

THE BERGEN ROAD - 142-25
THE PINE TREE ROAD - 141-20
AT #1 of State Road #8

FIELD BOOK

361

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THE BERGEN ROAD

22

21

+15

△

R

20

19

18

17

16

15

14

13

12

11

10

9

8

7

6

+61

△

L

5

4

3

2

1

0

East

SECS 31-30 etc

T. 142-R25

A. G. MASON
A. W. M
7-12-18

2

light

very light

light clear & heavy clear

with S side sec 31
Invert - A side

slow

42

41

40

39

38

37

36

+41

35

34

+37

33

+50

32

31

30

29

28

27

+80

+33

26

25

24

+88

23

△

L

△

R

△

L

△

L

^

4' box req.

38450-40 Fill 2'

33450 to 35-Fill
2' high

light

4' box req.

x
x
x

3' box (invert) req.

River 100' East

O.G.M 7-12-12
AUM

4

60

59

+91 D L

+50

58

57

+50

56

+60 D R

+25

55

54

53

52

51

50

49

+43

48

47

46

45

44

43

42

Fill 150' long

↓ FILL ↓
↓ FILL ↓

Heavy

4' box

1 box 4'

Heavy

4' box

78

+25

77

+91

76

+48

△

L

75

74

73

+28

△

L

72

71

70

+43

△

R

69

+50

68

67

66

65

64

+88

△

L

63

62

61

O.G.M. 7-12-18
A.W.M.

5

Fill 3' ↑
↓

Light
X

6' box

↑
Fill 3'
↓

Heavy
X

6' box

med
↓

99
98
97
96
95
94
93
+05
92
91
90
+49
89
88
+24
87
86
85
84
83
+37
82
81
80
+20
79

△

R

△

R

△

L

△

R

^
Fill 2'

v

^
Fill 2 1/2'

v

Heart Med

A' box

^
Back

^
light

O.G.M.
AUM 7-12-18

7

3' box req.

+60

+41 Δ

21

20

19

18

17

16

15

114+06 Δ L

14

13

12

11 +50

10

9

8

7

6

5

4

3

2

1

100

11-12 Fin 2'
00A50 = S.L. line
bet 29+30-

Rock

Med

Light

0.6M. 7-12-18
PUM

8

41

40

39

38

37

36

+94 Δ

R

35

34

33

32

+74 Δ

L

31

30

+12 Δ

L

29

28

+51 Δ

R

27

26

25

+55 Δ

R

24

+47

23

122

35 to 41 Exc 500 Cu. Yds

Stony Ridge

Light Bear
Heavy Grub

29 to 30 Exc 100

126 to 128+50
Exc. 300 Cu. Yds

21+41 to 24+55

(+F 250 Cu. Yds

Sec line 529-30
1742 K. to Cor.

Light

62
 61
 60
 59
 +34
 58
 57
 56
 55
 54
 53
 52
 51
 / 50
 +9
 +12 Δ L
 48
 +54 Δ L
 47
 46
 +16 Δ R
 45
 44
 43
 / 42

Med
 ↓

41 Col.
 61 to 63 + 50 F/N 3'

3' / 1/4

56 to 57 + 50 Ex 150 G.V.

Med
 ↓

47 to 51 Ex 300 G.V.

Med → Right
 ↓

41 to 45 Ex 300 G.V.

+13 Δ R

83

82

81

80

79

+06 Δ R

78

77

76

75

+07 Δ L

74

73

72

+92 Δ R

71

70

69

+81 Δ R

68

67

66

65

64

63

X

Heavy

77 to 79 Ex 150 C.Y.

↑

Med

Med

65 to 68 Exc 300 C.Y.

205

+50

204

203

202

+50 Δ

R

201

200

199

198

+33 Δ

R

197

196

195

194

193

+77 Δ

L

192

191

190

89

88

87

86

85

184

o.g.m. 7-12-18
A.W.M.

11

A' box

203-205 Ex 200 C.V

X Med

> Light
" Grub → Heavy

Med

193-185 Ex 150 C.V

225
 224
 +60 Δ L
 223
 222
 +50
 221
 +33 Δ L
 220
 219
 218
 217
 +50
 216
 +13 Δ R
 215
 214
 213
 212
 211
 210
 209
 208
 207
 206

OGM
HW 7-12-18

12

Spring 100' W

On Ridge at Camps

X Med

Hog Backs

212

Med Heavy

209-211 Ex 200 G.Y.

3' box

1
 F2
 X
 F11
 2

241+08

240

+16 Δ

L

239

238

237

236

235

+20 Δ

R

234

233

232

231

230

229

228

+30 Δ

R

227

226

End of Survey - Intersec
old Road

236-239 Ex 500 C.Y.
(Fill)

231-233 Ex 300 C.Y.

Heavy

Med

Heavy

Bids Aug. 27-18

Frank Simpson - Pomer

Clear + Grab - 250⁰⁰

Spool C. / Evl 30¢ 1700⁰⁰

T.P. 450⁰⁰

10% alt. Exp. 250

15 lots @ last 2750

300

3050

C.E. Clemens 26 175⁰⁰

Clear + Grab + T.P. (+lots) 2727⁰⁰

Exc 33¢ 1320

3547

THE PINE TREE ROAD

1st 1/2 MILE - On the 17 line Sec 2-141-76
To be cleared-grubbed and graded

Fill	Vol	1050' long	Dirt	16' x 1'	623 cu. yds
"	"	2	125'	2' x 12'	112
		3	150	1/2 x 12	34
		4	150	1 x 10	56
		5	100	1 x 10	37
		6	300	1/2 x 10	36
		7	400	1/2 x 10	74
		8	150	1/2 x 10	28
		9	250	1/2 x 10	19
		10	100	1/2 x 10	19
		11	100	1/2 x 10	19
		12	875	1 x 10	415
		13	500	1 x 10	185
		14	1075	1 x 10	507
					2214

REMER TWP.

7-11-18 15

200' ties to be removed
1 Timber Col. req. 6' dia x 12' long
50' Sordoray 42" x 16'

Estimate - PINE TREE ROAD

1/2 mile - H. Line Sec 2

Clear 33' wide - 2A @ 50 3100.00

Grub 33' .. 2A .. 50 100.00

Tumpike 2640' @ 8¢ 211.20

411.20

Removing Ties on 1/2 mile - (includes 200' sidehill) 50.00

Reshaping 1/2 mile 25.00

50' Corduroy 1' x 12' @ 25¢ 12.50

3 Timber logs - 6' w x 12' long @ 20 60.00

2214 Cu. Yds. Exl. @ 40¢ 885.60

Misc. 100.00

TOTAL - \$ 1544.30

Nov. 11-18

Est'd amt dirt on Pine Tree Corduroys

1st - Short one 1' x 8' 50 C.Y.

2nd - Long 6" x 8' 150 ..

3rd - " 6" x 8' 200

400 ..

35

35)300(

70

2000

1200

140.00

100.00

PIT No. 1 (1A.) (CASS)

1/4 SEC. 6 - T. 144 N. R. 31 W.

Beg. at a point on the west line of section 6, T. 144 N., R. 31 W., 140 ft. north of the SW corner, thence north on the west line of said section 160 ft., thence east 272.25', thence south 160 ft., thence west 272.25 ft. to the point of beginning, and containing one acre.

