5

FIELD BOOK

60

Nº 155

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tabels see end of book.

2494
160
2494

S.A.R. #	Job #	Data	Pg. to Pg.
Unorganized		Transit Notes	1 – 3
142-25		Levels & X-Sec. Notes	5 – 11
2	2703	Transit Notes	12 – 21
2	2703	Level & X-Sec Notes	22 – 38
Slater Twp. Bet Sec's 16, 17, 20, 21, 28, 29		Level & X- . .	38 – 44
2	2703	Check Levels & Slope Stakes	45 – 61
2	2703	Re-X-Sec. Notes	11
2	2703	Offtake Sta 205+	62
2	2703	Re-X-Sec Notes	63 – 64
2	2703	Finish Stakes	64 – 73
2	2703	. . . .	73 – 78
2	2703	Re-X-Sec Notes.	79

Transit Notes

East + West 1/4 Line Thru

Sec. 34 – T 142 N. R 25 W

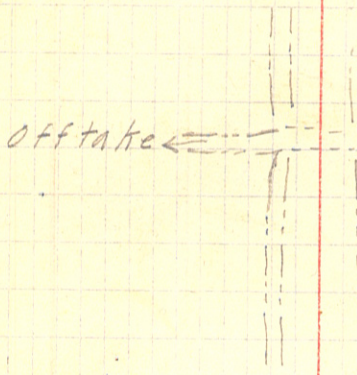
Sta	Defl.	Angle	Bearing
18+50			
9+95.1	R	0°55'	N84°30'E
8+95	8+51 = 105+00		
0+00			N83°30'E

UNORGANIZED 142-25

4-26-26

Party { A.R. Tadsman
W.C. Robbie - Ch.
A.J. Nelson - Ch.

Weather - Cool + Cloudy



Appx. 1/4 Cor. Bet { Secs. 33 & 34
142-25

R.P.s { 12" Cedar - S.E. 46.0'
8" " Stump S.W. 41.5'

Beginning of S.D. 8+40

Beginning of swamp

R.P.s { 14" Birch S.W. 46.1'
15" " S.E. 42.9'

Pg. 1

Sta

31+70

23+00 = 120+37

21+66

40

35

Beginning of Ditch

30

25

End of Side D

2

	Def'l	Angle	Bearing
67+93			
62+40	L	0°55'	N82°30E
57+73			
P.O.T. 51+00			

4-27-26
Weather - Cool & Cloudy

Center of Willow River →

65

1/4 Cor Det. Sec. 34 & 35
142-25

RP's { Cedar B.T. N. 20.7'
" " S.E. 19.4'

60

End of Side Ditches

55

RP's { 12" Cedar - S.E. 23.5'
4" " N.E. 37.2

50

45

Level Notes

East & West 1/4 Line Thru Center of Sec. 34 - 142-25

Sta	−	HI	+	Elev	
B.M.		106.72	6.72	100.0	
−2+00	7.2			99.5	
−1+00	3.7			103.0	
−0+85	2.6			04.1	
0+00	2.8			03.9	
0+83	9.6			97.1	
1+00	8.9			97.8	
1+18	8.9			97.8	
TP+54	12.68			94.04	
+		96.51	2.47		
2+00	3.9			92.6	
+63.8	6.2			90.3	
	7.6			88.9	
3+00	6.6			89.9	
+78	3.7			92.8	
4+00	4.2			92.3	
+41	7.7			88.8	
5+00	7.5			89.0	
+30.5	7.3			89.2	
TP +47	7.5			89.0	
6+00	12.67			83.84	
+		84.89	1.05		+47→
7+00	8.4			76.5	

4-27-26

Party { Taubman - R
W.C. Hobbie - Rod
A.J. Nelson - Axe

On 12" Birch Stub SE of Sta 0+00

L 6.2 6.7 — 6.8 5.9 L
16 14 — 16
CS 8.1 6.5 7.7 6.2 — 5.5 6.1 4.5
29 16 14 8 — 9 12 16 L
CS 8.4 7.2 8.2 6.6 — 6.9 7.3 6.0
28 18 14 9 — 10 13 16 L
L 5.7 7.0 5.9 — 7.8 6.5 7.9 L
16 14 10 — 12 13 30
L 4.9 6.2 5.4 — 6.3 7.1 6.5
16 14 11 — 16 12 15 L
L 5.7 7.3 5.9 — 7.8 6.9 L
18 15 10 — 13 17
L 5.6 5.8 7.6 6.0 — 6.6 7.9 6.8 7.1
32 19 15 10 — 10 13 15 32 CS
L 2.0 4.8 5.9 5.6 — 6.0 6.8 5.7 5.0
39 19 14 6 — 11 13 16 35 CS
CS 4.8 6.0 7.2 6.2 — 5.9 6.3 5.5 4.0 L
35 18 14 9 — 10 13 16 29
L 6.7 7.7 6.7 — 6.3 7.2 5.6
14 12 9 — 8 11 18 L

Bottom of 12"x 20" C.M.C.

L 6.0 6.3 — 5.2 5.7 4.6 5.9
28 10 — 9 13 15 27 L
CS 8.4 7.1 8.0 6.8 — 6.1 6.7 4.5 4.3
32 14 13 9 — 10 12 15 35 CS
V 7.3 7.8 7.2 7.8 6.2 — 6.6 5.6 4.5
38 25 13 12 7 — 13 15 35 L
V 6.4 6.0 6.9 — 5.9 4.6 3.2
29 14 10 — 13 16 37 CS
L 5.3 5.7 6.9 — 5.7 6.3 5.8 5.4
37 17 12 — 7 11 17 30 CS
L 4.7 6.0 5.3 — 5.6 4.1 3.0
20 16 5 — 14 17 34 L
CS 4.5 4.3 5.6 — 4.6 3.4 1.8
31 16 12 — 11 14 29 L
CS 5.8 5.5 6.9 — 6.2 4.8 2.9
33 20 16 — 14 17 33 L
L 6.5 5.4 6.2 — 5.1 5.9 5.0 4.2
26 16 14 — 8 11 13 28 L

5

Sta	–	HI	+	Elev
TP BM.	11.88			73.01
+		73.04	0.03	
8+00	3.2			69.8
8+40	4.3			68.7
+95.1	5.2			67.8
9+00	5.3			67.7
10	6.0			67.0
11	7.0			66.0
12	6.5			66.5
13	6.4			66.6
TP 14	7.30			65.74
+		69.57	3.83	
15	3.4			66.2
16	3.5			66.1
17	4.6			65.0
18	5.3			64.3
+50	5.0			64.6
BM.	3.62			65.95
19	5.4			64.2
20	5.2			64.4
21	5.2			64.4
22	4.5			65.1
TP 23	3.62			65.95
+		70.0	4.05	

℄ of Ditch

On Cedar Stump

℄ of S.D.

CS 5.4 31 5.1 20 5.9 14

L 6.3 2.5 6.8 15 6.7 7

8.2 15 6.5 13 5.9 5

8.4 14 6.6 12 6.6 6

7.9 14 6.2 11 6.2 4.

8.4 15 6.5 12 6.5 5

8.1 15 6.5 13 6.5 5

7.9 15 5.9 13

8.5 14 6.8 11

7.9 7.3 7.7 12 7.6 15 7.7

6.9 11 5.9 11 6.0 11

7.6 15

7.7

On 7" Cedar Stub S. of Sta 18

6.9

7.1

7.0 16

L 6.2 24

CS

℄ of Ditch

S.W. of Sta 8+00

℄ of S.D.

5.3 11 6.1 13 4.8 15 L

6.6 12 5.5 20 L

6.4 6 6.4 12 8.6 14

6.7 6 6.7 12 8.8 14

6.2 5 5.9 13 7.5 15

6.5 5 6.0 13 7.9 15

6.5 5 6.5 12 8.1 15

5.7 14 7.5 16

6.3 13 7.8 15

6.0 13 7.7 15

6.0 14 7.3 15

7.1 15

7.6

6.9

6.9

6.9 15

5.5 24 CS

5.6 24

Sta	—	H.I. 70.0	+	Elev.
24	4.1			65.9
25	4.5			65.5
26	4.7			65.3
27	4.3			65.7
BM.	3.08			66.92
28	4.6			65.4
29	5.5			64.5
30	5.9			64.1
31/2	6.8			63.2
3 1/2	6.6			63.4
TP 2	6.13			63.87
+		67.82	3.95	
33	4.6			63.2
34	5.0			62.8
35	4.5			63.3
36	4.7			63.1
37	4.7			63.1
38	4.3			63.5
39	4.1			63.7
B.M.	3.05			64.77
+30	6.0			61.8
40	4.4			63.4
TP41	4.08			63.74
+		68.74	5.00	

℄ of Ditch H.I. 5.6 ℄ of Ditch

L
L
L
L
L

L
5.3
2.6
5.5 CS
2.6
5.4 CS
2.6

On 10" Cedar Stump S.E. of Sta 27+00

CS 6.5 2.2 5.5 2.4 CS
CS. 6.1 1.9 5.1 2.2 CS
CS 6.0 2.0 5.6 2.2
CS 5.8 2.1 5.7 2.1 CS

8.1 1.3 7.6 1.4
7.2 1.3 7.3 1.4
6.7 6.7
7.0 6.6
7.2 6.5
7.0 1.7 6.8 1.4
7.6 6.8
7.3 7.1

On 12" Sprucestump S.E. of Sta 39+00

Bottom of Ditch
7.1 7.1
7.2 7.2

Sta	−	H.I. 68.74	+	Elev.
42	4.8			63.9
43	4.6			64.1
44	4.8			63.9
45	4.4			64.3
46	4.4			64.3
47	4.7			64.0
48	4.4			64.3
49	4.1			64.6
TP 50	2.85			65.89
+		72.54	6.65	
51	5.5			67.0
52	6.1			66.4
53	4.8			67.7
54	4.5			68.0
55	4.6			67.9
56	4.2			68.3
B.M.	3.02			69.52
57	4.0			68.5
58	3.4			69.1
TP 59	1.55			70.99
+		73.52	2.53	
+55	2.2			71.3
60	3.2			70.3

℄ of Ditch

7.1
15
7.4

6.7

7.0

6.8
16
6.4

7.0

7.3

7.6

8.1
14
6.6
14
7.2
14
7.5
14
7.3
14
7.4
16

℄ of Ditch

7.2
14
7.5

6.7

6.7

6.8
16
6.2

6.6

6.7

7.2

8.0
14

7.9
13
7.2
14
7.8
13
7.6
16

5.6
13

5.6
13

On 12" Spruce S.E. of Sta 56+00

7.4
14
8.2
14

5.6
13
5.6
13

5.6
11
5.6
11

7.6
15
7.6
13

L

5.4
2.3

5.8
3.0

L

L

5.6
3.0

6.1
3.0

L

L

5.2
3.2

5.2
3.2

L

Sta	−	H.I. 73.52	+	Elev
61	6.0			67.5
62	7.4			66.1
+ 40	8.6			64.9
63	8.7			64.8
T.P. B.M.	7.65			65.87
+		68.52	2.65	
64	4.5			64.0
65	4.5			64.0
66	4.9			63.6
67	5.3			63.2
+88	7.4			61.1
+ 93	9.3			59.22

	L	H.I. 56	R	
CS	5.5 25		9.7 20.0	CS
CS	6.0 25		5.5 25	CS

On 24" Tam N.E. of Sta 63+00

Bottom of Willow River

	Off ta	ke Ditch		Sta 39 + 30
	−	HI	+	Elev
BM		68.24	3.47	64.77
0+00=39+30	6.4			61.8
1	6.4			61.8
2	6.3			61.9
3	6.7			61.5
4	6.8			61.4
TP	4.55			63.69
+		66.14	2.45	
5	4.9			61.2
6	5.0			61.1
7	5.7			60.4
8	5.5			60.6
9	6.0			60.1
TP	3.55			62.59
+		66.29	3.70	
10	6.3			60.0
11	6.6			59.7
12	6.7			59.6

On 12" Spruce Stump SE. of Sta 39

Off tie to Ditch Sta 18+57

Sta	−	HI	+	Elev
BM		69.99	4.04	65.95
0+00	7.4			62.6
1	7.4			62.6
2	7.6			62.4
3	8.2			61.8
4	8.7			61.3
+24	8.9			61.1

S.A.R #2-2703

+25 = 0.0		
37+50		Grade
38		72.6
+50		71.7
39		71.2
+50		71.0
40		

On 7" Cedar Stub S of Sta 18+00.

