

HACKENSACK-LONGVILLE ROAD

LEVEL BOOK No 1

FIELD BOOK

361

140

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L.

R.

	+S	π	-S	Rod.	Elv.
U.S. B.M.	2.75	1392.92			1390.17
T.P.	8.24	98.30	2.86		90.06
T.P.	5.51	97.21	6.60		91.70
B.M.	5.86	9847	4.60		92.61
0+00		$\frac{11.17}{87.30}$		4.6	93.9
1+00				7.0	91.5
+35				5.9	92.6
2+00				5.4	93.1
+55				4.6	93.9
3+00				5.4	93.1
4				8.0	90.5
5				9.3	89.2
+35				9.6	88.9
6				11.3	87.2
T.P.	11.04	98.34	11.17		87.30
7				11.6	86.7
8				8.8	89.5
9				8.5	89.8
+65				5.8	92.5
10				5.1	93.2
+50				5.0	93.3
11				5.3	93.0
+40				4.2	94.1
12				5.1	93.2
13				5.3	93.0

OK 0+0 13+63 Relocation 13+63
to 33+65

SP in Tel Pole R# 0+20

L.	$\frac{6.2}{24}$	$\frac{6.9}{20}$	$\frac{4.6}{12}$	4.6	$\frac{5.6}{23}$	$\frac{7.3}{30}$			
L.	$\frac{4.7}{30}$	$\frac{7.6}{26}$	$\frac{7.0}{21}$	$\frac{6.5}{14}$	7.0	$\frac{7.0}{5}$	$\frac{8.4}{12}$	$\frac{7.7}{14}$	4.
L.	$\frac{4.0}{31}$	$\frac{4.0}{25}$	$\frac{6.3}{21}$	$\frac{5.9}{21}$	5.9	$\frac{5.9}{8}$	$\frac{6.9}{11}$	$\frac{6.7}{14}$	$\frac{6.4}{28}$
L.	$\frac{2.7}{31}$	$\frac{4.8}{25}$	$\frac{4.6}{22}$	5.4	$\frac{5.9}{6}$	$\frac{6.4}{9}$	$\frac{5.8}{12}$	L.	
L.	L.	$\frac{2.5}{31}$	$\frac{4.6}{27}$	4.6	$\frac{4.6}{3}$	$\frac{5.8}{8}$	$\frac{4.5}{11}$	L.	
L.	$\frac{3.1}{31}$	$\frac{5.2}{25}$	$\frac{5.0}{21}$	5.4	$\frac{5.4}{2}$	$\frac{6.2}{5}$	$\frac{6.2}{6}$	$\frac{5.5}{7}$	$\frac{6.0}{29}$
L.	$\frac{7.3}{24}$	$\frac{8.5}{21}$	$\frac{8.0}{17}$	8.0	$\frac{9.5}{8}$	$\frac{9.5}{9}$	$\frac{8.6}{13}$	L.	
L.	L.	$\frac{8.1}{23}$	$\frac{9.3}{21}$	9.3	$\frac{11.2}{10}$	$\frac{11.2}{13}$	$\frac{11.0}{14}$	$\frac{12.2}{30}$	L.
L.	$\frac{7.9}{28}$	$\frac{9.0}{21}$	$\frac{9.0}{11}$	9.6	$\frac{9.6}{5}$	$\frac{11.3}{8}$	$\frac{11.3}{10}$	$\frac{10.5}{13}$	$\frac{12.5}{31}$
	$\frac{9.4}{28}$	$\frac{11.4}{22}$	$\frac{10.7}{17}$	11.3	$\frac{11.3}{5}$	$\frac{13.0}{10}$	$\frac{12.7}{12}$	$\frac{13.6}{26}$	

On T6 Cor. T.P.

L.	$\frac{11.4}{30}$	$\frac{12.5}{26}$	$\frac{12.4}{20}$	$\frac{11.6}{18}$	11.6	$\frac{11.6}{5}$	$\frac{13.2}{9}$	L.	
L.	L.	$\frac{8.2}{24}$	$\frac{9.2}{21}$	$\frac{8.8}{17}$	8.8	$\frac{8.8}{13}$	$\frac{10.5}{16}$	$\frac{10.5}{18}$	$\frac{8.4}{22}$
	$\frac{3.6}{36}$	$\frac{6.5}{26}$	$\frac{8.1}{22}$	8.5	$\frac{9.7}{11}$	L.			
	$\frac{1.5}{33}$	$\frac{2.7}{22}$	$\frac{5.9}{15}$	$\frac{5.2}{12}$	5.8	$\frac{6.3}{10}$	$\frac{7.6}{23}$	L.	
	$\frac{4.4}{34}$	$\frac{3.9}{20}$	$\frac{5.2}{15}$	$\frac{5.2}{13}$	$\frac{4.9}{10}$	5.1	$\frac{5.1}{12}$	$\frac{7.9}{30}$	
L.	L.	$\frac{2.4}{18}$	$\frac{5.0}{11}$	$\frac{4.6}{9}$	5.0	$\frac{5.0}{13}$	$\frac{7.3}{29}$	L.	
		$\frac{2.0}{35}$	$\frac{5.3}{15}$	5.3	$\frac{5.3}{7}$	$\frac{6.0}{17}$	L.		
	$\frac{0.8}{32}$	$\frac{1.9}{19}$	$\frac{4.2}{11}$	4.2	$\frac{4.2}{12}$	$\frac{4.0}{16}$	$\frac{5.4}{33}$	in field	
		$\frac{4.0}{33}$	5.1	$\frac{5.1}{25}$	L.				
L.	$\frac{4.6}{29}$	5.3	$\frac{4.3}{15}$	$\frac{6.0}{33}$					

O	+S	π 9834 ✓	-S	Rod.	E/v
B.M.	4.10	1398.33	4.11		1394.23 ✓
+65				6.5	91.8
14				8.3	90.0
Δ +66				12.0	86.3
15				12.6	85.7
T.P.	3.47	1389.70 ✓	12.10		1386.23 ✓
+60				3.4	86.3
16				4.6	85.1
+60				7.5	82.2
17				8.0	81.7
+45				7.9	81.8
+51				12.4	77.3
18				8.0	81.7
Δ +64				6.8	82.9
19				6.6	83.1
20				7.2	82.5
T.P.	6.64	1389.84 ✓	6.50		1383.20 ✓
21				8.4	81.4
22				8.4	81.4
23				7.1	82.7
+50				5.3	84.5
24				4.6	85.2
+50				5.1	84.7
25				6.6	83.2
26				7.8	82.0
					18" P.I. needed.

Sp. 17 T.P. RA

L	1.5	3.1	6.5	6.5	6.5	9.7		
	$\frac{4.9}{33}$	$\frac{7.6}{18}$	$\frac{8.3}{14}$	8.3	$\frac{8.8}{9}$	$\frac{10.5}{15}$	$\frac{11.3}{30}$	
	$\frac{9.0}{33}$	$\frac{10.3}{26}$	$\frac{10.4}{17}$	$\frac{12.0}{14}$	12.0	$\frac{16.4}{33}$		
	$\frac{9.1}{22}$	$\frac{11.1}{15}$	$\frac{11.3}{6}$	$\frac{12.1}{4}$	12.6	$\frac{12.6}{10}$	$\frac{16.9}{33}$	
						$\frac{3.4}{15}$	$\frac{7.6}{33}$	
	4.1 higher than 4					4.1 higher than ctr.		
	$\frac{4.2}{33}$	$\frac{5.0}{18}$	$\frac{7.0}{13}$	7.5	$\frac{7.5}{7}$	$\frac{8.6}{16}$	$\frac{11.8}{33}$	
L	$\frac{10.8}{13}$	$\frac{8.8}{10}$	$\frac{8.0}{6}$	8.0	$\frac{8.0}{4}$	$\frac{10.8}{9}$	L	
L	$\frac{11.3}{16}$	$\frac{7.9}{9}$		7.9	$\frac{7.9}{2}$	$\frac{11.7}{10}$	L	
Bottom ditch.		2.4" P.I. needed.						
	$\frac{8.3}{33}$	$\frac{8.5}{18}$	$\frac{8.0}{8}$	8.0	$\frac{8.0}{3}$	$\frac{9.5}{18}$	$\frac{10.9}{18}$	
L	$\frac{3.7}{15}$	$\frac{6.8}{7}$	6.8	$\frac{6.8}{12}$	$\frac{9.6}{20}$	$\frac{9.9}{29}$	$\frac{11.4}{33}$	
	$\frac{2.7}{33}$	$\frac{4.2}{16}$	$\frac{6.6}{9}$	6.6	$\frac{6.6}{10}$	$\frac{9.6}{18}$	$\frac{10.1}{28}$	$\frac{11.4}{33}$
		$\frac{4.3}{33}$	$\frac{6.5}{3}$	7.2	$\frac{7.2}{10}$	$\frac{9.1}{17}$	$\frac{9.6}{25}$	$\frac{10.8}{33}$
								9.8
								19.9
					$\frac{6.2}{33}$	8.4	$\frac{8.5}{13}$	$\frac{10.8}{33}$
					L	8.4	$\frac{8.4}{9}$	$\frac{10.9}{33}$
L	$\frac{5.5}{12}$	$\frac{7.3}{8}$	7.1	$\frac{7.1}{7}$	$\frac{10.7}{33}$			
$\frac{3.2}{33}$	$\frac{3.8}{12}$	$\frac{6.0}{9}$	$\frac{5.5}{5}$	5.3	$\frac{5.3}{5}$	$\frac{7.6}{22}$	$\frac{11.0}{33}$	
L	$\frac{2.9}{16}$	$\frac{5.0}{10}$	$\frac{4.6}{2}$	4.6	$\frac{4.6}{6}$	$\frac{7.6}{15}$	$\frac{8.1}{22}$	$\frac{11.0}{33}$
L	$\frac{2.1}{15}$	$\frac{5.1}{9}$	$\frac{5.1}{5}$	5.1	$\frac{5.1}{7}$	$\frac{8.8}{14}$	$\frac{9.1}{9}$	$\frac{12.1}{33}$
$\frac{2.1}{33}$	$\frac{3.1}{17}$	$\frac{1.1}{10}$	$\frac{1.1}{9}$	6.6	6.6	$\frac{7.0}{7}$	$\frac{8.8}{12}$	$\frac{8.8}{19}$
L	$\frac{8.9}{20}$	$\frac{8.3}{11}$	$\frac{9.0}{11}$	$\frac{9.0}{10}$	$\frac{7.8}{8}$	7.8	$\frac{7.8}{4}$	$\frac{10.1}{15}$
							$\frac{11.9}{20}$	$\frac{13.1}{33}$