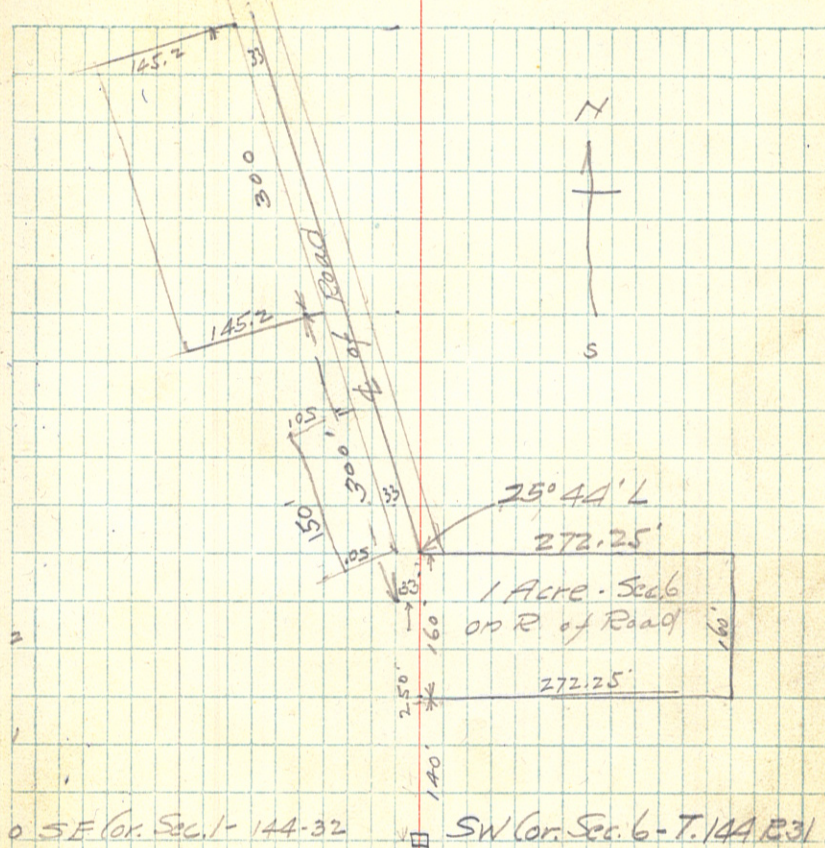
PIT No. 2 (2A)

1/4 SEC. 1, T. 144 N., R. 32 W. (HUBBARD)

Beg. at a point on the east line of section 1, T. 144 N., R. 32 W., 300 feet north of the SE corner, thence N. $25^{\circ} 44'$ W along the center line of S.P.H. No. 82 a distance of 550', thence southwesterly at right angles to said center line of S.P.H. No. 82 a distance of 158.4 ft., thence $S 25^{\circ} 44' E$ 550 ft., thence northwesterly 158.4' to the point of beginning, and containing 2.0 Acres.

