

Level Book 1

S. H. R. # 80

FIELD BOOK

360

24

✓ S. R. H. #80

B.M.	3.57	1003.57		1000.00
			3.0	1000.6
1			3.9	999.7
2			4.5	99.1
3			4.5	99.1
4			4.0	99.6
00			3.8	99.8

T.P. 5.20 1005.20 3.57 1000.00

1			5.8	999.4
2			6.3	98.9
3			8.2	97.0
+40			8.1	97.1
4			7.2	96.0
5			4.5	00.7
6			4.8	00.4
7			4.2	01.0
8			3.7	01.5
9			3.6	01.6

T.P. 5.10 1006.14 4.16 01.04

10			4.8	01.3
11			4.3	01.8
12			4.5	01.6
13			4.5	01.6
14			4.5	01.6
15			4.6	01.5

L.

R 10-30-14 11

Spike in Cor Fence P. 24' L of 00
Top of Rail N.P. Xing.

C.D. Ganzert
C.J. White
C.J. Bark

	97.0				97.0
	18				18
PIPE	95.5	95.9	97.1	97.1	95.4
	18	10	7	5	18
	98.7			98.4	97.1
	18			5	16
	01.1		01.3		00.7
	23		8		21

Very Sandy

S. R. H. # 80
1006.14

16				5.7	00.4
17				5.9	00.2
18				5.4	10 00.7
19				6.5	9 99.6
T.P.	6.85	1006.87	6.12		00.02
+53	S. End of Bridge			7.5	9 99.4
	Bottom of Pillager Cr.			12.6	9 4.3
	W. Level "			11.4	9 5.5
	High Water "			8.5	9 8.4
+77	N. End of Bridge			7.6	9 9.3
20				7.8	9 9.1
21				7.2	9 9.7
22				6.3	00.6
23				4.6	02.3
24				3.3	03.6
25				3.2	03.7
26				2.2	04.7
27				2.9	04.0
28				2.7	04.2
B.M.	4.55	09.50	1.92		04 9.5
29				5.6	03.9
30				5.2	04.3
31				5.4	04.1
32				6.2	03.3
33				4.7	04.8

L. R 10-30-14 2,

	00.9	99.8	00.8		00.6	99.6	01.3
	17	13	11		8.5	16	22
	99.2	98.4			00.2	99.1	00.9
	17	13			9	17.5	21
	99.7	98.6	00.4		00.6	98.5	99.7
	20	16	6		9	18	23
	97.2	96.7	99.4		99.2	97.1	97.7
	16	12	4		8	16	22
	97.6	95.8	95.8	99.4	99.3	96.5	96.5
	21	15	10	4	8.6	16	20
	Bottom of Creek						
	Water Level						
	High Water						
	95.0	95.0	99.3		99.3	97.6	96.7
	18	8.4	6		7	11	17
	95.0	95.0	99.3		99.3	97.6	96.7
	18	8.5	6		7	11	18
	96.5	98.0	98.1	99.7	99.7	98.2	98.1
	15	13	7	3.6	6.6	11.4	18
	98.0	99.6	00.4		00.6	98.5	98.9
	13.6	10	6		7	10	19
		01.3	00.5		00.6	00.6	02.3
		21	17		21	25	27
	Spike Tel Pole 30 R of 27+35						

S. R. H.

11

S. R. H. #80

100950

33+70			3.7	05.8
34			4.0	05.5
35			4.8	04.7
36			5.3	04.2
+32			4.8	04.7
37			4.6	04.9
+50			3.9	05.6
38			4.1	05.4
39			4.5	05.0
T.P.	7.70	13.09	4.11	05.39
40			7.2	05.9
41			7.5	05.6
42			8.3	04.8
+66			8.5	04.6
43			7.4	05.7
44			4.6	08.5
45			3.5	09.6
46			3.7	09.4
47			4.1	09.0
48			3.0	10.1
49			5.6	07.5
T.P.	6.13	14.48	4.74	08.35
+40			7.2	07.3
50			7.1	07.4
51			6.9	07.6

L

R

10-30-14

3

$\frac{0.23}{18}$	$\frac{0.33}{9}$	$\frac{0.41}{6}$	$\frac{0.41}{8}$	$\frac{0.27}{11}$	$\frac{0.27}{18}$	
(Pipe) $\frac{0.26}{18}$	$\frac{0.26}{12}$	$\frac{0.50}{6}$	$\frac{0.47}{10}$	$\frac{0.29}{14}$	$\frac{0.29}{18}$	
$\frac{0.48}{21}$	$\frac{0.39}{17}$	$\frac{0.48}{12}$	$\frac{0.51}{9}$	$\frac{0.37}{17}$	$\frac{0.55}{25}$	
$\frac{0.59}{22}$	$\frac{0.50}{16}$	$\frac{0.62}{9}$	$\frac{0.58}{8}$	$\frac{0.44}{17}$	$\frac{0.58}{24}$	
$\frac{0.55}{21}$	$\frac{0.46}{19}$	$\frac{0.46}{12}$	$\frac{0.58}{7}$	$\frac{0.58}{8}$	$\frac{0.46}{17}$	$\frac{0.58}{24}$

15" PIPE

$\frac{0.68}{19}$	$\frac{0.61}{12}$	$\frac{0.74}{6}$	$\frac{0.72}{6}$	$\frac{0.61}{10}$	$\frac{0.67}{18}$		
$\frac{0.64}{19}$	$\frac{0.57}{13}$	$\frac{0.72}{7.5}$	$\frac{0.76}{4}$	$\frac{0.59}{11}$	$\frac{0.57}{16}$	$\frac{0.65}{19}$	
$\frac{0.67}{17}$	$\frac{0.59}{15}$	$\frac{0.61}{11}$	$\frac{0.79}{5}$	$\frac{0.75}{6}$	$\frac{0.65}{9.5}$	$\frac{0.64}{17}$	$\frac{0.73}{20}$

Sandy

S. R. H. # 80

101483

74			46	10.2
75			5.0	09.8
76			5.1	09.7
77			5.2	09.6
78			4.8	10.0
79			4.4	10.4
T.P	4.77	15.64	3.96	10.87
B.M.			5.05	10.59
80			5.1	10.5
81			4.4	11.2
82			4.8	10.8
+64			4.9	10.7
+70			4.4	11.2
83			4.4	11.2
84			4.3	11.3
85			3.6	12.0
86			3.6	12.0
87			3.4	12.2
T.P	3.04	15.93	2.75	12.89
88			3.6	12.3
+30			3.7	12.2
+36			4.4	11.5
89			4.5	11.4
90			4.4	11.5
91			4.4	11.5

L

R

5
10-30-14

09.5	08.7	10.1	10.3	09.1	08.4	09.5	
16	13.6	8	3	6.6	7.1	12	
09.2	08.3	08.7	09.8	08.8	08.3	09.3	
11	7.6	12	2	5	8.6	10.6	
09.1	08.2	08.7	09.7	08.3	08.1	09.1	
18	17.5	12	2.6	6	9	11	
09.0	08.0	08.0	09.5	08.5	08.9		
17	7.6	7.4	4.5	7	14		
09.3	08.5	08.5	09.6	08.5	08.7	09.4	
19	17.8	14	5	10.6	12.4	13	
09.9	09.0	09.4	10.2	09.1	09.1	10.1	
19	17	11.5	4.5	9	11	12	
Spike Fence Post 30'L of 79+15							
10.2	09.2	09.6	10.5	10.6	09.8	09.3	10.0
15	13.5	10	17.6	3	6.4	9.5	10.5
11.0	09.8	10.3	11.0	11.2	10.0	11.0	
15.5	7.3	9.6	7	2.8	8.6	11	
10.5	09.7	10.8	10.9	10.2	09.7	10.6	
13.5	11.8	6.5	3	2	7.4	10.4	
10.4	09.1	10.7	10.9	09.6	10.5		
25	23	7	4	9	10.6		
10.2	08.3	09.0	11.0	11.0	09.4	10.3	
25.5	24.6	20	12.5	3	9	10	
10.2	08.3	09.0	11.3	10.7	09.8	10.8	
26	24.5	20	11	3.5	8.8	11	
10.2	08.3	09.0	11.6	10.9	10.3	10.3	
26.5	25	20	12	3.5	6	18	
11.0	08.6	08.7	12.2	10.6	11.5		
27.6	26	20	12	8	11		
11.0	08.6	08.7	12.1	11.8	10.2	11.0	
27.5	26	20	12	2	5	10.5	
11.0	08.5	08.7	12.1	12.0	10.2	10.8	
27.5	26	20	12	3.4	7.6	10.5	
11.4	08.5	09.1	12.1	12.1	10.4	11.2	11.2
27	26	18	10	2	6	10.6	15
11.3	08.3	09.4	12.1	12.1	10.7	10.4	11.1
25	22	18.5	10	3.6	7	11	12
11.2	10.7	11.7	11.7	11.5	10.4	10.5	11.2
25	25.6	10	10	5	7.8	11	12
11.2	10.5	10.5	11.7	11.5	10.5	11.0	
25	24.6	13.6	7	4	7.5	12	
10.7	09.4	09.4	11.4	11.5	10.3	10.2	10.8
24.5	22.6	19	16	4.8	6.8	10	11
11.0	09.3	09.8	11.8	11.7	10.0	10.1	10.8
23	22	15	10.8	3.5	9	11.8	13

Work done this year
needs crowning & widening on R. Side
Good Material
Hard pan & clay

S. R. H. # 80

1016.91

110				4.6	12.3
111				4.6	12.3
112				4.6	12.3
113				4.6	12.3
114				4.2	12.7
115				4.2	12.7
116				3.8	13.1
T.P.	5.31	18.54	3.68		13.23
117				5.6	12.9
118				5.2	13.3
119				4.5	14.0
120				2.8	15.7
B.M.				1.16	17.38
121				4.7	13.8
122				4.9	13.6
123				5.5	13.0
124				5.7	12.8
125				5.8	12.7
126				5.8	12.7
T.P.	4.51	17.55	5.50		13.04
127				4.5	13.1
128				4.4	13.2
129				4.7	12.9
130				4.6	13.0
131				4.3	13.3

L

R

7.
10-30-14

120	101	10-1	12.8	12.2	13.3	13.3	12.5	12.2
22	20	18.6	17	8.0	2	4	20	
121	11.7	10.6	10.4	11.4	13.1	14.0	14.3	13.2
25	24	22.5	20.7	17.6	13	7.5	6	9
			15.1	10.3	10.6	15.5		16.2
			26	23	22	14		18

Spike in J.P. Tree 12+35 35 R

13.0	102	10.3	11.6	13.8	13.8	13.1	13.0
24.5	22.5	21	19	7	6.5	7.5	20
			12.3	12.3	13.1	13.6	12.3
			19	7	7.5	7.5	9
							19

(sand)

S. R. H. #80

1017.55

132				3.9	13.7
133				0.8	16.8
T.P.	8.70	25.62	0.63		16.92
134				5.8	19.8
135				5.7	19.9
136				5.6	20.0
137				5.3	20.3
138				5.4	20.2
139				7.2	18.4
T.P.	4.02	19.71	9.93		15.69
140+04				4.2	15.5
141				4.6	15.1
142				4.8	14.9
B.M.				5.91	13.80
143				4.6	15.1
144				4.7	15.0
+30				6.2	13.5
				11.1	08.6

L

R

10-30-14

8

C.D.C.
C.J.W.
C.J.B.

				19.4		16.8		15.8
				20		11		20
				24.1	22.4	20.1	19.7	18.3
				22	11	5	5	10.6
				24.7	21.9	20.3	19.7	17.1
				26	9	6	4.0	17
				23.3			20.0	18.4
				23			7	16
				23.5				17.6
				19				16
				22.3	21.8			19.1
				22	13			16
				20.3	19.7	18.7		17.0
				15	6	4		16
				20.0	18.8	15.3	15.4	14.4
				21	12	9.6	13	17
				21.2	20.0	15.2	15.0	11.7
				24	18	12	9	15
				21.9	18.7	15.3	15.3	11.5
				27	22	14	10	14
								17
				Spike in W.P. Trace 15 R 142+85				
				21.9	19.9	14.5	14.7	11.4
				24	17	12	11	15.5
				21.4	18.0	14.4	14.9	11.9
				22	19	12.5	9	13.5
				22.9	18.7	13.2	12.7	11.1
				26.20	11.6	7	15	17
								20

(TP 405)

Water Level Pillager Lake 10/30-14

✓ S. R. H. #80

1021.55

187+50			0	21.9
T.R	5.48	22.10	4.93	16.62
188			5.5	16.6
189			5.0	17.1
190			4.9	17.2
191			4.4	17.7
T.P	4.47	22.27	4.30	17.80
192			5.1	17.2
193			4.3	18.0
+60			5.2	17.1
194			5.7	16.6
B.M.		3.22		1019.05

L.

R

10-31-14 12

$\frac{15.8}{21}$	$\frac{16.2}{85}$	$\frac{20.3}{6}$		$\frac{30.2}{25}$
$\frac{15.5}{16}$	$\frac{16.3}{12}$		$\frac{20.0}{3}$	$\frac{29.6}{28}$
$\frac{15.3}{20}$	$\frac{15.3}{9}$		$\frac{17.5}{11.5}$	$\frac{20.0}{15}$ $\frac{22.5}{22}$
$\frac{16.0}{18}$	$\frac{16.0}{6}$	$\frac{17.1}{4}$	$\frac{17.3}{9}$	$\frac{20.2}{12}$ $\frac{24.2}{23}$
$\frac{16.0}{18}$	$\frac{16.8}{6.5}$		$\frac{17.8}{9.0}$	$\frac{20.3}{13.5}$ $\frac{24.7}{24}$
$\frac{16.2}{16}$	$\frac{16.2}{4.5}$		$\frac{17.7}{14}$	$\frac{21.1}{18}$ $\frac{22.6}{22}$
$\frac{15.0}{20}$	$\frac{16.1}{15}$	$\frac{17.9}{9}$	$\frac{18.0}{8.5}$	$\frac{20.7}{11}$ $\frac{23.9}{22}$

(Sandy)

Swamp

Spike in Poplar Tree 35' L of 194

S. R. H. # 80

B.M.	848	1027.53		1019.05
194+56			91	18.7
195			53	22.2
+56			37	23.8
196			66	20.9
+10			86	18.9
+62			85	19.0
197			77	19.8
+47			73	20.2
198			73	20.2
T.P.	10.89	32.65	5.77	21.76
199			11.0	21.7
200			10.8	21.9
+60			85	24.2
201			88	23.9
202			11.5	21.2
203			13.8	18.9
T.P.	2.73	24.96	10.42	22.23
204		25.00	6.4	18.6
205			6.7	18.3
B.M.			9.96	1015.00
+65			7.6	17.4
+65			5.7	19.3
206			5.5	19.5
207			4.9	20.1

L.