O	+S	1389.84	-S	Rod	Elv.
27		1389.84 7.18 1382.66		8.1	81.7
28 T.P.	5.01	1387.67	7.18		1382.66
28		4.51 83.16		5.2	82.5
29				6.4	81.3
30				11.9	75.8
31				9.8	77.9
32				5.5	82.2
+20				6.1	81.6
+25				4.7	83.0
+80				2.9	84.8
33				3.8	83.9
34				5.9	81.8
35				6.5	81.2
T.P.	7.55	1390.71	4.51		1383.16
B.M.		1384.98	5.73		1384.98
36				6.9	83.9
37				6.0	84.7
38				5.4	85.3
39				5.1	85.6
40				4.2	86.5
+40				3.1	87.6
41				5.0	85.7
42				6.9	83.8
43 +25				6.2	84.5
43				7.1	83.6

L	R	4
		$\frac{4.9}{10}$ 5.1 $\frac{8.4}{3}$ $\frac{7.7}{9}$ $\frac{8.0}{22}$ $\frac{9.1}{33}$
		$\frac{4.7}{20}$ $\frac{5.7}{18}$ $\frac{5.7}{17}$ $\frac{5.2}{13}$ 5.2 L.
		L. L.
		L. L.
		$\frac{7.6}{30}$ 9.8 $\frac{11.7}{30}$
		L. $\frac{5.4}{15}$ $\frac{6.6}{13}$ $\frac{6.6}{10}$ $\frac{5.9}{7}$ 5.5 $\frac{5.9}{9}$ $\frac{7.3}{33}$
		L. $\frac{4.9}{4}$ 6.1 $\frac{6.1}{7}$ 5.1 $\frac{5.1}{22}$ 5.8 $\frac{5.1}{27}$ $\frac{5.1}{30}$ $\frac{5.2}{36}$
		L. 4.7 $\frac{5.8}{7}$ $\frac{5.8}{4}$ $\frac{5.0}{10}$ $\frac{5.0}{23}$ $\frac{5.6}{28}$ $\frac{4.8}{33}$
		$\frac{3.9}{33}$ 2.9 $\frac{3.5}{19}$ 4.6 $\frac{4.6}{24}$ $\frac{3.7}{30}$ $\frac{3.6}{33}$
		$\frac{4.2}{33}$ 3.8 $\frac{3.9}{24}$ $\frac{5.1}{26}$ $\frac{5.1}{28}$ $\frac{4.5}{33}$
		L. L.
		L. 6.5 $\frac{5.4}{33}$
		L. $\frac{7.2}{6}$ $\frac{8.0}{5}$ 6.9 $\frac{6.9}{15}$ $\frac{7.9}{21}$ $\frac{6.9}{22}$
		L. $\frac{6.4}{10}$ $\frac{7.0}{7}$ 6.0 $\frac{6.5}{15}$ $\frac{7.1}{20}$ $\frac{6.2}{21}$ L.
		L. $\frac{5.6}{8}$ $\frac{6.3}{7}$ 5.4 $\frac{5.3}{13}$ $\frac{6.2}{20}$ $\frac{5.2}{21}$ L.
		L. $\frac{5.1}{11}$ $\frac{6.3}{10}$ $\frac{5.1}{4}$ 5.1 $\frac{5.2}{11}$ $\frac{5.9}{18}$ $\frac{5.2}{19}$ L.
		L. $\frac{5.0}{13}$ $\frac{5.3}{10}$ 4.2 $\frac{4.2}{10}$ $\frac{4.4}{15}$ $\frac{3.2}{17}$ L.
		$\frac{3.9}{27}$ $\frac{3.3}{15}$ $\frac{4.1}{13}$ $\frac{3.3}{9}$ 3.1 $\frac{3.1}{8}$ $\frac{4.0}{14}$ $\frac{3.0}{16}$
		L. $\frac{4.7}{16}$ $\frac{5.8}{14}$ $\frac{5.0}{17}$ 5.0 $\frac{5.0}{4}$ $\frac{5.5}{10}$ $\frac{4.9}{11}$ L.
		L. $\frac{7.1}{8}$ $\frac{8.3}{16}$ $\frac{6.9}{8}$ 6.9 $\frac{6.9}{21}$ $\frac{7.3}{6}$ $\frac{6.8}{7}$ L.
		L. $\frac{7.0}{16}$ $\frac{7.8}{14}$ $\frac{6.2}{7}$ 6.2 $\frac{6.2}{2}$ $\frac{6.9}{8}$ $\frac{6.2}{10}$ L.
		L. $\frac{7.4}{14}$ $\frac{8.3}{12}$ $\frac{7.1}{5}$ 7.1 $\frac{7.1}{5}$ $\frac{8.0}{10}$ $\frac{7.1}{12}$ L.

⊙	+S	π	-S	Rod	Elev
T.P.	5.40	1390.71 89.79	6.32		1384.39
44				6.2	83.6
45				7.1	82.7
46				7.1	82.7
+70				6.7	83.1
47				5.3	84.5
+25				4.6	85.2
Δ +53 ^s				4.3	85.5
48				5.5	84.3
49				7.8	82.0
50				4.8	85.0
51				2.2	87.6
T.P.	9.83	97.32	2.30		87.49
52		1391.60		9.3	88.0
53				5.6	91.7
B.M.			5.72		1391.60
+50				4.9	92.4
54				5.9	91.4
55				10.2	87.1
56				12.7	84.6
57 T.P.	10.00	95.12	12.20		85.12
57				11.5	83.6
58				11.0	84.1
59				10.4	84.7
60				5.1	90.0

	L.	R.	5
	5.7 12	7.1 10	6.2 5
Swamp	8.6 9	7.1 7	7.1 4
	8.4 10	7.1 5	7.1 8
	8.1 12	6.7 8	6.7 14
	6.5 14	5.3 8	5.3 10
5.8 33	4.5 20	5.6 17	4.4 9
3.9 33	3.2 25	4.6 19	4.3 14
	2.6 20	5.5 10	5.5 5
6.4 33	8.8 14	7.8 10	7.8 2
3.3 23	4.8 14	4.4 10	4.8 4
	0.7 33		2.2 12
	8.7 16	9.6 14	9.3 8
		7.0 33	5.6 10
sp in 14 N.P.	7.8 33	6.3 18	4.9 9
	8.2 33	6.2 20	6.6 9
	10.6 23	11.4 15	11.4 6
Swamp	13.9 10	12.7 4	12.7 6
	12.4 5	11.5 3	11.5 8
	12.0 6	11.0 4	11.0 8
	11.6 5	10.4 2	10.4 10
6.0 33	4.4 16	5.1 10	5.9 7
			5.1 9
			5.1 14
			2.9 21

O	+S	π	-S	R.	EI.
		95.12 ✓			
61				3.1	92.0
62				7.3	87.8
T.P.	1.48	89.52 ✓	7.08		88.04 ✓
63		$\frac{12.70}{76.82}$		0.8	88.7
+85				4.2	
64				4.7	
+30				6.0	
+35				6.2	
65				10.8	
66				12.8	
T.P.	10.40	87.22 ✓	12.70		76.82 ✓
67				12.1	
+60				11.6	
68				9.0	
+42				4.8	
+80				4.2	
69				6.3	80.9
70				9.9	77.9
T.P.	5.66	81.98 ✓	10.90		76.32 ✓
B.M.			5.01		1376.97 ✓
71				4.6	75.5
72				4.5	75.6
+50				3.9	76.2
73				0.4	79.7 ✓
T.P.	12.72	91.78 ✓	1.06		79.06 ✓

$\frac{6.8}{11.1}$ $\frac{5.3}{5.3}$ $\frac{10.0}{5.3}$ $\frac{8.0}{5.7}$ $\frac{7.0}{13.3}$ $\frac{9.0}{5.3}$ $\frac{11.7}{5.3}$ $\frac{5.0}{5.6}$ $\frac{6}{17}$

Revised of Curve
 L. $\frac{8.6}{8}$ $\frac{7.3}{4}$ $\frac{7.3}{8}$ $\frac{8.2}{13}$

L. $\frac{2.1}{14}$ $\frac{1.2}{4}$ $\frac{0.8}{2}$ 0.8 2.1 $\frac{1.2}{15}$ $\frac{2.4}{35}$

L. $\frac{2.9}{33}$ $\frac{2.1}{13}$ $\frac{3.6}{10}$ $\frac{4.3}{7}$ 4.2 $\frac{4.2}{8}$ $\frac{8.3}{33}$

L. $\frac{1.5}{31}$ $\frac{4.5}{23}$ 6.0 $\frac{6.0}{16}$ $9.2/33$

L. $\frac{2.9}{33}$ $\frac{2.9}{9}$ $\frac{6.2}{3}$ 6.2 $\frac{6.2}{16}$ $9.1/33$

L. $\frac{8.8}{33}$ $\frac{11.1}{8}$ $\frac{10.8}{3}$ 10.8 $\frac{10.8}{8}$ $\frac{11.9}{12}$ $\frac{13.8}{33}$

L. $\frac{16.5}{33}$ $\frac{12.1}{8}$ 12.1 $\frac{12.1}{8}$ $\frac{13.3}{12}$ $\frac{14.2}{14}$

L. $\frac{16.3}{33}$ $\frac{11.6}{18}$ 11.6 $\frac{11.6}{15}$ $\frac{13.3}{33}$

L. $\frac{13.7}{28}$ $\frac{9.0}{11}$ 9.0 $\frac{9.0}{15}$ $\frac{12.7}{33}$

L. $\frac{11.2}{33}$ $\frac{4.8}{11}$ 4.8 $\frac{4.8}{14}$ $\frac{7.7}{24}$ $\frac{7.5}{32}$

L. $\frac{10.4}{33}$ $\frac{5.2}{10}$ 4.2 $\frac{5.2}{14}$ $\frac{5.9}{33}$

L. $\frac{12.1}{33}$ $\frac{8.3}{10}$ 6.3 $\frac{5.2}{14}$ $\frac{5.9}{33}$

L. $\frac{9.2}{33}$ $\frac{2.7}{4}$ $\frac{8.9}{4}$ $\frac{9.9}{3}$ 9.9 $\frac{9.9}{5}$ $\frac{8.9}{6}$ $\frac{10.3}{19}$ $\frac{12.6}{33}$

Sp. in 4" J.P.A.R.T. 70

$\frac{6.3}{33}$ 4.6 $\frac{4.6}{13}$ $\frac{7.3}{33}$

$\frac{7.4}{9}$ 4.5 $\frac{4.5}{12}$ $\frac{7.5}{21}$ $\frac{9.6}{33}$

$\frac{7.1}{33}$ $\frac{6.1}{26}$ $\frac{3.9}{14}$ $\frac{3.9}{12}$ 3.9 $\frac{3.9}{10}$ $\frac{6.1}{16}$ $\frac{8.7}{33}$

$\frac{3.1}{33}$ $\frac{0.4}{10}$ 0.4 $\frac{0.4}{6}$ $\frac{2.4}{33}$

⊙	+	π	-	R	EI
		91.78 ✓			
+35				9.0	82.8
74				5.4	86.4
+60				4.7	87.1
75				5.8	86.0
76				8.2	83.6
T.P.	6.93	1390.64	8.07		83.71 ✓
		10 43			
77		1380.21		5.2	85.4
+20				4.4	86.2
78				7.9	82.7
+85				7.5	83.1
79				7.8	82.8 ✓
T.P.	5.25	1385.46	10.43		1380.21
80				9.7	75.8
PC+44 ²				11.0	74.5
81				12.2	
+50				10.4	
82				7.7	
+50				6.0	
83				7.9	
+50				10.2	
84				11.0	
+50				9.1	
85				6.5	
+50				6.0	
P.T.+78 ⁶				6.8	

Abandoned.
See page 26
for continuation
of Levels.

