.59	105.59	104.9	
0.33 18	1.54 3.4	105.92	104.4	102.5	
19	5.85 7.46		100.1 99.7	98.46	
20	8.36 9.5		97.56	96.42	
	7.18		98.74	T.P. in road	



Stakes set 6' west of center, cut

Grade		Elev	Grade	Cut	Cut from bottom of present of stake ditch below stake
Grade 1	0	101.4	100	1.4	
1.86	2	102.76	99.85	2.91	2.4 1.36
2.86	3	104.11	99.70	4.41	3.9
2.91	4	103.82	99.55	4.27	3.75
.76	5	101.76	99.40	2.36	1.85
.31	6	101.36	99.25	2.11	1.60
.16	7	100.96	99.10	1.86	1.35
Grade 8	7	100.84	98.95	1.89	1.4
Grade 9	8	100.36	98.80	1.56	1.05
.11	9	100.06	98.65	1.41	.90
1.66	10	102.11	98.50	3.61	3.10
2.71	12	103.26	98.35	4.91	4.40
4.82	13	105.02	98.20	6.82	6.30
5.85	14	104.7	98.05	6.65	6.15
7.2	15	107.0	97.90	9.1	8.6
8.45	16	107.6	97.75	9.85	9.35
7.8	17	106.9	97.60	9.3	8.8
7.45	18	105.59	97.45	8.14	7.65
5.2	19	104.4	97.30	7.1	6.6
1.31	20	100.1	97.15	2.95	2.35
	20	97.56	97.	.56	.06

May 16.  
Road on line between  
34 & 35  
Road from N.E. Cor.

805.7 - Dog random  
2660.4  
26.3

805.7; 2660.4; X; 26

26  
48342  
16114  
2660 20948 21 8.87 805.7 2660.4  
1862.28  
232540  
212832  
212808  
1971

7.87

3.3 26  
231  
290  
264  
260

3.3

24171  
24330  
24171  
1590



J. Greene

J. Murchie

L. Penny

Sec. 34 - 1/4 Cor. East

Sta	0	=	N.E-34 Flynn's Cor
	8	=	wet - Culvert
	11	=	wet - Fill

18+73.4'

26+597

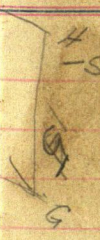
21 Low

Lunch for 3 <sup>\$</sup>.55

Hand-drawn surveying diagram on grid paper. The diagram shows a polygonal area with vertices labeled A, B, C, D, E, F, G, H, I, J, K, L. The diagram includes various measurements in feet (e.g., 56', 60', 66', 120.5', 130', 142', 148', 156', 163', 260', 340', 360', 380', 400', 420', 440', 460', 480', 500', 520', 540', 560', 580', 600', 620', 640', 660', 680', 700', 720', 740', 760', 780', 800', 820', 840', 860', 880', 900', 920', 940', 960', 980', 1000') and a central circular feature labeled 'N 1/2'.