R

11-2-14

13.

Spike in Poplar Tree 35' L 194

	$\frac{18.6}{25}$			$\frac{18.8}{19}$
	$\frac{191}{24}$	$\frac{189}{8}$	$\frac{219}{3}$	$\frac{25.4}{22}$
	$\frac{197}{20}$	$\frac{191}{95}$	$\frac{217}{9}$	$\frac{27.5}{20}$
$\frac{147}{23}$	$\frac{16.4}{16.5}$	$\frac{18.5}{17}$	$\frac{18.8}{2}$	$\frac{26.7}{22}$
$\frac{14.8}{20}$	$\frac{15.4}{17}$	$\frac{19.0}{12}$		$\frac{21.2}{9}$
	$\frac{18.2}{17}$	$\frac{20.0}{12}$	$\frac{20.3}{2}$	$\frac{22.4}{18}$
		$\frac{17.9}{20}$	$\frac{19.0}{14.5}$	$\frac{19.7}{3}$
				$\frac{25.8}{12}$
				$\frac{26.8}{22}$
	$\frac{17.2}{19}$	$\frac{18.4}{13}$	$\frac{19.5}{11}$	$\frac{19.6}{7}$
				$\frac{21.7}{11}$
				$\frac{23.3}{23}$
				$\frac{19.1}{4}$
				$\frac{19.9}{18}$
	$\frac{19.0}{17.5}$	$\frac{21.5}{5}$		$\frac{22.0}{10}$
	$\frac{18.5}{21}$	$\frac{20.3}{5}$		$\frac{21.4}{14}$
				$\frac{22.8}{16.5}$
				$\frac{22.8}{24}$
	$\frac{17.5}{20}$	$\frac{20.5}{9.5}$	$\frac{23.9}{2}$	$\frac{22.4}{10}$
	$\frac{18.3}{19}$	$\frac{19.9}{10}$	$\frac{23.6}{5}$	$\frac{21.9}{13}$
	$\frac{15.3}{19}$	$\frac{16.6}{14}$	$\frac{20.7}{9.5}$	$\frac{21.4}{23}$
		$\frac{13.6}{20}$	$\frac{16.1}{12.5}$	$\frac{24.1}{7}$
				$\frac{24.9}{12}$
				$\frac{24.9}{23}$
				$\frac{23.9}{9.5}$
				$\frac{26.7}{9}$
				$\frac{28.1}{27}$
				$\frac{21.5}{3.5}$
				$\frac{25.8}{8.5}$
				$\frac{30.7}{21}$
				$\frac{19.1}{5}$
				$\frac{22.8}{8}$
				$\frac{30.2}{24}$
	$\frac{12.4}{17}$	$\frac{14.0}{12.5}$	$\frac{18.4}{3.5}$	$\frac{18.8}{8}$
	$\frac{12.8}{22}$	$\frac{14.5}{12}$	$\frac{18.1}{5.5}$	$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$
				$\frac{18.8}{8}$
				$\frac{21.4}{10}$
				$\frac{25.2}{24}$
				$\frac{18.3}{6.5}$
				$\frac{20.3}{7}$
				$\frac{24.6}{23}$

S. R. H. # 80

✓ T.P	0.87	1057.49	45.59	6.77	44.72
222+50				0.9	44.7
23				3.7	41.9
224				8.4	37.2
225				11.5	34.1
226				12.0	33.6
T.P	0.27	34.59	11.27		34.32
+ 424	P.C.			1.8	32.8
227				5.2	29.4
228				9.8	24.8
229				12.1	22.5
T.P	4.94	27.93	11.60		22.99
+50				6.4	21.5
+55				8.9	19.0
Water Level				8.0	19.9
+65				6.4	21.5
+85				5.5	22.4
230				5.2	22.5
+50				4.8	23.1
231				6.8	21.1
+50				4.1	23.8
232				2.5	25.4
+50				0.1	27.8
T.P	12.01	39.56	0.38		27.55
233				8.5	31.4

L

R

11-2-14¹⁵

	$\frac{441}{23}$		$\frac{441}{23}$
	$\frac{448}{22}$		$\frac{432}{24}$
	$\frac{383}{18}$		$\frac{390}{20}$
	$\frac{343}{21}$		$\frac{338}{20}$
	$\frac{354}{19}$	$\frac{344}{11}$	$\frac{331}{8}$
	$\frac{333}{21}$	$\frac{315}{115}$	$\frac{324}{95}$
	$\frac{292}{20}$	$\frac{276}{145}$	$\frac{289}{115}$
	$\frac{262}{21}$	$\frac{259}{35}$	$\frac{252}{55}$
			$\frac{241}{15}$
			$\frac{25.5}{3}$
			$\frac{25.3}{16}$
			$\frac{24.6}{23}$
			$\frac{337}{18}$
			$\frac{334}{23}$
			$\frac{304}{20}$
			$\frac{25.5}{3}$
			$\frac{25.3}{16}$
			$\frac{24.6}{23}$
			$\frac{21.1}{2}$
			$\frac{21.1}{18}$
			$\frac{20.5}{18}$
			$\frac{23.1}{22}$
			$\frac{23.9}{11}$
			$\frac{24.8}{75}$
			$\frac{24.8}{15}$
			$\frac{27.5}{5}$
			$\frac{268}{7}$
			$\frac{27.4}{13}$
			$\frac{27.8}{24}$
			$\frac{30.2}{6.5}$
			$\frac{32.8}{13.5}$
			$\frac{32.8}{20}$
			$\frac{31.6}{28}$
			$\frac{31.7}{3}$

Bottom of Big Spring Cr.

= High Water

SANDY

	S	R	H	#80
✓				
	1039.56			
B.M.				1.98 37.58
233+40				5.1 34.5
234				2.3 37.3
235				0.3 39.3
T.P.	9.33	48.80	0.09	39.47
236				5.5 43.3
237				5.1 43.7
238				5.9 42.9
239				9.0 39.8
240				8.8 40.0
+70				6.1 42.7
241				6.2 42.6
242				8.9 39.9
243				4.3 44.5
T.P.	13.01	57.85	3.96	44.84
+60				9.2 48.7
244				8.8 49.1
245				6.2 51.7
246				3.3 54.6
+25				4.1 53.8
247				1.1 56.8
248				1.1 56.8
T.P.	8.85	65.99	0.71	57.14
249				9.1 56.9
250				6.8 59.2

Li R. 11-2-14¹⁶

Spike in J.P. Tree 35' R 200+40

33.7	35.1	35.5	34.1	35.6	35.6
<u>24</u>	<u>17</u>	<u>4</u>	<u>6</u>	<u>10</u>	<u>20</u>
	36.0		38.1		
	<u>19</u>		<u>20</u>		
	37.1		39.6	41.5	
	<u>19</u>		<u>10</u>	<u>23</u>	
	41.7			44.3	
	<u>17</u>			<u>20</u>	
	42.8		44.1		
	<u>18</u>		<u>20</u>		
	41.0		45.4		
	<u>19</u>		<u>26</u>		
	37.6		42.3		
	<u>21</u>		<u>27</u>		
	41.2	39.9	42.1		
	<u>23</u>	<u>9</u>	<u>28</u>		
	41.7		42.9		
	<u>19</u>		<u>20</u>		
	43.1		40.6		
	<u>21</u>		<u>20</u>		
	41.5		39.9	39.1	
	<u>22</u>		<u>115</u>	<u>21</u>	
	44.3		44.9		
	<u>19</u>		<u>23</u>		
	49.0		48.5	47.9	
	<u>19</u>		<u>3.5</u>	<u>22</u>	
	50.4		48.9		
	<u>18</u>		<u>20</u>		
	52.6		52.5		
	<u>23</u>		<u>19</u>		
	57.2		52.1		
	<u>24</u>		<u>19</u>		
	56.2		52.3		
	<u>22</u>		<u>21</u>		

(K.P. 5)

✓ S. R. H #80
1065.99

251				48	61.2
252				45	61.5
B.M.				1.33	64.66
+80				5.2	60.6
253				6.7	59.3
254				12.8	53.2
T.P.	12.88	66.25	12.62		53.37
+40				14.9	56.4
+75				14.9	51.4
255				13.2	53.1
+65				8.6	57.7
256				9.6	56.7
+50				10.2	56.1
257				7.6	58.7
T.P.	11.50	77.13	0.62		65.63
258				10.9	66.2
+30				9.8	67.3
259				10.5	66.6
260				8.5	68.6
261				2.7	74.4
T.P.	11.70	87.82	1.01		76.12
262				7.9	79.9
263				5.6	82.2
264				1.3	86.5
+50				0.0	87.8

△ R. 11-2-17

Spike N.P. Tree 35' R 252+15

56.6
20
53.5
18
56.0
19

58.4
21
57.9
21
57.3
24

64.1
20
65.0
19
65.1
19
66.1
20

67.6
20
69.1
21
69.4
22
70.1
23

71.6 73.6 74.7
22 7 5

74.8 76.1 78.5
3 7 25

76.7 80.3
23 2
78.3
22
82.8
22
84.7
23

80.4 81.8 84.0
5 9 23
82.7 84.0 87.1
8 10 25
86.7 88.0 91.1
8.5 10 27
91.3
26

S. R. H

S. R. H. # 80

1087.82

265				1.9	85.9
T.P.	2.18	86.58	3.42		84.40
266				5.2	81.4
267				10.1	76.5
+50				10.7	75.9
T.P.	11.65	88.75	9.48		77.10
268				12.5	76.3
269				8.5	80.3
270				3.1	85.7
T.P.	10.51	1098.76	0.50		88.25
B.M.				6.28	92.48
+60				9.3	89.5
271				8.3	90.5
+35				7.1	91.7
272				4.8	94.0
T.P.	12.92	1111.02	0.66		98.10
273				10.6	1100.4
274				4.1	06.9
275				1.0	10.0
T.P.	7.32	1118.17	0.17		1110.85
276				5.8	12.4
277				4.7	13.5
278				2.8	15.4
B.M.			167		16.50

L

R

11-2-14 18

$\frac{83.0}{22}$	$\frac{85.9}{8}$	$\frac{86.9}{10}$	$\frac{89.5}{28}$
$\frac{78.4}{23}$	$\frac{81.9}{12}$	$\frac{83.5}{14}$	$\frac{85.1}{27}$
$\frac{74.7}{19}$	$\frac{77.5}{5}$	$\frac{77.7}{14}$	$\frac{78.8}{12}$
$\frac{74.6}{19}$	$\frac{76.8}{11}$	$\frac{78.7}{27}$	$\frac{80.2}{28}$
$\frac{76.3}{20}$	$\frac{77.3}{15}$	$\frac{79.6}{30}$	
$\frac{80.4}{23}$	$\frac{83.4}{23}$	$\frac{85.0}{13}$	$\frac{86.6}{24}$
$\frac{86.3}{22}$			
Spike in J.P. Tree 30'R 270+60			
$\frac{89.6}{21}$	$\frac{88.9}{2}$	$\frac{87.8}{9}$	$\frac{89.4}{23}$
$\frac{94.0}{19}$	$\frac{92.1}{14}$	$\frac{91.2}{7.5}$	$\frac{89.7}{20}$
$\frac{93.8}{23}$		$\frac{92.1}{20}$	
$\frac{94.0}{23}$		$\frac{94.0}{22}$	
$\frac{01.0}{18}$		$\frac{00.8}{20}$	
$\frac{07.9}{24}$		$\frac{06.9}{20}$	
$\frac{10.6}{24}$	$\frac{10.6}{3}$	$\frac{10.0}{2}$	$\frac{10.0}{22}$
$\frac{12.6}{22}$		$\frac{12.7}{22}$	
$\frac{13.7}{20}$	$\frac{15.4}{6}$	$\frac{14.8}{4}$	$\frac{14.3}{22}$
Spike in small J.P. Stump 277+90 35'R			

Very Sandy

12

S. R. H. # 80

B.M.	12.60	1129.10		1116.50
279			92	19.9
280			48	24.3
+35			30	26.1
281			05	28.6
T.P.	12.82	41.67	0.25	28.85
282			82	33.5
283			20	39.7
T.P.	12.78	53.80	0.65	41.02
284	Ext.		11.2	42.6
285			7.4	46.4
286			5.0	48.8
287			4.0	49.8
288			3.9	49.9
289			3.7	50.1
290			5.3	48.5
T.P.		3.33		50.47

L.

R

11-3-14 19

Spike in small J.P. Stump 277790 35' R

285	277	25.3
23	135	10
30.6	30.2	26.2
26	175	11
29.0		
19		

24.6	25.8	25.8
85	11	23
26.1	27.6	27.6
7	11	21
28.6	27.3	26.8
3	7	18

34.0	33.2
22	11
40.1	39.3
17	5
	4

31.9
19
38.3
20

44.1	43.3	42.6
18	3	2
46.5	45.5	46.5
16	13	8.5
		6.5

43.2	42.5
6	21
45.6	
20	

48.4
17

49.2
17

1265

S. R.H. 80

T.P	5.06	1158.53		1150.47
291			5.4	50.1
292			3.4	52.1
293			5.3	50.2
294			8.5	47.0
+25			9.0	46.5
295			7.1	48.4
296			3.2	52.3
297			2.6	52.9
T.P	5.55	58.77	2.31	53.22
298			4.8	54.0
+85			2.7	56.1
299			3.0	55.8
B.M			2.98	55.79
300			4.8	54.0
301			5.3	53.5
302			5.5	53.3
303			3.8	55.0
304			2.7	56.1
T.P	0.81	56.96	2.62	56.15
305			3.4	53.6
306			8.1	48.9
+70			9.9	47.1
307			9.8	47.2
308			9.3	47.7

L

R

20

11-5-14

C.D.G.
C.J.W.
E.W.B.
C.J.B.

12" Pipe.