⊙	+	π	-	R	EI
		91.78 ✓			
				9.0	82.8
				5.4	86.4
				4.7	87.1
				5.8	86.0
				8.2	83.6
	6.93	1390.64	8.07		83.71 ✓
		10 43			
		1380.21		5.2	85.4
				4.4	86.2
				7.9	82.7
				7.5	83.1
				7.8	82.8 ✓
	5.25	1385.46	10.43		1380.21
				9.7	75.8
				11.0	74.5
				12.2	
				10.4	
				7.7	
				6.0	
				7.9	
				10.2	
				11.0	
				9.1	
				6.5	
				6.0	
				6.8	

On Transit Hub

L.	$\frac{7.9}{33}$	$\frac{5.2}{7}$	5.2	$\frac{5.2}{6}$	$\frac{3.0}{13}$	$\frac{2.1}{33}$
	$\frac{7.4}{33}$	$\frac{7.4}{9}$	4.4	$\frac{7.4}{9}$	$\frac{3.9}{14}$	$\frac{4.1}{33}$
L.	$\frac{7.0}{21}$	$\frac{7.8}{19}$	$\frac{7.0}{17}$	$\frac{7.0}{6}$	$\frac{7.9}{4}$	7.9
	$\frac{10.8}{33}$					FD Rt. 77+25.
L.	$\frac{8.3}{26}$	$\frac{9.4}{23}$	$\frac{9.4}{21}$	$\frac{8.3}{18}$	$\frac{8.6}{8}$	$\frac{9.2}{4}$
	$\frac{9.2}{33}$	$\frac{9.2}{2}$				7.5
L.	$\frac{8.2}{25}$	$\frac{10.3}{21}$	$\frac{9.4}{17}$	$\frac{9.4}{6}$	$\frac{9.8}{4}$	$\frac{7.8}{2}$
	$\frac{3.7}{30}$					7.8
L.	$\frac{11.3}{6}$	$\frac{9.7}{7}$	9.7	$\frac{9.7}{10}$	$\frac{10.4}{13}$	$\frac{8.0}{28}$
Swamp.	L.	$\frac{11.6}{6}$	11.0	$\frac{9.9}{9}$	$\frac{9.9}{18}$	$\frac{10.8}{22}$
						$\frac{9.2}{26}$
Swamp	L.		12.2	$\frac{12.2}{4}$	$\frac{10.2}{13}$	$\frac{10.2}{24}$
						$\frac{11.3}{33}$
L.	$\frac{11.6}{13}$	10.4	$\frac{9.6}{3}$	$\frac{9.6}{13}$	$\frac{10.3}{25}$	$\frac{11.0}{33}$
	$\frac{8.0}{33}$	$\frac{7.7}{22}$	7.7	$\frac{9.7}{26}$	$\frac{11.0}{33}$	
	$\frac{2.1}{30}$		6.0	$\frac{8.6}{15}$	$\frac{13.2}{33}$	
	$\frac{1.8}{33}$		7.9	$\frac{1.40}{30}$		L.
	$\frac{4.0}{33}$		10.2	$\frac{1.4.4}{33}$		
	$\frac{5.8}{33}$		11.0	$\frac{15.2}{33}$		
	$\frac{5.4}{33}$		9.1	$\frac{14.7}{33}$		
	$\frac{1.8}{33}$		6.5	$\frac{8.6}{15}$	$\frac{14.0}{26}$	L.
	$\frac{1.8}{33}$		6.0	$\frac{10}{10}$	$\frac{13.8}{33}$	
	$\frac{1.2}{33}$		6.8	$\frac{9.1}{22}$	$\frac{12.0}{33}$	

O	+	π	R.	Elv.
T.P.	5.50	1384.56	6.40	1379.06
86		85.46 6.75 1378.11	5.1	
○ +42			2.4	
B.M.			2.24	1382.32
87			6.1	
88			12.3	
+60			14.3	
89			14.3	
90			14.4	
+70			13.8	
91			9.9	
T.P.	12.69	1390.80	6.45	1378.11
+60		3.99 1386.81	7.6	
92			7.2	
+35			8.6	
93			4.2	
94			4.7	
B.M.	4.66	91.47	3.99	1386.81
95			5.8	
+50			6.9	
96			6.5	
+50			4.7	
97			5.9	
98			14.3	
T.P.	1.57	80.93	12.11	1379.36

1384.56
2.24
1382.32

5.3
2.9
7.6
1.7
6.7

8

On P.T. hub.

$\frac{1.1}{33}$ 5.1 $\frac{10.0}{33}$
 $\frac{1.1}{33}$ 2.4 $\frac{3.9}{16}$ $\frac{7.4}{33}$

Sp. in Large R.P. R+ 87

$\frac{5.6}{33}$ 6.1 $\frac{5.6}{33}$

L 12.3 $\frac{10.4}{33}$

L 14.3 L. Swamp.

L 14.3 L. "

L L. "

L L. low swamp

L 9.9 $\frac{12.4}{33}$

$\frac{9.3}{33}$ 7.6 $\frac{7.6}{13}$ $\frac{9.6}{33}$

L 7.2 $\frac{8.2}{33}$

$\frac{6.7}{33}$ 8.6 $\frac{9.6}{26}$ $\frac{9.3}{33}$

L 4.2 $\frac{4.2}{20}$ $\frac{4.6}{33}$

L 4.7 $\frac{4.7}{19}$ $\frac{5.2}{33}$

Sp. in Top of 4" d.P. stump 2' high. 50' West 94+68

L 5.8 L.

L L.

L L.

L L.

L 5.9 L.

L 14.3 $\frac{11.1}{33}$

①	+	π	-	R.	E.
B.M.		80.93			1375.57
99			5.36		14.2
T.P.	2.58	1370.88	12.63		1368.30
100		1367.04		4.0	66.9
101				3.7	67.2
T.P.	1.61	1370.65	1.84		1369.04
N.L.		68.97		4.00	66.65
Δ + 46°				4.0	66.7
Δ 102 + 88°				3.3	67.4
Δ 104 + 78°				3.7	67.0
105				3.6	67.1
106				3.7	67.0
107				3.2	67.5
T.P.	8.30	77.27	1.68		1368.97
108.		1373.61		10.1	67.2
109				10.2	67.4
+67		77.27		10.0	67.3
110		75.66		5.0	72.3
B.M.			3.66		1373.61
111				3.9	73.4
T.P.	12.04	1387.70	1.61		75.66
+80				4.1	83.6
112				3.3	
+40				11.6	
T.P.	0.38	1376.88	11.70		1376.50

5.6 $\frac{80.93}{5.36}$ $\frac{95}{39}$ $\frac{133}{27}$ $\frac{142.5}{101+46}$ $\frac{5.6}{102+88.5}$ $\frac{179-60}{84-0.9}$ $\frac{9}{95.85}$

Sp. in 5" Pop. RT 98 + 30
L. 14.2 $\frac{11.6}{33}$ Enter swamp

Sp. in Tam stp. near 101 on RT.
in small pot hole.
0.6

7 floating
Boys
around
pot hole

$\frac{10.9}{5.3}$ $\frac{12.1}{5.6}$ $\frac{6.5}{5.1}$

leave swamp.
Sp. in N.P. RT 109 + 75
 $\frac{8.9}{33}$ 5.0 $\frac{3.0}{33}$
3.9 $\frac{7.25}{33}$ higher than E.

$\frac{9.4}{33}$ 4.1 $\frac{3.2}{16}$ $\frac{3.8}{33}$
 $\frac{4.6}{33}$ $\frac{3.8}{17}$ 3.3 $\frac{3.8}{100}$ $\frac{5.0}{33}$
 $\frac{5.1}{33}$ 11.6 $\frac{19.3}{33}$

O	+	↑	-	R.	E.
		76.88			
+70		$\frac{9.39}{67.49}$		8.2	
113				10.7	
+50				12.5	
114				12.4	
+25				11.5	
+50				8.3	
+75				9.2	
115				9.7	
T.P.	244	1369.93	9.39		1367.49
+75		$\frac{4.27}{65.66}$		4.0	
116				6.4	
117				6.6	
118				7.2	62.7
T.P.	2.95	1367.71	4.27		65.66
119				4.9	62.8
120				4.1	63.6
121				4.7	63.0
122				4.5	63.2
+62				4.7	
T.P.	10.02	1374.33	3.40		64.31
123				6.9	
+60				4.9	
124				6.4	
+30				10.4	
125				10.1	

10

higher than E

		8.2	$\frac{11.7}{76}$	L. swamp
	$\frac{3.7}{33}$	$\frac{8.9}{15}$	$\frac{10.7}{6}$	10.7 L.
		$\frac{9.2}{33}$	$\frac{12.5}{12}$	12.5 L.
swamp	L.		12.4	L.
	L.		11.5	L. leave swamp
	L.			L.
		$\frac{8.9}{33}$	9.7	$\frac{12.4}{33}$
	L.		4.0	$\frac{2.6}{33}$
	L.			L. Enter swamp
				L. swamps
				L.
				L.
				L.
				L.
				L.
				L.
				L. leave swamp
	L.	6.9	$\frac{7.5}{33}$	
		$\frac{9.9}{33}$	4.9	$\frac{3.0}{33}$
	L.	$\frac{9.6}{27}$	6.4	$\frac{4.4}{33}$
Swamp	L.		10.4	$\frac{7.3}{33}$ enter swamp
	L.		10.1	$\frac{8.5}{33}$ leave "

O	+	π	-	R.	E
		74.33 $\frac{207}{72.26}$		8.4	
+50				2.2	72.1
T.P.	11.60	1383.86 $\frac{0.18}{53.68}$	2.07		1372.26
+60				3.0	
T.P.	12.63	1396.31 $\frac{1.29}{95.02}$	0.18		1383.68
+80				4.7	
127				3.6	
+30				1.7	
T.P.	3.33	1398.35 $\frac{7.68}{1390.67}$	1.29		1395.02
+60				4.1	94.3
128				6.6	91.8
B.M.	3.60	1394.27 $\frac{4.59}{1389.68}$	7.68		1390.67
+30				5.7	88.6
129				5.0	89.3
130				4.6	89.7
131				8.4	85.9
132				6.1	88.2
133				6.4	87.9
+50				4.7	89.6
T.P.	0.45	90.13	4.59		1389.68
134				2.8	87.3
135				4.2	85.9
136				5.9	84.2
+90				5.5	84.6
137				6.2	83.9

56
52 11

L	C	R
$\frac{0.7}{33}$	2.2	$\frac{3.5}{33}$
L.	3.0	L.
$\frac{2.4}{33}$	$\frac{4.4}{15}$	3.6
L.	L.	L.
L.	L.	L.