Gravel Pits -
On S.P.H. No. 82 -
Sec. 6 - T. 144 - R. 31

ZUELOW - R. 17
LA PORTE



Truc B.
18+997 N23°32' L N1°31' W

18

17+355° N24°50' L N22° 01' E

17

16

15

14

13

12+332° N26°43' L N46°51' E

12

11

10

9+45° N26°30' R N73°34' E

9

8

7+50° N90° 9' R N41° 44' E

7

6+50° N28°05' R N37°35' E

6

5

4

3

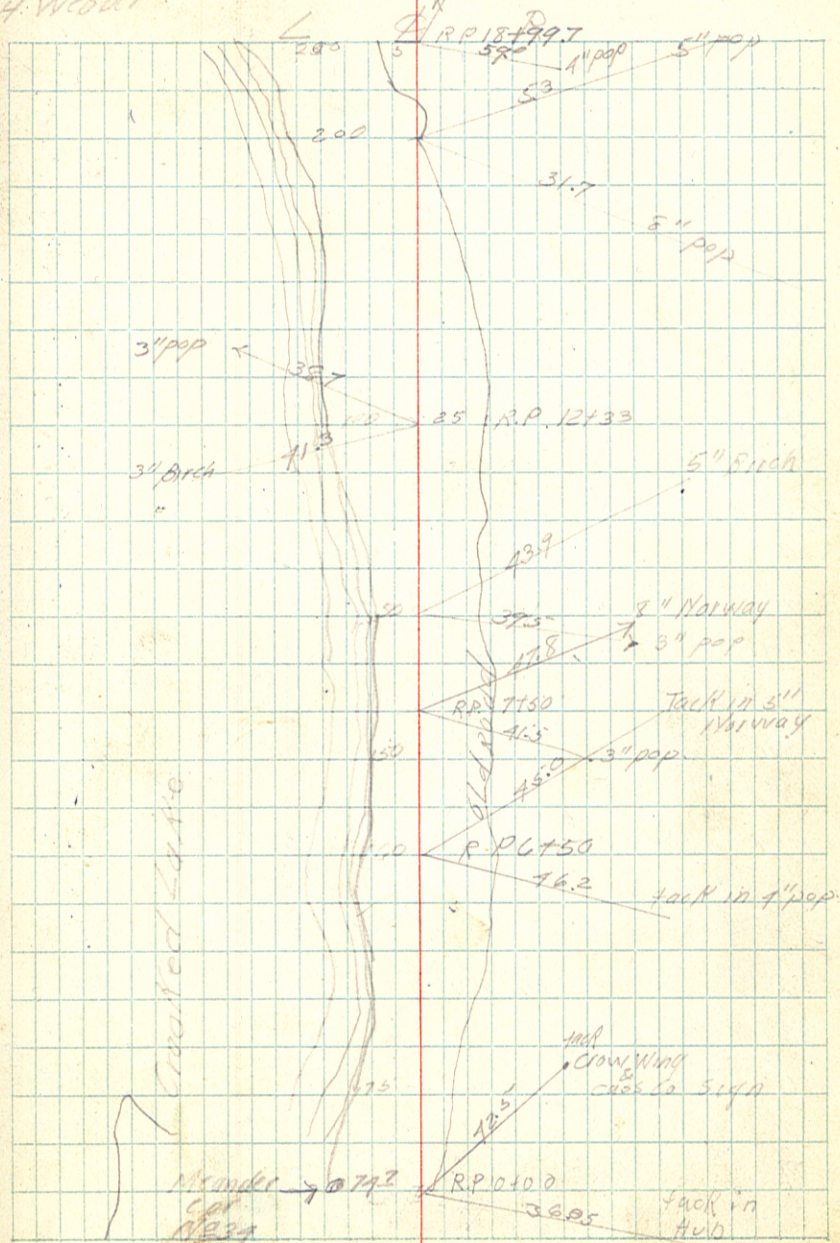
2

1

00 N9°30' E 8°00' VAD

F.W.M.
J.F.P.
H. Webber

Lat N° 1 state Road #8
10" dry pine stump
Aug 16, 1915



TRUGB

2132
2102

150 Tot.

36

35

34

33

32

31

30+05.7 Δ6°15' L N71°07' E V

30

29

28+56.9 Δ7°23' L N72°22' E V

28

27

26+113 Δ4°17' R N59°45' E L

26

25+10.2 Δ18°53' R N40°28' E L V

25

24+04.0 Δ22°36' R N21°35' E V

24

23

168 N1°31' W

22

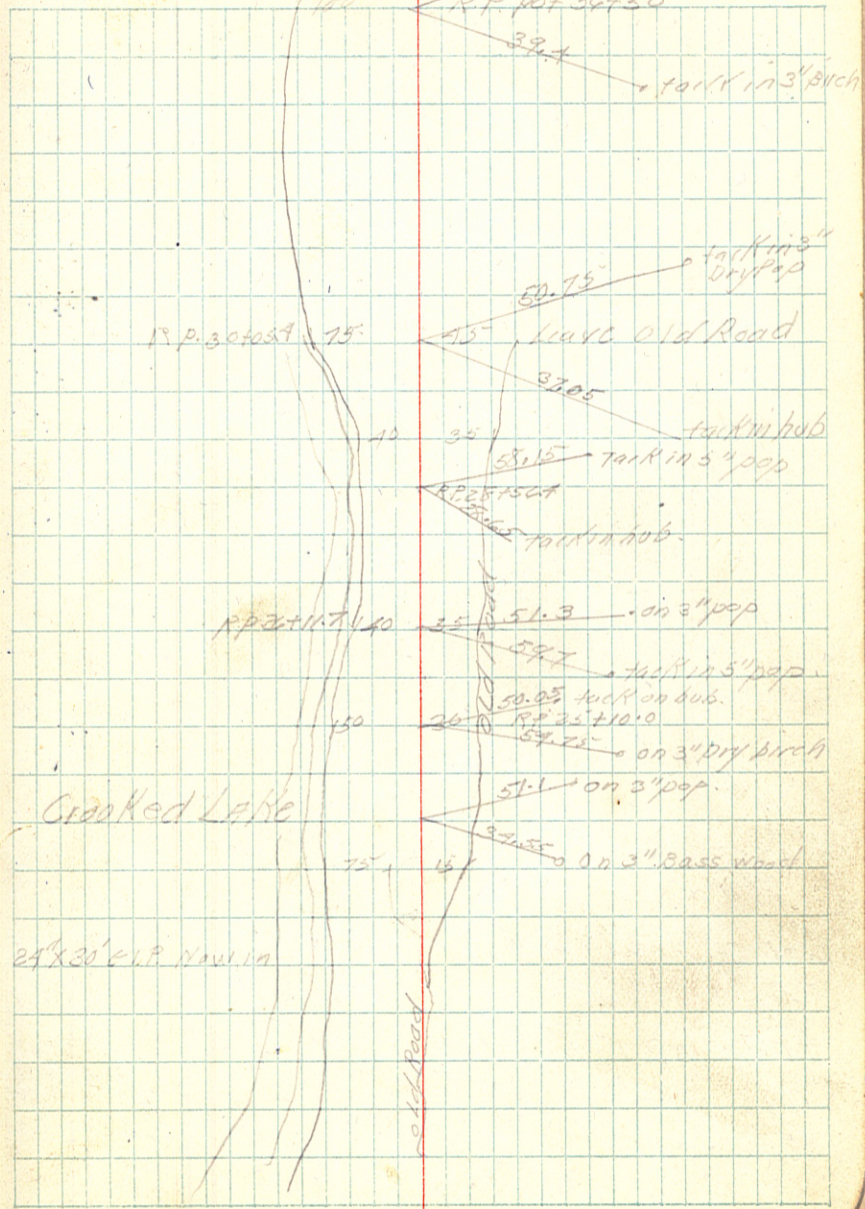
21

20

19

Aug 16, 1978

A.W.M.
J.F.P.
H.W.



True Bearing

+13° END

70

69

68

67

+71° S 47° 08' L N 29° 36' W Changed Line

+75° S 44° 04' L N 26° 32' W ←

+82° 63 1/4 Line

61

63

62

61

61

59

38

S 71° 08' 5 L N 13° 08' L N 17° 32' E

8 N 31° 40' E

Aug 16, 1918
A.W.M.
J.F.P.
H.W.

21

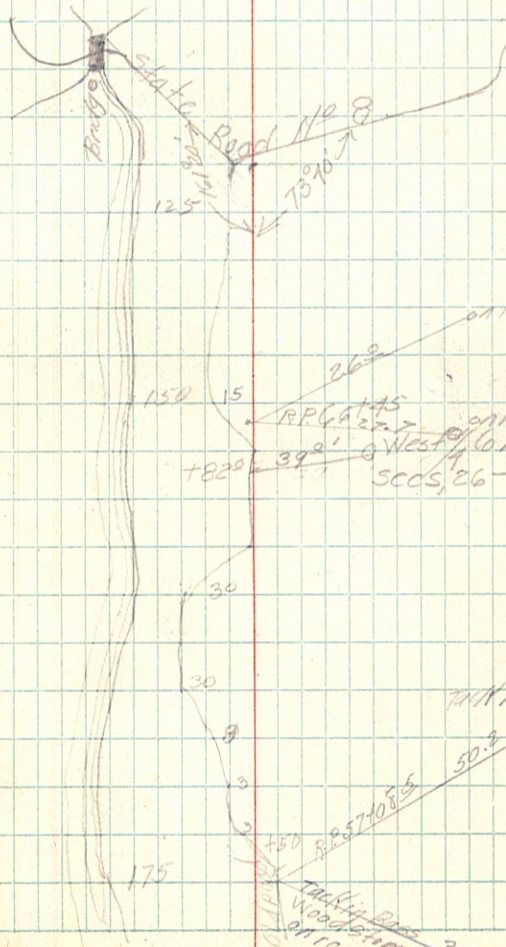
On big sign board.

390'

R.P.S. 70 + 13° END.

24° to Lushers Sign Post

CROWNED LARK



150

15

+82°

30

30

9

3

2

175

Tank in 3rd maple

50.3

Tank in Woodcamp on top 38 out

August 1918

A.W.M.
J.F.P.

Sta	B.S.	I.I.	Red	F.S.	Elev.
BM.	12.93	112.93			100.00
00			6.3		06.6
1			4.7		08.2
2			4.3		08.6
3			5.9		07.0
4			7.0		05.9
+50			8.2		01.7
5			10.2		02.7
6			10.8		02.1
+50			12.7		00.2
TP.	5.78	^{5.99} 107.44		11.27	101.66
7			6.8		00.6
+50			8.1		99.3
8			6.2		01.2
9			5.8		01.6
+75			5.7		01.7
10			4.8		02.6
11			4.9		02.5
+75			5.7		01.7
12			6.6		00.8
+33			8.1		99.0
13			11.1		96.3
TP.	3.10	^{3.96} 103.54		7.60	99.84
14			4.8		96.7
15			6.8		96.9

L		R	
BM spike in 4" poplar 45' left of Sta 00+40			
04.2		07.1	
20		15	
04.3		102	
25		20	
06.0		10.0	
25		20	
04.6		08.7	
20		20	
02.9		08.2	
25		22	
02.7	03.0	06.7	
20	15	20	
LEVEL		05.1	
		25	
98.5	00.6	LEVEL	
25	10		
97.9		02.2	
	20	25	
97.6		02.7	
20		25	
93.4	96.9	03.1	
20	15	20	
	98.0	02.3	
	15	20	
	98.6	02.2	
	20	20	
	98.1	03.1	
	20	25	
97.8	01.5	04.1	
24	12	15	
98.6	01.8	03.6	
25	12	25	
	98.5	LEVEL	
	20		
	98.4	LEVEL	
	20		
	96.9	99.7	
	25	20	
	97.8	97.8	
	25	20	
94.9		LEVEL	
20			
95.3		98.3	
15		20	

Sta	B.S.	H.I.	Rod	F.S.	Elev
		103.54			
16			5.7		97.8
17			5.6		97.9
+35			5.7		97.8
18			5.6		97.9
B.M.				332	100.22
19			5.0		98.5
+15			5.7		97.8
20			7.8		95.7
+60			7.6		95.9
21			8.5		95.0
22			10.0		93.5
+68			11.8		91.7
			14.0		89.14
23			11.0		92.5
+62			3.8		99.7
24			2.3		103.3
T.P.	280	105.44		0.90	102.64
25			4.7		100.7
110			7.6		100.8
26			6.0		99.4
27			7.2		98.2
28			8.9		96.5
+56			8.6		96.8

Aug 21/1918

23

H	I	R
950		LEVEL
15		
956		LEVEL
20		
		LEVEL
978		LEVEL
18		
SPIKE in 5" poplar 30' R STA 18+30		
		LEVEL
938	983	965
20	7	15
913	939	960 946 934
20	12	7 10 20
	927	966
	15	20
	30	935
	15	20
	LEVEL	934 947 928
		7 8 20
	903	929 920
	15	7 20
Bottom Culvert		
903	904	923
20	10	8
		15
	979	992
	18	7
	972	914
	20	10
		15
966	995	LEVEL
18	12	
962	986	LEVEL
18	15	
	940	979
	15	7
	914	976
	25	18 20
	986	965
	18	10
925	940	941
15	12	10
		10 20 20

Sta	B.S.	H.I.	Rod	F.S.	Elev
		105.44			
29			77		97.7
+50			90		96.4
30			94		96.0
+75			80		97.4
31			74		98.0
+75			70		98.4
T.P.	502	^{1.38} 104.06		6.40	99.04
32			58		98.3
+60			74		96.7
33			68		97.3
+65			78		96.3
B.M.				9.28	94.78
34			65		97.6
+50			2.1		02.0
T.P.	1142	⁹⁷¹ 113.77		1.71	102.35
35			24		11.4
T.P.	1275	¹²⁸⁷ 126.14		0.38	113.39
+50			9.7		16.4
36			16.2		15.9
+50			8.6		17.5
37			6.3		19.8
38			5.2		20.9
39			4.0		21.8

Aug 21 1918.