Spike in J.P. Tree 35' L of 299

54.8	54.4	54.8	54.4	55.1
13.5	12	7	11.5	14
56.1	55.5	56.1	55.5	55.5
13	11.5	8	16.5	11
53.9	52.8	53.6	53.1	54.8
15	13	7	8.5	24
48.0	47.5	48.8	48.8	49.1
14	10	5.5	4	27
46.4	45.8	47.0	47.2	47.0
14	13.5	6	7	12
47.2	46.6	47.7	46.9	47.3
16	10	8	4	13.5

✓ S. R. H. #80
1156.96

309 ✓			6.1	50.9
T.P.	12.57	63.72	5.81	51.15
310 ✓			11.2	52.5
311 ✓			6.5	57.2
B.M.			6.96	56.76
T.P.	11.73	75.26	0.19	63.53
312			10.8	64.5
313			2.7	72.9
T.P.	12.05	1186.43	0.88	74.38
314			5.4	81.0
T.P.	11.54	1197.26	0.71	85.72
315			9.5	87.8
316			4.8	92.5
+50			3.3	94.0
317			1.6	95.7
T.P.	12.24	1209.46	0.04	97.22
318			11.2	98.3
319			8.0	1201.5
320			4.3	05.2
T.P.	12.42	1221.14	0.74	1208.72
321			10.5	10.6
+45			8.9	12.2
322			5.4	15.7
323			2.0	19.1
+70			6.1	15.0

L. R. 11-5-14 21

$\frac{51.6}{16}$	$\frac{49.7}{12}$	$\frac{49.7}{12}$	$\frac{50.9}{6}$	$\frac{50.5}{4}$	$\frac{49.4}{9}$	$\frac{49.4}{11}$	$\frac{49.9}{12.5}$
$\frac{52.3}{20}$	$\frac{51.1}{12}$	$\frac{52.5}{6}$	$\frac{52.3}{3.5}$	$\frac{51.7}{5.5}$	$\frac{51.2}{20}$	$\frac{56.7}{8}$	$\frac{56.3}{11.5}$
$\frac{55.0}{18}$	$\frac{55.0}{12}$	$\frac{51.1}{6}$					
$\frac{64.7}{24}$	$\frac{64.0}{15}$	$\frac{63.4}{12.5}$	$\frac{64.6}{6}$	$\frac{64.4}{7}$	$\frac{63.4}{10.5}$	$\frac{64.3}{12}$	$\frac{65.8}{27}$
	$\frac{71.4}{16}$	$\frac{71.4}{10.5}$	$\frac{72.9}{6.5}$	$\frac{72.9}{5}$	$\frac{71.8}{8.5}$	$\frac{71.8}{11}$	$\frac{72.6}{12.5}$
	$\frac{81.1}{23}$			$\frac{81.0}{5}$	$\frac{80.3}{10}$	$\frac{81.8}{13.5}$	$\frac{82.9}{29}$
$\frac{88.8}{24}$	$\frac{89.6}{14}$	$\frac{87.2}{11}$	$\frac{87.8}{7.5}$	$\frac{88.0}{5}$	$\frac{87.3}{8.5}$	$\frac{90.6}{13.5}$	$\frac{90.6}{18}$
	$\frac{93.9}{16}$	$\frac{91.7}{12.5}$	$\frac{92.5}{7}$	$\frac{92.5}{3.5}$	$\frac{91.6}{7}$	$\frac{92.4}{9.5}$	$\frac{91.1}{24}$
	$\frac{92.8}{16}$	$\frac{92.8}{8.5}$	$\frac{94.0}{5}$	$\frac{94.0}{5}$	$\frac{92.6}{10}$	$\frac{92.6}{16}$	
	$\frac{94.0}{16}$	$\frac{94.5}{10}$	$\frac{95.5}{4.5}$	$\frac{95.7}{6.5}$	$\frac{95.1}{9.5}$	$\frac{97.2}{12}$	$\frac{98.3}{28}$
	$\frac{96.9}{16}$	$\frac{96.9}{11.5}$	$\frac{98.3}{5}$	$\frac{98.3}{5.5}$	$\frac{97.7}{9.5}$	$\frac{99.3}{11.5}$	$\frac{01.8}{2.5}$
	$\frac{00.6}{18}$	$\frac{00.6}{15}$	$\frac{00.2}{12.5}$	$\frac{01.5}{4}$	$\frac{01.5}{5.5}$	$\frac{00.6}{9}$	$\frac{02.1}{11}$
	$\frac{02.6}{19}$	$\frac{03.7}{12}$	$\frac{05.0}{6}$	$\frac{05.2}{3.5}$	$\frac{04.5}{6}$	$\frac{04.5}{8.5}$	$\frac{05.9}{11}$
	$\frac{11.3}{18}$	$\frac{09.3}{12.5}$	$\frac{10.7}{6}$	$\frac{10.6}{4}$	$\frac{09.6}{9}$	$\frac{10.3}{12}$	$\frac{10.3}{18}$
		$\frac{11.5}{26}$	$\frac{10.9}{10}$	$\frac{12.2}{5}$	$\frac{12.2}{3.5}$	$\frac{10.7}{7}$	$\frac{10.9}{11.5}$
	$\frac{15.9}{18}$	$\frac{15.9}{14}$	$\frac{15.0}{10.5}$	$\frac{15.7}{7}$	$\frac{15.7}{5.5}$	$\frac{14.8}{18}$	$\frac{15.7}{18}$
		$\frac{19.1}{14}$	$\frac{20.1}{10.5}$	$\frac{18.7}{7}$	$\frac{19.1}{5.5}$	$\frac{18.3}{12}$	$\frac{18.3}{18}$
	$\frac{15.2}{18}$	$\frac{25}{15}$	$\frac{14.6}{13}$	$\frac{15.6}{8}$	$\frac{15.0}{2.5}$	$\frac{12.6}{9}$	$\frac{12.6}{18}$

S. R. H # 80

12.21.14

324			69	14.2
T.P.	8.48	23.07	6.55	14.59
325			8.7	14.4
+70			5.3	17.8
326			4.8	18.3
+70			6.1	17.0
327			8.2	14.9
+25			10.0	13.1
T.P.	4.62	16.96	10.73	12.34
+71			4.6	12.4
328			3.5	13.5
+35			3.4	13.6
329			6.2	10.8
+85			8.1	08.9
330			9.3	07.7
+25			11.2	05.8
+70			12.3	04.7
T.P.	0.18	1205.00	12.14	1204.82
331			2.2	02.8
B.M.			6.25	1198.75
332			8.1	96.9
333			10.9	94.1
334			8.7	96.3
T.P.	0.47	1197.00	8.47	1196.53
+75			2.6	94.4

L. R.

11-5-14 22

	14.3	14.5	14.2	12.4	11.5	(12" Pipe)
	26	7	2	9	20	
16.3	13.8	14.6	14.4	12.4	12.4	
25	12	55	35	85	18	
18.5	19.5	17.5	17.5	19.6	18.1	
26	13	10	6	10	23	
19.5	19.5	17.9	17.7	18.2	16.2	
19	13	10	7	9	22	
21.1	13.8	17.1	17.4	15.5	15.5	
24	13	10	8	19	19	
	18.2	16.6	14.9	13.9	13.9	
	26	13	11	18	18	
	14.0	12.9	12.1	12.1	12.1	
	23	13.5	4	18	18	
	14.6	12.2		11.6	13.9	
	26	13.5		15	28	
15.0	15.0	13.8		12.1	12.1	
18	14	11.5		22	22	
	12.4	10.9	10.1	10.5	10.5	
	26	13	11	12.5	20	
11.0	11.0	09.0	08.6	06.2	06.2	
19	13	9.5	10	22	22	
09.4	09.4	08.0	07.6	05.2	05.2	
19	13	11	6	21	21	
07.1	05.9	05.9	05.6	04.0	04.0	
25	9.5	9.5	4	8	20	
06.1	06.1	04.6		02.2	02.2	
19	12.5	10		21	21	
05.5	04.0	03.1		99.7	99.7	
29	13.5	12		19	19	
Spike in Oak Tree 2019 331+35						
00.3	99.0	97.4	96.9	93.2	93.2	
20	12	10.5	5	21	21	
97.8	95.3	94.2	94.1	91.4	89.1	(12" Pipe)
24	12	11.5	4	11	23	
01.4	99.9	96.8	95.4	93.8	93.8	
24	14	11	13.5	27	27	
99.5	98.0	94.6	94.5	92.3	92.3	
27	14	11	12.5	25	25	

S. R. H. #80

1197.00

335			4.6	92.4
T.P.	0.36	85.91	11.45	85.55
336			2.8	83.1
+30			5.9	80.0
337			10.5	75.4
T.P.	0.61	74.17	12.35	73.56
338			8.6	65.6
T.P.	0.19	61.54	12.82	61.35
339			3.0	58.5
B.M.		3.42		1158.12

L.

R

11-5-14 23

$\frac{97.1}{26}$	$\frac{95.8}{14.5}$	$\frac{92.9}{11}$	$\frac{91.8}{13}$	$\frac{90.0}{28}$
	$\frac{84.5}{25}$		$\frac{83.3}{9}$	$\frac{82.2}{13.5}$
$\frac{78.8}{23}$	$\frac{78.1}{11}$	$\frac{80.0}{6.5}$	$\frac{80.0}{10}$	$\frac{77.3}{17}$
$\frac{78.8}{22}$	$\frac{76.4}{11}$	$\frac{75.6}{10}$	$\frac{75.4}{22}$	$\frac{77.3}{27}$
	$\frac{67.5}{18}$	$\frac{64.5}{6.5}$	$\frac{65.5}{8}$	$\frac{63.7}{14}$
	$\frac{58.0}{18}$	$\frac{58.0}{5}$	$\frac{58.5}{16}$	$\frac{57.6}{24}$

Spike in Poplar Tree 339+25 23L

S. R. H 80

B.M.	0.75	1158.87		1158.12
339+70			4.3	54.6
340			6.8	52.1
+30			10.1	48.8
341			12.6	46.3
T.P.	2.39	49.04	12.22	46.65
342			5.8	43.2
+50			5.5	43.5
343			7.1	41.9
344			9.1	39.9
+75			6.0	43.0
345			4.7	44.3
T.P.	763	55.79	0.88	48.16
+45			10.9	44.9
346			7.5	48.3
+65			2.6	53.2
347			4.6	51.2
+30			6.8	49.0
+60			13.3	42.5
T.P.	0.38	43.20	12.97	42.82
348			4.5	38.7
349			7.9	35.3
350			9.8	33.4
351			6.1	37.1
+50			4.9	38.3

L.

R.

11-9-14 24

C.D.C.
C.V.W.
C.V.B.
E.W.B.

Spike in Poplar Tree 339+25 23'L

55.0	53.8	54.6	54.4	54.2	54.7
8	6	3	12	15	16
52.0	52.0	51.5	52.2	52.3	52.3
18	7	6	65	125	15
48.9	47.2	46.0	46.0	43.6	
22	85	7	8	125	
44.8	43.8	42.8	43.2	41.5	40.9
22	65	5	9	13	22
45.0	43.9	42.9	43.0	41.5	40.5
20	75	75	7	14	26
	45.3	43.6	40.7	40.0	39.3
	22	7	15	165	24
	41.0	39.2	39.4	38.4	38.0
	25	35	10	13	20
49.4	47.0	43.9	43.0	43.3	42.7
30	9	5	35	4	11
49.2	47.6	44.8	44.0	43.0	40.5
25	105	65	65	115	20
	49.0	45.7	44.6	41.3	39.3
	31	125	4	95	20
51.7	49.5	48.0	47.8	44.7	
28	115	85	8	18	
56.8	56.0	53.5	53.0	55.8	54.6
28	85	4	15	19	53
	56.0	56.2	51.0	51.7	51.4
	25	10	25	4.5	16
	49.5		49.0	48.5	49.2
	22		8	11	30
	42.5		42.5	45.1	45.1
	20		85	16	27
	38.7		39.2	41.2	41.2
	20		14	20	25
	32.4			36.6	
	27			20	
	33.4		33.9	34.7	34.7
	20		95	14	22
	37.1		36.6	36.7	
	22		7	16	
	39.7	39.4	38.2	37.2	
	21	3	15	22	

S. R. H #80

1143.20

T.P.	10.33	48.40	5.13	38.07
352			10.6	37.8
+30			10.0	38.4
+90			4.2	44.2
353			4.2	44.2
+45			6.1	42.3
354			8.3	40.1
B.M.			10.33	38.07
355			10.7	37.7
+65			8.7	39.7
356			10.7	37.7
T.P.	0.34	38.50	10.24	38.16
+50			0.0	38.5
357			3.3	35.2
358			11.0	27.5
T.P.	2.28	29.25	11.53	26.97
359			6.1	23.2
+50			7.6	21.7
360			6.3	23.0
+45			4.3	25.0
361			5.1	24.2
+6.5			5.5	23.8
362			9.7	19.6
T.P.	1.72	18.30	12.67	16.58
+65			6.7	11.6

L

R

25

11-9-14

	$\frac{37.7}{20}$	$\frac{37.7}{3}$	$\frac{38.8}{15}$	$\frac{38.6}{12}$	$\frac{36.3}{20}$
	$\frac{46.4}{24}$	$\frac{45.9}{6}$	$\frac{44.2}{4}$	$\frac{43.8}{10.5}$	$\frac{43.4}{14}$
	$\frac{42.3}{20}$		$\frac{42.3}{13}$	$\frac{43.5}{13.5}$	$\frac{43.3}{20}$
	$\frac{38.3}{24}$	$\frac{39.3}{11}$	$\frac{38.8}{10}$	$\frac{39.7}{7}$	
	$\frac{36.6}{20}$	$\frac{36.6}{9.5}$	$\frac{37.8}{7}$	$\frac{37.7}{3}$	$\frac{37.5}{20}$
	$\frac{40.3}{20}$	$\frac{40.3}{15}$	$\frac{39.0}{13}$	$\frac{39.7}{5}$	$\frac{41.0}{7}$
		$\frac{34.8}{18}$	$\frac{37.4}{10.5}$	$\frac{37.7}{6}$	$\frac{39.7}{22}$
	$\frac{36.9}{29}$	$\frac{38.5}{14}$	$\frac{37.9}{12.5}$	$\frac{38.5}{10}$	$\frac{40.2}{35}$
		$\frac{32.7}{25}$	$\frac{34.7}{16}$	$\frac{37.4}{3}$	$\frac{38.7}{23}$
		$\frac{28.2}{18}$	$\frac{28.2}{6}$	$\frac{27.5}{18}$	
		$\frac{23.2}{18}$		$\frac{22.1}{3}$	$\frac{22.1}{6}$
	$\frac{17.9}{24}$	$\frac{19.9}{11}$	$\frac{21.6}{8}$	$\frac{21.6}{4}$	$\frac{20.5}{7}$
	$\frac{23.6}{18}$	$\frac{23.6}{10}$	$\frac{23.0}{9}$	$\frac{23.0}{5.5}$	$\frac{24.2}{7}$
	$\frac{25.0}{18}$	$\frac{25.0}{11}$	$\frac{24.2}{7}$	$\frac{25.0}{5}$	$\frac{26.4}{7}$
		$\frac{24.9}{19}$	$\frac{24.2}{9.5}$	$\frac{24.2}{20}$	
	$\frac{21.6}{21}$	$\frac{21.2}{11}$	$\frac{22.5}{10}$		$\frac{24.9}{20}$
	$\frac{17.7}{18}$	$\frac{17.2}{17}$	$\frac{18.3}{9.5}$	$\frac{18.3}{1.5}$	$\frac{21.8}{22}$
			$\frac{10.3}{19}$	$\frac{11.4}{11}$	$\frac{11.2}{4}$
					$\frac{14.7}{21}$

S. R. H #80

111830

363			78	10.5
364			10.4	07.9
365			9.0	09.3
366			2.1	16.2
T.P.	0.63	11.79	7.14	11.16
367			3.9	07.9
+55			6.7	05.1
368			10.0	1101.8
+35			12.4	1099.4
369			10.7	01.1
370			11.6	00.2
T.P.	0.34	1101.05	11.08	1100.71
+40			5.8	95.3
371			9.0	92.1
372			12.9	88.2
B.M.			82.4	1092.81
T.P.	0.78	1088.96	12.87	1088.18
+65			1.7	87.3
373			3.9	85.1
+30			5.6	83.4
374			11.9	77.1
T.P.	0.12	76.75	12.33	76.63
375			7.4	69.4
+50			11.1	65.7
376			12.4	64.4

L.