Spruce Oak Rt. 128+10

$\frac{3.5}{33}$	$\frac{4.2}{19}$	$\frac{5.2}{15}$	$\frac{5.2}{12}$	5.7	$\frac{5.7}{4}$	$\frac{6.1}{7}$	L.
$\frac{1.7}{33}$	$\frac{4.3}{12}$	$\frac{5.8}{10}$	5.0	$\frac{5.0}{6}$	$\frac{6.3}{12}$	$\frac{4.6}{33}$	L.
L.	$\frac{7.1}{33}$	$\frac{4.1}{7}$	4.6	$\frac{4.6}{13}$	$\frac{3.4}{17}$	$\frac{4.8}{33}$	L.
L.	$\frac{8.9}{8}$	$\frac{8.4}{6}$	8.4	$\frac{8.4}{6}$	$\frac{9.0}{8}$	$\frac{10.2}{33}$	L.
$\frac{6.1}{33}$	$\frac{4.5}{13}$	$\frac{7.2}{10}$	$\frac{6.1}{3}$	6.1	$\frac{6.1}{7}$	$\frac{9.1}{33}$	L.
L.	L.	6.4	$\frac{8.4}{33}$	6.4	$\frac{5.2}{12}$	$\frac{3.6}{18}$	$\frac{5.4}{33}$
$\frac{5.8}{33}$	$\frac{2.9}{12}$	$\frac{4.8}{5}$	4.7	4.7	4.7	4.7	4.7
L.	$\frac{3.1}{23}$	$\frac{3.4}{6}$	2.8	2.8	$\frac{2.8}{6}$	$\frac{4.5}{15}$	L.
L.	L.	$\frac{5.3}{11}$	4.2	4.2	$\frac{4.2}{10}$	$\frac{5.2}{17}$	$\frac{4.6}{20}$ L.
L.	$\frac{6.7}{13}$	$\frac{7.2}{11}$	$\frac{7.2}{10}$	$\frac{5.9}{3}$	5.9	$\frac{5.9}{8}$	$\frac{6.8}{12}$ L.
L.	$\frac{6.5}{25}$	$\frac{5.7}{14}$	$\frac{7.2}{12}$	$\frac{5.3}{4}$	5.5	$\frac{5.5}{6}$	$\frac{6.8}{12}$ L.
$\frac{5.9}{21}$	$\frac{7.2}{12}$	$\frac{7.8}{10}$	$\frac{7.2}{9}$	6.2	6.2	$\frac{7.2}{10}$	$\frac{4.7}{16}$ L.

○	+	↑	-	R	EI
+71		90.13 72.3 82.90		11.3	78.8
138				8.7	81.4
139				7.5	82.6
T.P.	544	88.34 370 84.64	7.23		1382.90
140				7.0	81.3
141				6.8	81.5
142				6.7	81.6
143				4.8	83.5
144				3.0	85.3
145				4.0	84.3
146				4.4	83.9
B.M.	6.67	1391.31 225 1389.06	3.70		1384.64
147				4.0	87.3
+50				3.1	88.2
148				4.1	87.2
149				5.1	86.2
+25				5.0	86.3
150				6.4	84.9
151				6.3	85.0
152				2.1	89.2
T.P.	10.76	1399.80 225 1389.06	2.25		1389.06
153				7.4	92.4
154				3.3	96.5
T.P.	12.63	1410.63 182 1398.00	1.82		1398.00
+35				11.7	98.9

12

Bottom	Ditch	h.	which	cross	here
L.	$\frac{24}{11}$	$\frac{87}{6}$	87	$\frac{87}{6}$	$\frac{92}{12}$ L. <small>wooden box</small>
	$\frac{91}{33}$	$\frac{70}{19}$	$\frac{75}{13}$	7.5	$\frac{75}{5}$ $\frac{61}{10}$ L. <small>16x10x15 ditch drains south</small>
L.	$\frac{84}{10}$	$\frac{70}{7}$	7.0	$\frac{70}{3}$	$\frac{84}{10}$ L.
L.	$\frac{57}{18}$	$\frac{77}{12}$	$\frac{68}{6}$	6.8	$\frac{68}{10}$ $\frac{79}{13}$ L.
L.	$\frac{46}{10}$	$\frac{67}{4}$	6.7	$\frac{67}{6}$	$\frac{78}{12}$ $\frac{70}{14}$ L.
L.	$\frac{40}{13}$	$\frac{54}{11}$	$\frac{48}{6}$	4.8	$\frac{48}{5}$ $\frac{60}{10}$ $\frac{51}{13}$ L.
	$\frac{081}{33}$	$\frac{30}{9}$	3.0	$\frac{30}{3}$	$\frac{37}{5}$ L.
L.	$\frac{48}{12}$	$\frac{40}{10}$	4.0	$\frac{51}{4}$	L.
	$\frac{46}{20}$	$\frac{54}{13}$	$\frac{44}{11}$	4.4	$\frac{54}{11}$ L. <small>146+45 PD L.</small>
Sp. in T.P. f. 146+30					
L.	$\frac{30}{23}$	$\frac{40}{12}$	4.0		L.
L.	$\frac{16}{15}$	$\frac{31}{11}$	3.1		L.
	$\frac{25}{33}$	$\frac{53}{14}$	$\frac{41}{8}$	4.1	$\frac{41}{3}$ $\frac{49}{4}$ L.
slough	L.	$\frac{63}{12}$	$\frac{51}{10}$	5.1	$\frac{51}{5}$ $\frac{62}{10}$ $\frac{53}{11}$ L. <small>56 105</small>
slough	$\frac{66}{33}$	$\frac{48}{18}$	$\frac{62}{15}$	5.0	$\frac{63}{7}$ $\frac{63}{9}$ $\frac{50}{11}$ $\frac{58}{33}$
slough	L.	$\frac{78}{12}$	$\frac{64}{9}$	6.4	$\frac{64}{2}$ $\frac{75}{8}$ L.
"	L.	$\frac{76}{10}$	$\frac{63}{7}$	6.3	$\frac{63}{4}$ $\frac{75}{7}$ L.
	$\frac{07}{16}$	$\frac{32}{13}$	$\frac{21}{10}$	2.1	$\frac{21}{2}$ $\frac{27}{3}$ $\frac{10}{7}$ L. <small>Draw to Rt. 150+78=an 8x8x16 W.B.</small>
L.	$\frac{82}{16}$	$\frac{86}{14}$	$\frac{74}{10}$	7.4	$\frac{83}{4}$ L.
	$\frac{54}{33}$	$\frac{45}{11}$	$\frac{33}{9}$	3.3	$\frac{33}{3}$ $\frac{46}{11}$ $\frac{53}{33}$
L.	$\frac{110}{15}$	$\frac{117}{12}$	11.7	$\frac{117}{6}$	$\frac{125}{8}$ $\frac{125}{9}$ $\frac{115}{10}$ $\frac{90}{22}$ L.

O	+	π	-	R.	Elev
		1378.97			
		4.52			
		74.45			
193				4.9	74.1
194				4.3	74.7
195				4.0	75.0
T.P.	2.46	1376.91	4.52		1374.45
		5.50			
		1371.41			
196				2.9	74.0
197				3.3	73.6
198				4.4	72.5
199				5.1	71.8
200				5.0	71.9
201				4.6	72.3
202				4.6	72.3
203				5.6	71.3
T.P.	4.05	1375.46	5.50		1371.41
		3.58			
		1371.88			
204				4.6	70.9
205				4.6	70.9
206				4.8	70.7
207				5.0	70.5
208				4.6	70.9
209				3.7	71.8
T.P.	5.02	1376.90	3.58		1371.88
210				4.7	72.2
211				5.0	71.9
B.M.			4.08		1372.82
212				5.2	71.7
213				6.0	70.9

L.	$\frac{5.7}{11}$	$\frac{4.5}{3}$	4.9	$\frac{5.9}{8}$	$\frac{5.5}{10}$	L.	
	L.	4.3	$\frac{4.3}{5}$	$\frac{5.5}{8}$	$\frac{5.7}{11}$	$\frac{5.1}{13}$ L.	
L.	$\frac{4.4}{16}$	$\frac{5.0}{13}$	$\frac{5.0}{11}$	$\frac{4.0}{8}$	4.0	$\frac{4.7}{5}$ $\frac{5.8}{10}$ $\frac{5.2}{11}$	
	L.						
	L.	$\frac{3.6}{15}$	$\frac{2.9}{12}$	2.9	$\frac{4.5}{7}$	$\frac{3.5}{10}$ L.	
L.	$\frac{3.3}{17}$	$\frac{4.3}{16}$	$\frac{3.3}{8}$	3.3	$\frac{3.3}{2}$	$\frac{4.6}{6}$ $\frac{4.6}{8}$ $\frac{3.6}{9}$ L.	
	L.		$\frac{4.6}{20}$	4.4	$\frac{5.0}{3}$	L.	
L.	$\frac{5.0}{19}$	$\frac{5.5}{16}$	$\frac{4.5}{8}$	5.1	$\frac{5.6}{1}$	$\frac{5.6}{2}$ $\frac{5.1}{3}$ L.	
	L.		L.	5.0	$\frac{5.0}{5}$	$\frac{6.0}{6}$ $\frac{5.4}{7}$ L.	
L.	$\frac{4.8}{14}$	$\frac{5.7}{12}$	$\frac{4.6}{9}$	4.6	$\frac{4.6}{6}$	$\frac{6.4}{12}$ $\frac{5.2}{15}$ L.	
L.	$\frac{4.6}{16}$	$\frac{5.5}{12}$	$\frac{4.6}{8}$	4.6	$\frac{4.6}{5}$	$\frac{6.1}{9}$ $\frac{6.1}{12}$ $\frac{4.8}{16}$ L.	
	$\frac{5.6}{19}$	$\frac{6.6}{18}$	$\frac{6.6}{16}$	$\frac{5.2}{4}$	5.6	$\frac{6.8}{5}$ $\frac{5.8}{6}$ L.	
	L.						
L.	$\frac{4.2}{17}$	$\frac{5.2}{16}$	$\frac{4.6}{12}$	4.6		L.	
L.		$\frac{4.9}{17}$	$\frac{4.1}{6}$	4.6	$\frac{6.1}{8}$	$\frac{5.1}{10}$	
L.		$\frac{5.8}{11}$	$\frac{4.7}{4}$	4.8	$\frac{5.4}{5}$	$\frac{5.8}{7}$ $\frac{5.0}{12}$ L.	
L.		$\frac{5.9}{13}$	$\frac{5.0}{9}$	5.0	$\frac{5.6}{8}$	$\frac{4.6}{10}$ L.	
$\frac{6.0}{15}$	$\frac{7.0}{14}$	$\frac{7.0}{13}$	$\frac{4.6}{9}$	4.6	$\frac{4.6}{2}$	$\frac{6.7}{6}$ $\frac{6.3}{8}$ L.	
$\frac{3.0}{18}$	$\frac{6.0}{16}$	$\frac{6.0}{15}$	$\frac{4.2}{13}$	3.7	$\frac{3.7}{5}$	$\frac{5.2}{8}$ $\frac{5.2}{20}$ $\frac{4.2}{21}$	
$\frac{4.9}{21}$	$\frac{7.0}{19}$	$\frac{7.0}{18}$	$\frac{4.7}{13}$	$\frac{4.5}{8}$	4.7	$\frac{5.9}{5}$ $\frac{5.9}{8}$ $\frac{4.8}{9}$ L.	
L.	$\frac{5.4}{21}$	$\frac{6.7}{18}$	$\frac{6.7}{17}$	$\frac{5.0}{13}$	$\frac{4.6}{7}$	5.0	$\frac{5.8}{3}$ $\frac{5.8}{5}$ $\frac{5.2}{6}$ L.
Sp	117	12" Pop.	25' Lt.	211 + 75			
	$\frac{5.5}{18}$	$\frac{6.5}{17}$	$\frac{6.5}{16}$	$\frac{5.9}{12}$	$\frac{4.6}{7}$	5.2	$\frac{5.9}{4}$ $\frac{5.9}{7}$ $\frac{5.4}{8}$ L.
$\frac{5.2}{25}$	$\frac{6.4}{23}$	$\frac{6.4}{22}$	$\frac{5.3}{20}$	$\frac{4.9}{17}$	$\frac{4.9}{6}$	6.0	L.