End of Ditch

Shoulder			
	7.6	7.8	6.5
5.6	20	25	26.6
	7.7	8.0	6.1
5.6	19	25	27.6
	7.5	7.5	5.5
5.6	19	26	28.4
	7.2	7.7	5.3
0.6	17	26	28.5
	7.4	7.7	5.4
5.6	18	24	26.8
	7.0	7.5	5.2
5.6	15	21	23.5

Transit Notes From

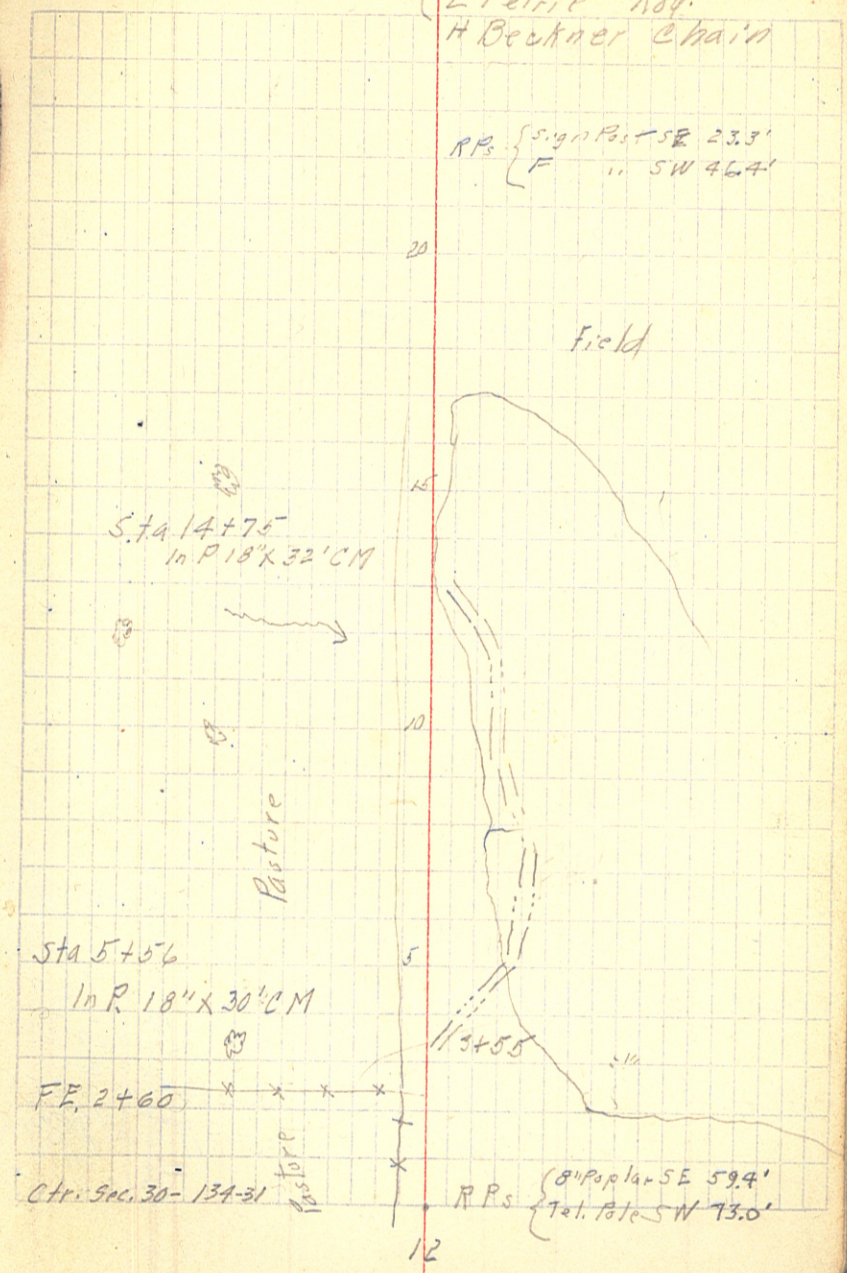
S.A.R. #2 Job #2703

Sta	Defl. Angle	Mag. B. Cm. B
PC 22+31.18 Fwd = 22+30.18 Back		
14+75		
5+56		
0+00		N8° W

11-23-26

Party { R.A. Dahms Engr.
A.R. Taubman Asst. Engr
E Petrie Rod.
H Beckner Chain

RPs { Sign Post SE 23.3'
F " SW 46.4'



Sta	Defl	Angle	Mag. B	C. B
P.T. 41+35.24 Back = 42+88.23 Fwd				
P.I. 39+17.4	R	88°18'	N9°30'W	N9°46'W
	Δ = 15°	T = 370.83'	E = 150.39'	L = 588.67
PC 35+46.57				
PT 28+28.29 Back = 29+89.42 = +91.6				
P.I. 26+10.3 Fnd	L	89°34'	S82°30'W	S82°26'W
	Δ = 15°	T = 379.12	E = 156.2	L = 597.11

Defl's
+35.24 = 44°09'
41 = 41°30'
+50 = 37°45'
40 = 34°00'
+50 = 30°15'
39 = 26°30'
+50 = 22°45'
38 = 19°00'
+50 = 15°15'
37 = 11°30'
+50 = 7°45'
36 = 4°00'

10' Brush

Ck 66'

Defl's
+28.29 = 44°47'
28 = 42°40'
+50 = 38°35'
27 = 35°10'
+50 = 31°25'
26 = 27°40'
+50 = 23°55'
25 = 20°10'
+50 = 16°25'
24 = 12°40'
+50 = 8°55'
23 = 5°10'
22+50 = 1°25'

45

Field

RPs { F. Post SW 36.7'
" " NW 34.1' }

40

West 1/16 Cor. on N. Line
Sec. 30-134-31

RPs { Fence Post NW 41.4'
Tel. Pole SW 33.8' }

RPs { F Post NW 32.7'
" " NE 30.1' }

35

Field

15 5686.8

F E 31+10
in P 12"×16' C.M.

30

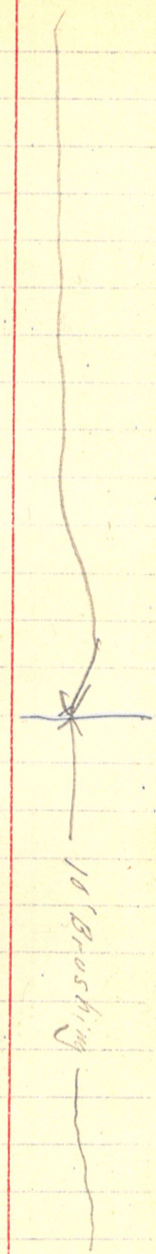
RP's { F. Post SW 43.8'
F. " NW 44.0' }

1/4 Cor. on N. Line
Sec. 30-134-31

RPs { Tel Pole SE 31.1'
F. Post NE 56.5' }

25

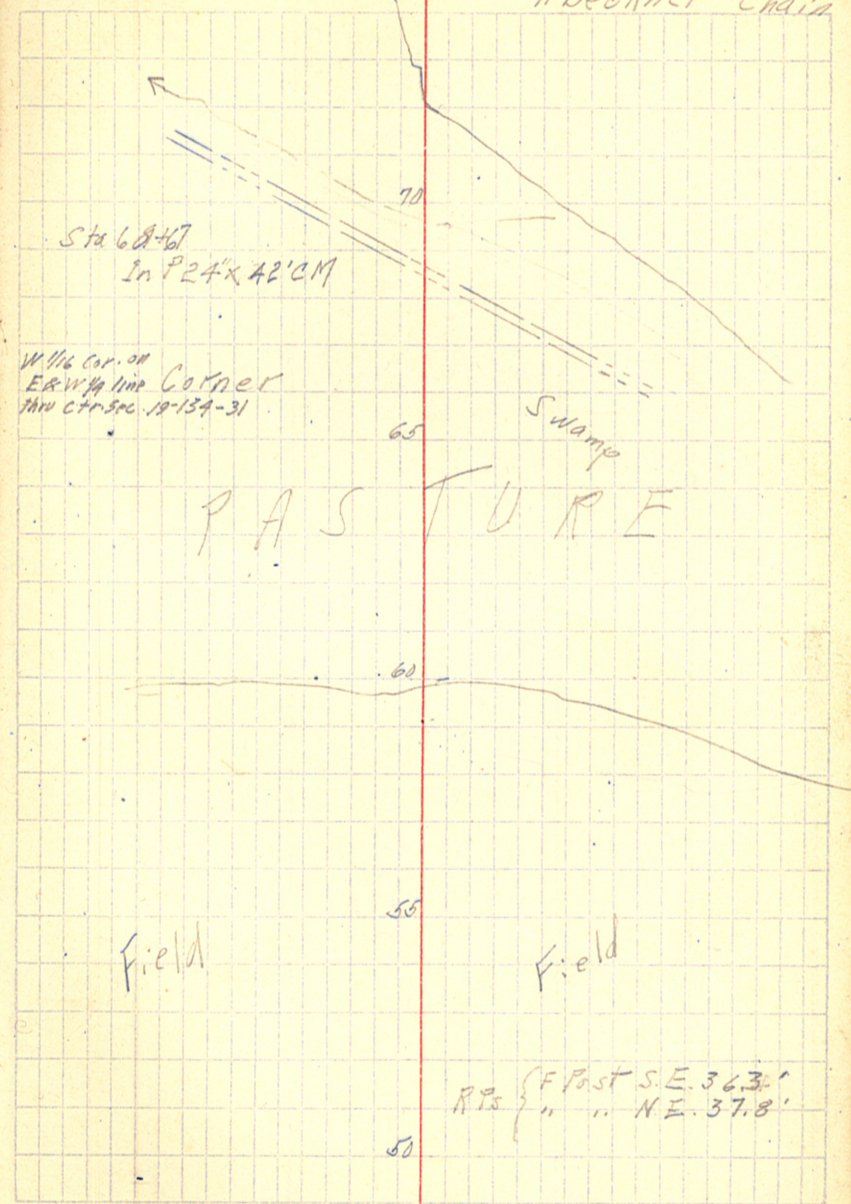
46+00
65+56 (?)



P.T. 51+00

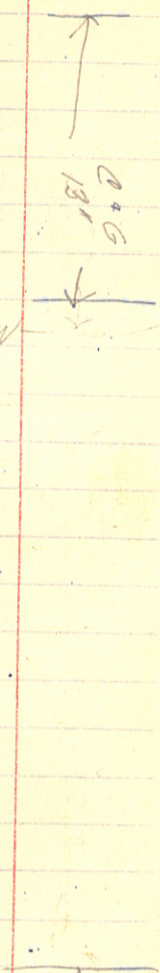
11-27-26

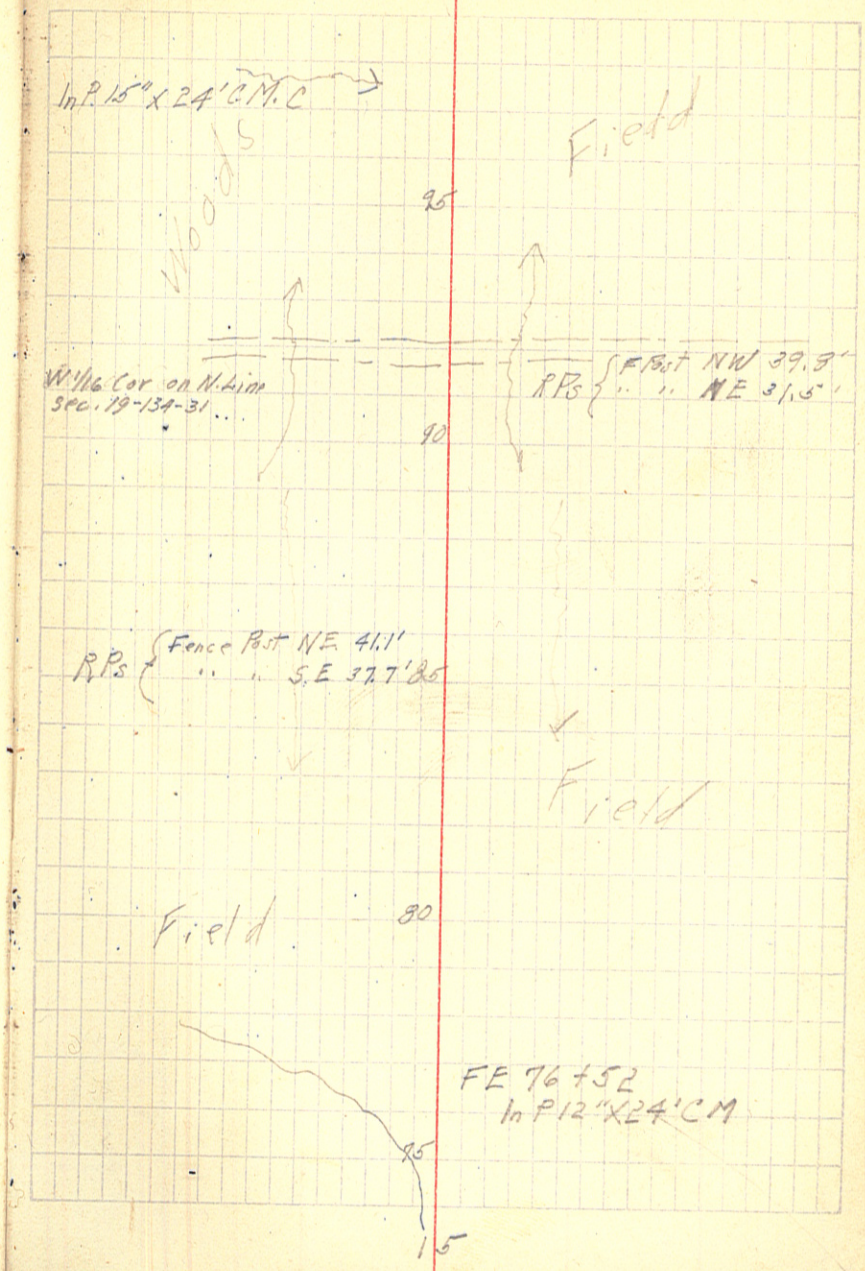
Party { Taubman Asst Engr
E Petrie Rod
H Beckner Chain