R.

26

11-9-14

	$\frac{04.7}{21}$	$\frac{06.8}{3}$	$\frac{07.9}{14}$	$\frac{09.6}{17}$	$\frac{10.6}{24}$
	$\frac{05.5}{22}$	$\frac{07.0}{13}$	$\frac{09.1}{45}$	$\frac{11.8}{11.5}$	$\frac{14.6}{29}$
	$\frac{13.2}{20}$	$\frac{13.5}{95}$	$\frac{14.6}{8.5}$	$\frac{17.8}{24}$	
	$\frac{04.6}{22}$	$\frac{06.2}{9}$	$\frac{10.2}{6}$	$\frac{11.3}{14}$	$\frac{13.1}{22}$
	$\frac{01.6}{21}$	$\frac{05.1}{5}$	$\frac{05.1}{5}$	$\frac{07.3}{7.5}$	$\frac{10.0}{24}$
	$\frac{97.3}{21}$	$\frac{96.0}{20}$	$\frac{02.6}{3.5}$	$\frac{02.6}{11}$	$\frac{04.1}{13}$
	$\frac{97.9}{21}$	$\frac{97.9}{21}$	$\frac{01.2}{9.5}$	$\frac{01.2}{19}$	$\frac{06.1}{24}$
	$\frac{00.8}{19}$	$\frac{02.9}{16}$	$\frac{02.9}{16}$	$\frac{02.9}{16}$	$\frac{02.9}{16}$
	$\frac{97.2}{20}$	$\frac{98.4}{10.5}$	$\frac{98.4}{10.5}$	$\frac{98.7}{13}$	$\frac{98.7}{18}$
	$\frac{97.2}{20}$	$\frac{95.3}{18}$	$\frac{95.3}{18}$	$\frac{95.3}{18}$	$\frac{95.3}{18}$
	$\frac{91.0}{22}$	$\frac{87.8}{11}$	$\frac{88.2}{5}$	$\frac{87.2}{7.5}$	$\frac{88.2}{17}$
	Sate 17 Poplar Tree			$\frac{372+10}{10}$	$\frac{30}{1}$
	$\frac{86.7}{10}$	$\frac{86.7}{10}$	$\frac{86.9}{7}$	$\frac{86.7}{10}$	$\frac{89.6}{12.5}$
	$\frac{87.1}{20}$	$\frac{86.3}{11.5}$	$\frac{84.6}{10}$	$\frac{85.0}{16}$	$\frac{90.9}{26}$
	$\frac{76.8}{17}$	$\frac{83.4}{18}$	$\frac{83.4}{10}$	$\frac{84.0}{10.5}$	$\frac{76.0}{12.5}$
	$\frac{67.7}{19}$	$\frac{69.1}{16.5}$	$\frac{77.1}{7}$	$\frac{76.0}{10}$	$\frac{77.3}{15}$
	$\frac{63.6}{16}$	$\frac{65.5}{12}$	$\frac{76.8}{17}$	$\frac{68.6}{12.5}$	$\frac{66.3}{21}$
	$\frac{63.6}{13}$	$\frac{64.4}{6.5}$	$\frac{63.6}{16}$	$\frac{65.5}{6}$	$\frac{63.6}{8}$
				$\frac{63.6}{11}$	$\frac{63.6}{20}$

Dare Gravel (stand)

S. R. H. #80

1076.75

376+65				11.6	65.2
377				95	67.3
T.P.	520	72.79	9.16		67.59
+50				5.2	67.6
378				61	66.7
+63				4.0	68.8
379				4.9	67.9
+60				77	65.1
380				85	64.3
381				84	64.4
382				69	65.9
T.P.	.759	74.03	6.35		66.44
383				6.7	67.3
B.M.				883	65.20
+70				5.0	69.0
384				5.3	68.7
+60				5.5	68.5
385				5.4	68.6
+30				5.4	68.6
386				6.3	67.7
T.P.	6.81	74.52	6.32		67.71
+65				7.2	67.3
387				7.5	67.0
388				8.1	66.4
+50				8.0	66.5

L.

R

27

11-9-14

$\frac{63.6}{18}$	$\frac{64.1}{4}$	$\frac{65.2}{2}$	$\frac{65.2}{9}$	$\frac{64.4}{22}$
	$\frac{63.6}{23}$		$\frac{67.6}{175}$	
$\frac{68.4}{23}$	$\frac{68.4}{85}$	$\frac{67.4}{7}$	$\frac{67.6}{105}$	$\frac{66.9}{21}$
	$\frac{66.0}{20}$	$\frac{68.5}{13}$	$\frac{66.5}{11}$	$\frac{65.4}{15}$
$\frac{70.2}{20}$	$\frac{70.2}{15}$	$\frac{67.6}{145}$	$\frac{68.8}{20}$	$\frac{71.0}{19}$
$\frac{69.3}{20}$	$\frac{69.3}{155}$	$\frac{67.6}{145}$	$\frac{67.3}{20}$	$\frac{68.7}{24}$
$\frac{63.1}{19}$	$\frac{63.8}{12}$	$\frac{64.9}{8}$	$\frac{63.4}{7}$	
	$\frac{63.3}{11.5}$	$\frac{64.1}{8.5}$	$\frac{64.2}{3}$	$\frac{63.4}{6}$
	$\frac{63.0}{7.5}$	$\frac{63.7}{5}$	$\frac{64.0}{5}$	$\frac{63.5}{6.5}$
$\frac{63.0}{16}$	$\frac{64.8}{9}$		$\frac{65.8}{9}$	$\frac{64.1}{17}$
			$\frac{65.6}{19}$	
$\frac{63.7}{20}$	$\frac{65.0}{11}$	$\frac{66.5}{9}$	$\frac{67.3}{10}$	$\frac{66.5}{16}$
			$\frac{66.3}{20}$	$\frac{70.3}{24}$
Spike in Poplar 383+15 20'L				
$\frac{64.2}{19.5}$	$\frac{65.8}{12}$	$\frac{68.0}{8}$	$\frac{69.3}{10}$	$\frac{68.6}{12}$
	$\frac{64.0}{22}$	$\frac{65.0}{13.5}$	$\frac{68.5}{13.5}$	$\frac{68.6}{16}$
		$\frac{68.0}{6}$	$\frac{69.2}{9}$	$\frac{72.2}{23.5}$
	$\frac{64.1}{15}$	$\frac{67.6}{9}$	$\frac{68.5}{8}$	$\frac{68.5}{17.5}$
			$\frac{68.1}{2.7}$	$\frac{74.2}{26.0}$
$\frac{64.1}{24}$	$\frac{66.3}{13.5}$	$\frac{67.8}{10}$	$\frac{67.7}{16.5}$	$\frac{68.1}{2.7}$
$\frac{64.1}{23}$	$\frac{66.4}{14.5}$	$\frac{68.5}{7.5}$	$\frac{67.7}{13}$	$\frac{67.7}{15.5}$
			$\frac{67.9}{11}$	$\frac{73.1}{21.5}$
$\frac{64.0}{18}$		$\frac{67.0}{11}$	$\frac{68.6}{6.5}$	$\frac{74.2}{20}$
			$\frac{67.9}{11}$	
	$\frac{64.1}{17}$	$\frac{66.9}{10}$	$\frac{66.3}{6.5}$	$\frac{67.0}{8.5}$
	$\frac{64.1}{16}$	$\frac{66.5}{9}$	$\frac{67.1}{3}$	$\frac{67.0}{18}$
	$\frac{63.5}{8.5}$	$\frac{66.4}{1.5}$	$\frac{65.9}{7.5}$	$\frac{65.9}{10}$
			$\frac{70.9}{14}$	$\frac{72.6}{26}$
			$\frac{67.0}{5}$	$\frac{67.0}{12}$
			$\frac{65.7}{10}$	$\frac{65.7}{12}$
			$\frac{65.7}{10.5}$	$\frac{69.3}{16.5}$
			$\frac{66.4}{10.5}$	$\frac{70.7}{21}$
			$\frac{64.7}{18}$	
			$\frac{65.7}{20}$	

✓ S. R. H. #80
1074.52

389				5.9	68.6
+32				4.7	69.8
+66				4.1	70.4
390				4.3	70.2
391				4.6	69.9
392				5.0	69.5
393				5.0	69.5
394				4.9	69.6
T.P.	3.28	73.10	4.70		69.82
395				3.1	70.0
396				4.8	68.3
+70				6.9	66.2
397				7.1	66.0
398				7.3	65.8
+70				7.3	65.8
T.P.	5.71	71.92	6.89		66.21
399				6.1	65.8
400				5.2	66.7
401				5.0	66.9
402				4.8	67.1
B.M.				6.25	65.67
Water Level Rock Lake				9.7	62.2
403				4.4	67.5
404				3.7	68.2
+60				4.7	67.2

L. R. 11-9-14 28

65.0	68.0	68.6	67.1	72.8
13	6.8	7	12	19
66.6	69.0	69.8	69.3	77.6
20	9.5	6.5	9.5	12
68.8	70.1	69.1	69.1	75.2
15	8	11	13	21
69.1	68.7	70.2	69.0	69.0
21	14	7.5	13	16
67.6	68.5	70.1	68.8	68.8
14	10.5	5	9	14
70.5	68.1	68.1	69.3	69.4
20	17.5	16	10.5	7
69.6	68.1	69.1	68.9	66.9
17	14	10.5	10	17
68.0	65.9	65.9	67.7	65.1
16.5	14	12	7.5	17
64.5	64.1	65.8	66.1	64.4
27	19.5	13.5	4	9.5
62.8	65.5	65.8	66.5	64.8
12.5	6.5	11	14	17.5
62.6	65.3	65.7	68.4	72.3
15.5	10.5	4.5	8	24
62.6	65.8	65.6	67.8	69.6
19	10.5	3.5	7	22
65.0	66.0	66.1	66.1	66.1
16	11	10	20	20
65.3	65.3	66.7	67.0	67.0
16	10.5	5	16	16
65.7	67.2	67.2	67.2	67.2
16	6.5	16	16	16
Spike in N.P. Tree 30' L 402				
66.5	66.5	67.2	67.2	64.4
16	12.5	8.5	4.5	16
64.0	65.3	68.7	65.3	64.4
21	8	11	19	16
64.1	65.7	67.8	65.2	64.4
14.5	6	10	14	16

S. R. H #80

1071.92

405				6.5	65.4
T.P.	10.62	75.74	6.80		65.12
+40				11.3	64.4
406				11.3	64.54
407				8.4	67.3
408				6.4	69.3
+70				3.7	72.0
409				3.6	72.1
410				7.8	67.9
T.P.	7.05	1075.41	7.38		68.36
411				8.7	66.7
412				7.8	67.6
413				8.0	67.4
414				2.5	72.9
T.P.	10.85	85.20	1.06		74.35
415				8.7	76.5
416				5.4	79.8
417				3.4	81.8
418				4.0	81.2
419				7.4	77.8
420				8.4	76.8
421				8.7	76.5
422				11.3	73.9
423				13.0	72.2
T.P.	0.07	72.71	12.56		72.64

L

R

11-9-14

29

$\frac{64.6}{76}$ $\frac{64.6}{8}$ $\frac{65.5}{6}$

$\frac{66.1}{9}$ $\frac{64.4}{13.5}$

$\frac{64.5}{15}$ $\frac{65.2}{13}$ $\frac{65.2}{9}$

$\frac{64.5}{20}$

$\frac{68.2}{22}$

$\frac{66.5}{18}$

$\frac{70.9}{21}$

$\frac{68.1}{20}$

$\frac{72.8}{22}$

$\frac{71.0}{20}$

$\frac{73.3}{23}$

$\frac{70.7}{21}$

$\frac{70.4}{22}$ $\frac{69.0}{9.5}$ $\frac{67.5}{6.5}$

$\frac{67.7}{11}$

$\frac{67.0}{14}$ $\frac{66.0}{22}$

$\frac{69.9}{22}$ $\frac{68.3}{8.5}$ $\frac{65.9}{5.5}$

$\frac{66.7}{8}$ $\frac{65.1}{16}$ $\frac{65.1}{20}$

$\frac{69.7}{21}$ $\frac{67.1}{17}$ $\frac{67.9}{13}$

$\frac{65.6}{5}$ $\frac{65.1}{10}$

$\frac{69.6}{20}$ $\frac{69.2}{13.5}$ $\frac{67.0}{11}$ $\frac{67.5}{7.5}$

$\frac{67.5}{6}$ $\frac{64.9}{12.5}$ $\frac{64.9}{18}$

$\frac{75.4}{17}$ $\frac{74.6}{10}$ $\frac{72.2}{6}$

$\frac{72.8}{12}$ $\frac{71.4}{17}$

S. R. H #80

1072.71

424			2.1	70.6
425			3.7	69.0
426			3.8	68.9
427			4.3	68.4
428			7.0	65.7
+52			7.4	65.3
+60			9.2	63.5
+68			7.4	65.3
429			7.2	65.5
+70			6.7	66.0
430			6.4	66.3
431			6.0	66.7
432			4.8	67.9
T.P.	3.70	72.04	4.37	68.34
433			4.5	67.5
434			5.2	66.8
435			5.7	66.3
436			4.6	67.4
437			5.5	66.5
B.M.			4.97	67.07
438			9.5	62.5
+10			10.0	62.0
439			6.5	65.5
440			2.7	69.3
441			0.7	71.3
T.P.	3.11	74.69	0.46	71.58

L

R

30

11-9-14

640	652
85	65
640	652
85	65
643	654
85	55
654	661
70	55

650	634
6	75
650	634
6	75
654	643
5	8
652	650
8	14

Spike in Cor. Fence Post 33 R 435+85

S.R.H #80

107469

442			2.4	72.3
443			3.3	71.4
444			6.3	68.4
445			9.6	65.1
+50			10.4	64.3
446			9.1	65.6
447			6.1	68.6
T.P.	3.48	72.46	5.71	68.98
448			2.1	70.4
449			2.9	69.6
450			4.6	67.9
451			6.1	66.4
452			7.4	65.1
453			8.8	63.7
454			7.7	64.8
T.P.	2.91	67.96	7.41	65.05
455			1.9	66.1
456			3.7	64.3
457			6.0	62.0
458			6.9	61.1
+33			6.8	61.2
+35			7.8	60.2
+38			6.7	61.3
459			5.9	62.1
460			2.9	65.1

11-9-14

31

✓
C.R.D.