O	+	X	-	R	Elv.
		1376.90			
214		4.07 1372.83		6.8	70.1
215				7.0	69.9
216				5.4	71.5
217				5.5	1371.4
T.P.	9.13	1381.96	4.07		1372.83
218		5.25 1376.71		9.8	72.2
219				7.0	75.0
220				6.0	76.0
221				3.9	78.1
222				4.6	77.4
223				6.7	75.3
224				6.6	75.4
T.P.	5.58	1382.29	5.25		1376.71
225	r	4.82 1377.47		7.1	75.2
226				7.0	75.3
+50				6.2	76.1
227				7.0	75.3
228				6.8	75.5
229				5.8	76.5
230				6.8	75.5
231				4.4	77.9
T.P.	9.77	1387.24	4.82		1377.47
232				9.8	77.4
233				10.7	76.5
234				10.9	76.4

29
17
46 16

L	C	R
5.7 71.71	5.6 5.6	4.5 4.5 5.6
2.5 24.23	2.3 2.0	1.8 7 1 6.8
5.6 72.72	5.8 5.8	4.7 4.7 5.5 7.0
2.5 23.22	2.2 2.1	1.8 7 3 1 7.0
5.7 45.45	5.4 5.4	4.6 4.6 5.7 7.0 7.0
2.7 24.23	2.3 2.1	1.8 8 5 2 1 5.4
	L. 5.4 4.6 4.3 4.8	2.1 1.9 1.3 7 5.5
		L. 9.3 10.1 8.9
	L. 2.5 2.4 2.3	2.0 8 7.6 7.0
L. 4.6 8.2 8.2	6.6 6.1 6.3 6.9	6.0
L. 2.6 2.4 2.3	2.1 1.5 8 7	L.
L. 4.0 7.8 7.8	4.3 4.1 4.7 5.3	L.
L. 2.8 2.6 2.5	2.2 1.6 1.0 9	3.9
L. 3.9 7.4 7.4	4.5 4.1 4.5 5.6 5.6	4.6
L. 3.8 3.2 3.1	2.8 1.8 1.2 1.0 4	4.6
	L. 6.0 7.5 7.5 5.2 7.6	6.7 5.2
	L. 2.9 2.7 2.6 2.2 1.0	3 8
	L. 7.1 5.5 5.5 6.6	6.6
	L. 2.6 2.1 1.0 8	L.
L. 7.2 5.7 7.0	7.7 7.1 7.1	7.1
L. 2.5 2.5 1.8	8 7 4 3	L.
L. 7.0 6.1 5.5	6.1 6.9 7.6 7.6	7.0
L. 2.5 2.3 1.6	1.1 8 7 5 3	L.
	L. 4.1 5.3 5.3 6.2	L.
	L. 3.3 2.5 1.3 1.0	6.2
2.9 6.0 6.0	4.9 4.9 6.5	7.0 4.3
3.3 3.1 2.9	2.3 1.1 5	7.0 3 8 L.
	L. 5.2 5.2 6.2	6.8 5.9 6.8
	L. 5.3 6.6 6.6 5.8	4 3.3 L.
	L. 1.2 8 5 1	5.8
L. 4.7 5.5 5.6	6.8 6.8	L.
L. 3.3 2.2 2.7	5 5	L.
L. 5.7 4.9 5.1	5.9 5.9	4.4
L. 2.7 1.7 1.1	9 5	L.
	L. 10.0 10.7 9.8	L.
	L. 10.8 9.7 10.7 10.7	L.
	L. 10.5 9.9 10.3 10.9	L.
	L. 2.8 2.0 1.5 1.2	10.9

Swamp

O	+	π	-	R.	EIV.
		1387.24			
235		^{5.03} 1382.21		8.3	78.9
236				5.4	81.8
237				4.7	82.5
+75		87.24		5.9	81.3
238		^{2.29} 84.95		5.1	82.1
T.P.	8.62	90.83	5.03		1382.21
B.M.		^{4.62} 86.21	2.29		1384.95
239				10.7	80.1
240				8.5	82.3
+30				5.7	85.1
241				4.8	86.0
242				5.9	84.9
243				8.0	82.8
+50				5.3	85.5
T.P.	2.47	1388.68	4.62		1386.21
244		^{8.80} 1379.88		6.1	82.6
+20				8.6	80.1
245				10.0	78.7
+25				9.8	78.9
+60				6.2	82.5
246				8.1	80.6
T.P.	6.47	86.35	8.80		1379.88
+50				7.1	79.3
247				5.1	81.3
+60				8.2	78.2

17

L.	C.	R.
⁹¹ 33	⁹⁶ 30	⁹¹ 14
⁷⁰ 33	⁶⁶ 15	⁷⁰ 12
⁶⁷ 33	⁵¹ 21	⁵⁶ 12
L.	⁶¹ 16	⁶⁸ 14
L.	⁵² 21	⁵⁸ 14
	⁸³ 4	⁸³ 4
	⁵⁴ 4	⁵⁴ 4
	⁴⁷ 9	⁴⁷ 9
	⁵⁹ 10	⁵⁹ 10
	⁵¹ 10	⁵¹ 10
		^{5.7} 33
		^{3.9} 33
		L.
SP. IN 14" W.P.		
		L.
⁹³ 33	⁷⁸ 22	⁹⁰ 14
	⁸⁸ 33	⁶¹ 21
L.	⁶⁷ 29	⁵⁸ 21
	⁹¹ 33	⁸⁰ 22
	⁸² 27	⁷⁵ 20
		^{8.0} 11
		^{8.5} 6
		^{9.0} 6
		^{9.2} 33
		^{8.3} 33
		L.
		^{8.0} 10
		^{7.0} 33
^{8.3} 33	^{9.2} 31	^{8.2} 27
		^{7.9} 10
		^{5.3} 6
		L.
		^{9.4} 33
		^{8.9} 28
L.	^{9.7} 28	^{9.0} 25
L.	^{9.8} 28	^{8.3} 19
L.	^{9.8} 28	^{8.5} 20
L.	^{9.5} 28	^{8.6} 18
L.	^{9.5} 28	^{9.3} 19
		^{7.6} 9
		^{8.2} 9
		^{8.8} 10
		^{8.6} 10
		^{10.0} 10
		^{10.0} 10
		^{9.8} 10
		^{9.8} 10
		^{6.2} 3
		^{6.2} 3
		^{8.1} 5
		^{8.1} 5
		L.
		^{3.0} 33
		^{2.6} 33
		L.
		^{9.8} 10
		^{9.8} 10
		^{6.2} 3
		^{6.2} 3
		^{8.1} 5
		^{8.1} 5
		L.
		^{7.1} 10
		^{7.1} 10
^{5.0} 33	^{5.7} 27	^{5.2} 18
	^{5.9} 10	^{5.9} 10
	^{5.1} 6	^{5.1} 6
	^{5.8} 11	^{5.8} 11
		^{5.1} 33
		L.
		^{8.2} 11
		L.

Sta.	+S	↑	-S	Rod	Elev.
		86.35			
248		5.65		9.3	77.1
+60		80.70		8.8	77.6
249				7.7	78.7
+60				4.9	81.5
250				7.2	79.2
+25				9.3	77.1
251				9.6	76.8
+60				4.8	81.6
B.M.	456	1385.26	5.65		1380.70
252		58		4.3	90.0
253		79.5			
254					
255					
256					
-257					
T.P.	445	1389.96	5.50		1379.76
258				5.1	
259				5.6	
+50				4.1	
260				5.5	
+75				6.5	
261				3.1	
+20				4.6	
262				4.7	84.6
T.P.	0.6	1385.36	4.50		1384.76

VOID

VOID from
B.M.

		L	C	R	
		9.0	8.0	9.3	
		26	18	11	9.3
		9.5	8.9	7.9	8.4
		28	26	18	13
		7.7	7.6	8.3	8.3
		3.3	5.1	4.1	5.1
		3.5	3.1	2.0	1.9
		4.3	7.1	6.4	7.4
		3.5	3.1	2.0	1.9
		2	8.8	7.6	2.8
		10.0	8.9	8.3	8.7
		2.8	2.5	2.0	1.4
		6.3	7.8	7.3	6.9
		3.3	2.8	2.5	1.8
					7
					4.8
					4.3
					1.6
S.P. in T.P. on Line					
					5.3
					5.3
					5.8
					5.9
					5.8
					5.1
					5.6
					4.1
					5.5
					6.5
					3.1
					4.6
					4.7

VOID

1385.26
550.18
1379.76

4.15
1383.91
1389.26
1383.91
5.35

Sta	+S	T	-S	Rod	Elev
		1385.36			
262+40				4.1	81.3
263				10.9	74.5
T.P.	0.8	1375.46	10.7		1374.66
264				6.3	
T.P.	2.8	1366.96	11.3		1364.16
+75				6.3	
265				6.6	
266				9.4	
267				9.2	
+75				8.4	
268				7.4	
269				3.6	
270				7.0	
B.M.		1366.96	5.82		1361.04
+50				12.3	7
271				13.7	
272				13.8	53.2
273				13.8	
274				3.8	
275				1.9	
276				11.7	
277				6.6	
T.P.	12.67	1373.38	6.25		1360.71
T.P.	12.46	1385.33	6.51		1372.87
278				11.7	

rod

L C.R.