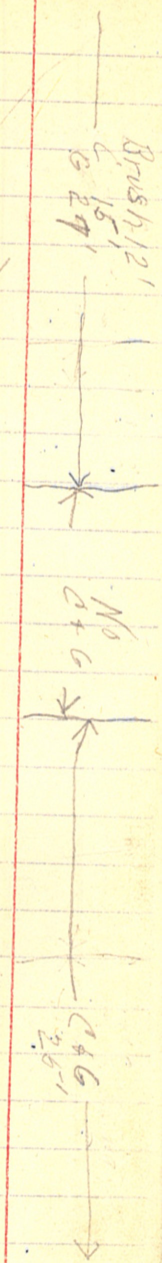
14

	Defl	Angle	Mag. B	C. B
97+00				
P.I. 91+94	R	0°08'	N10°W	N1°08'W
P.O.T. 85+00				

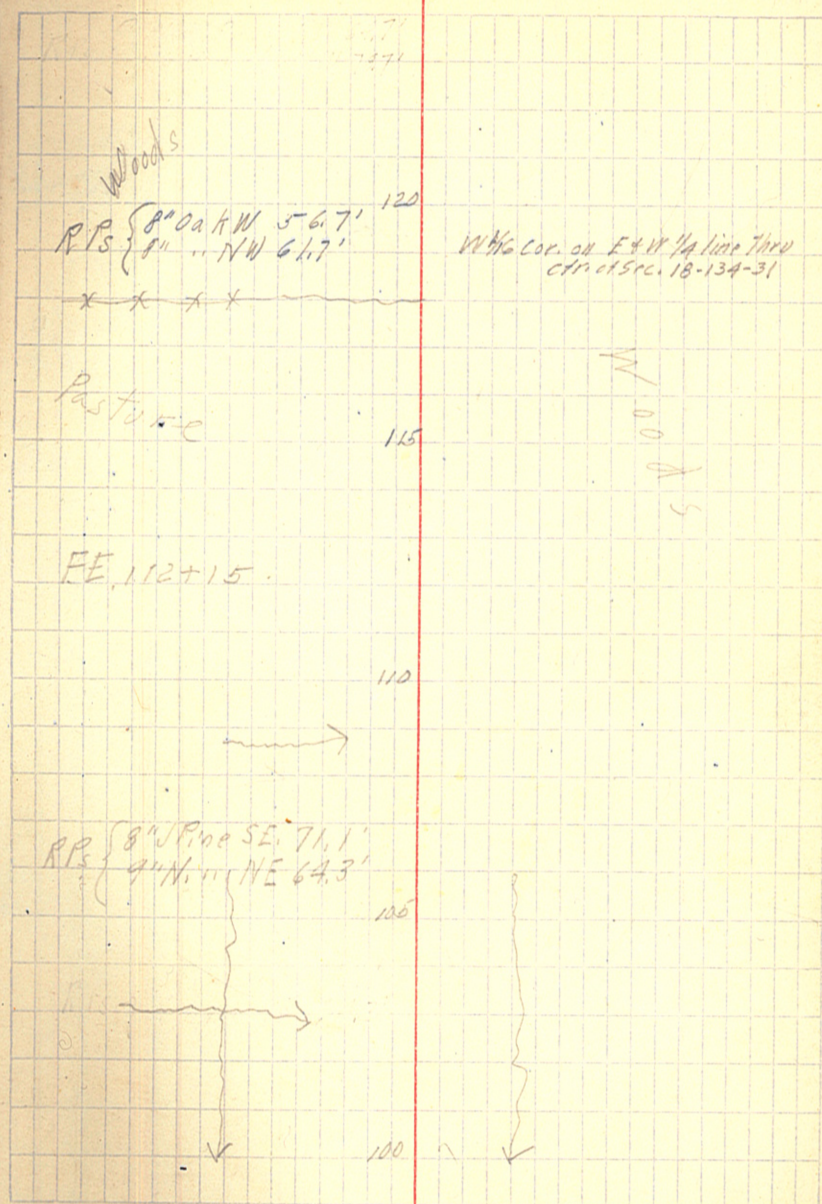




P.I. 119+00	R	0°08'	N9°30'W	N9°W
P.T. 106+95.5				

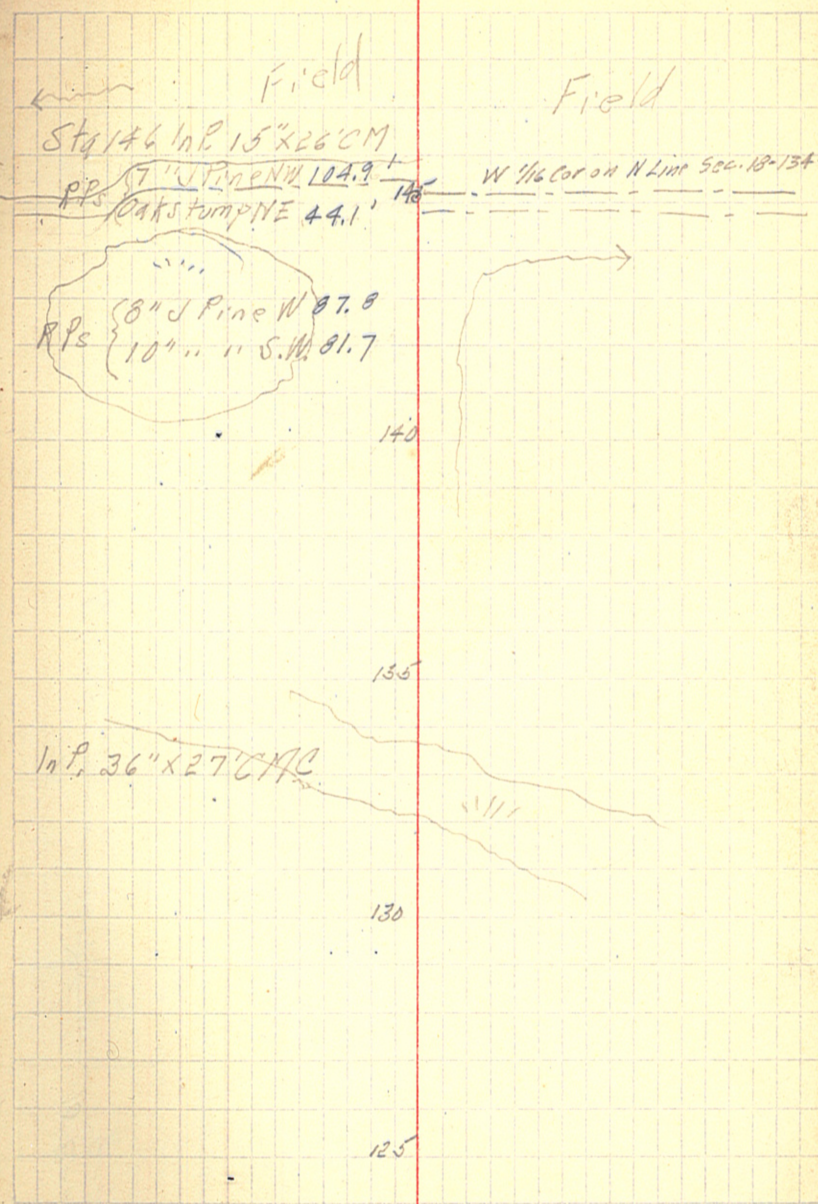


12-2-26



PT 147+10.1 = +09.9				2°06'	
				147 2°03'	
				146 1°33'	
P.I. 145 Ex. 3.9	L	4°12'	Δ 4°12' D 1°L T 210.1 L 420	145 1°03'	(N13°12'W)
				144 0°33'	N14°30'W
				143 0°03'	
PC 142+89.9					
POT 142+67.0					Brush 16' Clear 16' Grub 32'
	145				
	91.94				
	53 86				
	26 53				
	118+47				
133+37					

12-3-26



P.T. 168+81.86 Back = 168+87.13
P.I. 167+80 L 31°20' N45°W N44°32'W
P.C. 166+72.97 Δ = 15° T = 107.13' L = 208.89

Ext =

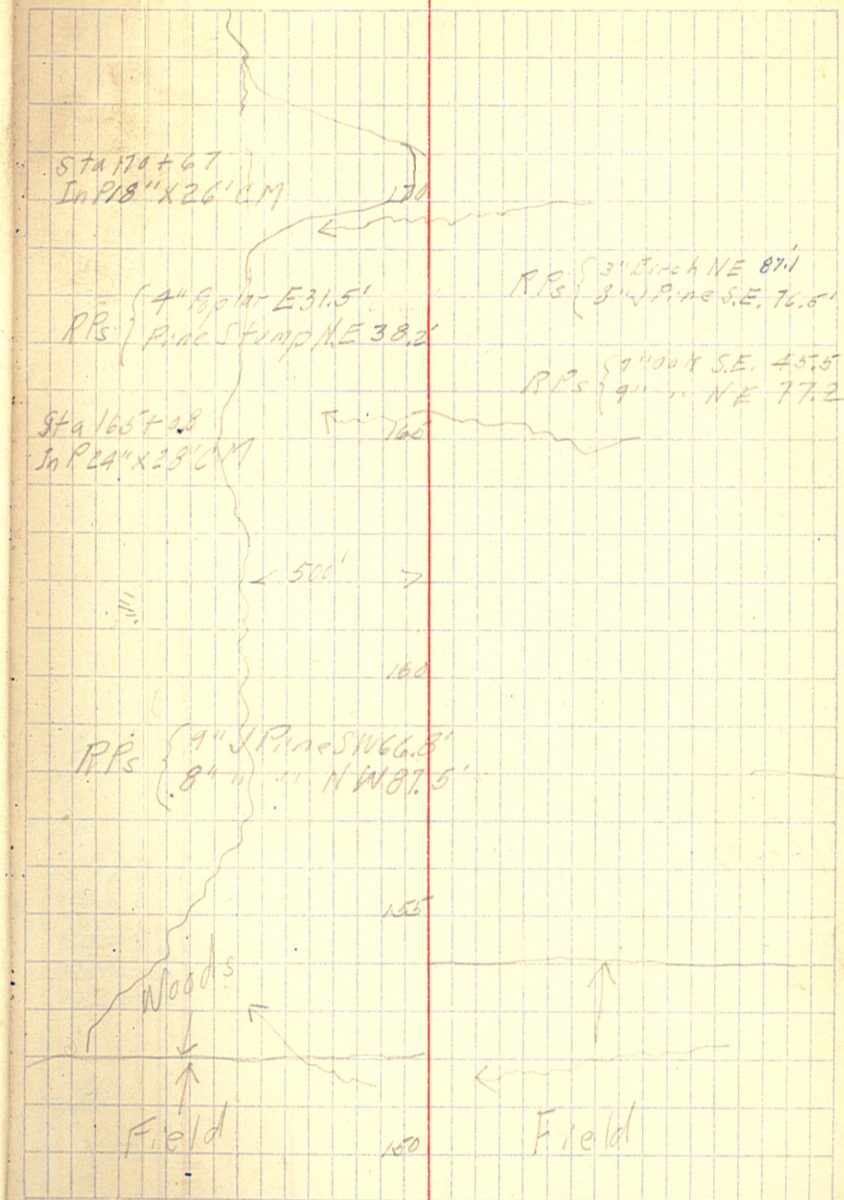
Defls
+81.86 = 15°40'
+50 = 13°16'
168 = 9°31'
+50 = 5°46'
167 = 2°01'

Revised See Page 21

P.O.T. 158+50

16' Clearing

10' Brushing Grubbing



12-7-26

(20)

195

190

185

180

175

PT 182+40.7 Back = 182+49.58 Fwd.

PI 181+22.2 R 36°53' N7°30'W N7°39'W

Δ=15° T=127.38' E=20.7' L=245.88'

PC 179+94.82

Revised See Page 21

Defls
+90.7=18°26'
182=15°23'
+50=11°38'
131=7°53'
+50=4°08'
180=0°23'

Sta 174

RPs { 2" J Pine S 54.5'
4" " " W 35.4

RPs { 8" J Pine NW 49.7'
10" " " NE 47.0'

RPs { 8" J Pine W 53.0
3" N Pine NW 60.1'

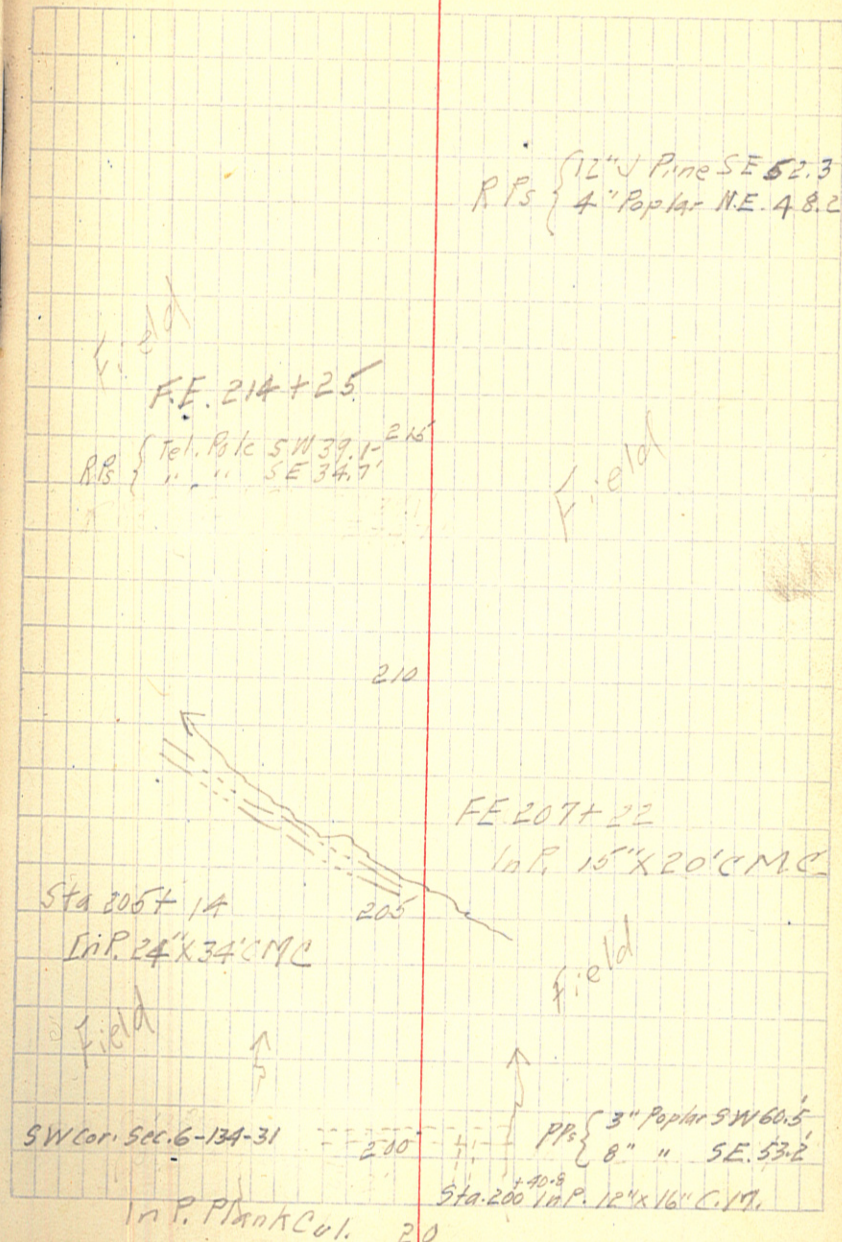
≒ Approx. 1/4 Line

19

219	End of Survey			
P.O.T. 213+30.6				
P.I. 200+40.8 L	6°18'	N8°30'W	N7°57'W	

C + 6°16'

12-7-26



PT
184+40.63 Fd.
184+18.49 Bk.

PC
178+03.77

PT
170+47.81 Fd.
170+34.41 Bk.