S. R. H. #80

1067.96

461				43	63.7
+247				3.6	64.4
B.M.	3.82	69.08	2.70		65.26
462				3.3	65.8
+50				5.0	64.1
463				4.3	64.5
464				3.8	65.3
465				6.6	62.5
+35				7.8	61.3
466				6.7	62.4
+25				6.4	62.7
+60				7.8	61.3
467				7.5	61.6
+75				3.6	65.5
468				4.0	65.1
T.P.	3.64	69.27	3.45		65.63
B.M.			2.79		66.48

✓

11-9-14 32

1/4 Cor. Cor. Bet Sec 9 & 10 134-30
Spike in Fence Cor Post 33' R of 1/4 Cor.

12" Pipe

12" Pipe

Spike in N. Pine Tree 35' R 467 + 80

✓ S. R. H #80

T.P.	0.32	1066.80		1066.48
469			2.5	64.3
470			4.6	62.2
471			6.8	60.0
+50			7.6	59.2
472			6.8	60.0
473			7.8	59.0
474			7.9	58.9
+70			7.9	58.9
T.P.	0.0	1059.25	7.55	58.25
475			1.1	58.2
476			2.2	57.1
477			3.4	55.9
478			4.6	54.7
+70			5.4	53.9
+72			5.1	54.2
479			5.0	54.3
480			5.0	54.3
481			5.4	53.9
482			5.4	53.9
T.P.	4.00	57.95	5.30	53.95
483			4.4	53.6
484			4.5	53.5
485			4.7	53.3
486			4.6	53.4

L.

R 11-11-14 33

C.D.C.
C.J.W.
C.V.B.

12" Pipe

$\frac{52.1}{55}$ $\frac{53.3}{2.5}$

$\frac{53.0}{6}$ $\frac{52.1}{8.0}$

S. R. H #80

1051.95

487			4.9	53.1
+63 ⁴	= 00		4.7	53.3
B.M.			5.05	1051.90
T.P.	4.93	54.47	4.41	53.54
T.P.	12.52	70.50	0.49	51.98
T.P.	12.62	81.39	0.73	69.77
T.P.	112.4	1093.59	0.0.4	82.35
T.P.	3.60	85.66	11.53	82.06
T.P.	7.55	87.90	5.31	80.35
T.P.	9.88	89.23	8.55	79.35
T.P.	5.57	85.27	9.53	79.70
B.M.			2.97	82.30
B.M.			4.52	1080.75

B.M.	2.22	1062.44		1060.22
648+12 ⁴			3.7	58.7
+35			4.3	58.1
649			5.1	57.3
650			4.7	57.7
651			4.5	57.9
652			4.2	58.2
653			4.5	57.9
654			4.5	57.9

11-11-14

34

(old B.M. = 1051.90)

Spike Cor Fence Post 75' N.E. of 487+63⁴

From Sta 487+63⁴ to 648+12⁴
Road is completed.

(old B.M. = 81.30)

= Old B.M. Elev 100.00 35' R of Sea Cor

Spike in Fence Post 35' R " " "

(old B.M. = 1079.75)

= Old B.M. Elev. 77.92

Sec. Cor

53.3	52.7	53.3	56.9	57.6	56.2	56.3
16	13	10.5	6	9.5	11	2.8
54.4	53.1	54.3	55.8	56.7	55.0	55.6
15	13.5	11.5	5	8.5	12	2.4
54.8	53.6	53.6	55.0	56.4	55.6	54.5
16.5	16	11	11	9.5	9	11

56.0	54.2	54.2	55.9	57.0	57.0	56.2	55.5
16.5	16	12	11	6	7	10	11

Sample 51

↓

S. R. H # 80

T.P.	6.19	64.49	4.14	58.30
655			6.3	58.2
656			6.2	58.3
657			5.7	58.8
+50			4.5	60.0
658			4.5	60.0
+50			5.3	59.2
659			5.0	59.5
660			4.6	59.9
+60			4.0	60.5
661			2.1	62.4
T.P.	10.77	74.04	1.22	63.27
+40			10.1	63.9
+45			9.9	64.1
662			8.8	65.2
663			6.1	67.9
664			4.5	69.5
+25			5.0	69.0
665			8.5	65.5
666			9.5	64.5
667			9.3	64.7
+40			8.3	65.7
668			5.7	68.9
T.P.	11.25	81.82	3.47	70.57
669			7.4	74.4
	2921		88.3	

L

R

11-11-14

35

	$\frac{61.2}{27}$	$\frac{61.2}{15}$	$\frac{62.2}{9.5}$	$\frac{61.4}{15}$	$\frac{59.9}{17}$
	$\frac{66.0}{27}$	$\frac{63.7}{23}$	$\frac{63.3}{16.5}$	$\frac{63.7}{13}$	$\frac{60.9}{14}$
		$\frac{66.9}{28}$	$\frac{66.0}{18.5}$	$\frac{64.1}{12}$	"
			$\frac{67.5}{22}$	$\frac{65.0}{10.5}$	$\frac{61.0}{23}$
			$\frac{68.4}{25}$		$\frac{64.1}{19}$
			$\frac{69.3}{23}$	$\frac{65.9}{7}$	$\frac{65.0}{20}$
	$\frac{68.4}{24}$	$\frac{66.8}{14}$	$\frac{65.4}{11}$	$\frac{63.5}{5}$	$\frac{62.1}{15}$
	$\frac{63.4}{21}$	$\frac{62.8}{17}$	$\frac{63.6}{12}$	$\frac{61.9}{9.5}$	$\frac{61.9}{18}$
		$\frac{63.7}{17}$		$\frac{63.1}{16}$	
	$\frac{64.7}{16}$	$\frac{64.1}{15}$	$\frac{64.1}{11.5}$	$\frac{64.7}{10.5}$	$\frac{63.7}{8.5}$
(washout)	$\frac{67.9}{20}$	$\frac{64.9}{15.5}$	$\frac{68.1}{11}$	$\frac{67.8}{9.5}$	$\frac{67.8}{16}$
	$\frac{73.5}{17}$	$\frac{67.8}{16}$	$\frac{67.8}{13}$	$\frac{73.4}{9}$	$\frac{72.7}{10}$
					$\frac{71.7}{13}$
					$\frac{72.5}{16}$

✓ S. R. H #80

1080.82

670				5.9	75.9
671				6.6	75.2
672				6.5	75.3
673				6.0	75.8
674				3.0	78.8
T.P.	10.89	90.43	1.28		80.54
675				7.8	83.6
676				5.6	85.8
B.M.				3.91	1087.52
677				4.8	86.6
678				4.5	85.9
679				5.0	86.4
680				6.3	85.1
681				7.5	83.9
T.P.	4.5	88.11	7.87		83.56
682				5.2	82.9
683				5.5	82.6
684				5.6	82.5
685				4.7	83.4
686				4.5	83.6
687				4.0	84.1
688				2.6	85.5
450				1.3	86.8
689				2.4	85.7
690				3.1	85.0
T.P.	3.52	88.82	2.81		85.30

L

R

$\frac{73.9}{18}$	$\frac{69.3}{14}$	$\frac{74.3}{95}$	$\frac{94.9}{7}$	$\frac{73.5}{14}$	$\frac{74.0}{15.5}$
$\frac{73.9}{20}$	$\frac{72.4}{18}$	$\frac{72.4}{13}$	$\frac{74.0}{10}$	$\frac{74.0}{105}$	$\frac{72.8}{13}$
$\frac{73.9}{21}$	$\frac{73.0}{18.5}$	$\frac{73.0}{13}$	$\frac{73.9}{7.5}$	$\frac{73.6}{16}$	$\frac{73.7}{15}$
Same as Ref 72					
(Old B.M. = 108652) - Spike in Gate Post 35' of 676+70					
$\frac{81.2}{20}$	$\frac{79.0}{17.5}$	$\frac{79.8}{14.5}$	$\frac{81.4}{15}$	$\frac{81.8}{8}$	$\frac{81.2}{7.5}$
					$\frac{80.3}{11}$
					$\frac{81.1}{13.5}$
$\frac{83.5}{24}$					$\frac{83.4}{7}$
$\frac{83.6}{20}$	$\frac{83.6}{14}$	$\frac{84.7}{9}$			$\frac{80.6}{10.5}$
					$\frac{81.3}{14}$
					$\frac{80.6}{13.5}$
					$\frac{83.1}{18.5}$
					$\frac{83.7}{18}$

✓ S. R. H #80

1088.82

690+35			2.8	86.0
691			4.9	83.9
692			4.6	84.2
693			4.2	84.6
694			2.6	85.2
695			1.1	87.7
T.P.	1249	1000.74	0.57	88.25
696			10.7	89.0
697			7.9	91.8
698			4.9	94.8
699			2.5	97.2
700			0	0.02
T.P.	1113	1110.67	0.20	1000.54
701			7.2	04.5
+613		Sec. Cor.	5.0	06.7
702			4.8	1105.9
B.M.			5.26	1106.41
703			3.2	08.5
704			0.0	10.7
T.P.	1229	1123.43	0.53	1110.14
705			9.5	13.9
706			7.4	16.0
707			3.7	19.7
708			1.3	22.1
T.P.	3.55	26.46	0.52	22.91
	3946		-1.82	

L

R

11-11-14

37

84.6	82.5	82.5	84.7
27	21	17.5	12.5
	16	8.8	5.5

84.4	81.5	81.5	84.2
5.5	9.5	12.5	16.5
82.8	81.7	81.7	81.5
4.5	8	13.5	16

→ (old B.M. = 1105.41)
Spike in Poplar Tree 30' R. of 702

S. R. H #80

1126.46

709			3.2	23.3
710			2.4	24.1
711			3.4	23.1
712			5.6	20.9
713			8.0	18.5
714			11.2	15.3
715			12.6	13.9
T.P.	9.28	23.28	12.46	14.00
716			9.5	13.8
717			9.7	13.6
718			7.6	15.7
719			5.3	18.0
720			5.4	17.9
+60			4.7	18.6
721			1.3	22.0
T.P.	8.00	29.62	1.66	21.62
722			6.0	23.6
723			4.8	24.8
724			5.0	24.6
+35			3.5	26.1
T.P.	11.13	40.67	0.08	29.54
725			8.9	34.8
726			5.3	35.4
727			4.8	35.9
B.M.			1.96	1137.71

11-11-14

38

$\frac{19.3}{17}$ $\frac{18.3}{14}$ $\frac{20.2}{10}$

$\frac{21.1}{5}$ $\frac{18.5}{2.5}$ $\frac{21.0}{15.5}$

$\frac{20.4}{14.5}$ $\frac{19.9}{12}$ $\frac{22.3}{4}$
 $\frac{22.4}{18}$ $\frac{21.7}{16}$ $\frac{21.7}{13.5}$ $\frac{23.5}{9.5}$
 $\frac{23.1}{20}$ $\frac{22.3}{19}$ $\frac{22.3}{16}$ $\frac{23.6}{8.5}$

$\frac{23.1}{7.5}$ $\frac{21.3}{11.5}$ $\frac{21.3}{14.5}$ $\frac{24.3}{18.5}$
 $\frac{23.6}{3.5}$ $\frac{22.4}{6}$ $\frac{22.0}{20}$
 $\frac{23.6}{1.0}$ $\frac{22.3}{6}$ $\frac{22.3}{20}$

← (old B.M. = 1137.71)

Spike in Burn 4 Stump 50' L 727

S. R. H #80
1140.67

728			4.1	35.6
729			4.0	35.7
730			2.6	38.1
731			3.2	37.5
731			5.3	35.4
+20			6.3	34.4
+60			8.2	32.5
732			8.8	31.9
T.P.	883	40.33	8.17	32.50
733			10.0	31.3
734			7.3	34.0
735			0.8	40.5
T.P.	758	47.79	1.12	40.21
+50			7.6	40.2
736			6.1	41.7
737			3.2	44.6
738			4.1	43.7
739			6.5	41.3
+50			8.1	39.7
740			10.7	37.1
741			12.2	35.6
T.P.	430	40.06	12.03	35.76
B.M.			4.28	35.78
742			5.4	34.7
743			5.5	34.6

L.