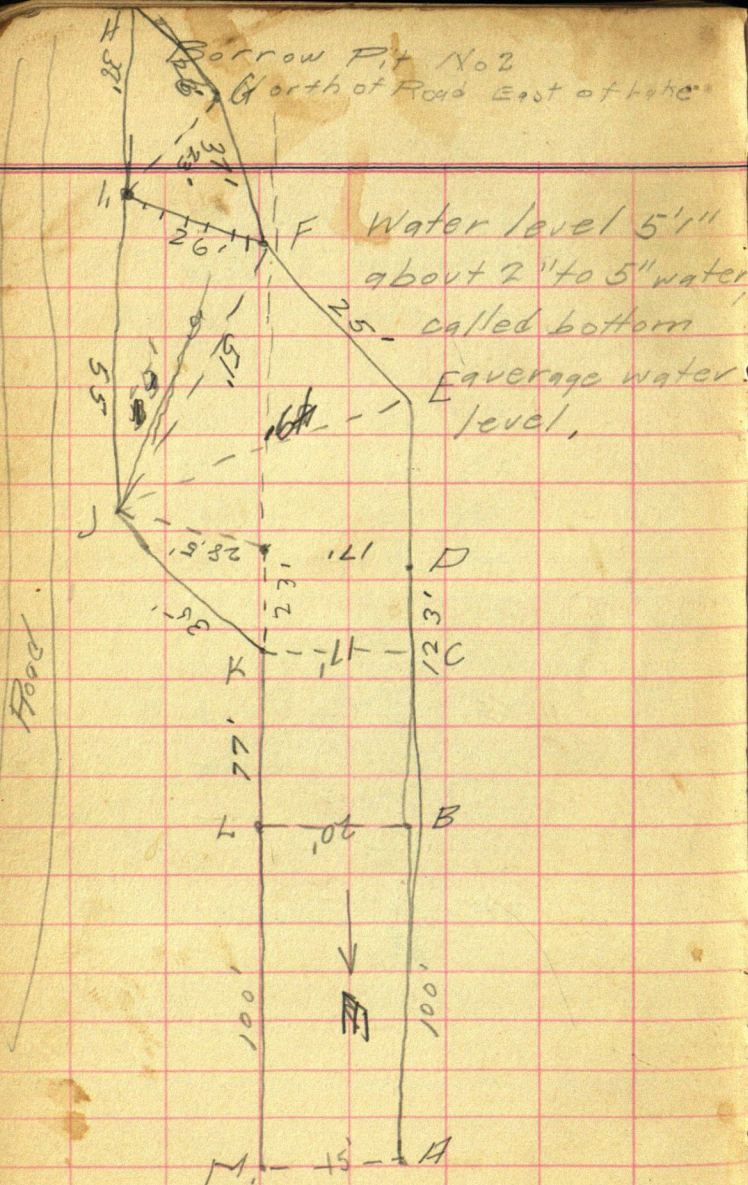
85  
64  
21



H.I	S	Elev	Point
2'2"	4'5"		A
3'	5'7"		B
3'4"	5'11"		C
2'11"	6'0"		D
2'5"	5'8"		E
1'3"	5'5"		F
4'1"	2'9"		G <sup>v</sup>
1'1"	2'9"		H <sup>v</sup>
1'1"	4'6"		I
2'5"	5'9"		J
2'4"	5'4"		K
3'5"	5'1"		L
3'1"	4'7"		M.

1'10" 5'6" Island.  
5.5  
3.7

North of Road East of Lake

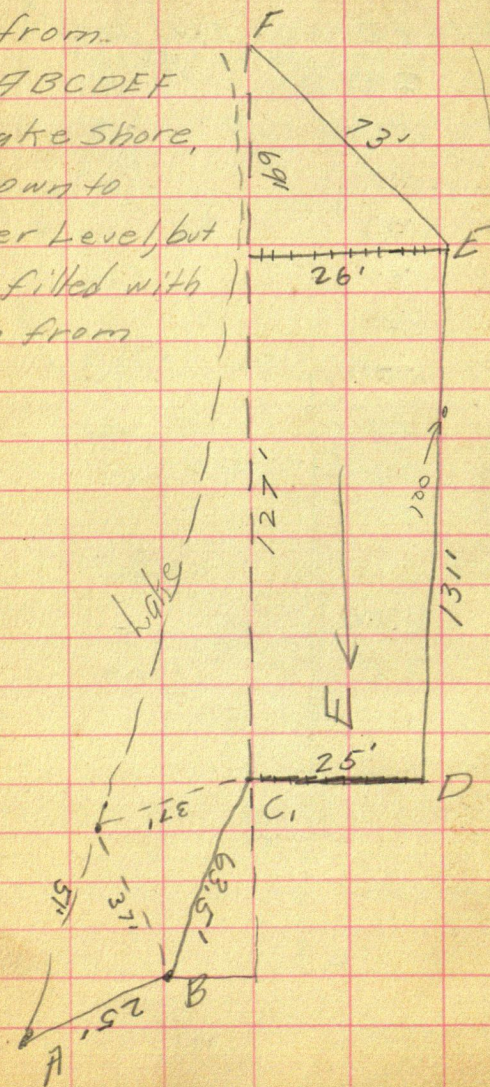




-S	H.I	+S	Elev Point
		5'11"	Water Level
		2'9"	A
		1'11"	B
		1'3"	C
		1'7"	D
		1'5"	E
		1'10"	F
		1'4"	G
		2'3"	H
		2'6"	I
		3'	J
		2'	K
		2'4"	L
		2'8"	M

Barrow Pit ~~from~~ No 3  
 North side of Road,  
 East side of Lake

Cut from  
 line ABCDEF  
 to Lake Shore,  
 Cut down to  
 water level, but  
 part filled with  
 wash from  
 lake





-S	H.I	+S	Elev	Point
		3'5"		F
		2'11"		E
		3'5"		D
		2'5"		C
		3'1"		B
		3'2"		A
		5'7"	= water level	





59  
210  
719 817

Cente	N.Dith	S.D	N.B	S.B.	Point
48"	7'3"	6'6"	4'7"	3'10"	14'10'
4'10"	7'6"	6'6"	4'	2'9"	Stal.
4'9.5"	8'7"	6'7"	-2"	9"	0+50
4'9"	7'9"	6'11"	5'5"	2'8"	0
5'0					-15
	7'4"	7'4"	4'10"	4'10"	-30

20' Crown 1' Dressing.  
6" Crown.

- 38'  
Stal.  
0+50  
4  
7+11

6'  
15"  
60' Long.

$$\begin{array}{r}
 1001514 \\
 825 \overline{) 1350} \\
 \underline{825} \phantom{0} \\
 4250 \\
 \underline{4125} \phantom{0} \\
 1250 \\
 \underline{825} \phantom{0} \\
 3250 \\
 \underline{3300}
 \end{array}$$



537

135 | 825

675

500

405

950

945

001514

2100

1514 00

3028

3179400

537

3.18

491

48

578

491

491

72

35

526

15

21

15

30

3.15

42

72

38

2760

216

600

576

6 5 4 3 2 1

868

550

318

7 2 0 1 1 12

4 13

23 24

25

36

2.9

1.5

5.8

2.9

2.5

5.4

78 - 4.50

3.3 - 4.00

4.42 - 3.50

4.1 - 3.00

4.2 - 2.50

5280

21120

17840

4.7

33

4.73

3.4

5.01

3.6

1.5

5.18

33

4.85

103.68

28.58

5.18

1288 14-8 - 7

52

7

364

168

772

14

168

108-16

16-2x4-8

14-2x4-8

14

4.725

9.275

5.18

33

5.1

5.133

3.84

14

675

2700

675

9.450

675

4.725



4501.8

3161

340.8

4501.8

3161

1340.8

4501.8

2693

1808.8

1808.8  
26.80

904.4

1340

4522

670

2261

335

268  $\overline{) 1808.8}$   
1608

2008

1876

1320  
1340