24

Li	±	R
92.9	94.1	96.6
15	11	8
		94.1
		15
93.9	96.2	02.3
12	8	15
		93.1
		15
97.1		105.9
13		15
95.1		06.0
15		20
94.7		01.5
18		20
95.7		LEVEL
15		
95.0		96.7 95.9
18		12 15
94.7	96.7	94.9
20	7	16
B.M. spile in 5' poplar 30' h. sta 33+90		
95.0		96.0
18		15
96.9	00.0	01.4
20	13	18
055	09.8	10.3
17	7	18
121		155
13		25
104	143	LEVEL
20	10	
	134	LEVEL
	15	
	14.9	LEVEL
	15	
	18.1	21.2
	14	20
	21.2	21.4
	18	20

Aug 21. 1918

25

Sta	BS	HI	Rad	F.S.	Elev
		126.14			
+127			15		21.6
10			19		21.2
+70			10.4		15.7
41			9.3		16.8
42			6.6		19.5
+70			8.6		17.5
T.P.	276	121.00 ^{5.14}		790	118.24
43			9.3		11.7
+30			14.5		06.5
44			6.6		14.4
+10			3.1		17.9
45			4.0		17.0
46			9.0		12.0
47			13.2		07.8
T.P.	150	110.55 ^{17.45}		1195	109.05
48			5.6		05.0
49			10.0		08.2
50			5.1		05.5
+29			4.7		05.9
B.M.				1023	100.32
51			9.8		00.8
+50			11.8		98.8
52			10.3		00.3

L	R	R
Level	23.0	
	20	
199	Level	
20		
Level		
18.0	14.0	
18	15	
15.7	18.7	Level
16	13	
14.7	14.0	Level
15	12	
Level		
08.9	04.3	
15	15	
13.1	15.0	10.8
17	7	20
14.0	15.2	15.6
15	12	15
12.9	15.0	Level
18	12	
03.0	09.4	Level
17	12	
04.0	11.0	Level
16	8	
01.2	04.2	03.2
20	10	20
Level		98.9
		20
03.1	04.9	03.1
20	15	15
03.0	05.3	02.4
20	10	20
B.M. = spike in 6" poplar 40' L sta 50700		
Level		97.0
		20
Level		95.7
		18
Level		99.0
		20

Sta	B.S.	I.I.	Rod	F.S.	Elev.
		110.55			
53			3.7		07.2
54 ⁸	D		0.6		10.0
54			1.8		08.8
TP	372	2.47 113.02		125	109.30
55			12.4		00.5
170			14.5		98.5
56			11.0		02.0
+50			5.3		07.7
57			3.8		09.2
+085	D		3.5		04.5
58			6.7		06.3
59			12.0		01.0
60			13.9		99.1
+40			11.3		01.7
61			17.7		01.3
62			11.1		01.9
63		1023	12.5		00.5
TP	137	102.79		1160	101.42
64			6.0		96.8
65			7.8		95.0
66			9.5		93.3
+719	D		9.6		94.2
67			9.8		93.0
68			10.0		92.8

Aug 21, 1918
sultry

L	R	R
	033	08.7
	20	20
	07.0	09.1
	17	12
	05.4	08.4
	20	12
		LEVEL
	01.9	99.0
	20	20
	00.9	00.5
	25	20
		LEVEL
	04.8	07.0
	12	10
	04.5	07.7
	20	10
	04.3	07.7
	20	10
	03.5	06.5
	20	10
		03.9
		20
		98.4
		20
		98.8
		15
		30
		01.3
		18
		20
		LEVEL
		02.0
		20
		98.5
		25
		35
		03.3
		20
		93.9
		75
		96.3
		70
		97.7
		20
	91.7	91.3
	20	10
		94.3
		6
		91.8
		20
		LEVEL
		93.5
		20
		95.0
		15
		LEVEL
		LEVEL

Aug 21, 1918

sta	BS	HI	Rod	FS	Elev
		102.79			
69			9.7		93.1
70			9.5		93.3
+10 ^o	End		8.7		94.1
B.M.	4.13	⁵⁰⁷ 97.72		9.20	93.59
				10.17	87.53

LEVEL
 LEVEL
 LEVEL
 B.M. on concrete at sign post 40' west of sta 70+00
 High point of concrete.
 Water level created Lake - Aug 21, 1918.

Borgen Road

Sta.	B.S.	H.I.	Rod	F.S.	Elev.
BM.	822	108.22			108.00
00+00	LOW		10.3		97.9
00	LOW		9.2		99.0
1			6.2		02.0
2			3.4		04.8
3			5.1		03.1
4			8.0		00.2
+80			12.1		96.1
+90			11.7		96.5
5			14.6		93.6
+10			12.3		95.9
+61	Δ L		9.3		98.9
T.P.	673	108.02		6.93	101.29
6			5.6		02.9
7			3.8		04.2
8			3.2		04.8
+55			3.1		04.6
+78 ²	Δ R.		5.2		02.8
9					
10			4.1		03.9
11			3.7		04.3
12			3.3		04.7
13			3.7		04.3
T.P.	157	108.00		1.99	106.59
+76			3.9		04.2
14			3.6		04.5

J. Parnisell Aug 30 1918.
E. Cromett.

28

L R.

BM. 110.00 taken in paper 25' to 00+75'
00+00 Hub marked ¹⁹ 79+83² and 37+30
= 660' E of S N cut 500 31-142-2.5-

Level Birch

Level 11

Level 11

Fence Level 11

Level 11

Level 11

convert

Level 11

Level 11

97.6 99.811

13 15

Top Big Hub. Sta 57+60 11

98.9 03.8

33 13 11

Level 11

Level 11

Level 11

Level 11

Level 11

Level 11

Level 11

Top 10+60

04.8

15 04.0

WILLOW

Estimate On
Clearing Bergen Road.

Sta to Sta

1	"	9	800		800
10	"	10+50	50		50
11+35	-	23+30	1195		1195
24+25	-	80+00	5575		5575
			7620	lin ft Clearing & Grubbing	

This Estimate.
6 Acres Clearing.
6 Acres Grubbing.

Simpson will finish to Sta 116 in several days and if you give him estimate to 116 there will be 8.5 Acres of clearing and same in grubbing.

from sta 1 to 80 all is cleared grubbed and piled

Estimated clearing done from sta 116 to 291+08
End. 9.4 acres.

Estimated clearing for entire road. 17.9 Acres.
" " " " " " 17.9 Acres.

116
33

348
348

43560 | 382800 | 9
392040

5280 | 369600 |
3680 | 316800 |
5280

112
336
336

43560 | 582800 | 8.4
348480
343200

76

5280
3680
2875
138

Sta	BS	HI	Rod	F.S.	IKV
		106.46			
78+30			3.8		02.7
+70			3.9		02.6
79			2.1		04.4
+20	A	R	1.5		05.0
TP	6.34	111.68		11.2	105.34
+70			7.6		04.1
80			7.8		03.9
+30			8.6		03.1
81			9.1		02.6
+30			8.7		03.0
82			4.9		04.6
+37	A	L	5.1		06.6
83			4.7		07.0
+15			5.6		06.1
84			5.6		06.1
85			3.5		08.2
+25			2.0		09.7
TP	3.21	113.15		17.4	109.94
+45			3.5		09.7
86			5.3		07.9
BM				5.48	107.67
87			9.3		04.9
+24			7.1		04.8
TP	2.20	108.87		6.98	106.17

Aug 31/1918.