19

6.1	4.1	L
33.0	2	10.9 L
	6.3	L
2	6.3	L
	6.6	L
	9.4	L
	9.2	L
	8.4	L
	7.4	L
	3.6	L
	7.0	L
Sp, 10 5" 18' RT. Sta. 270		
	12.3	L
	13.7	L
	13.8	L
	13.8	L
	13.8	L
	13.9	L
	11.8	L
5.6	6.6	L
33.0		
12.4	11.7	L
33.0		

rod

8.2

5.0

11.7

3.0

Sta	+ S	↑ [5.33]	- S	Rod	Elev.
279					
+45					
BM.			5.34		1379.99
280				2.6	
+20				1.7	
T.P.	5.52	1389.70	1.15		1384.18
+50		9.65		2.9	
281				9.6	
282					
283				10.6	
284				10.3	
285				11.8	
286				9.8	
T.P.	10.00	1390.05	9.65		1380.05
287		4.17		8.9	
288				9.1	
289		90.1		7.4	
290		5.0		5.7	
291		8		5.1	
BM.			4.17		1385.88
291+80.4				4.6	

void

	C	R
L	7.8	L
L	4.6	L
Spr in White pine 75' - 17' 279+50		
	4.0	
	53.0	2.6
	2.3	53.0
	55.0	1.7
	3.9	
	53.0	2.9
L	9.6	L
<i>void</i>		
L	9.8	L
L	10.6	L
L	10.3	L
L	11.8	L
L	9.8	L
L	8.9	L
L	9.1	L
L	7.4	L
	5.7	
L	5.1	L
Spr in Poplar Tree - 25' - 12'		
L	4.6	L

Levels on Main Line sta. 316+ to 252

316
252
60 21

← 32.5 + 14° = Clin

B.M.	791	64.12		1356.21
316+73.8			4.4	59.7
T.P.	11.94	75.03	1.03	63.09
316		⁴⁹ 75.54	-	11.1 63.9
315			2.8	72.2
T.P.	9.96	83.50	1.99	73.54
314			7.0	76.5
313			6.0	77.5
+50			6.9	76.6
312			6.1	77.4
311			3.8	79.7
310			3.3	80.2
309			3.7	79.8
308			2.8	80.7
T.P.	3.32	84.73	2.09	81.41
307			5.2	79.5
+45			4.0	80.7
306			6.3	78.4
305			6.9	77.8
304			5.0	79.7
303			5.6	79.1
+45			3.5	81.2
302			5.0	79.7
301			6.6	78.1
300			7.2	77.5

M.C. I.P.

Int. with C Line

		84.73			
T.P.	5.84	83.54	7.03		77.70
299		^{3.05} 80.49	-	6.0	77.5
298				6.0	77.5
297				5.5	78.0
296				4.7	78.8
295				4.2	79.3
294				3.6	79.7
293				2.9	80.6
292				3.4	80.1
T.P.	2.83	83.32	3.05		80.49
291				3.6	79.7
290				4.2	79.1
289				5.9	77.4
288				7.8	75.5
287				7.6	75.7
T.P.	2.90	78.89	7.33		75.99
286		^{3.93} 74.94		4.2	74.7
285				6.4	72.5
284				4.8	74.1
283				5.2	73.7
282				4.2	74.7
281				4.1	74.8
T.P.	9.68	84.62	3.95		74.94
+85				8.5	76.1
+60				3.9	80.7

80.4
80.0
SON. I.P. Sec. Cor
79.7

slough

6104
55.39
5.65

79.99
74.61
5.38

23

		84.62			
① +48'		12.23		3.3	81.3
+25		72.39		6.6	78.0
280				7.3	77.3
+20				10.2	74.4
279				12.4	72.2
B.M.			10.01		1374.61
T.P.	1.04	73.43	12.23		72.39
278		12.46 60.97		5.3	68.1
T.P.	1.58	62.55	12.46		60.97
277				7.4	55.2
276				12.8	49.8
T.P.	8.96	58.96	12.55		50.00
275		1.23 57.73		11.4	47.6
274				11.4	47.6
273				11.6	47.4
272				11.4	47.6
271				11.3	47.7
+40				9.7	49.3
270				4.6	54.4
B.M.			3.57		1355.39
269				1.3	57.7
T.P.	3.94	61.67	1.23		57.73
268				2.8	53.9
267				9.7	52.0
266				9.7	52.0

Sp in W.P. Lt. 279

Sp in Pop Rt. 270

		61.67			
265		^{6.70} 54.97		6.8	54.9
T.P.	12.49	67.46	6.70		54.97
+50		^{0.92} 66.54		10.8	56.7
264				3.7	63.8
T.P.	8.72	75.26	0.92		66.54
263				6.2	69.1
T.P.	10.07	85.12	0.21		75.05
262		^{5.13} 79.99		6.6	79.5
0 + 83 ²				4.1	81.0
+25				6.0	79.1
261				4.4	80.7
+50				8.3	76.8
260				8.0	77.1
+40				5.5	79.6
259				7.0	78.1
T.P.	5.00	84.99	5.13		79.99
258				6.4	78.6
257				5.6	79.4
256				5.9	79.1
255				4.9	80.1
254				5.7	79.3
253				5.1	79.9
252				5.1	79.9
B.M.			4.50		1380.49

80.70
80.49

 .21

sp in T.P. = 1380.70

Levels on A⁰⁰ Line

O	+	π	-	R.	ELV.
B.M.	12.55	1394.87			1382.32
T.P.	0.89	88.50	7.26		87.61
81+00		^{7.26} 87.61		15.9	72.6
+50				14.9	73.6
82				10.9	77.6
+50				5.2	83.3
83				1.8	86.7
T.P.	10.77	1398.38	0.89		87.61
84		^{10.85} 88.33		7.3	91.1
85				7.1	91.3
86				7.4	91.0
+50				7.7	90.7
87				7.5	90.9
+50				6.0	92.4
88				6.0	92.4
89				4.9	93.5
90				8.2	90.2
91				9.0	89.4
92				8.8	89.6
+75				8.4	90.0
93				8.6	89.8
+60				9.8	88.6
T.P.	7.12	95.45	10.05		1388.33
94				7.3	88.2
Δ +62				8.8	86.7

7-28-19
R. CVW-OR.SJ.

76

Sp in W.P.R. 87+50.

L.	15.9	^{15.9} 7	^{13.2} 17	^{13.2} 28	^{13.7} 33
L.	14.9	^{13.7} 13	^{12.7} 16	^{12.7} 25	^{13.3} 33
	^{12.2} 33	^{10.3} 9	^{10.3} 19	^{11.1} 33	
^{5.0} 33	^{4.1} 6	^{6.1} 2	^{6.1} 1	5.2	^{5.1} 14
^{5.7} 33	^{1.3} 7	^{2.5} 5	1.8	^{1.8} 12	^{2.7} 17
				^{2.0} 19	^{4.5} 33
L.	^{6.3} 7	^{7.8} 4	7.3	^{7.3} 11	^{8.5} 20
	^{6.1} 33	^{6.7} 12	^{8.1} 7	^{7.1} 10	^{8.0} 14
L.	^{6.5} 13	^{8.1} 9	^{8.1} 6	^{7.4} 7	^{8.5} 14
	^{7.4} 5	^{7.4} 5	7.4	^{7.4} 9	^{8.0} 16
		^{8.1} 5	^{7.4} 5	^{8.5} 16	^{8.8} 20
L.	^{9.2} 6	^{7.7} 2	7.7	^{7.7} 9	^{9.1} 12
	^{8.3} 8	^{7.5} 2	7.5	^{7.5} 10	^{8.4} 12
L.	^{7.8} 10	^{6.8} 6	^{6.3} 4	6.0	^{6.0} 8
	^{6.0} 33	^{6.7} 9	^{6.3} 4	^{6.0} 8	^{6.7} 14
	^{5.2} 33	^{6.7} 4	^{6.0} 7	^{6.0} 8	^{6.3} 11
	^{5.2} 33	^{4.1} 5	4.9	^{4.9} 11	^{3.0} 18
	^{7.7} 33	^{9.2} 4	^{8.2} 1	8.2	^{9.4} 10
L.	^{8.8} 11	^{9.9} 8	^{9.9} 5	^{9.3} 4	9.0
	^{9.2} 13	^{9.6} 11	^{9.6} 8	^{8.8} 5	^{8.8} 9
L.	^{8.1} 12	^{9.0} 10	^{9.0} 6	^{8.4} 4	8.4
	^{9.7} 6	^{8.6} 2	8.6	^{8.6} 10	^{9.3} 12
L.	^{12.9} 14	^{11.7} 6	^{9.8} 2	9.8	^{9.8} 10
	^{10.9} 19	^{9.6} 7	^{7.3} 3	7.3	^{7.3} 14
	^{11.5} 14	^{9.7} 6	8.8	^{9.7} 16	^{6.1} 20
				^{9.4} 16	^{4.0} 26
				^{2.1} 30	L.

○	+	π	-	R.	E/v.
95		95.45 12.72 82.73		12.0	83.5
T.P.	8.08	90.81 2.99 87.82	12.72		82.73
+40				9.1	81.7
+80				10.0	80.8
96				9.6	81.2
97				7.9	82.9
+60				5.9	84.9
98				5.9	84.9
+30				5.1	85.7
99				5.8	85.0
+75				4.9	85.9
100				5.9	84.9
+70				8.8	82.0
+85				9.0	81.8
101				9.2	81.6
102				6.2	84.6
+75				3.0	87.8
T.P.	4.12	91.94 4.49 87.45	2.99		87.82
103				4.8	87.1
104				6.9	85.0
105				8.6	83.3
106				9.9	82.0
107				9.0	82.9
B.M.			4.49		1387.45
108				4.8	87.1

L.	C	R.	27
L. 14.6	12.0	12.0	9.2 31
7		15	17 20 50
L. 9.7	9.1	9.1	9.1 8.6 6.6
9	4	9.1	18 24 33
L. 12.0	10.0	10.0	10.0 11.8
9	4	10.0	8 15 L
L. 11.8	9.6	9.6	9.6 12.2
8	4	9.6	8 13 L.
L. 7.9	8.6	7.9	8.9 10.5
8	5	7.9	16 33
L. 5.4	6.8	5.9	8.2
10	6	5.9	33
L. 5.3	6.5	5.9	6.3
10	7	5.9	20 L.
L. 3.9	5.6	5.1	6.1
11	6	5.1	20 L.
L. 5.6	6.5	5.8	6.1 6.6 7.9
11	8	5.8	9 12 33
	9.3	4.9	4.6 3.2
	33	12.4.9	12 15 33
12.9	8.3	5.9	5.5 2.4 0.7
33	8	4	12 16 33
L. 14.8	5.8	8.8	8.8 9.5 6.5
17	3	8.8	9 12 17
L. 14.8	9.0	9.0	9.0 10.0 10.0
18	3	9.0	9 14 27
L. 14.8	9.2	9.2	9.2 10.2 5.9
17	3	9.2	10 15 20
12.8	6.2	6.2	6.2 2.8
33	8	6.2	12 26
32	0.8	3.0	3.0 3.5 ← higher than 4.
33	10	6	11 15
9.2	5.2	5.0	4.8 2.8
33	10	6	20 25 L.
8.8	6.8	7.5	6.9
33	16	11	7 6.9
10.4	9.4	8.6	8.6 7.4 6.4
33	12	8	9 12 33
13.1	11.6	9.9	9.9 10.8 10.2
33	12	7	7 10 13 L.
12.9	9.0	9.0	9.0 9.4 9.1 7.7
33	7	9.0	4 6 10 11 L.
sp. in T.P. Rt.	107 + 40	- 25' Rt.	
10.9	7.5	4.8	4.8 2.9
33	21	10	7 11 L.