R

39

11-11-14

$\frac{29.8}{18}$	$\frac{29.0}{15.5}$	$\frac{29.0}{11.5}$	$\frac{30.5}{6.5}$	$\frac{30.7}{4}$	$\frac{29.8}{6}$	$\frac{29.8}{16}$
$\frac{32.5}{15.5}$	$\frac{31.3}{13.5}$	$\frac{31.3}{7.5}$	$\frac{32.7}{5.5}$		$\frac{31.6}{20}$	
$\frac{39.5}{16}$	$\frac{38.1}{13}$	$\frac{38.1}{6.5}$	$\frac{39.3}{5}$		$\frac{38.6}{6}$	$\frac{36.7}{14.5}$ $\frac{37.7}{18.5}$
$\frac{41.1}{17}$	$\frac{40.2}{14}$	$\frac{42.2}{18.5}$	$\frac{41.9}{10}$			$\frac{38.2}{20}$ $\frac{40.0}{21}$
	$\frac{44.0}{20}$	$\frac{44.0}{76}$	$\frac{42.8}{72}$	$\frac{44.1}{8.5}$		$\frac{42.7}{18}$
$\frac{43.0}{17.5}$	$\frac{41.8}{13.5}$	$\frac{41.8}{10.5}$	$\frac{42.8}{8.5}$			$\frac{41.2}{23}$
$\frac{35}{18}$	$\frac{33.6}{15.5}$	$\frac{33.6}{12.5}$	$\frac{34.6}{10}$		$\frac{34.0}{4.8}$	
→ 61d BM. = 34.78						
Spike in Poplar Tree 40.15 741						
$\frac{32.3}{16}$	$\frac{32.3}{8.5}$	$\frac{33.8}{5}$		$\frac{33.1}{5}$	$\frac{31.6}{10}$	

✓ S.P.H #80

1149.06

743+40			4.2	35.9
744			4.3	35.8
745			6.9	33.2
746			10.8	29.3
T.P.	1.01	28.91	12.16	27.90
747			4.5	24.4
748			8.8	20.1
T.P.	*0.40	16.13	12.18	16.73
749			15	15.6
750			5.2	11.9
751			7.1	19.0
752			8.8	08.3
753			9.5	09.6
754			9.5	09.6
T.P.	3.96	1110.75	9.34	07.79
755			4.1	07.7
756			4.3	07.5
B.M.			3.97	1107.78
757			4.4	07.4
758			4.6	07.2
759			4.6	07.2
760			4.9	06.9
761			4.4	07.4
762			4.0	07.5
763			4.0	07.8

L. R 40

11-11-14

35.3	32.6	34.9	34.4
21	14	7.5	21
34.5	32.3	32.3	34.6
18	14	11	7.5
31.7	30.0	30.0	32.2
18	13	10	6
27.8	27.0	27.0	28.3
13.5	11	8.5	5
23.4	22.1	23.1	23.4
14	11	8	6.5
18.8	17.5	17.5	19.8
16.5	13	11	8
			23.4
			16
			19.1
			18

(Old BM = 1106.78)
 Spike in Poplar Tree 40' TP 756+50

✓ 1 S. P. H #80

1110.75

T.P.	9.54	18.53	3.76		27.79
764				9.0	08.5
765				7.8	09.7
766				6.4	11.1
767				4.9	12.6
768				3.4	14.1
769				0.3	17.2
T.P.	11.68	29.20	0.01		19.52
770				9.3	19.9
771				5.4	23.8
772				2.8	26.4
773				0.9	28.3
T.P.	9.83	38.30	0.73		28.47
774				9.7	28.6
775				8.8	29.5
776				7.8	30.5
777				4.7	33.6
778				2.6	35.7
779				1.6	36.7
T.P.	9.00	45.69	1.61		36.69
780				7.6	38.1
+60				5.1	40.6
781				4.9	40.8
B.M.			3.58		42.11

11-11-14

41

→ (old. BM = 41.11)

Spike in Cor Fence Post 35' L 780 + 85

✓ S.R.H #80

B.M.	4.02	1145	13	1142.11
782				4.1 42.0
783				4.7 41.4
784				4.8 41.3
785				6.0 40.1
786				6.8 39.3
787				8.4 37.7
788				10.0 36.1
T.P.	5.99	42.31	9.81	36.32
789				7.2 35.1
790				6.9 35.4
791				6.1 35.2
792				4.7 37.4
793				4.9 37.4
794				4.8 37.5
795				4.2 38.1
796				3.1 39.2
797				1.8 40.5
798				0.3 42.0
T.P.	10.96	53.17	0.10	42.21
799				9.6 43.6
800				8.4 44.8
801				6.7 46.5
802				4.8 48.4
803				2.5 50.7

11-12-14

42

Spike in Cor Fence Post 35' 780+85

C.D.C.
C.J.B.

11-12-14 worked $\frac{1}{2}$ day
(started to snow in a.m. and
continued all day)

$\frac{46.9}{13}$ $\frac{461}{10.5}$ $\frac{474}{6.5}$

$\frac{474}{5.5}$ $\frac{461}{8.5}$ $\frac{471}{12}$

✓ S. R. H #80
1153.17

804				52.7
T.P.	9.32	62.09	0.40	52.77
B.M.				7.45 1154.64
805				5.8 56.3
806				4.7 57.4
807				5.8 56.3
808				7.7 54.4
809				10.5 51.6
810				13.5 48.6
T.P.	0.33	50.38	12.04	50.05
811				4.1 46.3
812				5.3 45.1
813				6.2 44.2
814				6.7 43.7
815				8.1 42.3
816				9.9 40.5
T.P.	4.04	44.65	9.77	40.61
817				5.1 39.6
818				5.5 39.2
819				4.5 40.2
820				4.8 39.9
821				4.4 40.3
822				5.4 39.3
823				5.5 39.2
824				7.5 37.2

11-12-14 43

Old B.M. = 53.64
Spike in Poplar Tree 40' L 804

818+50 to 819+50 Borrow. Low ground

✓ S.H.R. #80

		1144.65			
T.P.	1.21	38.45	7.41		37.24
825				2.5	36.0
826				3.2	35.3
827				2.6	35.9
828				5.2	33.3
829				5.1	33.4
+50				6.5	32.0
830				7.1	31.4
831				8.2	30.3
832				10.2	28.3
T.P.	2.54	31.02	9.97		28.48
B.M.				3.92	27.10

11-12-14

44

828 to 828+50 Borrow Low ground.

(old B.M. = 26.10)

→ Spike in Oak Tree 60' P 832+90

✓ S R H #80

B.M.	3.22	1130.32		1127.10
833			4.5	25.8
+08.8			4.5	25.8
834			5.3	25.0
835			5.2	25.1
836			4.8	25.5
837			3.6	25.7
838			1.9	28.4
T.P.	12.33	40.80	1.85	28.47
839			10.0	30.8
840			6.5	34.3
841			3.7	37.1
842			1.4	39.4
T.P.	10.01	49.86	0.95	39.85
843			8.7	41.2
844			7.0	42.9
845			5.7	44.2
846			3.6	46.3
847			2.5	47.4
T.P.	4.72	52.41	2.17	47.69
+7.5			5.1	47.3
848			6.0	45.4
+4.5			8.5	43.9
849			6.2	45.2
850			6.6	45.8

L

R 45
11-16-14

4 Gor

worked 2 day too
windy + cold.

C.D.C

C.V.W.

C.W.B.

472
25

47.2
17
46.1
23
46.8
18
47.0
21

42.5
7

46.4
8

46.9
10.5
42.5
10.5

41.4
15
38.8
18
37.2
24
36.6
28

41.4
20

42.5
11

S. R. H #80

1152.41

851				5.8	46.6
+60				4.6	47.8
852				2.1	50.3
T.P.	8.95	59.36	2.00		50.41
853				6.6	52.8
854				5	54.3
855				5.3	54.1
+20				7.3	52.1
+70				7.3	52.1
856				8.7	59.7
+30				5.5	53.9
857				5.2	54.2
858				5.5	53.9
859				6.3	53.1
T.P.	1.33	54.97	5.72		53.64
860				3.0	52.0
861				4.9	50.1
862				5.8	49.2
863				6.0	49.0
864				5.2	49.8
865				5.0	50.0
T.P.	4.75	54.40	5.32		49.65
B.M.				2.72	50.68
866				4.6	49.8
867				4.9	49.5

R.

11-12-14

46

47.0
18

45.6
9

42.9
24

Survey Abandoned

53.3
27

52.3
14
52.9
18

45.2
13.5

48.2
18
49.8
19

Spike in W.P. Tree 60' P 865

S. R. H #80

115440

868				5.1	49.3
869				4.7	49.7
870				4.2	50.2
871				3.8	50.6
872				3.0	51.4
T.P.	10.60	62.49	2.51		51.89
873				9.6	52.9
874				8.1	54.4
875				6.1	56.4
876				4.9	57.6
877				3.1	59.4
+45				2.6	59.9
+61				1.4	60.1
+71				1.4	60.1
878				1.6	60.9
879				0.5	62.0
T.P.	7.20	68.99	0.70		61.79
880				6.3	62.7
881				5.1	63.9
882				4.7	64.3
883				4.0	65.0
884				3.5	65.5
885				2.0	67.0
+58				0.6	68.4
886				1.0	68.0

L

R

11-16-14

47

47.5	46.2	48.3
15.5	13	7

48.3	46.7	47.2
5.5	10	14

Old R.R. Grade

" " "

J

S. R. H # 80

1169.99

T.P.

0.38

68.61

11-16-14 48

S. R. H # 80

T.P.	729	1175.90		1168.61
887			9.4	65.5
+40			9.3	65.6
888			6.6	69.3
889			5.5	70.4
890			4.8	70.1
891			4.9	71.0
892			4.7	71.2
893			4.1	71.8
894			3.1	72.8
T.P.	575	78.73	2.92	72.98
B.M.			5.66	73.07
895			5.3	73.4
896			4.6	74.1
897			4.8	73.9
898			5.5	73.2
899			5.9	72.8
900			5.2	73.5
901			3.3	75.4
T.P.	1118	86.93	2.98	75.75
902			9.6	77.3
903			6.8	80.1
904			5.2	81.7
905			4.4	82.5
906			4.3	82.6

11-17-18 49

C.D.O.
C.J.B.

(Worked 2 day Levels)

(old B.M. = 720.7)

Spike in Tel Pipe 893+60 40'L

Pipe.

S. R. H #80

1186.93

907			4.7	80.2
908			5.1	81.2
909			5.4	81.5
T.P.	2.51	84.49	4.95	80.98
910			3.3	80.2
911			4.0	80.5
912			4.6	79.9
913			5.5	79.0
914			6.9	77.6
B.M.			6.04	78.45
915			8.1	76.4
916			8.3	76.2
T.P.	1.68	78.60	7.57	76.92
917			3.2	75.4
918			6.7	70.9
T.P.	4.60	70.30	11.90	66.70
919			7.3	64.0
+50			10.4	60.9
920			12.1	59.2
921			12.1	59.2
922			9.2	62.1
923			5.5	65.8
+45			3.7	68.6
924			2.4	69.9
925			2.7	68.6

L.

R.
11-17-14

50

On Iron Pipe Sec. Cor

	56.9	57.9
	13	4
59.5	60.2	61.0
14	12	95
	63.2	64.6
	12	8

	57.4	56.7
	7	13
60.5	59.8	59.4
7	85	13
	63.6	
	16	

S. R. H #80

117130

✓
926

4.2

67.1

927

6.0

65.3

T.P.

6.12

65.18

L.

R.

51

11-17-14

C.D.O

C.W.B

$\frac{63.3}{22}$

$\frac{630}{11}$

$\frac{643}{20}$

✓ S.R.H. #80

T.P.	0.46	1165.64		1165.18
928			6.2	59.4
929			7.6	58.0
T.P.	0.60	55.05	11.19	54.45
930			2.3	52.8
931			8.3	46.8
+55			10.3	44.8
932			9.8	45.3
+70			10.9	44.2
933			10.4	44.7
934			5.4	49.7
935			2.3	52.8
T.P.	4.80	59.51	2.34	52.71
936			3.2	54.3
+35			2.3	55.2
937			2.4	55.1
+25			2.9	54.6
938			6.3	51.2
+50			6.1	51.4
939			5.4	52.1
940			6.8	50.7
941			7.5	50.0
T.P.	8.63	59.14	7.00	50.51
B.M.			8.88	50.16
942			8.5	50.6

L. R. 52
11-18-14

(worked 3 day levels) C.D.C. C.S.W. C.J.B.

	$\frac{58.0}{25}$	$\frac{57.8}{11}$	$\frac{60.2}{23}$
$\frac{56.8}{15}$	$\frac{55.3}{12}$	$\frac{56.9}{8}$	$\frac{56.5}{14}$ $\frac{55.5}{20.5}$ $\frac{57.8}{24}$
$\frac{51.2}{13}$	$\frac{50.0}{12}$	$\frac{51.4}{7.5}$	$\frac{51.4}{14.5}$ $\frac{49.7}{23.5}$ $\frac{52.1}{26.5}$
$\frac{44.8}{18}$	$\frac{44.8}{4.1}$	$\frac{45.5}{2.5}$	$\frac{45.5}{6}$ $\frac{44.9}{8.5}$ $\frac{44.0}{1.8}$
	$\frac{40.1}{6}$	$\frac{44.1}{3.5}$	$\frac{44.1}{5.5}$ $\frac{40.9}{9}$
	$\frac{42.8}{18}$	$\frac{42.0}{11.5}$	$\frac{43.2}{20}$
	$\frac{43.6}{23}$		$\frac{44.4}{18}$
$\frac{48.2}{18}$	$\frac{47.2}{17}$	$\frac{47.2}{14}$	$\frac{49.6}{8}$
$\frac{48.0}{18}$	$\frac{47.6}{17}$	$\frac{47.2}{14.5}$	$\frac{49.8}{10}$
	$\frac{49.8}{70}$		
	$\frac{49.8}{70}$		
	$\frac{50.0}{9}$	$\frac{51.3}{22}$	$\frac{49.8}{70}$ $\frac{48.8}{75}$ $\frac{48.8}{16}$

Spike Fence Post 50' L 941

✓ S. R. H # 80
1159.14

943				6.6	52.5
944				4.8	54.3
945				3.9	55.2
946				2.9	56.2
947				1.9	57.2
T.P.	10.99	68.66	1.47		57.67
948				10.1	58.6
949				9.2	59.5
950				8.1	60.6
951				5.0	63.7
952				1.3	64.4
T.P.	9.50	76.99	1.17		64.49
953				7.0	69.0
954				4.7	72.3
955				3.9	73.1
956				4.5	72.5
957				6.5	70.5
958				8.4	68.6
959				11.0	65.0
960				12.7	64.3
T.P.	1.10	65.54	12.55		64.44
961				3.1	62.4
962				5.4	60.7
943				8.5	57.0
EX III				10.20	55.34

11-18-14

53

Spike in Poplar Tree 963450 soil.