L R

37

Brush	$\frac{02.7}{15}$	$\frac{04.5}{7}$	1-15 L
"			
"		Level	$\frac{03.8}{15}$
"			L
TP on small hub near 79+20			
Brush			
"		Level	$\frac{02.7}{15}$
"			L
"			L
"			L
"		$\frac{04.0}{15}$	$\frac{05.4}{20}$
"			
"		$\frac{05.8}{20}$	$\frac{07.5}{20}$
"			
"		$\frac{04.7}{15}$	$\frac{07.1}{20}$
"		$\frac{07.4}{15}$	$\frac{09.5}{20}$
"		$\frac{03.9}{15}$	$\frac{10.5}{20}$
"			
"		$\frac{08.2}{25}$	1-15 L
"		$\frac{07.3}{15}$	$\frac{08.9}{15}$
BM for K in burned Pine Swamp 25' L 85+80			
Brush			L
			L
TP Top of 2031			

Sta	BS	HI	Rod	FS	Elev
		118.29			
TP	955	⁹³⁰ 127.59		0.25	118.04
97+35			8.5		19.1
98			6.8		20.8
99			5.4		22.2
+30			4.0		23.6
100			5.3		22.3
101			6.5		21.1
+30			7.2		20.9
TP	1122	⁶¹⁹ 133.78		56.3	121.96
102			13.1		20.7
103			9.9		23.9
104			9.4		24.4
105			7.6		26.2
106			6.3		27.5
BM				5.15	128.63
107			5.9		27.9
+10			6.2		27.6
+20			7.6		29.2
108			7.9		28.9
109			1.4		32.7
TP	1096	^{10.25} 144.85		0.71	133.07
110			8.9		35.1
+40			8.0		36.0
111			9.2		37.8

Aug 31, 1918

L

R

L = level

Brush		L
"	level	29.8 15
"		L
"		L
"		L
"	22.9 15	19.9 15
TP top 101 + 30		
Brush		L
"		L
"		L
"		L
"		L
BM stuck in 10' poplar 30' 106 + 25		
"	28.4 15	level
"		level
"		level
"	29.5 15	level
"		level
TP on small stake near sta 109		
Brush		level
"		level
	35.7 15	33.8 20

Sta	BS	HI	Rod	FS	Elev
		14403			
111+20			4.2		34.8
+ 40			7.5		36.5
112			6.7		37.3
113			2.4		41.6
TP	908	⁸⁵⁶ 15259		052	143.51
114			6.0		46.6
+60°	Δ		5.1		47.4
+60			4.2		48.4
115			5.0		47.6
+35			7.2		45.9
116			11.2		41.4
+70			10.7		41.9
117			6.6		46.0
+20			7.3		45.3
+40			7.9		44.7
+60			6.7		45.9
+90			6.0		46.6
118			4.5		46.1
TP	546	⁷⁶⁰ 147.99		506	147.53
+70			6.4		41.9
119			7.2		40.8
120			12.7		35.3
+80			15.0		33.6
121			13.8		34.2

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Brush		Level
"		Level
"	$\frac{385}{15}$	Level
"	$\frac{418}{15}$	Level
TP top 113+00		
Brush	$\frac{508}{15}$	$\frac{416}{15}$
"		
"		
"	$\frac{448}{15}$	$\frac{456}{15}$
"		
"	Level	$\frac{426}{15}$
"	Level	
"	$\frac{436}{15}$	$\frac{470}{15}$
"		
"	$\frac{438}{15}$	$\frac{459}{15}$
"		
"		
TP top 118	$\frac{461}{15}$	$\frac{487}{15}$
Brush		
"	$\frac{378}{15}$	$\frac{433}{15}$
"	$\frac{342}{15}$	$\frac{360}{15}$
"	Level	$\frac{340}{15}$
"	Level	$\frac{351}{15}$

Sta	BS	HI	Rod	F.S.	Flev
		14799			
121+11.0 Δ L			13.1		399
T.P.	990	¹⁷² 146.27		1162	13637
+60			11.2		351
+22			10.6		357
+40			11.1		353
+75			10.5		358
123			58		405
+17			16		447
B.M.			299		14325
T.P.	1168	¹⁰²⁶ 156.53	142		14485
124			8.2		483
+28			10.3		462
+55 D R			6.4		50.1
+75			4.7		57.8
125			5.9		58.6
+80			6.7		49.8
126			8.5		48.0
+35			11.6		44.9
+70			12.9		43.6
T.P.	00.07	¹²³² 144.21	1239		144.14
127			7.4		36.8
+15			12.9		31.3
+20			11.6		32.6
+51 Δ R			12.8		31.4

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Brush	Level	35.1	
		¹⁵	
Top 121+71			
Brush culvert	L		
"		237	Level
"		¹⁵	
"	L		
"	L		
"		415	395
		¹⁵	¹⁵
= SEC 295301792 North To Corner			
B.M. truck in pine stump		25	R Sta 123+15
Brush			
"		460	465
		¹⁵	¹⁵
"	Level	420	
"		¹⁵	
"		495	521
		¹⁵	¹⁵
"		512	543
		¹⁵	¹⁵
"		497	500
		¹⁵	¹⁵
"			
"	Level	470	
		¹⁵	
"	Level	461	
		¹⁵	
"		450	460
		¹⁵	¹⁵
"			
"		36.5	35.5
		¹⁵	¹⁵
"			
"		336	329
		¹⁵	¹⁵
		294	314
		¹⁵	¹⁵
		329	296
		¹⁵	¹⁵
		30.4	28.0
		¹⁵	¹⁵

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Sta	BS.	HI	Rod	FS.	FLY
		144.21			
T.P.	181	⁹⁵⁴ 137.65		11.37	132.84
128			10.7		29.0
+25			10.4		29.3
+70			5.9		28.8
129			5.6		29.1
+120	A		5.9		29.6
+35			5.0		29.7
+50			1.9		32.8
+76			2.3		32.4
130			4.0		30.7
+40			8.0		26.7
131			7.7		27.0
+90			9.3		25.4
+71			6.1		28.6
T.P.	190	²⁸ 137.93		1.62	130.03
132			7.4		27.5
+50			8.7		26.2
775			8.0		26.9
133			8.0		26.9
+50			11.0		23.9
134			9.5		25.4
775			12.7		22.2
135			11.2		23.7
+40			7.6		27.3

T.P. top 137451

BRUSH	level	25.4	
"		25.0	73
"		15	23.5
"		26.2	15
"		15	level
"		26.7	15
"		15	31.3
"		27.1	15
"		15	level
"		35.8	33.8
"		15	31.8
"		35.0	5
"		15	29.2
"		15	31.5
"		21.4	15
"		15	2.0
"		27.7	12
"		15	31.2
"		27.7	15
"		15	28.2
"		27.7	15
"		15	28.8
"		26.9	15
"		15	25.3
"		level	15
"		27.9	15

T.P. top 131774

BRUSH	level	22.0	
"		29.0	20
"		22	23.4
"		28.9	20
"		20	25.1
"		25.1	15
"		20	level
"		28.2	20
"		20.9	15
"		23.9	15
"		15	level
"		23.7	15
"		15	24.9
"		26.2	15
"		15	level

Sta	B.S.	H.I.	Rod	F.S.	Elev
		13793			
135+70			74		27.5
+83			45		30.4
+91	B	R	4.9		30.0
136			5.2		29.7
B.M.				5.96	129.47
+30			5.3		29.6
+90			11.5		23.9
137			11.7		23.2
+12			10.6		24.3
+40			9.5		25.4
+90			13.7		21.2
138			12.7		22.2
139			11.0		23.9
+20			10.0		24.9
+10			7.4		27.5
140			9.7		25.2
+10			9.1		25.8
+35			4.6		30.3
+80			2.3		32.6
141			1.0		33.9
T.P.	270	²⁵⁵ 137.98		0.15	134.78
+50			6.5		31.0
+42			1.7		32.8
+15			4.5		30

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40

	L	R
Brush		level
"		level
"		level
"	29.4	level
B.M. on high point of road 25' W of sta 135+91	¹⁵ 273	¹⁵ 321
Brush	<u>15</u>	<u>15</u>
"		
"	22.1	27.5
"	<u>15</u>	<u>15</u>
"		
"	22.4	27.4
"	<u>15</u>	<u>15</u>
"		
"	24.0	21.9
"	<u>15</u>	<u>15</u>
"	23.8	level
"	<u>15</u>	
"	22.6	29.6
"	¹⁵ 22.5	¹⁵ 29.5
"	<u>15</u>	<u>15</u>
"	27.2	33.4
"	<u>20</u>	<u>15</u>
"		
"	31.5	27.8
"	<u>20</u>	<u>15</u>
"	35.3	30.4
"	<u>20</u>	<u>20</u>
"		level
T.P. on small stake near 141		
Brush	29.2	36.0
"	<u>20</u>	<u>20</u>
"	24.3	36.2
"	<u>22</u>	<u>20</u>