0	+	π	-	R.	EIV
		919.4 12.88 79.06			
109				6.8	85.1
110				9.5	82.4
T.P.	1.09	1380.15 6.15 1374.00	12.88		1379.06
111				5.0	75.2
+80				7.7	72.5
112				7.6	72.6
113				6.3	73.9
T.P.	10.53	1384.53	6.15		1374.00
114		337 81.16		10.4	74.1
+30				9.0	75.5
115				10.5	74.0
116				8.3	76.2
Δ +38.7				4.7	79.8
117				4.2	80.3
+60				4.9	79.6
118				4.2	80.3
+50				3.0	81.5
119				6.5	78.0
120				6.1	78.4
+60				2.5	82.0
121				5.0	79.5
122				3.8	80.7
T.P.	12.95	1394.11	3.37		1381.16
123				7.5	86.6
124				4.3	89.8

803
725

5.7
5.7
121
5.7
5.7
3.5

3 28

	9.9	6.8		6.8	7.4	6.7		
	33	6	6.8	5	9	12		
	14.3	9.5		9.5	9.9	9.9	7.6	7.1
	33	10	9.5	5	6	8	11	33
	6.9	6.5	5.0	5.0	5.6	3.8	3.8	2.8
	33	22	9	5.0	12	21	27	29
	L.	9.6	7.7	7.7	10.0	L.		18" CA. reg'd.
		15	10	1	5			
	L.	8.5	7.6	7.6	9.1	L.		
		13	11	7.6	5			
	L.		6.3	6.3	7.2	L.		
				8	18			
	L.	8.4	9.2	10.4	14.0			
		17	15		33			
	10.1	9.4	9.4	9.0	13.8	14.8		
	33	12	4		25	33		
	L.	12.1	10.5	10.5	10.5	15.0		
		24	12		9	33		
	L.	8.7	8.3	8.3	8.4	10.4	12.6	
		22	2		26	44	50	
	L.	7.0		4.7	5.5	5.5	5.3	5.7
		26			4	7	9	24
	L.		0.2	4.2	4.5	12.5		50
		6			15	50		
above ϵ \rightarrow 8.0		2.1	4.9	4.9	4.9	7.7	10.4	
	33	12	5		9	14	33	
6' higher than ϵ	0.6	4.2	4.2	4.2	4.2	10.2		
	8	3			10	33		
above ϵ 5.5	3.5	3.0	3.0	3.0	3.0	6.9		14.0
	33	8	6		15	33		14.5
4.0 above ϵ	6.5	6.5	6.5	6.5	6.5	9.8		69.3
	33	6	2		11	33		
4.0	3.1	6.1	6.1	6.1	6.1	12.5		
	33	10	5		8	33		
5.0 above ϵ	3.0	2.5	2.5	2.5	2.5	5.3	7.3	
	33	10	8		9	20	33	
	1.0	5.0	5.0	5.0	5.0	5.7		12.5
	33	9	5.0		10	18		10.5
L.	3.8	4.3	3.8	3.8	3.8	4.8	1.8	74.0
	10	8	4		18	14	33	74.6
	L.	7.4	8.0	7.5	7.5	5.3	L.	74.0
		11	7	2	11	28		74.6
	5.2	4.4	5.0	4.3	4.3	4.7	3.8	54
	33	10	8		7	9	11	33

O	+	π	-	Levels on "A" R. Elv.
		94.11		
125		$\frac{12.55}{81.56}$		8.8 86.9
126				12.6 81.5
T.P.	3.10	1384.66	12.55	1381.56
127		$\frac{0.72}{1383.94}$		8.3 76.4
128				9.3 75.4
129				7.6 77.1
130				2.0 82.7
T.P.	9.22	93.16	0.72	1383.94
+85		$\frac{2.66}{1390.50}$		4.4 88.8
B.M.	2.87	93.37	2.66	1390.50
131				4.4 89.0

93.4
44
89.0

29

Line.

L	C	R
4.	7.4 8.9 8.8	8.8 10.6
	12 11 7	3 33
	9.6 10.4 12.9	12.6 10.6
	33 16 12	3 8
		12.6 15.6
		15 33
7.2	8.7 9.4 8.3	8.3 10.5
33	17 15 10	3 10
L.	9.9 10.3 10.3 9.3	9.3 11.0
	18 15 10 8	3 10
	7.8 8.8 7.6	7.6 8.3 10.3
	33 15 7	4 8 33
L.	4.1 2.0	2.0 2.4
	13 7	4 8
		3.0 above 4
		33
L.	2.5 4.9	4.4 4.7 1.4
	13 9	4 6 12
		L.
= 1390.67. Sp in Oak Rt. Δ 131+		
L.	3.9 4.9	4.8 3.4 3.5 2.5
	15 12 4.4	3 6 20 33

93.4
44
89.0

7-28-19
CJW-O.R.-S.J.
30

Levels on B¹ Line.

○	+	↑	—	Rod	Elv.
B.M.	1.00	1395.23			1394.23
T.P.	7.57	89.93	12.87		1382.36
15				5.7	84.2
+15				6.8	83.1
+40				9.4	80.5
T.P.	3.30	82.23	11.00		78.93
+75				3.8	78.4
16				5.6	76.6
17				6.3	75.9
18				6.5	75.7
19				6.6	75.6
20				6.5	75.7
21				6.4	75.8
+61				6.9	75.3
22				4.8	77.4
+67				6.3	75.9
23				6.5	75.7
24				6.3	75.9
25				6.6	75.6
26				6.3	75.9
27				6.4	75.8
28				6.6	75.6
T.P.	7.97	85.10	5.10		77.13
29				9.1	76.0
+60				9.6	76.5
30				8.2	76.9

Sp. in T.P.

2.1	3.2	3.3	4.1	4.1	5.7	11.4	L.	✓
3.3	2.6	2.2	2.0	8		3.0		
		3.5	4.2	4.2		11.6	12.5	
		3.8	3.0	2.1	6.8	2.1	3.3	
		4.0	4.0			12.5	L.	
		4.5	3.3		9.4	1.8		

3.8

L.

L.

L.

L.

L.

L.

L.

L.

L. 6.3 / 1.8 4.8 0.0 / 3.3

L.

L.

L.

L.

L.

Sp. in T.P. Lt. 28

Q	+	↑	-	Rod	ENV
		85.10			
+90				2.6	82.5
31				3.1	82.0
32				3.5	81.6
33				2.7	82.4
+64 ⁵ Δ				2.3	82.8
B.M.			0.00		1385.10 =

85.10
84.98
1.12

L C R.

31

	L		2.6	3.8					
				3.3					
	L		3.1	3.8					
				3.3					
	L		3.5	4.5					
				3.3					
	L	2.9	3.4	2.7	3.6	3.0			
		1.0	9		1.8	2.0	L		
	L	2.3	2.7	2.3	1.9	2.1	2.9	2.4	
		4	3		5	1.0	2.1	2.2	L

1384.98 sp. on T.P.L.A.

Levels on "C" Line.

L C R.

0	+	π	-	Rad	Elv.
B.M.	3.94	1384.64			1380.70
253		^{4.84} 79.80	4.9		79.7
T.P.	3.65	1383.45	4.84		79.80
+50			5.2		78.3
254			7.2		76.3
255			7.6		75.9
256			6.3		77.2
257			4.6		78.9
258			4.7		78.8
259			3.7		79.8
+45			2.5		81.0
260			2.5		81.0
T.P.	6.27	87.72	2.00		81.45
261		^{0.80} 86.92	7.0		80.7
+50			7.1		80.6
262			5.8		81.9
263			3.6		84.1
264			3.3		84.4
265			2.6		85.1
266			1.0		86.7
T.P.	2.77	89.69	0.80		86.92
267			3.1		86.6
268			4.3		85.4
269			6.9		82.8
270			8.8		80.9

Sp 117 T.P.											
	5.2	6.2	6.2	4.9	4.9	4.9	5.4	5.4	4.2		
	17	14	11	7	6	8	10	13			
				6.2	5.2	5.0	5.5	4.8	4.3		
				3	10	13	16	33			
				7.2	7.2	5.6	5.6	6.2	5.8	4.8	
				3	6	14	16	20	33		
				7.6	7.6	5.5	5.5	6.7			
				4	4	7	17	22	4		
				6.3	6.3	5.5	5.0	5.7	5.7	4.7	3.7
				3	3	14	17	19	20	33	
Center rd road.	4.9	5.8	5.0	4.6	4.6	5.5	5.5	4.7	4	Drains	
	3.6	5.1	5.1	4.2	4.2	5.5	4.9	5.3	2.1	LT 18"	
	27	24	22	16	10	10	13	22	2	22"	
	3.2	3.6	2.8	3.2		4.3	3.0	3.8			
	28	20	22		37	7	11	33			
	2.5	2.9	1.8	1.8	2.5	3.6	3.3	1.1	2.1		
	28	21	13	1	2.5	6	8	13	33		
	2.4	2.4	1.6	1.6	2.5	2.8	2.8	1.4	4		
	27	20	19	8	2.5	3	6	8			
			5.5	7.0							
			33	29	7.0						
	5.9	5.4	5.4	7.1							
	33	29	16	6	7.1						
			6.0	5.0	4.7	5.8	5.8	4.3			
			22	14	6	3	16				
	3.9	4.2	4.2	3.5	3.1	4.1	3.5	2.9			
	24	22	20	17	1	3.6	8	10			
	3.5	3.8	3.8	3.3		3.4	2.9				
	23	21	19	15	3.3	3	6				
	2.1	2.4	2.4	2.0	2.2	2.3					
	21	20	18	16	2	4					
	1.6	1.1	1.9	1.9	0.9	1.0	1.7	1.7	1.1		
	33	20	19	16	14	1.0	1	7	7	8	4
			4.2	4.5	4.5	3.9	3.1	3.5	2.8		
			18	17	14	12	1	5	8		
			4.1	3.8	5.4	4.6	4.7	3.8	3.6	2.6	4
			33	22	18	13	5	11	15	17	
				8.4	6.9	6.9	7.0				
				21	11	6.9	33				
			8.8	7.6	7.6	8.8					
			16	11	3						

Pot Hole
Drain south
along side
ditches.