S. R. H #80

1165.54

11-18-14 54

964			11.0	54.5
965			11.4	54.1
T.P	2.38	56.38	11.54	54.00
966			3.6	52.8
967			4.5	54.9
968			5.0	51.4
969			4.7	54.7
970			3.6	52.8
971			1.6	54.8
T.P	12.15	67.11	1.42	54.96
972			9.4	57.7
973			3.9	63.2
T.P	12.50	79.04	0.57	66.54
974			11.1	67.9
975			6.4	72.6
976			3.1	75.9
977			1.9	76.1
T.P	12.00	89.83	1.21	77.83
978			10.4	78.4
979			9.9	79.9
980			8.3	81.5
981			4.5	85.3
982			2.6	87.2
983			1.9	87.9
			2.0	87.8

S. R. H. #80

118983

984			3.5	86.3
T.P.	118	88.12	2.89	86.94
985			3.9	84.2
986			6.2	81.9
987			7.2	80.9
988			7.9	80.2
989			8.7	79.4
T.P.	283	86.53	9.42	79.70
+40			3.6	76.9
+65			5.4	76.1
990			8.5	73.0
+20			9.0	72.5
+70			8.5	73.0
991			8.0	73.5
+15			8.0	73.5
+65			4.4	77.1
992			3.5	78.0
993			4.4	77.1
+50			6.2	75.3
994			10.6	70.9
T.P.	282	72.16	12.19	69.34
+50			4.5	67.7
995			5.8	66.4
996			5.8	66.4
997			4.9	67.3

R

55

11-18-14

79.9 11.5	78.6 9.5	79.3 5.5		79.9 16
79.4 11.5	72.9 9.5	78.5 8		78.5 10
78.7 12.5	77.3 11.5	76.0 8.5		78.0 16
77.3 13	75.7 12.5	75.7 10.5	76.5 7	76.5 7.5
	75.7 12.5	74.2 10.5	74.7 7	76.2 10
	71.5 12.5	74.1 7.5	71.8 11.5	72.6 14
	68.1 5			77.6 22
	68.1 6	71.4 4		76.5 14
	68.1 7	72.0 5		70.8 11
	68.1 7	72.0 5		70.4 11
	72.8 11	75.7 9.5		72.0 9
77.8 11	76.3 10			89.4 11
	74.4 10	75.5 9.5		68.4 10
	75.5 11	72.7 8.5		77.0 13.5
	70.6 10	69.6 4.5		76.5 9.5
	64.1 6.5	66.3 4.5		77.4 11
	63.7 6.5	65.8 4.5		75.2 11.5
				75.1 12
				75.6 13.5
				69.7 9
				69.0 11.5
				69.0 13
				70.5 14
				66.3 8
				64.1 11.5
				65.8 8
				63.7 11.5

S. R. H # 80

1172.16

998				64	65.8
B.M.				4.87	67.29
999				6.8	65.4
1000				7.5	64.7
1001				8.4	63.8
T.P.	1.11	65.11	8.16		64.00
1002				2.2	62.9
1003				3.5	61.6
1004				4.7	60.4
1005				5.7	59.4
1006				7.1	58.0
1007				6.7	56.4
1008				10.3	54.8
T.P.	0.50	55.38	11.23		54.88
1009				1.3	54.1
1010				3.2	52.2
1011				4.6	50.8
1012				5.0	50.4
1013				5.1	50.3
1014				4.6	50.8
1015				4.1	51.3
1016				3.9	51.5
T.P.	2.46	54.01	3.83		51.55
1017				2.4	51.6
1018				1.6	52.4

11-18-14 56

(old B.M. = 66.29)

Spike in Tel Pole 25/997+90

S.R.H # 80

115401

1019			4.14	49.87
1020			1.5	52.5
1021			2.9	54.1
1022			4.6	49.4
1023			7.0	47.0
1024			10.3	43.7
1025			11.3	42.7
1026			11.7	42.3
1027			10.2	43.8
T.P.	1.77	45.57	10.27	43.80
1028			0.9	44.7
1029			0.6	45.0
1030			2.7	42.9
1031			6.5	39.1
1032			8.5	37.1
1033			8.4	37.2
1034			8.3	37.3
1035			7.8	38.2
T.P.	5.74	43.74	7.57	38.00
1036			4.5	39.2
1037			3.9	39.8
1038			4.5	39.2
1039			4.7	39.0
1040			4.0	39.7
			3.0	40.7

(old B.M. = 4887) 11-18-14

57

→ Spike Tel Pole 1021 + 40 25' L

1023 to 1025 Borrow

Cut & Fill & Borrow

39.8	Natural Ground
35.8	" "
35.9	" "
35.4	" "
37.5	" "

S. R. H ⁴ 80

1143.74

1041				2.2	40.9
T.P.	10.93	53.82	0.85		42.89
1042				10.0	43.8
1043				6.7	47.1
1044				4.3	49.5
1045				3.5	50.3
1046				4.2	49.6
B.M.				2.68	50.14
1047				5.1	48.7
1048				5.3	48.5
T.P.	9.07	57.56	5.03		48.49
1049				9.4	48.2
1050				8.1	49.5
1051				6.7	50.9
1052				4.3	53.3
1053				3.1	54.5
1054				4.8	52.8
1055				8.7	49.9
T.P.	0.05	46.68	10.93		46.63
1056				2.5	44.2
1057				4.9	40.8
1058				5.0	40.7
1059				4.8	40.9
1060				4.0	42.7
1061				3.7	43.6

11-18-14 ⁵⁸

(old BM = 50.14)
Spike Tel. Pole 30' 1046

41.2 Natural Ground
40.7 " "
40.9 " "

40.9	40.1	41.5	41.2	39.7	41.4
16	14	9	13.8	17	19

S. R. H. # 80

114568

1062				3.9	42.8
1063				5.8	40.9
T.P.	3.70	44.69	56.9		40.99
1064				5.0	39.7
1065				5.4	39.3
1066				4.9	39.8
1067				5.2	39.5
1068				5.5	39.2
1069				4.8	39.9
1070				2.7	42.0
T.P.	5.45	47.47	2.67		42.02
B.M.				2.77	44.70

11-18-14

59

Survey Abandoned

37.6 Natural Ground

37.3 " "

37.0 " "

38.1 " "

(old B.M. = 43.70)

Spike Tel. Pole 25' 1070 + 70

✓ S. R. H #80

B.M.	11.97	1156.67		1144.70
1071			12.8	439
1072			8.9	478
1073			6.8	48.9
1074			4.8	51.9
1075			3.2	53.5
1076			3.3	53.4
1077			3.5	53.2
1078			3.7	53.0
T.P.	4.78	57.94	3.51	53.16
1079			4.2	53.7
1080			3.0	54.9
1081			2.0	55.9
+65			1.7	56.2
1082			2.5	55.4
1083			6.3	51.6
1084			11.2	46.7
T.P.	0.19	45.75	12.38	45.56
+65			2.7	43.1
1085			6.6	39.2
+50			10.0	35.8
1086			11.9	33.9
T.P.	0.19	33.19	12.75	33.00
1087			2.7	30.5
1088			4.7	28.5

11-20-14 60

Spike in Tel Pole 25'L 1070+70

C.D.C
C.J.W.
C.J.B

✓

S. R. H # 80

113319

1089			8.6	24.6
1090			12.8	20.4
T.P.	3.25	23.66	12.78	20.41
1091			4.1	19.6
+10			4.1	19.6
+40			8.0	15.7
Water Level			8.9	14.8
+42			9.5	14.2
+52			10.2	13.5
+60			9.5	14.2
+62			7.8	15.9
+75			6.3	17.4
1092			7.4	16.3
1093			7.2	16.5
1094			6.8	16.9
1095			7.2	16.5
T.P.	3.70	20.81	6.55	17.11
+47			4.4	16.4
+49			7.0	13.8
Water Level			6.2	14.6
1096			7.0	13.8
+24			7.0	13.8
+25			4.3	15.5
1097			4.1	16.7
+72			5.5	15.3
+74			7.2	13.6

L

R

61

11-20-14

$\frac{23}{20} \cdot \frac{209}{18} = \frac{228}{16}$

$\frac{24.8}{17} = \frac{18.9}{20}$

$\frac{162}{18} = \frac{162}{8} = \frac{194}{4}$

$\frac{19.6}{7.5} = \frac{17.2}{10.5} = \frac{17.5}{17}$

Stony Brook Cr. H.W. 1170

$\frac{188}{20} = \frac{188}{9} = \frac{17.8}{6}$
 $\frac{188}{20} = \frac{17.8}{9} = \frac{16.4}{6}$

$\frac{13.5}{2} = \frac{13.5}{16}$
 $\frac{10.4}{16}$

Stony Brook Cr

Bottom " "

" " "

Bottom " "

S.R.H #80

1120 81

✓ W.L.				66	14.2
1097+98				72	13.6
1098				54	15.4
+50				53	15.5
+70				33	17.5
1099				32	18.6
B.M.				1.63	19.18
1100				21	18.7
T.P.	11.93	31.33	1.41		19.40
1101				10.0	20.3
1102				111	20.2
+50				11.4	19.9
1103				8.8	22.5
+45				2.1	29.1
T.P.	8.78	39.92	0.19		30.14
1104				7.4	32.5
1105				4.1	35.8
+55				28	37.1
1006				3.8	36.1
1107				91	30.8
T.P.	1.00	28.47	12.45		27.47
1108				3.4	25.1
1109				67	20.8
1110				91	19.4
1111				10.6	17.9

Stony Brook Cr.

(old B.M. = 1818)

Spike Tel Pole 25' L 1099

29.6				20.5
25				21
31.2				26.5
19				25
36.6	38.2	35.1		35.8
100	13	9		20
37.3	35.9	35.9	37.2	36.0
16	100	100	8	21
35.7	35.1	35.1	35.1	37.9
17	15	12	10.5	21

R. 62
11-20-14

S.R.H #80

112847

✓ 1112				116	159
T.P.	3.27	29.74	11.00		17.47
1113				4.5	16.2
1114				5.0	15.7
1115				4.7	15.0
1116				4.3	15.4
1117				5.6	15.1
+75				7.3	13.4
+80				9.9	19.8
+85				6.7	14.0
1118				5.7	15.0
1119				5.6	15.1
1120				4.1	16.6
T.P.	9.78	26.98	3.54		17.20
1121				8.0	19.0
+80				5.2	21.8
1122				4.9	22.1
1123				4.3	22.6
1124				4.7	22.3
B.M.				4.08	22.90
1125				5.9	21.1
1126				6.0	21.0
1127				6.0	21.0
1128				6.2	20.8
T.P.	5.47	26.70	5.75		21.23

63.

11+50 to 13+50 Borrow.

13.9 Natural Ground
14.0

Creek

12.9
13.5

(old PM = 21.90)

same Tel Pole 25 R 1123+80

S. R. H #80

1125.70

1129			6.0	20.7
1130			6.4	20.3
1131			5.6	21.1
1132			5.1	21.6
1133			4.7	22.0
1134			4.7	22.0
1135			4.4	22.3
1136			4.3	22.4
1137			2.5	24.2
1138			1.5	25.2
T.P.	2.90	28.40	1.20	25.50
1139			2.3	26.1
1140			2.3	26.1
1141			3.0	25.4
1142			3.5	24.9
1143			3.8	24.6
+25			3.8	24.6
+50			4.6	23.8
B.M.			0.95	27.45
1144			5.7	23.3
1145			5.6	22.8
1146			5.9	22.5
1147			5.6	22.8
1148			5.6	22.8
1149			5.6	22.8

64

Cold PM = 26.45
 Swamp
 Spike in Dead Oak Tree 40' R 1144

S. R. H #80

1128.40

1150				5.2	23.2
1151				4.6	23.8
T.P.	5.40	30.15	3.65		24.75
1152				5.9	24.3
1153				5.9	24.3
1154				5.8	24.4
1155				5.1	25.15
1156				5.3	24.95
1157				5.2	25.0
1158				5.0	25.2
1159				3.5	26.7
T.P.	11.14	40.12	1.17		28.98
1160				9.1	34.0
1161				6.5	33.6
1162				3.9	35.2
B.M.				4.52	35.60
1163				2.2	37.9
T.P.	7.83	46.46	1.49		38.63
1164				6.9	39.6
1165				5.1	41.4
1166				4.3	42.2
1167				4.8	41.7
1168				5.8	40.7
1169				6.1	40.4
1170				3.9	42.6

65

1129.11

~~old~~ BM = 34.60
 Spike in Cor Fence Post 40' R 1161 + 75

✓ S.R.H #80

1145.46

1171			1.5	45.0
T.P.	10.44	55.11	1.79	44.67
1172			7.1	48.0
1173			4.5	59.6
1174			3.1	52.0
1175			3.6	50.5
1176			5.6	49.5
1177			9.4	45.7
1178			12.7	42.4
1179			13.9	41.2
B.M.	2.82	45.94	11.99	43.12
1180			4.8	41.1
1181			4.1	41.8
1182			3.7	42.2
1183			4.7	41.2
1184			4.7	41.2
X1185			3.2	42.7
1186			2.1	43.8
1187			1.1	44.8
1188			0.6	45.3
T.P.	9.32	54.56	0.70	45.24
1189			8.1	46.5
1190			7.1	47.5
1191			5.8	48.8
1192			4.7	49.9

66

1168 to 1169 + 50 Barrow Swamp

(old. BM = 42.12)

Spoke in Oak Tree 50' R 1179 + 25

S.R.H #80

115456

1193			3.6	51.0
1194			2.0	52.6
T.P.	11.48	64.65	1.39	53.17
1195			9.6	55.1
1196			7.5	57.2
1197			5.4	59.3
1198			4.6	69.1
1199			4.9	59.8
1200			5.6	59.1
1201			6.1	58.6
1202			6.1	58.6
B.M.	1.10	59.30	6.45	58.20
1203			1.8	57.5
1204			3.1	56.2
1205			4.3	55.0
1206			6.4	52.9
1207			10.7	48.6
1208			13.5	45.8
1209			13.6	45.7
1210			10.9	48.4
T.P.	8.80	54.35	10.75	48.55
+60			7.0	50.4
1211			7.9	49.5
1212			7.8	49.6
1213			6.6	50.8

L.