Sta	B.S.	H.I.	Rod	F.S.	Elev
		137.48			
142+40			83		29.2
+60			6.9		30.6
143			10.1		27.9
+25			9.0		28.5
+50			9.7		27.8
144			10.1		27.4
+20			8.1		29.1
+70			7.3		30.2
145			6.0		31.5
+16 ⁰	B	R	5.1		32.4
+35			4.9		32.6
+60			8.9		28.6
146			10.9		26.6
+35			8.3		29.2
+70			8.9		28.6
147			8.0		29.5
+35			9.0		28.6
+54	A	L	6.0		31.5
T.P.	713	37.5 140.93		3.98	1335.0
+80			5.1		35.6
148			5.6		35.3
+87			4.2		36.7
+42	A	L	7.7		36.2
+90			9.9		31.0

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71

BRUSA	271	32.1
	<u>20</u>	<u>20</u>
"	252	30.7
	<u>25</u>	<u>20</u>
"	289	30.6
	<u>10</u>	<u>6</u>
"		level
"		level
"		level
"		level
"	262	28.9
	<u>25</u>	<u>25</u>
"	279	33.3
	<u>20</u>	<u>21</u>
"		level
"		level
"	28.7	32.8
	<u>20</u>	<u>20</u>
"	29.4	32.2
	<u>23</u>	<u>20</u>
"		level
"		level
"		level
"		level
"	27.9	level
	<u>20</u>	
"	27.7	27.6
	<u>15</u>	<u>20</u>
"		level
"		level
"	27.8	level
	<u>20</u>	
"	30.1	level
	<u>20</u>	
"	35.1	28.9
	<u>20</u>	<u>20</u>
Top 147+54		
BRUSA		
"	40.1	33.1
	<u>23</u>	<u>20</u>
"		level
"		level
"	38.7	33.8
	<u>20</u>	<u>15</u>

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L 4 R

Sta	BS	HI	Rod	FS	ELY
		14093			
149			9.6		31.3
+35			7.8		33.1
150			8.7		32.2
+20			8.7		32.0
+65			14.0		26.9
151			12.3		28.6
+50			14.5		26.9
152			12.8		28.1
+20			12.9		28.0
+30			9.7		31.2
153			8.6		32.3
T.P.	435	²³² 138.61		467	134.6
+25			5.3		34.3
154			7.4		31.2
+35			7.5		31.1
+60			4.7		33.9
155			3.7		34.9
156			10.0		28.6
+30			12.3		26.1
T.P.	0.48	¹¹¹⁷ 127.44		11.65	126.96
B.M.				3.52	123.92
157			16.2		17.2
+90			13.8		13.6
158			14.0		13.4

Brush & Stumps	27.7	34.3
"	²⁵ 29.9	²⁵ 101.00
"	²⁵ 29.8	²⁵ 31.2 28.2
"	²⁵ 30.8	²⁵ 28.0
"	²⁰ 28.7	²⁰ 25.1
"	²⁰ 101.00	²⁰ 24.6
"	¹⁵ 28.1	¹⁵ 25.2
"	²⁰ 31.1	¹⁵ 25.2
"	²⁵ 32.2	³⁰ 26.8
"	²⁰	²⁰
"	²⁶ 32.1	²⁰ 30.5
Top 153		
B.M. 53	35.9	33.1
"	¹⁵	²⁰
"	level	
"	level	
"	33.0	level
"	²⁰	
"	level	
"	29.6	28.2
"	²⁰	¹⁵
"	25.1	27.9
"	²⁰	²³
B.M. jack in burned pine stumps of 156 & 55		
Brush	level	
"	level	
"	level	

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Sta	B.S.	H.I.	Rod	F.S.	Elev
		127.44			
158+34			11.8		12.6
159			13.8		13.6
T.P.	178	^{10.17} 117.27		119.5	115.99
+40			2.4		11.9
160			5.2		12.1
+60			4.1		11.2
161			5.1		12.2
162			8.8		08.5
+30			9.8		07.5
+60			7.6		09.7
163			8.9		08.9
+20			8.3		09.0
+60			3.7		13.6
164			3.5		13.8
T.P.	1059	^{8.69} 125.96		190	115.37
+50			12.3		13.7
165			4.2		21.8
+30	Δ R		1.6		24.9
T.P.	190	^{10.2} 126.98		0.88	125.08
+70			7.4		22.6
+95			10.6		16.9
166			10.1		16.9
+90			13.1		13.9
167			16.7		10.3

L & R

culvert	level	
	level	
Top 159		
Brush	level	
"	level	
"	level	
"	130	10.8
	20	25
"	level	
" Culvert	level	
"	level	
"	level	11.5
"	level	20
"	level	12.4
		20
"	10.6	15.9
	15	7.5
"	10.9	15.8
	20	8
		20
T.P. top 164		
Brush & rock	18.4	4.8
	20	15
	18.3	level
	25	
	23.2	level
	20	
RP on Rock at sta 16+35		
Brush	23.2	20.9
	20	20
	18.3	11.8
	20	1.8
	18.3	14.8
	20	20
"	17.0	13.1
	20	20
"	12.3	level
	20	

Sta	BS	HI	Rod	Fs	Elev.
		12698			
168			158		11.2
+30			13.9		13.1
+81	Δ P		12.1		14.9
TP	1075	¹⁶² 12860		913	117.85
169			14.0		14.6
+40			16.4		12.0
170			16.8		11.8
+30			16.0		12.6
171			8.5		20.1
+75			5.8		22.8
+92	Δ P		5.0		23.6
172			9.9		23.7
173			1.4		27.2
TP	580	⁵²⁹ 13389		0.51	12809
173+30			5.9		28.0
+85			7.9		26.0
174			6.6		27.3
+07	Δ L		9.9		29.0
175			6.1		27.8
176			2.6		31.3
TP	1130	¹⁰²⁹ 144.18		101	15288
+50			14.9		32.3
177			9.5		31.7
+60			7.9		36.3

Aug 31 1910

14

	L	R
Brush	1242	
"	1242	
"	$\frac{155}{15}$	$\frac{147}{15}$
Top 162481		
Brush	$\frac{132}{20}$	$\frac{151}{25}$
"	$\frac{14.6}{20}$	$\frac{13.2}{20}$
"	1242	
"	1242	
"	$\frac{213}{20}$	1242
"	$\frac{225}{15}$	$\frac{247}{15}$
"	1242	$\frac{244}{20}$
"	1242	$\frac{254}{20}$
"	1242	$\frac{275}{15}$
TP on small stalks near 173		
Brush	$\frac{267}{15}$	$\frac{289}{15}$
"	$\frac{24.8}{15}$	$\frac{260}{15}$
"	$\frac{24.0}{25}$	$\frac{24.0}{15}$
"	$\frac{24.2}{20}$	1242
"	$\frac{261}{26}$	$\frac{246}{15}$
"	$\frac{302}{15}$	$\frac{325}{15}$
Top 174		
Brush	1242	$\frac{325}{15}$
"	1242	$\frac{329}{20}$
"	1242	$\frac{372}{15}$

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Sta	B.S.	HT	Rod	FS	Elcy
		144.18			
178			45		39.7
+06	D R		49		39.3
+33			95		39.7
+80			5.4		38.6
179			6.9		37.4
+50			1.6		42.6
180			6.4		37.8
+30			6.6		37.6
181			7.6		36.6
+60			3.2		41.0
182			4.7		39.5
T.P.	129	276 141.72		405	140.13
+70			6.2		35.2
183			9.5		31.9
+13	D R		10.3		31.1
T.P.	382	461 136.81		213	132.99
+60			5.2		31.9
184			8.8		28.0
+60			7.0		29.8
185			8.7		28.1
+50			9.8		27.0
186			10.9		25.9
+45			7.1		29.7
187			5.4		31.4