○	+	π	-	Rod	Elv.
		89.69 757 82.12		8.6	81.1
T.P.	5.88	88.00 880 1379.20	7.57		82.12
271				6.7	81.3
272				5.8	82.2
273				5.4	82.6
274				4.6	83.4
275				3.7	84.3
276				5.4	82.6
277				8.4	79.6
B.M.	12.20	1391.40 764 83.76	8.80		1379.20
279				13.5	77.9
280				12.3	79.1
281				8.4	83.0
282				4.1	87.3
283				4.6	86.8
284				6.9	84.5
+50				10.0	81.4
285				9.5	81.9
T.P.	3.55	87.31	7.64		83.76
286				6.4	80.9
287				5.6	81.7
288				5.1	82.2
289				6.4	80.9
+20				8.1	79.2
290				8.3	79.0

33

L.	8.7	7.7	7.7	8.6	L.				
	16	11	3						
L.	7.3	6.2	6.2	6.7	L.				
	14	10	3						
		6.7	5.8	6.0	6.9	5.9	L.		
		13	10	5.8	9	11			
		6.1	5.4	6.4	6.4	5.9	L.		
		12	10	5.4	14	16			
L.	4.8	5.3	5.3	4.6	5.4	4.4	L.		
	19	17	13	7	12	16			
L.	3.4	4.3	4.3	3.7	3.7	4.3	4.3	3.2	L.
	19	17	13	9	6	10	13	16	
		3.2	5.4	5.4	5.4	5.8	4.5	4.5	2.0
		20	16	5.4	2	9	18	22	27
L.		9.8	7.9	8.4	9.7				
		13	8		5				
Sp. in Cor. F.P. Lt. Δ 278 + 73.2									
					L.				
					L.				
					L.				
					L.				
					L.				
					L.				
					9.0	10.0	9.0		
					33		33		
					8.0				
					33	9.5	L.		
					7.9	6.4	5.4		
					33		33		
					6.6	5.6	4.6		
					33		33		
					7.1	5.1	4.1		
					33		33		
					7.0	6.4	L.		
					33				
					L.		L.		
					L.	8.3	9.3		
							33		

		87.31 ✓		
T.P.	1.79	1381.15 ✓ <small>12.00 1369.15</small>	7.95	79.36 ✓
291			7.6	73.6
+40			11.9	69.3
292			13.7	67.5
T.P.	0.45	1369.60 ✓ <small>9.17 1360.43</small>	12.00	1369.15 ✓
⊙ +83.5			9.7	59.9
293			9.3	60.3
T.P.	7.99	68.42 ✓ <small>0.15 68.27</small>	9.17	1360.43 ✓
294			5.0	63.4
295			5.5	62.9
Δ +60.3			2.1	66.3
T.P.	5.88	74.15 ✓ <small>11.05 63.10</small>	0.15	68.27 ✓
296			9.8	64.4
297			5.8	68.4
+50			3.7	70.5
298			4.8	69.4
+65			7.2	67.0
T.P.	0.40	63.50 ✓ <small>10.74 52.76</small>	11.05	1363.10 ✓
+85			0.8	62.7
299			2.8	60.7
+43			11.2	52.3
T.P.	3.73	56.49 ✓ <small>10.74 45.75</small>	10.74	1352.76 ✓
300			6.0	50.5
BC+269			5.2	51.3
+50			5.0	51.5

34

	8.5	7.6	L.	
	3.3			
	12.9	11.9	L.	
	33			
	L.	L.		
Pop sp. in A	Stamp on Line.			
	L.	9.7	3.5 90	
		9.3	3.5 90	
		L.		
	8.9	5.0	2.7 60	
	25			
	L.	5.5	5.5 50	18" CM Req'd.
	5.1	5.1	2.1	18" CM Req'd.
	86	31	15	18" CM Req'd.
On Δ stump.	(40' Ext. Req'd on this Curve)			
	L.	11.8 20	9.8 33	7.3 33 (18" CM Req'd.)
		8.2 25	5.8	L.
		8.5 33	3.7	2.7 33
		8.5 33	4.8	L.
	23.4 30	13.9 15	7.2	5.2 15 L.
on Beach	14.2 33	12.8 23	0.8	6.3 above & 15
"	15.4 33	12.1 12	2.8	7.0 above & 30
"	15.9 33	13.0 6	11.2	0.0 13
				16.5 above & 22
				21.8 above & 33
	7.7 33	6.0	6.0 12	0.8 23 11.7 above & 33
	7.1 33	5.2	2.4 26	8.3 above & 33
	6.5 33	5.0	1.9 33	

New Elevations on Change
South side Webb Lake.

Taken		From	Topog.
291	73.6	+10	69.0
+05	73.0	+35	70.0
+17	72.0	+55 297	70.2
+26	71.0	+07	70.0
+35	70.0	+45	69.0
+49	69.0	+78	68.0
+63	68.0	+87	67.0
+90	67.0	+91	66.0
292	66.7	+93	65.0
+23	66.0	+99	64.0
+53	65.0	298	63.7
293	64.2	+05	63.0
+04	64.0	+15	62.0
+37	63.0	+25	61.0
+61	62.0 ✓	+75	52.0
+90	61.5	+85	51.0
294	61.4	299	50.7
+07	62.0	+19	52.7
+18	63.0	+23	51.7
+48	64.0	+55	52.0
+75	64.8	+85	53.0
+85	65.0	300	53.2
295	64.8	+50	53.7
+07	65.0	301	53.4
+23	66.0	+50	53.0
+40	67.0	+95	52.0
+80	68.0	302	51.8
296	68.6	+45	51.0

Used by Westmans
Revised by Westmans

³⁰² +67	50.0
+83	49.0
303	48.2
+05	48.0
+15	47.0
+35	46.0
+45	45.0
+60	45.0
+80.7	45.5

Elevations on curve at 311+21.7 to
314+48.9

312	= 59.2
+50	= 59.6
+90	= 60.8
313	= 60.4
+10	= 60.0
+30	= 59.0
314	= 57.7

		56.49 ✓		
301		1.12 55.37	3.4	53.1
+50			3.4	53.1
302			3.7	52.8
B.M.	1.11	56.48 ✓	1.12	1355.37 ✓
+50		3.26 53.22	4.2	52.3
303			5.3	51.2
+50			6.3	50.2
304			8.6	47.9
+20			11.2	45.3
W.L.		56.48 10.90 45.58	10.90	45.58
+35		10.90 45.58	11.6	44.9
+50			11.3	45.2
305			10.4	46.1
306			9.2	47.3
+60			4.5	52.0
T.P.	10.99	64.21 ✓	3.26	53.22 ✓
307		1.46 62.75	2.6	61.6
+10			1.6	62.6
T.P.	9.30	72.05 ✓	1.46	62.75 ✓
308			8.9	63.2
309			4.2	67.9
+30			6.3	65.8
+80			6.9	65.2
310			5.6	66.5
+30			5.8	66.3

35

		6.3	3.4	2.6	
		33		33	
Beach		6.1	3.4	2.2	L.
		33		11	
		6.5	3.7	2.3	3.6
		33		13	33
Sp in Top Pop stump Rt. 302 + 25					
		6.4		2.8	2.9
		33	4.2	10	33
		7.4		2.7	
		33	5.3	5.3	
Sand		9.4		5.1	L.
		33	6.3	9	
		10.8		8.0	
		36	8.6	33	
	9.2	9.6	11.0	9.4	9.5
	33	20	15	6	36
W.L. Webb Lake 7-31-19					
		8.2	11.3		
		33	12	11.3	L.
	7.3	7.3	9.3	10.4	11.0
	33	28	19	10	18 L.
			7.4	9.2	L.
			33		
	4.7	3.0	4.5	4.5	9.5
	33	21	10	20	33
		13.0	5.7	2.6	1.1
		33	2.3		33
		13.0	3.5	1.6	L.
		33	21		
On Transit Hub.					
	-13.0	8.9			
	35	25	8.9		L.
		6.2	4.2		L.
		33			
		8.9			L.
		33	6.9		5.9
		8.6			33
		33	5.6		3.6
		7.0	5.8		3.4
		33			33

53.22
10.99
64.21

311		72.05 ✓ <small>10.85 61.20</small>	11.3	60.8 ✓
T.P.	1.75	1362.95 ✓ <small>0.74 62.21</small>	10.85	1361.20 ✓
312			4.7	58.3
+85			7.3	55.7
T.P.	5.60	67.81 ✓ <small>9.53 58.28</small>	0.74	62.21 ✓ <small>Down on Beach not needed.</small>
313				
314			10.6	57.2
T.P.	8.79	67.07 ✓ <small>9.16 57.91</small>	9.53	58.28 ✓
315			10.0	57.1
316			9.4	57.7
T.P.	8.02	65.93 ✓ <small>0.56 65.37</small>	9.16	57.91 ✓
317			6.3	59.6
318			3.2	62.7
T.P.	9.17	74.54 ✓ <small>11.84 62.70</small>	0.56	65.37 ✓
+50			7.4	67.1
319			5.5	69.0
+35			4.3	70.2
B.M.			7.63	1366.91 ✓
320			9.5	65.0
+60			12.5	62.0
T.P.	1.16	63.86 ✓ <small>11.15 52.71</small>	11.84	1362.70 ✓
321			6.0	57.9
Δ +71.6			10.0	53.9
322			11.6	52.9
T.P.	11.41	64.12 ✓ <small>11.15 52.71</small>	11.15	52.71 ✓

L.	11.3	8.3 33		
7.2 33	4.7	2.2 24	L.	
11.4 6	7.3 2	7.3	0.7 4.5	L. Breaks off to PI on Beach.
		10.7 14	7.0 28	5.1 50
	10.6	7.3 20	6.2 37	L.
		8.1 13	6.0 46	3.4 66
	9.4	6.6 12	4.1 50	
	12.2 20	9.3 16	6.3 40	
7.5 33	4.3 27	3.2	L.	
	L.	7.4	L.	
	L.		L.	
	4.3 33	4.3	6.6 33	
	Sp. in N.P. Lt. 319 + 75			
	L.	9.5	10.5 33	
	L.	12.5	13.5 33	
	L.		L.	
12.0 16	10.0 6	100	12.3 15	L.
13.5 24	12.7 13	11.6 6	11.6	13.3 6 L.