PC
165+12.19

181+22.2	R	36°53'	Δ 36°53'		18°26'
			D 6° R	184	17°53'
				+50	16°23'
			T 318.43	183	14°53'
			L 614.72	+50	13°23'
				182	11°53'
			E 51.7	+50	10°23'
				181	8°53'
				+50	7°23'
				180	4°53'
				+50	2°53'
				179	1°23'
				+50	
					15°40'
167+80	L	31°20'	Δ 31°20'	170	14°38'
			D 6° L	+50	13°08'
				169	11°38'
			T 267.81	+50	10°08'
			L 522.22	168	8°38'
				+50	7°08'
			E 36.8	167	5°38'
				+50	4°08'
				166	2°38'
				+50	1°08'

Level Notes

SAR #2 Job #2703

Sta	−	H.I.	+	Elev	
BM (Old)		1252.75	2.65	1250.10	
B.M.	0.87			1251.88	✓
TP	6.33			1246.42	
+		1252.47	6.05		
B.M.	2.28			1250.19	
0+00	6.9			45.6	
0+00	6.8			45.7	
1+00	6.0			46.5	
2+00	5.9			46.6	
3+00	6.0			46.5	
4+00	6.0			46.5	
5+00	6.0			46.5	
6+00	6.0			46.5	
7+00	5.6			46.9	
5+56	8.00			44.5	
TP	5.63			1246.84	
+		1254.48	7.64		
+35	7.3			47.2	
8+00	6.5			48.0	
9+00	4.8			49.7	
+50	4.3			50.2	
10	4.5			50.0	
11	5.2			49.3	
12	6.7			47.8	

11-24-26

L H.I. = 5.2 R

On 10" Poplar Stump W of Sta 11+00

On 4" " W. of Sta 9+00

On 20" Oak Stump NW of Sta 2+00

5.6 5.4 6.7 6.6 5.3 — 5.2 5.8 8.6 8.6 6.5 4.5
36 20 18 14 10 — 12 18 32 24 28 35
4.7 4.9 7.2 6.1 5.3 — 5.4 6.9 9.2 9.2 6.1 6.5
36 21 17 14 11 — 15 18 22 24 28 37
6.0 6.6 5.9 7.2 7.0 5.3 — 5.5 6.6 9.2 9.1 6.9 7.0
38 27 20 16 12 9 — 13 18 26 25 29 33
5.5 6.0 5.9 6.4 — 5.2 6.1 6.6 8.7 9.2 7.3 7.4
34 18 13 10 — 11 15 18 21 25 27 33
4.6 5.4 6.5 6.5 6.4 — 5.3 7.6 7.6 6.0 5.4
33 20 18 14 10 — 10 17 23 22 26
4.7 5.6 6.3 6.5 5.3 — 5.4 7.5 7.6 6.5 6.8
33 19 17 15 10 — 10 15 17 19 33
CS 3.0 3.7 4.6 6.2 6.5 4.9 — 5.4 7.2 7.4 7.2
33 30 21 17 16 11 — 11 16 19 33
1.3 4.8 5.4 6.2 6.4 5.2 — 5.3 5.9 7.2 7.2 6.4 6.6
CS 33 24 18 16 13 9 — 11 13 16 18 20 31

Bot of C.M.C

6.5 1.2 6.0 6.1 5.3 — 5.4 7.5 7.5 6.9 4.9
CS 32 24 14 11 9 — 11 17 20 21 30
0.4 0.6 5.7 6.3 6.2 5.4 — 5.2 6.3 7.4 7.3 6.7 7.3
L 33 28 14 17 13 10 — 11 15 17 19 20 30
2.5 3.3 6.8 6.2 5.2 — 5.3 6.1 7.3 7.3 6.5 6.8
CS 33 22 17 14 9 — 11 15 17 19 21 28
3.5 3.4 3.9 5.0 6.4 6.4 5.7 — 5.3 6.2 7.5 7.7 6.8 7.1
L 33 31 25 20 16 14 10 — 11 16 17 19 20 33
3.7 4.1 5.8 6.0 5.3 6.6 6.5 5.4 — 5.7 7.5 7.6 6.9 7.1
CS 32 24 25 23 19 17 15 10 — 9 16 18 21 29
3.9 4.6 6.9 6.9 5.3 — 5.4 6.2 7.7 7.7 6.9 7.5
CS 33 22 17 13 10 — 9 12 16 18 20 29
4.1 4.8 6.7 6.6 5.2 — 5.7 7.4 7.7 6.5 7.0
CS 33 22 18 15 11 — 11 15 18 21 33

22

Sta	−	H.I. 1254.40	+	Elev.
13	7.9			46.6
14	8.1			46.4
15	7.8			46.7
TP	7.95			1246.53
+		1254.09	7.56	
14+75	10.7			43.4
16	7.0			47.1
17	6.5			47.6
18	5.9			48.2
19	4.9			49.2
20	3.7			50.4
21	2.2			51.9
22	1.0			53.1
B.M. TP	0.60			1253.49
+		1264.92	11.43	
P.C. +31.16	11.7			53.2
+50	11.9			53.0
23	11.5			53.4
+50	13.2			51.7
24	12.6			52.3
+50	10.9			54.0
25	9.3			55.6
+50	6.8			58.1

6.7

4.5 4.9 5.5 6.3 5.8 5.0 5.5 6.4 7.6 7.9 6.5 6.9
33 22 18 14 13 11 12 17 19 24 26 33
6.2 6.5 7.0 6.4 5.2 5.2 6.2 7.2 7.2 6.4 6.5
32 20 16 12 10 11 18 20 25 27 33
6.0 6.4 7.4 7.2 5.2 6.2 6.9 6.2 7.0 7.2 6.6 6.6
32 22 21 15 10 11 15 18 20 26 27 33

Bot. of C.M.C.
6.2 6.5 7.6 7.8 6.8 5.5 6.4 6.3 7.0 7.0 6.4 6.3
32 23 21 16 14 9 13 17 19 24 26 33
6.8 6.8 7.5 7.5 6.0 5.3 6.4 6.1 6.7 6.7 5.9 6.0
32 22 20 16 13 10 13 19 21 25 27 33
6.0 5.9 7.5 7.2 5.2 5.2 5.7 6.7 6.4 5.4 5.2 C.S.
32 21 17 16 10 13 19 21 25 28 33
6.0 6.0 7.3 7.2 5.6 5.2 5.3 6.6 6.5 4.5 4.4
31 22 19 16 13 12 16 18 23 28 33 C.S.
6.0 5.8 7.0 7.1 5.5 5.2 6.2 6.2 4.2 3.4 3.5
32 21 19 17 13 10 14 17 21 26 33
C.S. 6.7 5.2 6.8 6.9 5.5 5.2 6.0 6.2 3.0 2.6 C.S.
31 18 15 13 11 10 13 18 24 31
C.S. 6.6 5.0 6.8 6.6 5.3 5.2 6.5 6.5 2.7 2.2 C.S.
32 17 14 12 10 11 14 17 22 33

On 3" Oak NW of Sta 19+00

H.I. = 51.5

5.6 4.6 6.5 6.6 5.6 5.6 6.5 6.4 3.2 2.7
32 18 16 13 9 11 16 18 23 34
4.9 4.6 6.2 6.2 5.6 5.6 6.2 6.1 3.8 3.0
32 19 15 12 9 13 15 18 23 33
7.3 6.3 6.6 5.6 5.9 5.6 6.2 6.4 4.9
28 13 11 4 6 18 21 24 27
5.3 5.5 5.0 3.3 3.0 3.5
37 28 6 9 20 33
C.S. 4.4 6.2 5.6 5.0 3.4 L
31 21 23 27 30
C.S. 4.2 6.7 6.9 C.S.
31 24 33
C.S. 4.0 6.5 7.2
40 24 33 C.S.
C.S. 3.7 4.7 6.6
34 19 32 C.S.

Sta	–	H I	+	Elev
26	1.6	1264.92		63.3
TP	1.69			1263.23
+		1274.15	10.92	
+50	6.7			67.4
27	4.5			69.6
+50	4.2			69.9
28	1.5			72.6
TP	0.50			1273.65
+		1284.86	11.21	
PT +28.3	10.5			74.4
30	10.1			74.8
31	5.8			79.1
+50	3.9			81.0
32	2.2			82.7
+50	1.0			83.9
33	0.9			84.0
34	2.8			82.1
+50	4.5			80.4
35	6.0			78.9
PC +46.57	7.5			77.4
TP 36	9.63			1275.23
+		1277.16	1.93	
+45	3.5			73.7

L H.I. = 5.5 R

	L	R	
	5.1/33 5.0/16	6.5/29 7.1/34	
	6.6/39 5.9/31 6.2/11	6.0/12 5.9/24 8.8/32	
L	6.8/30 6.0/10	5.5/2 8.6/7 7.7/10 7.2/19 7.9/31 8.6/35	
	6.4/33 6.9/22 5.8/8 6.4/6 5.6/3	5.2/1 5.5/16 6.6/23 5.9/24 5.5/32	L
L	4.8/26 5.1/18 6.5/14 6.1/11	6.0/10 7.0/12 6.4/16 4.4/19 4.0/27	L
L	4.6/39 4.6/19 6.7/13 6.1/10	6.1/8 6.8/14 6.2/17 4.3/19 4.0/27	L
L	4.3/29 4.5/19 6.5/14 6.2/11	6.0/10 6.6/15 4.2/19 3.8/27	CS
L	1.8/29 1.9/21 6.3/13	6.1/11 7.0/16 1.8/25	L
L	2.4/19 6.2/12	5.7/10 6.1/14 2.0/20	L
L	2.6/18 6.7/12	6.0/12 6.0/16 3.0/20	L
L	3.9/17 6.5/13	5.6/11 6.0/14 5.5/18 3.8/22 3.2/25	L
L	3.5/19 6.4/14 6.0/11	5.7/9 6.3/15 3.0/20	L
L	2.6/28 2.4/20 5.4/17 6.9/14 5.9/11	5.7/9 6.0/12 6.0/15 1.5/23	
CS	3.2/31 2.7/21 5.0/17 6.2/13 6.0/11	5.8/11 5.9/15 5.0/17 0.7/23	L
CS	5.2/27 5.0/17 6.9/14 6.0/11	6.0/13 6.3/15 3.2/21 2.7/26 3.0/35	
CS	8.4/29 8.2/24 8.6/18 6.1/10	6.1/11 7.0/15 5.8/18 5.5/25	CS
CS	9.6/32 9.4/23 9.1/19 6.1/12	5.9/7 7.8/13 8.5/17 7.0/20 7.5/30	

Sta	−	H.I. 1277.16	+	Elev
+50	4.9			72.3
37	6.4			70.8
+50	7.0			70.2
38	7.1			70.1
+50	7.3			69.9
39	7.3			69.9
+50	7.2			70.0
40	6.4			70.8
+50	6.6			70.6
41	6.0			71.2
B.M. (Old)	6.67			1270.49
PT+35.24	5.7			71.5
43	5.5			71.7
44	4.4			72.8
TP 45	2.95			1274.21
+		1283.43	9.22	
46	7.7			75.7
47	6.8			76.6
48	5.8			77.6
49	5.0			78.4
50	4.2			79.2
51	4.4			79.0
TP BM	10.03			1273.40
+		12.78.34	4.94	

11-26-24 H.I. = 5.5

7.4 38 4.3 24 4.4 13 4.6 3

4.0 33 4.6 21 5.4 18 6.3 12 5.6 7

5.7 28

6.1 31

5.9 24

6.2 23

5.8 25

CS

5.9 6.8 6.8 5.8
15 13 7 4

6.0 6.8 7.2 5.8 5.4
31 28 26 20 8

6.3 6.2 7.1 6.0
29 22 19 13

6.7 6.0 5.7 CS
7 9 30

4.9 32 CS

4.5 33 CS

4.8 33

4.9 31

5.2 26 4.7 37

6.0 32

5.6 23 5.3 32

5.8 4 6.3 7 5.5 11 4.9 17 L

5.7 10 5.7 14 6.0 17 5.3 19 6.0 26 L

On 2 Nails in Tel. Pole W of Sta 39

6.3 20 6.7 18 6.5 14 6.8 12 L

6.3 33 6.6 20 6.8 18 6.7 12

6.5 21 7.0 18 5.9 12 L

6.6 33 6.1 20 7.2 18 5.7 11

5.8 10 5.8 13 6.1 15 6.4 17 5.2 21 5.0 26 L

5.7 16 5.7 13 6.1 18 5.1 21 4.8 26 L

5.6 13 6.0 17 5.8 19 4.4 27

5.3 14 5.8 15 6.0 18 4.6 20 4.0 27 CS

6.7 32 6.4 20 7.1 18 5.5 16

6.7 32 6.5 20 7.0 16 5.9 9

6.3 20 7.2 17 5.7 9 L

6.7 24 6.3 19 7.2 16 5.8 8 L

6.9 23 6.7 20 7.0 16 7.0 13 6.0 8 CS

7.2 23 7.0 20 7.6 17 6.9 13 5.8 8 CS

5.5 12 6.1 13 6.4 16 4.7 20 4.6 26 CS

5.5 13 6.1 17 5.0 20 4.1 27 CS

5.5 11 4.9 13 6.0 16 6.0 20 4.1 23 3.8 29 L

5.7 12 5.5 15 6.0 17 5.9 19 4.5 23 3.3 30 3.0 33 CS

5.3 12 4.8 14 5.4 17 4.5 20 3.1 31 2.3 34 CS

5.6 11 5.1 14 5.6 17 4.7 25 4.3 24 3.7 28 3.3 33

On Top of Large Boulder Approx. 300' W of Sta 51

Sta	−	HI 1278.34	+	Elev
52	1.2			77.1
53	4.4			73.9
54	7.9			70.4
55	10.5			67.8
TP	11.33			1267.01
+		1267.39	0.38	
56	3.2			64.2
57	6.7			60.7
58	9.9			57.5
59	12.6			54.8
TP	10.97			1256.42
+		1258.42	2.00	
+55	4.3			54.1
60	4.4			54.0
61	4.8			53.6
62	4.9			53.5
63	5.0			53.4
64	4.8			53.6
65	5.1			53.3
BM	4.95			1253.47
66	4.9			53.6
67	5.2			53.2
68	5.1			53.3
TP	5.38			1253.04
+		1260.19	7.15	
+67	12.5			47.7