	L	R
Brush	$\frac{335}{20}$	$\frac{423}{25}$
"	$\frac{325}{25}$	$\frac{423}{25}$
"	$\frac{329}{15}$	$\frac{362}{20}$
"	$\frac{348}{15}$	$\frac{378}{15}$
"	$\frac{388}{15}$	level
"	$\frac{416}{15}$	$\frac{394}{20}$
"	level	level
"	level	$\frac{344}{12}$ 338 25
"	$\frac{396}{15}$	$\frac{313}{15}$
"	level	level
"	level	$\frac{327}{15}$
Stake near 182		
Brush	level	level
	level	level
	level	level
Top 123413	level	level
Brush	$\frac{308}{15}$	$\frac{306}{15}$
"	level	$\frac{292}{15}$
"	$\frac{310}{25}$	$\frac{353}{15}$
"	$\frac{287}{15}$	level
"	level	level
"	level	$\frac{27.4}{15}$
"	level	level
"	level	level

STA	BS	HI	Rad	F	Elev
		13681			
187+80			6.8		30.0
188			4.9		31.9
+190			3.0		133.8
199			4.7		32.4
+20			6.4		30.4
T.P.	242	⁹³⁶ 127.45		11.98	127.83
196			7.6		19.9
191			6.7		20.8
192			7.6		19.9
+177	B L		7.2		20.3
B.M.				4.88	122.57
143			6.4		21.1
144			7.4		22.9
195			2.7		29.8
196			3.6		23.9
T.P.	6.11	¹³² 131.77		20.9	125.34
+30			8.7		23.1
+60			6.6		25.2
197			5.8		26.0
+85			3.0		28.8
197+33	D R		3.2		28.6
+85			1.7		27.1
198			5.8		26.0
+40			11.7		20.1

Aug 31 1945

L & R

Brush	$\frac{312}{15}$	level
"	$\frac{35.9}{15}$	$\frac{28.9}{15}$
"	$\frac{33.4}{15}$	$\frac{30.0}{15}$
"	$\frac{28.7}{15}$	$\frac{30.5}{15}$
"	$\frac{26.8}{15}$	$\frac{30.0}{5}$
"		$\frac{30.4}{15}$
"		$\frac{29.9}{20}$
"		level
"		level
"	level 17.7	level
"	level 12	level
"	level	$\frac{21.4}{20}$
B.M. on stump 26'R 192+77		
Brush		level
"		level
"	$\frac{24.3}{20}$	level
"	$\frac{23.7}{20}$	$\frac{24.2}{20}$
Top 194		
Brush	level	level
"		level
"	$\frac{35.2}{20}$	$\frac{24.5}{20}$
"	$\frac{25.5}{20}$	level
"	$\frac{25.8}{20}$	level
"	24.3	$\frac{24.1}{20}$
"	25	$\frac{23.8}{25}$
"	$\frac{21.2}{25}$	$\frac{20.7}{25}$
"	$\frac{16.0}{20}$	$\frac{20.7}{20}$

Aug. 31 1918 L & R

Sta	BS	HI	Rod.	FS	Elev.
		13177			
199			152		166
T35			141		177
TP	110	^{11 37} 12040		1297	11930
200			68		136
201			78		106
+20			86		118
+50	A R		80		124
+80			46		158
202			43		161
+60			38		166
203			65		139
+30			87		117
TP	748	^{5 32} 11503		1280	10760
204			90		061
+30			99		052
205			96		055
+50			97		053
+74	A R		47		103
206			61		090
+30			96		055
207			119		032
208			117		034
+10			110		071
209			86		085

Brush	level	level
"	$\frac{137}{20}$	$\frac{157}{20}$
"		
"	level	
"	$\frac{137}{20}$	level
"		
"	level	
"	$\frac{168}{20}$	$\frac{152}{5} \frac{12.7}{20}$
"	level	$\frac{23.0}{20}$
"		level
"	$\frac{149}{20}$	$\frac{137}{20}$
"		
Top 309	level	
Brush	level	level
" Culvert	level	
"	$\frac{14.7}{20}$	level
"		level
"		level
"		level
"		level
" Culvert	level	
"		
"	$\frac{036}{20}$	$\frac{02.6}{25}$
"		level
"		level

STA	BS	H.I.	ROD	F.S.	Elev
		106.71			
218			10.8		95.9
TP	533	⁵¹³ 101.61		10.44	96.28
219			4.1		97.5
+10			6.2		95.4
220			6.1		95.5
220+539	Marked	220+33	DL 7.4		97.2
221			6.3		95.3
TP	201	¹⁷¹ 103.32		0.30	101.31
221+50			9.3		94.0
+78	A L		1.7		01.6
222			2.1		01.2
+90			8.0		95.3
223			8.5		94.8
+66	A L		6.3		97.0
224			7.4		95.9
225			7.0		96.3
+60			2.7		00.6
226			3.2		00.1
TP	172	⁴¹ 102.41		2.63	100.69
227			4.4		98.0
+39	A A		5.4		96.8
+70			3.0		99.4
228			1.7		97.7
229			3.7		98.7

Sept. 1918
Raining

19

	I	R	
Brush		Level	
TP near 218 on small hub			
Brush	$\frac{100.95}{15}$	$\frac{98.8}{6}$	$\frac{03.0}{20}$
"	$\frac{98.7}{20}$	Level	
" From 20 to 21 = 100 level	$\frac{96.7}{20}$	Level	
"	5 feet	Level	
"		Level	
"		Level	Cedar Swamp
"		Level	
"	$\frac{96.5}{20}$	$\frac{03.8}{20}$	Level
"	$\frac{96.4}{20}$	$\frac{03.2}{15}$	Level Co. base
"			
"	$\frac{91.5}{20}$	$\frac{99.6}{20}$	
"	$\frac{97.0}{25}$	$\frac{00.8}{20}$	
"	92.9	99.7	$\frac{02.6}{27}$
"	$\frac{93.5}{40}$	$\frac{96.5}{20}$	
"	$\frac{95.6}{20}$	$\frac{03.4}{20}$	
"	$\frac{96.1}{20}$	$\frac{03.5}{20}$	
TP near 226 on small hub			
Brush	$\frac{95.0}{20}$	$\frac{100.0}{20}$	
"	$\frac{93.4}{20}$	$\frac{00.8}{20}$	
"	$\frac{98.7}{15}$	$\frac{01.7}{20}$	
"	$\frac{93.7}{15}$	$\frac{01.2}{20}$	
"	$\frac{96.5}{15}$	$\frac{100.9}{20}$	

STA	B.S.	H.I.	ROD	F.S.	Elev.
		102.41			
229+35			3.1		99.3
+80			2.8		99.6
230			4.1		98.3
+70			5.7		96.7
+80			5.0		97.4
231			8.1		94.3
TP	925	103.38		728	95.13
+10			10.8		90.6
730			9.8		94.6
760			10.9		92.5
232			13.8		90.6
+50			12.7		90.7
233			4.5		96.9
+25			4.0		99.4
+50			4.1		97.3
775			1.5		01.9
234			2.8		00.6
+20	A	N	5.1		98.3
B.M.				929	94.09
235			2.9		99.5
+30			4.1		99.3
236			5.1		98.3
237			7.2		96.2

Sept 11 1918
Rain 109

50

	L	R
Brush	$\frac{96.5}{20}$	$\frac{001.2}{20}$
"	level	
"	level	$\frac{99.8}{20}$
"	not needed	
"	level $\frac{97.6}{10}$	$\frac{00.8}{20}$
"	level $\frac{97.7}{5}$	$\frac{97.5}{20}$
"		
"	$\frac{92.7}{15}$	$\frac{90.5}{10}$
"	$\frac{92.7}{15}$	$\frac{98.5}{10}$
"	level	$\frac{98.5}{15}$ (2001)
"	level	
"	level	
"	$\frac{91.1}{20}$	$\frac{98.9}{20}$
"	$\frac{92.6}{25}$	$\frac{02.1}{20}$
"		
"	same slope as 234	
"	$\frac{94.1}{25}$	$\frac{04.0}{20}$
"	$\frac{94.6}{26}$ $\frac{96.2}{10}$	$\frac{02.5}{20}$
B.M. back in Pine Swamp	35' L	234+10
Brush	$\frac{94.7}{20}$	$\frac{04.3}{20}$
"	same slope as 234	
"	$\frac{96.4}{20}$	$\frac{01.9}{20}$
"	level	

sta	B.S.	H.I.	Rod	F.S.	Elev
		103.38	81		
+45			7.6		95.8
TP	675	103.21 ¹⁷		692	96.6
238			8.4		94.8
239			3.1		100.1
+16	A	L	1.9		101.3
TP	337	105.19 ¹⁹⁸		139	101.82
240			2.9		102.3
+60			2.7		102.5
241			5.2		100.0
241+08	End		5.8		99.4
BM.				694	98.25
+332	A	L	8.4		96.8
242			11.7		93.5
TP	145	96.59 ⁸⁶⁰		1255	94.64
+78			4.9		91.2
243			6.4		90.2
+30			6.1		90.5
+68			9.4		87.2
243+91	A	R	9.2		89.4
244			9.7		86.9

Sept 1, 1918. 51
 J.F. Tomasel. Level
 Earl. Cromett. Rod. Newman.
 L R

Brush	Level	
Top small hub on line	237+45.	
Brush	Level	95.8 ¹⁷⁵
"		92.7 ²⁰ 92.4 ²⁰
"		93.6 ²⁰ 93.8 ³⁰
TP near 239+16 on small hub,		
"		101.6 ²⁰ 101.0 ²⁰
"	Level	
"		94.2 ¹⁵ Level
"	Level	
BM back in 10' splice 20' L 241+08.		
in old road	Level	
" " "	Level	
"		
"	Level	
"	Level	
"	Level	
" Beginning of corduroy	Level	
on corduroy	Level	
" "	Level	
Approximately 1000' corduroy Elev 87.2		

Pine tree Road.

PIT. No 1

Sta
B.M. 100.00

00

+25

+65

+76

1+00

PIT. No 2

B.M. 100.00

1+00

0+88

0+75

0+50

0+25

0+00

Pine tree Road

Sept 14 1918

52

A.W.M.

J.F.P.

B.M. Tack in top of W Pine 15' R. 0+76

922.914 938.917 918.
12 9 3 1 0

937.993 949.933 935.
14 9 3 1 0

961.978 978.972 954 957.
18 11 6 3 1 0

967.976 975.960 960.
18 7 2 1 0

972.981 983.982 967 967.
20 12 8 3 1 0

B.M. R.R. spike on top 12" Tom Stump 20' L 1+10

L 98.1 R.

incl 98.3 100.0

98.0 98.7 99.7 98.3 98.7 98.3 99.1 100.0 99.3
26 14 9 5 0 6 7 12 24

98.7 99.3 100.0 99.6 98.5 99.2 98.8 100.2 100.0 99.8 98.7
27 15 10 6 5 0 6 7 12 17 28

99.0 99.6 100.0 100.2 99.0 99.8 99.0 100.1 100.0 99.6 99.7
25 17 11 7 6 8 6 7 12 15 28

98.8 99.5 99.6 100.1 100.2 100.1
18 8 0 6 18 26

PINE TREE Road

PIT No 3

BM.	100.00
1	
0+90	
0+82	
0+50	
0+35	
0+15	
00	

PIT No 4

BM.	100.00
1700	
+75	
+50	
+25	
00	

Sept 1918

53

L	±	R		
BM Tack in root of W Pine stump E'R stail +27				
978	982	998	982	971
25	19	13	9	7
971	968	979	100	979
25	5	6	11	17
971	99.7	99.4	97.6	96.7
25	20	13	8	7
980	977	991	98.6	96.5
28	20	12	8	7
954	961	97.5	970	955
28	20	12	7	6
941	946	958	95.5	94.5
25	20	12	8	7
927	928	933	934	956
15	7	0	6	12
902	923	925	942	957
0	6	7	18	28
X X X X				
BM Tack in W Pine 12' L 0794				
974	990	990	017	013
0	15	25	40	50
998	995	010	016	035
0	6	12	25	40
005	011	022	019	017
0	7	11	16	21
007	008	000	039	029
4	6	5	13	18
010	009	030	032	037
0	6	10	15	28
012	000	030	037	057
0	6	10	15	28

Rainy

PINE TREE ROAD

Pit No 5

BM 100.00

00

+20

+35

+50

+75

+100

Sept 14 1915

100.0

59

27
97.7 HI

L & R

BM RR spike top 12' W Pine 36' R 0+35

01.7 02.8 00.3 99.5 97.2 96.1
70 30 20 12 9 0

06.0 05.1 02.6 01.5 99.6 97.5
35 30 20 11 10 0

06.4 05.3 03.9 02.8 00.3 98.4
70 30 20 11 10 0

06.3 05.3 04.1 03.4 00.7 97.1
70 30 20 12 9 0

06.5 05.7 04.8 02.9 00.2
70 20 11 10 0

101.6 05.9 01.7 01.5
10 6 0

7/24/18 FEM
AUM

PETER'S ROAD

Beg. W 1/6 Cor. on South Line Sec. 33

T. 140 - R. 28

North 1320' to 1/6 Cor

" 930' on 1/6 Line

N 54° 30' W (Mag). 328⁵ Feet

N 43° W " 342⁵ "

S 63° W " 800 "

N 87° W " 288 " to waters

Edge - Wabeddo L.

Grade on Lat No 1 of State
Road No 8

Sta	Elev	Grade
51	102.0	
52	102.0	
53	105.0	0
54	105.0	0
55	103.0	4
56	103.00	0
57	106.00	9
58	106.00	0
59	102.00	4
60	100.50	15
61	102.0	0
62	102.0	0
63	101.0	9
64	99.0	18
65	96.0	27
66	94.5	36
67		
68		
69		
70		
+10 End	94.5	

KEITH'S RAILROAD CURVE TABLES.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle
of Intersection or I. P. = $23^{\circ} 20'$ to the R. at Station
542+72.

Ext. in Tab. IV opposite $23^{\circ} 20' = 120.87$
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20' = 1183.1$
 $1183.1 \div 10 = 118.31$.

Tab. V correction for A. $23^{\circ} 20'$ for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47 =$ corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 =$ L. C.

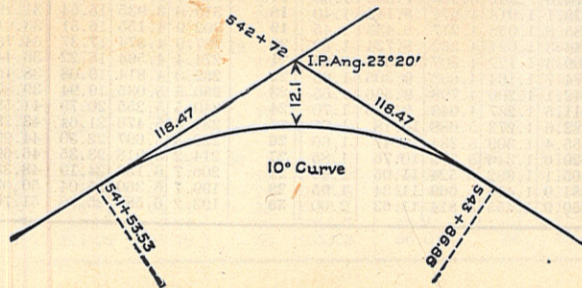
$2^{\circ} 19\frac{1}{2}' =$ def. for sta.	542	I. P. = sta.	542+72
$4^{\circ} 49\frac{1}{2}' =$ " " "	+50	Tan. =	1.18.47
$7^{\circ} 19\frac{1}{2}' =$ " " "	543	B. C. = sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' =$ " " "	+50	L. C. =	2.33.33
$11^{\circ} 40' =$ " " "	543+	E. C. = Sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$
 $2^{\circ} 19\frac{1}{2}'' =$ def. for sta. 542.

Def. for 50 ft. = $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft. = $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve.

(These tables are published in Field Books of
KEUFFEL & ESSER CO., New York, N. Y.)



A. LECHTERBERG

Wilson - 6
 \$450
 27.6
 700 AWST
 600

276 4. Clear - 225 - 690.00
 18.4 Grub 640.00
 1334.00

\$850 - for
 clear grub in Simpson Road
 7.15
 12.5
 19.30

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.