L H.I. 55 R

CS 63 6.8 6.1 6.8 6.7 5.7 / 23 19 16 14 12 8

L 5.9 6.1 6.4 5.9 / 19 16 12 9

CS 5.3 4.9 4.8 5.1 6.2 6.8 6.0 / 30 22 20 16 16 13 10

5.1 5.0 5.0 6.3 6.2 / 33 20 16 14 10

5.7 5.6 4.2 4.2 3.2 / 12 15 18 26 35

5.7 5.6 5.7 4.2 4.6 4.6 / 13 14 16 19 31 35

5.7 6.1 4.3 4.4 / 12 15 18 33

5.9 6.2 4.6 4.6 3.9 5.1 / 12 16 19 22 25 31

4.7 4.7 4.7 6.3 / 22 20 16 15

4.7 4.7 5.3 6.2 5.7 / 32 20 16 14 10

5.9 5.1 5.8 5.4 / 32 19 17 11

5.5 5.5 6.9 5.8 / 33 20 17 13

5.9 6.4 4.8 4.9 5.8 / 13 16 19 28 32

5.6 6.6 6.7 5.4 5.5 6.5 / 11 17 24 26 29 33

5.7 7.5 8.1 8.0 5.5 5.6 / 15 17 20 24 28 32

6.6 6.6 7.9 6.6 5.6 5.0 / 11 19 20 24 26 29

5.9 6.0 6.6 6.4 5.7 / 20 21 19 15 11

6.7 7.1 7.1 6.5 6.5 5.8 / 26 24 22 21 17 10

6.3 7.8 7.8 6.6 6.8 5.8 / 25 24 21 19 16 9

6.6 8.0 8.1 6.6 6.0 / 26 24 21 19 11

6.8 8.0 8.5 6.7 6.0 5.8 / 26 23 21 19 13 9

7.0 8.9 8.9 6.7 6.6 5.9 / 26 24 22 20 14 9

6.7 8.7 8.7 6.6 6.6 5.7 / 25 24 21 19 16 9

5.6 6.1 6.6 6.4 5.0 / 11 13 16 19 27 L

5.6 6.2 6.4 7.3 7.1 6.4 6.1 / 13 13 21 22 24 26 30

5.8 6.3 6.6 8.0 7.8 7.0 4.3 / 11 13 21 23 25 26 31

6.7 6.5 6.5 7.6 7.6 6.4 7.0 / 11 14 18 21 23 26 26 33

5.7 6.2 6.4 8.1 8.1 6.5 6.2 / 10 14 20 23 26 27 31

5.6 6.2 6.6 8.5 8.5 6.8 6.5 / 11 14 21 23 26 27 31

5.7 6.3 6.6 8.3 6.6 5.8 / 11 15 21 23 28 30

On 7" Poplar E of Sta 65

7.1 8.6 8.6 8.4 6.9 6.3 5.8 / 25 23 21 19 14 9

6.6 8.5 8.5 6.7 6.5 5.8 / 25 23 21 20 14 9

6.7 8.3 8.3 6.6 5.9 / 25 23 21 19 9

4.7 6.4 6.8 8.5 8.5 6.7 6.1 / 12 15 20 23 25 26 30

5.7 6.3 6.5 8.3 9.3 6.2 5.4 / 12 15 20 23 25 27 32

5.7 6.3 6.5 8.3 8.3 6.2 / 12 15 20 23 25 27

Bot of C.M.C.

Sta	−	H I	+	
69	6.9	1260.19		53.3
70	6.7			53.5
71	6.7			53.5
72	6.4			53.8
73	5.9			54.3
74	5.4			54.8
75	4.4			55.8
76	2.5			57.7
TP	0.42			1259.77
+		1272.10	12.33	
77	10.3			61.8
78	6.9			65.2
+60	4.9			67.2
79	3.3			68.8
TP	0.12			1271.98
+		1284.41	12.43	
80	11.8			72.6
+50	9.8			74.6
81	8.1			76.3
82	4.2			80.2
83	1.8			82.6
84	0.3			84.1
TP	0.33			1284.08
+		1290.51	6.43	

12-2-26 L 5.5 R

L	R
L 6.7/25 8.0/23 8.0/21 6.7/18 5.8/10	5.8/13 6.0/15 6.2/18 6.4/20 7.8/22 7.8/24 6.6/26 5.6/28
L 6.5/25 8.2/23 8.2/21 6.6/19 6.3/12 5.7/10	5.7/13 6.3/15 6.6/21 7.5/22 7.5/25 5.7/28
L 6.7/26 8.1/23 8.1/21 6.6/20 6.3/14 5.9/10	5.8/13 6.2/16 6.5/21 7.3/23 7.3/25 5.3/27 L
L 6.5/22 7.1/21 6.7/14 6.0/10	5.7/14 6.1/15 6.0/20 5.2/23 5.0/26 L
L 6.3/14 5.7/10	5.3/12 6.0/16 6.0/19 5.0/22 4.5/26
C.S. 6.8/30 6.5/14 5.9/10	5.4/15 5.5/23 4.2/27 4.0/33
CS 6.8/31 6.2/18 6.5/14 5.7/11	5.9/11 4.8/16 4.9/22 3.8/28 L
CS 7.6/27 6.9/15 5.9/11	4.9/14 5.6/18 4.2/23 3.9/31 CS
CS 8.6/26 7.9/16 6.8/12 5.7/6	5.4/11 6.0/16 6.4/19 5.7/21 4.8/32 CS
CS 6.7/33 6.1/23 5.9/15 6.6/10 6.0/9	6.0/11 6.4/13 4.6/18 4.8/26 3.0/32 CS
CS 5.4/24 4.7/14 6.6/12 6.2/9	5.7/10 6.3/13 1.6/21 1.5/25 1.2/31 CS
CS 6.1/29 5.2/21 4.8/13 6.2/11	6.0/12 6.3/13 1.1/23 0.9/32 0.4/37 CS
CS 4.7/34 4.0/27 3.6/18 6.8/11 6.4/10	6.0/10 6.4/12 1.7/23 0.7/31 0.3/36 CS
C.S. 5.4/33 4.7/27 4.4/21 5.0/20 6.0/12 6.6/11 6.1/10	5.8/11 6.1/13 1.3/24 0.3/30 0.0/37 CS
CS 6.3/33 5.0/20 5.8/18 5.8/15 6.0/10	5.8/12 6.2/14 2.7/21 2.1/25 1.8/36 L
CS 7.0/32 6.2/18 6.7/15 5.6/8 5.6/7	5.3/13 5.1/15 6.0/18 4.6/22 L
CS. 6.7/32 6.1/19 6.6/17 5.4/8 5.6/7	5.6/14 5.3/16 6.0/18 4.8/22 4.4/28 L
CS 6.7/33 5.6/20 6.4/16 5.3/8 5.5/7	5.5/12 5.3/14 6.1/18 4.8/20 4.9/32 L

Sta	−	HI	+	Elev.	
		1290.51			
85	5.7			1284.8	L
86	5.5			85.0	
87	5.4			85.1	
88	5.3			85.2	
89	5.2			85.3	
90	6.1			84.4	
91	7.3			83.2	
+94	8.9			81.6	
T.P. BM	12.32			1278.19	
+		1282.92	4.73		
92	1.3			81.6	
93	2.6			80.3	
94	5.4			77.5	
95	8.2			74.7	
96	9.5			73.4	
97	10.4			72.5	
97	12.2			70.7	
98	9.9			73.0	
99	8.1			74.8	
100	5.2			77.7	
101	1.2			81.7	
TP	1.08			1281.84	
+		1293.79	11.95		

12-2-26

55

L 5.8 5.3 6.4 5.4 5.5 — 6.8 5.6 6.6 6.9 5.2 L
29 18 15 8 6 13 14 18 20 24

L 5.5 6.7 5.5 5.6 — 5.7 5.4 6.3 5.7
18 15 8 6 13 14 18 21 L

L 5.4 6.5 5.6 — 6.6 5.4 6.6 5.7 5.9 L
18 13 8 12 13 18 21 31

L 5.5 6.4 5.3 5.6 — 5.6 5.4 6.3 5.6
18 15 8 7 12 13 18 22 L

L 5.4 5.6 6.6 5.4 — 5.6 5.4 6.6 5.9
30 19 16 8 12 13 17 21 L

L 5.2 5.1 6.3 5.6 — 5.6 5.5 6.5 5.9
30 18 15 8 11 13 17 20 L

L 4.5 5.9 6.0 5.5 — 5.7 5.7 7.0 6.1
30 19 15 11 11 13 18 21 L

4.6 5.2 6.0 5.6 — 6.0 6.5 6.2 6.6 L
32 22 17 12 13 18 21 30

On 4" Poplar E of Sta 92

L 5.0 6.1 6.1 5.5 — 6.0 6.6 6.1 6.5
21 19 15 11 12 17 19 32

L 4.4 6.5 6.5 5.7 5.9 — 6.9 5.7 6.8 6.8 5.7 6.6
23 18 15 17 18 10 11 16 18 22 28 CS

4.0 4.8 6.3 6.4 5.6 — 5.9 7.4 7.3 7.0 7.1
27 21 19 16 13 17 15 18 19 25 CS.

L 3.2 3.9 5.7 5.7 5.9 — 6.0 6.8 6.7 7.2
27 22 19 15 13 11 15 19 24 CS

4.1 4.2 5.4 6.7 6.5 5.7 — 6.0 7.3 L
30 27 24 20 16 11 9 14

5.1 5.9 6.9 6.9 5.6 — 5.7 7.2 L
28 24 22 14 11 9 12

Bot. of C.M.C.

CS 6.4 6.8 7.2 7.2 6.9 5.9 — 5.8 6.9 L
31 25 23 18 16 11 8 10

L 6.5 7.7 7.2 5.6 — 5.7 7.0 7.0 6.0
26 23 19 12 8 11 14 16 L

L 6.3 7.3 7.2 5.8 — 5.5 6.3 6.3 5.1 5.0 CS
22 20 17 12 9 13 14 17 21

L 6.0 7.4 7.2 5.9 — 5.5 6.1 5.8 3.9 4.0 3.8
23 19 17 12 10 13 14 18 21 32 CS

28

		1293.79		
102	7.3			1286.5
+60	4.8			89.0
103	3.7			90.1
104	0.5			93.3
TP	0.55			1293.24
+		1300.30	7.06	
+65	5.5			1294.8
105	4.7			95.6
106	3.1			97.2
107	3.7			96.6
108	4.0			95.5
BM	4.90			1295.40
109	5.1			95.2
110	5.1			95.2
111	5.4			94.9
112	5.4			94.9
113	5.8			94.5
114	6.2			94.1
TP	6.33			1293.97
+		1297.61	3.64	
115	4.1			93.5
116	4.7			92.9
117	5.1			92.5
118	5.2			92.4

12-4-26

5.5

L 5.7 6.3 6.2 5.8 — 30 18 16 14 — 5.5 5.9 9.0 L — 11 13 18

L 5.6 6.9 6.9 6.0 — 22 19 18 14 — 5.6 6.2 4.9 — 9 13 18 L

L 5.4 6.8 5.9 — 22 18 14 — 5.6 5.6 6.3 5.2 L — 9 11 13 16

L 5.3 6.5 5.6 — 23 19 14 — 5.6 6.5 5.3 5.4 — 9 13 16 21 CS.

L 5.2 6.1 6.1 5.6 — 23 21 19 16 — 5.8 6.5 5.6 6.1 — 9 12 16 24 CS

L 5.1 6.1 5.7 — 24 20 18 — 5.7 6.6 6.5 5.8 5.5 5.8 — 8 11 13 16 20 31

L 5.0 6.6 6.0 — 23 20 16 — 5.8 6.9 5.7 6.0 — 7 11 18 26 L

L 4.1 4.7 6.10 6.1 5.6 — 31 25 22 19 16 — 5.9 7.2 7.2 6.7 — 7 11 13 16 L

CS 3.7 4.4 6.0 6.0 5.5 — 31 24 21 19 17 — 5.6 6.7 7.0 6.5 — 6 9 12 13 L

On 10" N Pine SE of Sta 109

CS 4.5 5.5 6.2 6.2 5.5 — 31 27 23 19 16 — 5.7 6.7 6.7 5.8 — 7 10 12 14 L

CS 4.6 5.1 6.0 6.1 5.8 — 31 27 19 17 14 — 5.7 6.6 6.8 5.8 — 10 13 15 18 L

CS 4.2 4.8 5.8 6.3 5.5 — 30 21 18 16 14 — 6.6 6.4 6.5 5.9 — 12 14 16 19 L

CS 4.3 4.9 6.0 5.8 5.5 — 31 22 18 16 14 — 5.9 6.5 6.8 6.1 6.6 — 12 14 17 18 26 CS

CS 5.3 5.6 6.4 6.5 5.8 — 30 21 18 15 12 — 5.9 6.5 6.5 5.7 6.6 — 12 14 16 19 26 CS

CS 6.1 6.3 6.6 6.8 5.6 — 30 20 18 16 11 — 5.9 6.6 6.6 5.7 — 11 14 16 19 L

L 5.8 6.2 6.9 7.1 5.5 — 30 22 19 16 12 — 5.6 6.5 6.6 5.8 — 10 13 15 17 L

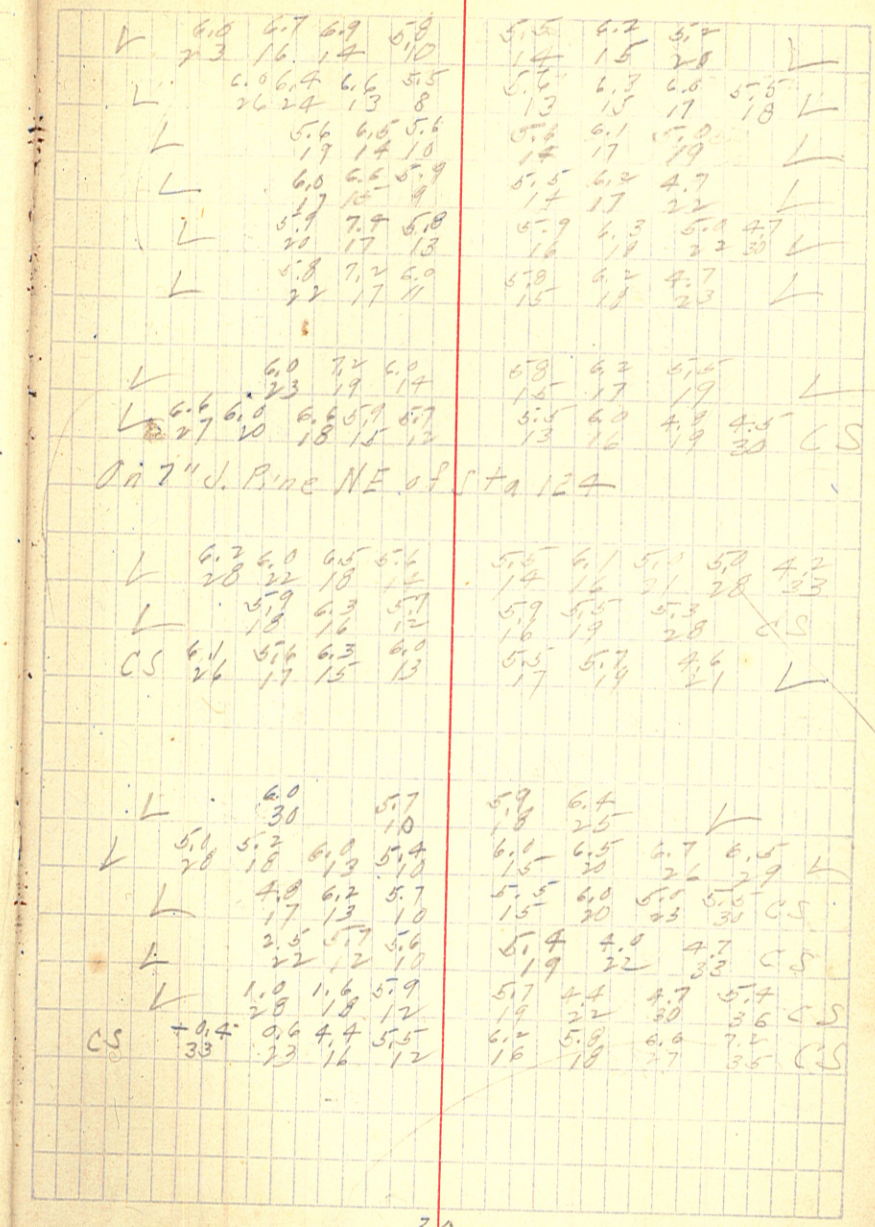
6.0 6.3 7.0 6.9 5.5 — 32 21 18 16 12 — 5.7 6.5 6.6 5.7 — 11 14 16 19 L

5.8 6.1 6.7 6.7 5.9 — 32 17 15 13 12 — 5.7 6.2 6.5 5.4 — 12 14 16 19 L

L 5.9 6.1 6.1 6.5 6.0 — 32 19 16 12 11 — 5.5 6.2 6.2 5.3 — 12 15 17 19 L

119	5.5	1292.61		1292.1
120	6.4			91.2
121	7.0			90.6
122	7.1			90.5
+70	7.5			90.1
TP123	8.14			1289.97
+		1290.25	0.78	
124	3.3			86.9
125	6.2			84.0
TPBM.	2.74			1287.51
+		1287.71	0.20	
126	6.4			81.3
127	8.6			79.1
128	11.5			76.2
TP	12.00			75.71
+		76.90	1.19	
129	4.3			72.6
130	5.1			71.8
+55	5.8			71.1
131	7.2			69.7
+50	8.7			68.2
132	12.0			64.9
TP	12.10			1264.80
+		1273.42	8.62	

5.5



30

		73.42			
+20	9.6			1263.8	
+52	11.2			62.2	
133	12.6			60.8	
+35	13.6			59.8	
+37	14.6	Top of CMC		58.8	
134	12.9			60.5	
+60 135	14.2			62.2	
	14.7			63.7	
+65	7.4			66.0	
136	5.7			67.7	
+45	3.3			70.1	
+75	2.6			71.4	
137	1.6			71.8	
+65	1.3			72.1	
138	1.1			72.3	
TP	0.64			1272.78	
+		1278.56	5.78		
BM	5.17			1273.39	
+55	5.0			73.6	
139	4.2			74.4	
+55	3.0			75.6	
140	1.3			77.3	
TP	0.73			1277.83	
+		1287.17	9.34		

→ On 7" d Pine N.W. of Sta 137

		1287.17		
+45	8.1			1279.1
141	6.9			80.3
+65	3.9			83.3
142	2.6			84.6
+45	1.7			85.5
+67.0	1.7			85.5
143	2.3			84.9
+80	4.2			83.0
144	5.0			82.2
+60	8.8			78.4
145	11.7			75.5
TP B.M.	9.95			1277.22
+		1280.57	3.35	
+40	7.4			73.2
+75	8.2			72.4
146	8.4			72.2
146	10.3			70.3
147	8.1			72.5
148	6.6			74.0
149	4.7			75.9
+45	3.8			76.8
150	3.0			77.6
TP	2.95			1277.62
+		1289.56	11.94	

12-7-26

5.5

CS 9.2/38 7.3/16 6.1/12 | 5.3/14 4.4/20 2.6/26 1.2/36 CS

CS 8.9/29 7.4/19 6.0/14 | 4.7/11 4.5/16 3.2/20 2.7/27 0.9/33 0.2/37

CS 7.7/28 5.8/15 | 5.6/12 3.6/19 2.3/27 1.9/31 1.4/38

CS 7.1/30 6.1/16 5.8/13 | 5.3/11 5.6/14 3.7/20 2.8/34

CS 6.0/28 5.2/16 5.5/13 | 5.3/9 5.5/14 3.0/19 2.6/32 L

CS 6.6/37 6.1/31 5.4/17 5.8/14 | 5.3/14 2.6/19 2.6/26 2.6/29 1.5/36

CS 7.2/35 6.2/26 5.5/16 | 5.6/9 5.3/14 2.4/18 2.3/26 1.6/34 L

CS 7.1/35 5.7/23 | 5.4/6 5.2/11 1.8/27 L

CS 6.8/33 6.4/29 5.4/20 5.1/8 | 5.6/3 6.2/7 5.0/11 2.2/33 L

CS 7.8/34 6.9/25 5.7/20 5.2/9 | 7.2/26 7.8/32

CS 7.8/33 6.9/26 5.3/22 5.1/12 | 6.2/24 CS

On 7" J. Pine S.E. of Sta 145

7.0/37 6.3/24 4.8/20 | 5.8/11 6.1/15 7.4/36

7.0/37 6.4/25 5.1/20 | 5.7/5 6.7/10 7.0/24 L

L 6.9/25 5.8/21 5.4/11 | 5.8/4 6.2/6 7.0/11 7.0/21 6.6/31

Bot. of C.M.C

6.1/34 5.8/29 6.2/25 6.0/21 | 5.2/9 4.7/14 4.2/29

6.0/38 5.7/25 6.6/22 5.9/17 | 5.6/9 5.2/12 5.0/30

6.0/33 6.5/19 5.6/16 | 5.6/6 6.1/20 5.4/25 5.0/39

7.0/35 6.4/23 6.6/18 6.0/16 | 5.7/7 6.4/11 5.7/14 4.9/30

7.0/36 6.2/22 6.5/18 6.0/16 | 5.6/9 3.3/14 2.0/29 L

		1289.56			
+60	11.9			1277.7	
151	11.7			77.9	
+55	12.8			76.8	
152	14.2			75.4	
+55	14.7			74.9	
153	14.5			75.1	
+65	12.0			77.6	
154	11.0			78.6	
155	8.3			81.3	
+60	7.0			82.6	
156	7.0			82.6	
+45	5.9			83.7	
157	4.6			85.0	
+55	2.4			87.2	
158	1.3			88.3	
+50	1.0			88.6	
159	1.6			88.0	
TP	3.75			1285.81	
+		1289.48	3.67		
160	3.7			85.8	
+35	4.4			85.1	
+75	5.0			84.5	
161	5.8			83.7	
+55	6.8			82.7	

6.4 5.8
34 15

5.7 6.3 6.3 4.9 4.2
6 8 14 18 34

CS 5.2 4.7 3.5
31 20 16

5.7 2.7 L
8 15

6.3 5.8 6.3 5.8
32 21 18 16

5.9 4.1 3.8
4 13 31

7.5 6.8 5.5
33 20 16

3.5 6.3 6.9 6.0 4.3
6 9 17 24 33

L 8.3 7.6 5.8
26 21 15

5.8 7.0 6.8 5.7
5 8 17 33

CS 8.0 7.0 5.6
27 20 15

5.7 6.7 7.2 7.0
6 9 14 29 CS

CS 6.2 6.0 5.5
35 20 15

5.5 6.4 6.7 5.7 5.2
8 12 22 26 34

CS 7.1 5.5
32 16

5.7 6.3 5.3 3.5 3.8
10 17 20 24 35

CS 8.0 6.1
32 15

5.5 2.5 1.2
14 21 37 CS

CS 8.5 5.8
32 14

5.5 5.9 2.9 2.4
15 14 20 33 CS

CS 9.7 7.6 6.1
30 16 12

5.7 5.9 4.9 2.8
11 14 18 33 CS

CS 10.0 8.4 6.1
25 16 11

5.6 6.8 3.3 0.9
12 13 28 34 CS

CS 10.1 9.0 6.0
24 17 11

5.6 6.0 3.9 1.5
12 15 20 33 CS

CS 10.0 8.7 6.6
23 15 11

5.6 6.0 1.6 0.3 +0.4
12 14 24 29 36 CS

9.5 8.3 6.0
25 15 11

5.8 6.1 1.9 0.4
11 15 22 31 CS

CS 10.0 6.1
31 12

5.6 5.9 2.7 1.1
11 14 22 33 CS

CS 8.7 5.9
31 11

5.4 5.8 3.3 1.9
10 13 19 33 CS

CS 7.4 7.0 7.1 5.7
34 19 17 11

5.7 6.0 4.9 3.8
10 13 17 28 CS

7.0 6.5 6.9 5.5
32 20 17 12

6.0 5.3 4.6
13 17 32

L 4.7 6.0 5.5
21 18 14

6.0 4.9 4.6
12 15 30

5.0 4.6 5.6 5.4
34 21 17 13

5.6 5.9 5.3 4.2
10 13 17 34

8.5 7.1 5.7
28 17 13

5.8 6.2 5.5 5.7
9 14 18 32

162	7.3	1289.48		1282.2
+70	8.1			81.4
163	7.4			82.1
+75	6.8			82.7
164	6.8			82.7
BM	9.10			1280.38
+80	7.7			81.8
165	7.5			82.0
165+08	10.6			78.9
+38	6.7			82.8
166	4.1			85.4
+60	3.2			86.3
PC +72.97	3.2		Void	86.3
167	2.9			86.6
+50	3.1			86.4
168	5.2			84.3
+50	7.2			82.3
PT +81.86	8.80			80.7
TP	8.80			1280.68
+		1285.38	4.70	
169	5.5			79.9
+50	8.5			76.9
170	10.8			74.6
+67	13.8	Bot. of CMC		71.6
+50	11.8			73.6

℄ Elev. projected to ℄ of 60C.

5.5

8.2/33 7.5/18 5.7/11 | 5.7/10 6.8/14 5.0/19 4.5/30 CS

CS 7.6/29 6.7/15 5.7/12 | 5.3/9 5.4/12 4.2/17 3.5/25 L

7.7/35 7.2/20 7.1/17 5.8/13 | 5.5/10 6.8/13 4.2/18 3.7/30

7.4/35 6.7/23 7.2/21 7.3/17 5.7/14 | 5.5/8 6.0/12 4.2/17 3.7/31

7.5/36 6.6/22 7.0/19 6.0/14 | 5.4/9 5.6/12 4.1/18 3.6/32

On 12" J. Pipe S. of Sta. 164

CS 8.6/32 7.7/19 6.0/15 | 5.7/7 6.5/12 5.8/17 5.2/32

CS 9.2/34 8.2/19 6.8/14 | 5.7/6 6.8/10 5.5/13 5.8/31

Bot. of CMC

CS 8.6/36 8.2/21 5.5/15 | 5.6/4 6.2/6 6.1/18 5.6/21 5.1/33 CS

CS 6.5/38 5.7/25 6.4/21 5.6/17 | 5.6/4 6.4/6 6.5/12 5.6/17 4.6/32 L

CS 5.1/44 3.9/34 4.0/26 5.5/21 | 5.5/6 3.6/11 L

CS 5.0/44 4.0/35 3.8/27 5.7/21 | 5.4/6 3.6/12 3.4/24 L

CS 4.9/21 4.4/27 4.1/20 5.9/13 | 5.0/12 3.5/17 3.3/28 L

CS 4.6/39 3.7/20 3.1/10 5.8/3 | 5.0/25 2.5/33 L

CS 5.6/43 5.7/33 4.0/12 5.6/5 | 5.5/24 3.8/28 L

CS 7.3/40 6.1/25 5.4/13 6.4/9 5.6/6 | 5.4/16 6.0/20 4.6/24 4.7/33 L

CS 9.0/40 6.7/28 5.8/13 6.3/10 5.7/7 | 5.5/15 6.6/18 5.7/22 5.4/31 CS

CS 10.6/31 8.4/13 6.0/9 | 5.4/12 4.5/17 4.5/24 3.0/34 CS

CS 10.8/31 8.6/17 5.7/9 | 5.5/13 6.2/17 4.6/24 3.7/31 CS

CS 9.6/24 8.2/14 6.3/9 | 5.8/10 7.0/14 5.2/25 4.6/23 CS

		1285.38		
171	12.1			1273.3
172	10.2			75.2
173	7.9			77.5
+60	6.4			79.0
174	5.2			81.2
+45	4.7			80.7
175	3.5			81.9
+65	0.9			84.5
TP	0.64			1284.74
+		1296.39	11.65	
176	10.0			86.4
+60	8.1			88.3
177	7.3			89.1
178	5.8			90.6
+50	4.2			92.2
179	3.2			93.2
TP	0.30			1296.09
+		1303.05	6.96	
C+94.82	5.8			97.2
180	5.6			97.4
+50	5.4			97.6
181	5.8			97.2
+50	5.9			97.1

℄ Elev. Projected to 60c.

void

55

Left					Right						
	8.5/35	8.0/23	7.0/16	6.0/11	5.5/10	6.7/14	5.3/20	4.9/32			
L			7.2/15	6.3/11	5.7/9	7.3/13	6.3/18	L			
L	5.6/30	6.0/17	6.5/14	6.0/11	5.8/10	6.5/13	6.8/22	6.4/34	L		
CS		5.0/30	4.5/17	5.8/14	5.9/13	6.5/23	5.0/30	4.5/35			
CS	5.6/31		4.8/18	6.0/14	5.8/12	6.5/15	6.4/21	3.6/28	2.6/35	CS	
CS		8.5/30	7.2/16	6.0/13	5.9/10	6.4/15	6.3/22	4.2/27	4.0/35	CS	
CS	8.3/31	7.2/22	6.8/17	6.3/14	5.8/11	6.4/18	5.8/23	4.5/27	3.5/35	CS	
CS	6.4/33	5.8/23	6.0/19	5.7/16	5.2/12	5.7/14	4.2/21	2.2/27	2.0/36	CS	
CS	6.7/33	6.1/23	7.0/18	5.7/13	5.4/11	6.0/14	3.1/25	2.9/34	CS		
CS	7.3/34	6.2/21	6.9/17	5.7/13	5.1/11	5.5/14	4.2/19	3.5/33	CS		
CS	7.0/32	6.2/20	6.6/17	6.0/13	5.3/12	5.8/14	4.5/19	3.7/32	CS		
CS		7.8/32	6.7/17	6.0/13	5.2/13	5.5/16	4.3/20	4.0/30	CS		
CS	6.4/33	6.2/27	7.4/18	5.6/13	5.7/12	6.3/14	4.9/19	4.4/29	L		
CS	7.0/34	6.6/22	7.6/18	5.7/12	5.4/11	6.4/15	4.9/18	L			
CS	7.1/33	6.9/23	7.0/20	6.0/13	5.7/12	6.5/16	5.4/29	L			
CS	7.1/33	6.9/23	7.0/20	6.0/13	5.7/12	6.6/16	5.4/20	L			
CS		7.0/33	6.8/21	5.6/17	5.6/7	6.0/9	5.0/14	4.7/24	5.4/29	4.7/35	L
		7.5/33	5.0/22	5.7/3	4.8/1	4.6/14	CS				
CS		7.4/39	7.0/25	5.0/19	5.4/7	3.9/14	3.5/24	L			

		1303.05		
182	5.3			1297.7
PT+40.7	5.3			97.7
T.P. BM	6.03			1297.02
+		1300.49	3.47	
183	3.7			96.8
184	4.9			95.6
185	5.2			95.3
186	4.6			95.9
187	5.1			95.4
188	5.4			95.1
189	6.5			94.0
TP	6.54			1293.95
+		1297.46	3.51	
190	4.8			92.7
191	5.4			92.1
192	5.5			92.0
+65	4.7			92.8
193	5.0			92.5
194	5.7			91.8
195	6.6			90.9
196	7.8			89.7
T.P.	7.63			1289.83
+		1292.36	2.53	

12-8-26

55

CS	7.6	6.7	7.2	5.9	5.5	4.2	3.9	CS	
	31	20	16	12	14	20	29		
L	6.5	7.4	7.2	5.8	5.6	5.9	4.8	L	
	17	14	12	9	14	17	21		
On 10" N.P. in E NW of St				193					
	6.0	6.7	6.8	5.8	5.6	6.2	5.7	4.7	
	18	16	13	10	13	15	19	29	
	6.1	6.7	6.9	6.0	5.5	5.8	6.2	5.3	
	18	15	13	9	12	15	16	19	
	6.6	6.5	6.6	5.9	5.7	5.8	4.8		
	20	17	14	10	12	16	21		
	6.7	7.3	7.3	6.9	6.2	6.1	6.5	6.4	5.5
	23	22	18	15	13	9	10	14	16
			6.2	7.0	6.0	5.5	6.2	5.7	4.7
			20	16	12	11	13	16	18
		6.9	7.4	6.6	6.7	5.8	5.5	5.8	6.4
		23	21	18	15	12	10	12	14
			6.0	7.8	7.0	6.1	6.0	6.7	6.4
			25	23	20	13	10	18	19
			6.2	7.1	6.7	5.8	6.1	6.4	6.4
			25	21	16	11	10	12	16
			7.0	7.4	7.2	6.2	5.9	6.4	6.8
			22	20	14	11	9	13	17
			6.7	7.1	7.1	5.9	5.6	6.2	6.2
			22	19	16	11	10	14	18
		6.9	7.0	7.0	6.0	5.7	6.4	6.2	5.7
		24	19	16	12	9	13	18	21
		6.0	6.7	6.7	5.9	5.6	6.7	6.7	5.7
		22	20	16	13	10	14	19	22
		5.6	6.8	6.7	5.9	5.8	6.7	6.7	5.8
		27	23	17	14	9	12	17	22
		5.8	7.2	7.1	5.9	6.3	6.8	6.7	5.8
		24	22	18	13	8	11	16	19
			5.7	7.0	6.9	5.8	6.9	6.9	5.9
			22	19	12	9	12	15	17

36

197	3.9	1292.36		1288.5
198	3.8			88.6
+65	4.1			88.3
199	4.6			87.8
200	5.6			86.8
201	6.7			85.7
TPBM	6.52			1285.84
+		1294.41	8.57	
202	8.6			85.8
203	8.2			86.2
204	8.1			86.3
205	7.1			87.3
+14	11.7	Bot. of CMC		1282.7
206	5.7			88.7
207	3.0			91.4
TP	0.32			1294.09
+		1306.21	12.12	
208	11.0			1295.2
209	6.2			1300.0
+50	3.5			1302.7
210	1.3			04.9
TP	0.27			1305.94
+		1318.36	12.42	

6.0 6.9 5.7 6.1 7.0 6.8 6.3
25 22 13 9 12 17 19
6.1 7.2 7.1 5.7 5.9 7.5 7.4 6.2
25 23 17 13 7 13 20 22
5.9 6.6 7.1 7.1 5.9 6.0 6.7 7.4 7.8 6.2
26 24 22 18 13 8 10 15 21 26
5.7 7.0 7.0 6.2 6.0 6.7 7.4 7.3 6.6
28 25 18 14 8 10 16 18 19
L 6.2 8.0 6.5 7.0 6.9 6.3 6.1 6.5 6.8 7.9 8.2 7.1 L
31 28 25 21 14 11 10 14 18 20 24 25
L 6.2 6.2 8.0 8.0 6.2 5.9 6.1 6.4 7.8 7.4 6.8 L
30 27 25 23 21 17 17 18 21 23 24

On Tel. Pole W of Sta 202

L 6.7 8.0 8.0 6.5 6.3 6.1 6.8 7.9 7.6 6.5 L
28 26 23 21 11 21 20 21 23 25
L 7.2 8.2 8.2 7.1 6.4 6.1 6.5 7.0 8.0 8.0 6.7 L
27 26 22 21 13 12 12 18 22 24 25
L 7.6 8.5 8.7 7.4 6.6 6.1 6.1 6.5 7.8 8.0 7.2 L
27 26 22 21 11 10 12 19 21 24 26
7.9 8.2 9.0 9.0 8.3 6.8 6.6 7.3 8.6 7.7 L
32 28 26 22 21 13 19 20 24 26

CS 8.8 7.1 6.3 6.1 6.7 6.5 5.9 5.7 CS
32 14 13 14 15 19 22 32
CS 8.5 6.8 6.3 6.3 6.5 4.4 3.6
30 17 15 13 16 21 33 CS

CS 8.0 7.1 6.4 6.5 4.6 3.2 CS
31 20 14 17 20 33
6.4 7.0 6.5 6.8 6.3 6.2 4.8 3.4
32 27 19 18 14 16 18 32 L
CS 6.9 6.6 6.3 5.6 3.7 3.0 CS
32 19 14 17 20 33
CS 6.4 6.2 6.8 6.0 5.2 3.3 2.7 CS
31 19 17 14 16 20 33

		1318.36		
214	8.5			1309.9
212	4.9			1313.5
+60	3.4			15.0
213	2.6			15.8
+30.6	2.0			16.4
+70	1.7			16.7
214	1.5			16.9
215	1.3			17.1
216	2.9			15.5
+50	4.1			14.3
217	5.7			12.7
+60	8.2			1310.2
218	10.1			08.3
TP	10.05			1308.31
+		1310.41	2.10	
219	6.6			1303.8
220	11.0			12 99.4
BM	2.82			1307.59

5.5

CS 5.9 3.2 5.1 1.6 6.1 1.4 4.5 1.3 6.2 1.6 2.9 1.9 2.7 3.2 CS

CS 6.8 3.1 5.8 1.6 4.4 1.3 6.1 1.3 5.2 1.6 2.9 1.9 2.2 3.2 CS

CS 6.5 3.2 5.6 1.6 6.6 1.4 6.3 1.4 4.9 1.6 2.8 2.0 2.2 3.3 CS

CS 6.2 3.1 5.7 1.6 6.4 1.3 5.8 1.3 5.6 1.5 2.6 2.1 2.6 3.3 CS

CS 6.2 3.1 5.4 1.5 6.4 1.2 5.6 1.5 4.7 1.3 2.4 2.1 1.8 3.3 CS

CS 6.9 3.1 5.1 1.5 6.3 1.2 5.6 1.5 4.9 1.7 2.0 2.2 1.8 3.4 CS

CS 5.8 3.1 5.0 1.4 6.2 1.2 5.9 1.5 2.7 2.1 2.5 3.3 CS

CS 5.6 3.2 4.8 1.6 6.2 1.2 5.4 1.6 3.1 2.2 2.3 3.4 CS

CS 5.3 3.0 4.9 1.6 6.3 1.2 6.1 1.6 3.3 2.2 2.8 3.4 CS

L 4.5 1.8 6.3 1.2 6.3 1.6 3.4 2.2 L

L 4.7 1.4 6.5 1.4 6.4 1.5 3.8 2.1 3.4 CS

L 4.8 2.0 6.3 1.4 6.2 1.6 3.6 2.0 L

L 4.7 1.7 6.4 1.1 6.8 1.9 5.8 1.4 6.4 1.5 4.6 2.0 L

On 12" Pine (old BM) SE of Sta 219

Slater Township 142-26

Between Secs 16, 17, 20, 21, 28, 29

	−	HI	+	Elev
BM		104.1	4.10	100.00
42	4.5			99.6
43	3.9			100.2
+96				
44	5.1			99.0
45	5.4			98.7
+69	4.0			100.1
+80	5.2			98.9
46	6.0			98.1
47	4.4			99.7
+79	2.5			101.6
TP	0.40			103.70
+		115.02	11.32	
48	10.4			104.6
49	1.1			113.9
TP	0.35			114.67
+		118.19	3.52	
+33	3.6			114.6
+78	8.8			109.4
50	10.6			107.6
TP	11.71			106.48
+		110.69	4.21	
50+76=57	6.2			104.5

4-30-27

Robt Pohl - Rod
Roy Pohl - Chain
Tavtman Asst Engr

On 46 "N. Pine S of Sta 41

swamp

1/4 Cor Bet. Secs 28 & 29-142-26

CS 7.6 12.2 13.4
43 18

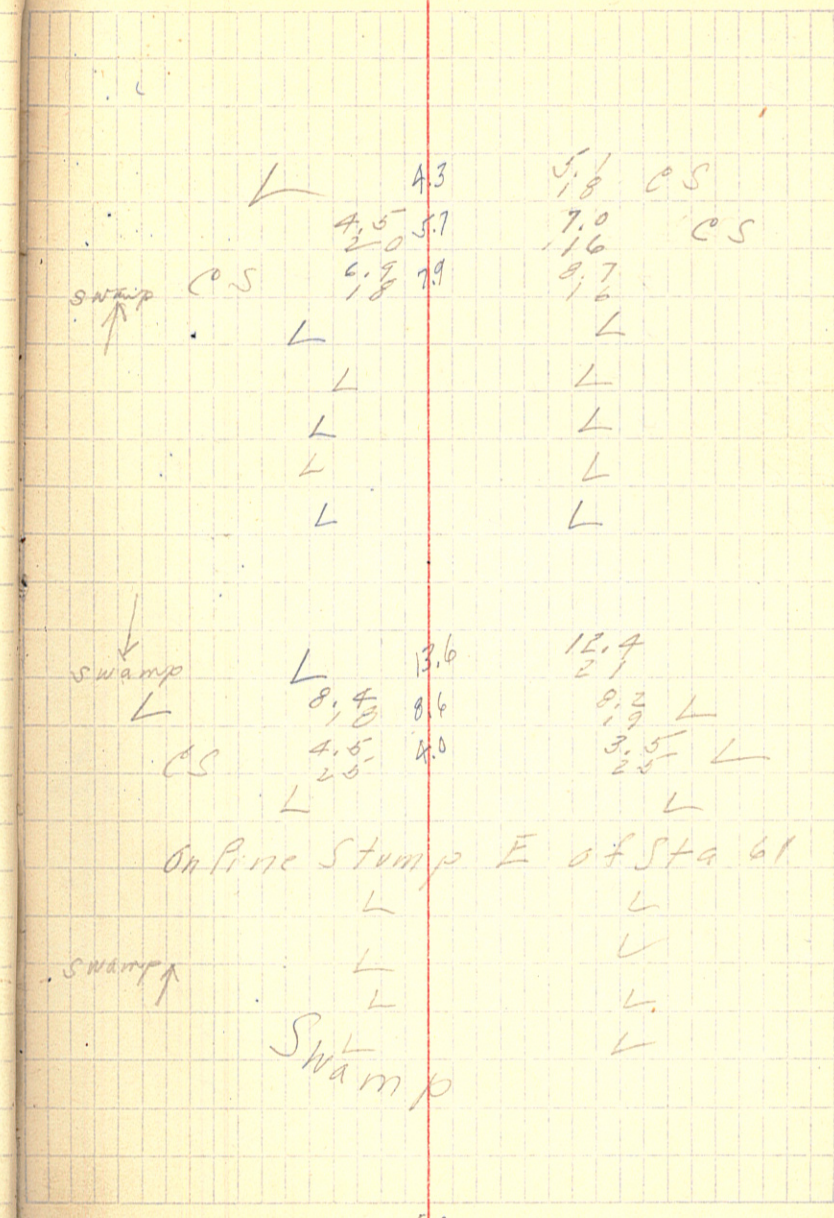
CS 4.6 7.8 12.6
40 20 13

CS 0.1 3.2 5.9 C.S.
8 11 13 24

0.6 2.0 3.6 6.9 8.0 CS
33 17 1 7 25

CS 5.6 6.8 10.5 12.4
2.9 19 15 28
8.8 12.5
18 19

		110.69			
+50	5.4			105.3	
52	6.5			104.2	
53	5.8			104.9	
+70	4.3			106.4	
54	5.7			105.0	
54+24=57	7.9			102.8	
+10	9.4			101.3	
55	9.4			101.3	
56	9.2			101.5	
57	9.3			101.4	
58	9.6			101.1	
T.P.	5.13			105.56	
+		115.41	9.85		
+55	13.6			101.8	
59	8.6			106.8	
60	4.0			111.4	
61	2.8			112.6	
TP BM	1.48			113.93	
+62	2.7	116.78	2.85	114.1	
63	5.2			111.6	
64	6.5			110.3	
65	7.4			109.4	
66	7.9			108.9	
TP	7.46			109.32	
+		117.31	7.99		



		117.31		
67	6.7			110.6
68	4.8			112.5
69	5.8			111.5
70	5.8			111.5
+ 31				
71	3.9			113.4
TP 72	4.13			113.18
+		118.00	4.82	
+56	4.4			113.6
+63	5.2			112.8
73	5.3			112.7
74	3.4			114.6
BM	2.92			115.08
BM		103.74	3.74	100.00
92	3.0			100.7
93	4.6			99.1
94	4.5			99.2
+60	7.6			96.7
95	7.6			96.7
96	8.2			95.5
97	8.1			95.6
+22	7.9			95.8

Swamp

Cor Secs 28, 29, 20, 21 - 142 - 26

4.3 2.2 4.8 5.5 2.2

Swamp

On Pine Stump E of Sta 74

On 3" Poplar E of Sta 93

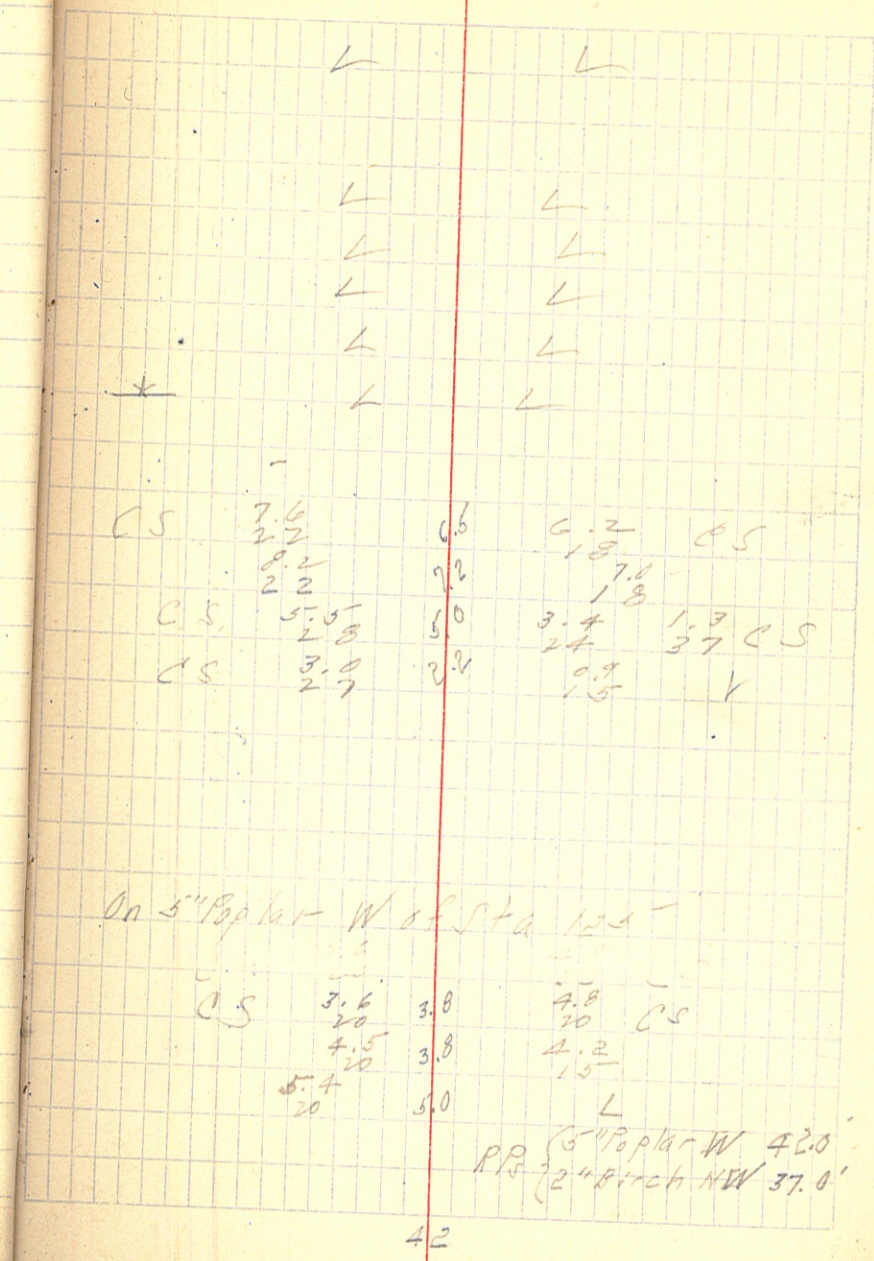
3.9 2.2 4.5 5.8 1.7 6.7 2.3

+60 Swamp

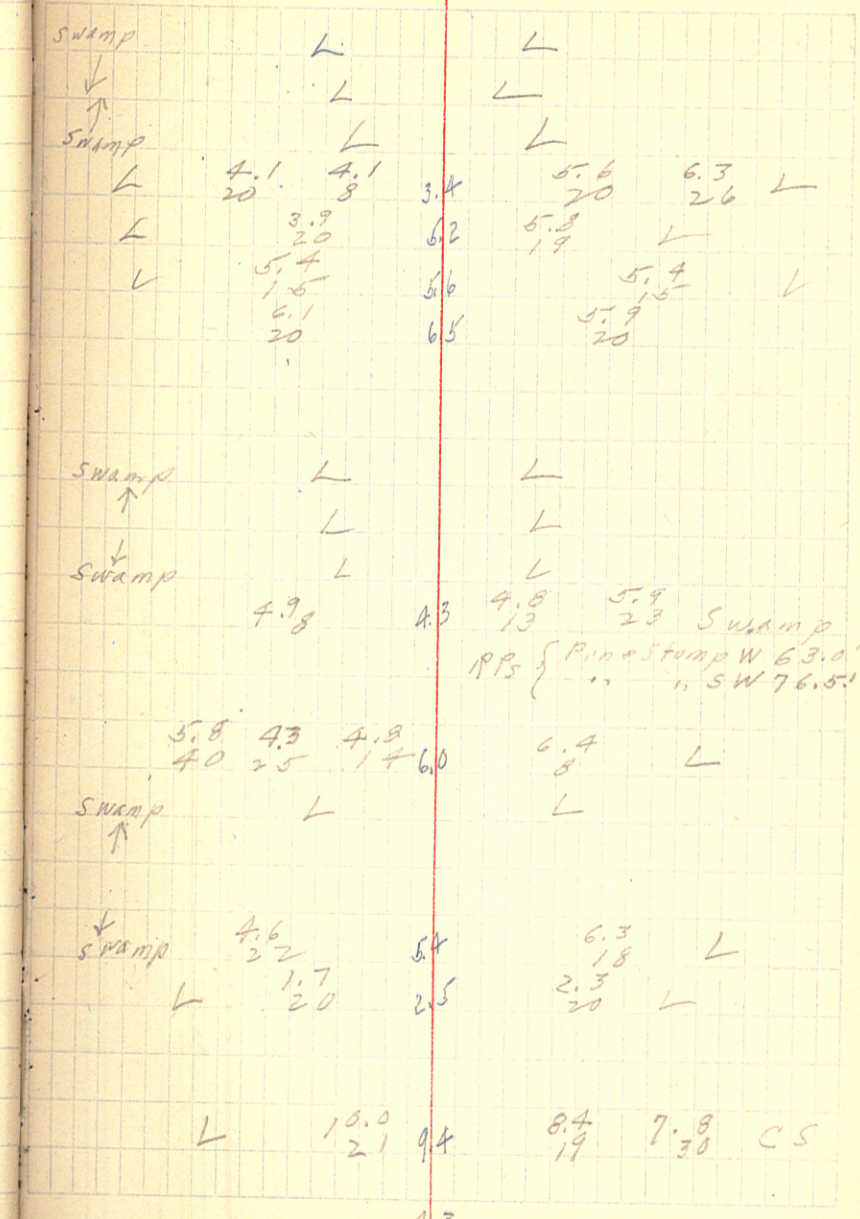
6.2 2.5 7.0 8.0 2.1

6.3 2.0 7.0 7.8 2.0

		103.74			
98	7.5			96.2	
TP	6.68			97.06	
+		107.60	10.54		
97+75	9.6			98.0	
99	11.2			96.4	
100	11.2			96.4	
+26	10.8			96.8	
+37	9.4			99.2	
TP	0.18			107.42	
+		118.72	11.30		
101	6.5			112.2	
+46	7.2			111.5	
102	5.0			113.7	
103	2.2			116.5	
+73	3.8			114.9	
104	5.3			113.4	
BM		104.14	4.14	100.0	
123	3.4			100.7	
124	3.8			100.3	
+70	3.8			100.3	
125	5.0			99.1	
125					



		104.14		
+50	6.2			97.9
+65	7.7			96.4
126	6.1			98.0
+55	3.4			100.7
127	5.2			98.9
+60	5.6			98.5
128	6.5			97.6
TP	6.64			97.50
+		103.24	5.74	
+13	6.3			96.9
+60	6.8			96.4
129	6.2			97.0
+67	4.3			98.9
+67	Δ P			
130	6.0			97.2
+05	6.4			96.8
131	6.6			96.6
132	6.6			96.6
133	5.4			97.8
+70	2.5			100.7
TP	1.30			101.94
+	[illegible]	112.61	10.67	
134	9.4			103.2



+23	6.1	112.61		106.5
+55	3.2			109.4
135	1.6			111.0
TP	0.67			111.94
+		118.02	6.08	
+60	△	L		
+60	5.8			112.2
136	5.6			112.4
+40	4.6			113.4
137	5.8			112.2
BM	7.83			110.19
138	5.2			112.8
139	1.1			116.9
TP	0.41			117.61
+		122.86	5.25	
140	4.8			118.1
141	5.8			117.1
+45	5.3			117.6
+70	7.4			115.5
142	8.0			114.9
+40	9.0			113.9
+75	8.3			114.6
143	5.5			117.4
144	5.3			117.6
BM	4.45			118.41
+35				

L 8.7/28 7.9/19 6.1 4.8/22 L
L 8.1/34 6.0/24 3.6/10 3.2 2.5/26 L
CS 3.0/34 1.4/19 1.6 2.1/27 L

RPs { Pine Stump NE 90'
" " SE 55.4

6.3/45 5.4/25 5.7/15 5.8 6.5/15 L
L 5.6 L
L 3.8/21 4.6 5.4/21 L

On 7" Basswood SE of Sta 137

CS 6.4/20 5.8 5.3/18 L
Swamp CS 7.7/18 5.3 4.2/21 L
↑ " L 8.9/13 7.4 4.2/22 3.5/34
L 8.9/7 8.0 6.2/17 4.2/27
L 9.0 8.6/19
↓ Swamp L L
L L

On 5" Poplar SW of Sta 144

1/4 Cor Bet. 16 & 17 - 142-26 44 RPs { B.T. Pine Stump S.W. 36.2'
F Post N.W. 36.1

Slope Stakes SAP #2 J6270

Sta	−	HI	+	Elev	Grade Elev.
BM 1		1250.92	0.73	1250.19	
0+00	5.5			45.4	46.1
1	4.6			46.3	46.3
2	4.5			46.4	46.6
3	4.6			46.3	46.8
4	4.6			46.3	47.1
5	4.6			46.3	47.3
+56	4.8			46.1	
6	4.7			46.2	47.4
7	4.2			46.7	47.4
TP	4.21			46.71	
+		54.95	8.24		
+35	8.0			47.0	47.4
8	7.1			47.9	47.4
9	5.5			49.5	47.5
BM	1.23			53.72	
+50	5.0			50.0	47.5
10	5.1			49.9	47.8
11	5.8			49.2	47.5
12	7.4			47.6	47.6
13	8.6			46.4	47.6
TP	8.58			46.37	
+		52.41	6.04		

May 12-1927 Party { Taubman – Asst. Engr.
Houston – Rod
Beckner – Chain

Weather – Clear & Warm

On 20" Oak Stump NW of Sta 2+00

D.C. 1.1		−0.8
21.7	−0.7	13.2 RP 46'
+0.5		−0.7
23.8	−0.6	12.3
D.C. 1.4		−0.5
22.1	−0.2	12.8
D.C. 1.0		−1.4
21.5	−0.5	14.1
D.C. 1.1		D.C. 0.3
21.7	−0.8	20.5
D.C. 0.8		−3.3
21.2	−1.0	17.5 RP 48'
D.C. 1.4		−3.3
22.1	−1.2	17.0
D.C. 1.7		D.C. 0.6
22.6	−0.7	20.9
	−0.4	
+5.4		D.C. 0.6
31.1	+0.5	20.9
+4.3		+0.5
29.5	+2.0	23.8

On 4" Rebar W of Sta 9+00

	+2.5	
+2.1		+0.6
26.2	+2.4	23.9 RP 49'
+2.9		D.C. 1.9
27.4	+1.7	22.9
+0.9		D.C. 0.8
24.4	0.0	21.2
D.C. 0.9		−2.0 S.D.
21.4	−1.2	15.0 +08 +1.2

45