R.
11-20-14 67

~~Old B.M. = 57.20~~

Spoke Tel Pole 20' R 1202 + 50

47.4 + 6.9 = 54.3
23 22 19 17

44.4
20

49.5 + 48.1 + 48.1 + 49.2
26 24 20.5 18
50.8
24
51.6
18

48.5 + 46.1
110 21

47.7
20
48.2
20

47.7
20

S. R. H #80

1157.35

1214				3.6	53.8
T.P.	11.67	67.64	1.38		55.97
1215				8.9	58.7
1216				3.9	63.7
T.P.	9.38	75.35	1.67		65.97
1217				7.7	67.7
1218				5.8	69.6
1219				4.8	70.6
1220				4.4	71.0
B.M.				4.40	70.95
1221				5.9	69.5
1222				9.6	65.8
T.P.	0.42	64.47	11.30		64.05
1223				4.3	60.2
1224				10.6	53.9
+50				13.7	50.8
T.P.	1.34	53.97	11.84		52.63
1225				5.1	48.9
1226				7.8	46.2
1227				13.6	40.4
T.P.	0.67	41.92	12.72		41.25
1228				11.1	30.8
T.P.	0.66	30.50	12.08		29.84
1229				8.4	22.1
B.M.			10.39		29.11

L.

R.

11-20-14 68.

$\frac{54.1}{20}$

$\frac{52.1}{18}$

$\frac{14.5}{10}$

→ Old B.M. = 69.95

Spike Fence Post 1220+25 25'R

→ Old B.M. = 19.11

Spike Cor Fence Post 1229+25 20'R

✓

S. R. H 80

B.M.	182	11 20.93		1129.11
1230			3.1	18.8
1231			5.2	16.7
1232			7.9	14.0
1233			10.0	11.9
1234			13.4	08.5
T.P.	128	11 11.71 11.50		11.10.43
1235			3.8	07.9
1236			4.1	07.6
1237			4.4	08.3
1238			4.3	07.4
1239			3.8	07.9
1240			4.3	07.4
1241			4.1	06.6
1242			2.5	09.2
T.P.	1017	19.32 2.56		09.15
1243			5.3	14.0
B.M.			3.26	16.06
+55			2.3	17.0
1244			2.1	17.2
+55			5.5	13.8
1245			4.9	14.4
+70			3.2	16.1
1246			1.7	17.6
T.P.	1004	28.21 1.15		18.17

L.

R 11-23-14 69

Spike Cor Fence Post 124425 20' R. c.o.c
 c.s.w.
 c.v. B.

1234 to 1241 Barrow.

064 Natural Ground.
 060
 060
 065
 072
 069
 05.9

(Old BM = 15.06)

Spike in Poplar Tree 1243460 25' L

15.7	14.9	14.7	13.0
15	14	5	18
	14.7		17.4
	21		18.5
	12.3		20
	20		18.4
			22
12.7		13.0	14.8
21		15	13.9
17.1	15.6	15	22
27	19	15.0	14.6
19.0	16.0	17.6	14.0
18	14	12	22
29.3			19.6
26			4
			15.8
			8
			14.7
			21

S. R. H # 80

1128.21

1246+65			6.0	22.2
1247			3.2	25.0
1248			4.3	23.9
1249			4.4	23.8
1250			4.7	23.5
1251			4.4	23.8
1252			4.7	23.5
1253			4.5	23.7
1254			4.7	23.5
T.P.	0.80	23.89	5.12	23.09
1255			1.6	22.3
1256			3.5	20.4
1257			6.1	17.8
1258			6.8	17.9
1259			5.6	18.3
1260			5.1	18.8
1261			6.3	17.6
T.P.	1.72	20.24	5.37	18.52
1262			3.3	16.9
1263			2.7	18.5
1264			5.5	14.7
1265			6.1	14.1
+40			5.5	14.7
1266			11.8	08.4
T.P.	1.32	10.26	11.30	08.94

L.

R.

11-23-14 70

$\frac{23.8}{18}$	$\frac{20.0}{14}$	$\frac{21.5}{10}$	$\frac{21.0}{5}$	$\frac{19.4}{18}$
$\frac{23.8}{20}$	$\frac{21.3}{17}$	$\frac{21.3}{14}$	$\frac{23.7}{10}$	$\frac{23.3}{35}$
				$\frac{22.2}{21}$

S. R. H. 80

11026

1267			47	5.6
1268			50	5.3
+70			65	3.8
+90			8.3	1102.0
1269			95	1100.8
+06			99	1100.4
+12	E.B.		10.2	1100.1
B.M.			446	05.80
T.P.	4.71	1103.58	11.39	1098.87
+15			9.0	1094.6
+26			9.6	94.0
+35			9.0	94.6
+37	E.B.		4.6	98.2
W.L.			8.4	1095.2
+50			62	97.4
T.P.	11.96	1100.83		1098.87
1270			120	98.8
1271			119	98.9
+60			10.2	1099.6
1272			72	1103.6
T.P.	9.63	1119.39	1.07	1109.76
1273			69	12.5
+22			62	13.2
+70			73	12.1
1274			7.0	12.4

started from old T.P.

L

R

11-23-14 71

04.0	02.7	02.7	04.3	04.6
15	13	9	7	18
04.0	02.7	02.7	04.1	04.3
15	13	9	7	18
04.7	02.0	02.9		03.7
16	11	5		18.5
	05.1	01.0		01.7
	16	9		85
99.9	97.9	99.8		99.8
16	10	5		16
96.2	96.8	99.4		99.4
18	11.5	5.0		6.5
95.4		98.5		95.2
18	11	5.5		14
				95.7
				15
				95.7
				18

Spike Service Tree to R 1269

Bottom of Mayo Brook

Bottom " " "

" " " "

Mayo Brook:

96.1	97.6	97.6	96.1
10	6.5	4.5	6.5

11.0	13.9
13.5	18
11.8	15.0
12	16.5
11.1	09.6
12	16
11.4	09.0
12	15

S. R. H #80

1119.39

1274+25				5.4	14.0
+60				2.3	17.1
T.P.	6.17	24.65	0.91		18.48
1275				4.7	20.0
+50				3.3	21.4
1276				3.5	21.2
1277				4.6	20.1
1278				5.4	19.3
1279				7.4	19.3
1280				7.9	16.8
1281				7.7	19.0
1282				7.2	17.5
T.P.	6.68	24.57	6.76		17.89
1283				4.7	19.9
1284				3.3	21.3
1285				2.6	22.0
1286				5.0	19.6
1287				9.0	15.6
1288				13.1	11.5
T.P.	0.38	13.16	11.79		112.78
1289				3.7	09.5
1290				4.6	08.6
B.M.				3.91	09.25
1291				5.4	07.8
1292				6.6	06.6

L.

R

11-23-14 72

$\frac{19.4}{18}$ $\frac{19.4}{5}$

$\frac{21.0}{18}$ $\frac{21.0}{5}$

$\frac{14.0}{12}$

$\frac{10.0}{16}$

$\frac{17.1}{17.5}$ $\frac{18.6}{20.5}$

$\frac{20.0}{19.5}$ $\frac{20.9}{22}$

→ (old B.M. = 0825)
Spike in J.P. Tree 30' L 1290+45

S. R. H #80

1113.16

11-23-14 73

X 1293				9.5	03.7
1294				11.7	1100.5
1295				11.7	1100.5
T.P.	5.12	1109.00	11.28		1101.88
-1296				5.5	01.5
1297				5.4	01.6
-1298				5.5	01.5
1299				5.3	01.7
1300				5.3	01.7
1301				5.3	01.7
1302				5.2	01.8
+50				5.2	01.8
1303				2.4	04.6
T.P.	11.92	15.95	2.97		04.03
+50				7.2	08.5
1304				6.8	09.2
1305				7.5	08.5
1306				7.1	08.9
1307				4.7	11.3
1308				4.0	12.0
1309				7.1	08.9
1310				9.0	07.0
T.P.	4.02	10.32	8.65		07.30
1311				4.0	07.3
+75				3.3	08.0
1312				4.6	06.7

S. R. H. #80

1110.32

B.M.			7.17	1104.15
1313			11.4	1099.9
T.P.	1.50	1100.25	12.57	1098.75
1314			5.4	94.9
+15			5.9	94.4
+45			5.8	94.5
W.L.			5.8	94.5
+80			6.1	94.2
1315			6.0	94.3
+60			4.5	95.8
1316			6.4	93.9
+59			5.9	94.4
+60			10.3	90.0
+66			10.3	90.0
+68			6.0	94.3
W.L.			9.2	91.1
1317			6.5	93.8
+40			6.6	93.7
1318			2.8	97.5
T.P.	12.32	1109.92	2.65	97.60
+15			11.1	98.8
1319			9.4	100.5
1320			8.5	1101.4
1321			2.1	07.8
T.P.	7.04	10.83	0.13	09.79

→ (old BM = 1103.15) p. 3-14 74.

Spoke in J.P. Tree 1312 + 50 35' P

92.3		92.5	
91.6	93.1	92.8	91.8
10.5	8.5	7	9.5
			Small Cr.
92.6	92.3	93.0	
20	13	5.5	
93.5	92.4	92.4	93.2
19.5	16.5	12.5	10.5
95.6	92.2	92.2	94.8
21.5	17	15	9
	94.0		
	21		
		93.6	
			Bottom of Cr. Branch of Mayo Cr.
			" " " " " "
		93.2	
			Branch of Mayo Cr.
	92.4	93.2	
	11	9	
			93.0
			91.8
			91.8
			14.5
			14.5
	95.3	93.6	
	17.5	14.5	
			95.9
			12
			93.6
			93.6
			96.4
			16
			17.5
			17.5

S. R. H # 80

1115.83

1321+80			5.4	10.4
1322			5.4	11.4
1323			6.3	10.5
1324			7.2	09.6
1325			6.5	10.3
1326			4.6	12.2
1327			3.5	13.3
1328			3.0	13.8
1329			3.3	13.5
1330			3.6	13.2
1331			3.8	13.0
T.P.	6.48	19.71	3.60	13.25
1332			6.5	13.2
1333			5.3	14.4
1334			4.5	15.2
1335			4.8	14.9
1336			5.2	14.5
1337			6.0	13.7
+16 ⁸			6.3	13.4
B.M.		4.37		15.34

11-23-14 75

old BM = (14.34)

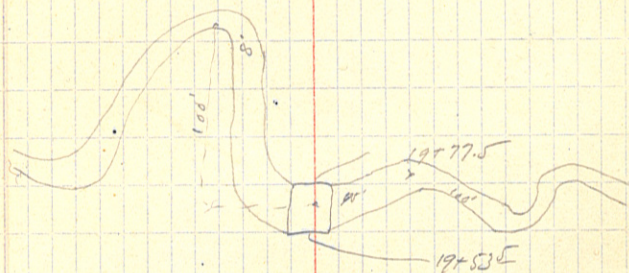
Sec. Cor N.E. Cor 3 - 136-30 N.W. Cor 2 - 136-30
Spike in J.P. Tree 60' R 1336 + 10

	F.S.	H.I.	B.S.	Elev.
	3.47	1008.42	3.47	1004.95
T.P.	5.70	1004.02	1.30	1002.72

19+53.5	75	94.5
+55	90	95.0
+64	98	94.2
+69	95	94.5
+70	75	96.5
+77.5	79	96.1
100' upstream	8.4	95.6
200 "	8.3	95.7
100 Down Stream	8.6	95.4
200 "	8.7	95.3

76

2' of Sand then sand & Gravel
very hard



Levels of Off-Take

Sta.	F.S.	A.I.	B.S.	ELV.
B.M.		1018.23	0.85	1017.38
T.P.	5.5	16.48	3.75	1012.73
00	3.8			1012.68
+08	4.4			1012.58
Water Level. Sta. 00+08				1010.59
1+00	3.9			1012.58
2+00	4.35			1012.13
3	4.35			1012.13
4	4.12			1012.36
5	4.6			1011.88
6	4.7			1011.78
+45	4.3			1012.18
T.P.	4.2	20.33	8.05	1012.28
7				
8				
T.P.	7.95	16.48	4.1	1012.38
9				
9+90				
10				
10+18	Water Level Pillager L.			1008.58

Fall from Ditch Level
at Road to Pillager L.
Water Level = 2 Feet.

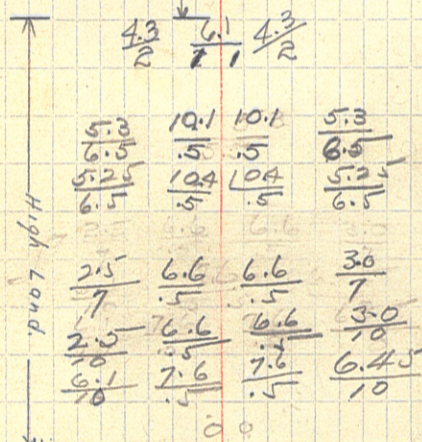
L. R. 77

(549, 120+35)

↓
Bottom of ditch.

To 6+45
From 00+08 Ditch is
4' x 2.5' x 2' deep.
From 6+45 to End
it is only 1' wide
on bottom.

←



Ditch should be cut
Deeper From 6+45 To
Lake (Sta. 10+18)

Centre Line

Sta.	F.S.	H.I.	B.S.	ELEV.
T.P.		^{55.52} 1145.42	5.05	1150.47
291	5.4			1140.02
292	3.4			1142.07
293	5.15			1140.21
294	8.6			1137.36
+25	9.0			1136.42
295	7.1			1138.32
296	3.2			1142.22
T.P.	3.15	^{52.27} 1148.67	6.40	^{49.12} 42.57
297	5.95			42.72
298	4.9			44.58
98+83 ²	2.95			45.92
299	3.15			45.52
B.M.	3.01			1145.66
300	4.85			43.82
301	5.3			43.64
302	5.6			43.07
303	3.8			45.59
T.P.	3.9	1147.96	2.30	(B.M.) 45.66
T.P.	6.8	1150.01	8.85	1141.16
B.M.	3.34			1146.67
T.P.	0.69	1160.60	11.28	1149.32
T.P.	0.39	1172.55	12.34	1160.21
T.P.	1.07	1182.18	10.70	1171.48
T.P.	0.47	1191.83	10.12	1181.91

L
178 78

39.47	41.42			
<u>38</u>	<u>17</u>			
35.7	36.9	36.5	37.8	38.4
<u>21</u>	<u>4.5</u>	<u>10</u>	<u>13.5</u>	<u>21</u>
36.3	36.3	36.2	35.6	37.3
<u>20</u>	<u>16.5</u>	<u>5.5</u>	<u>10.5</u>	<u>17</u>
38.2	38.0	38.4	37.1	38.0
<u>21</u>	<u>14</u>	<u>7.5</u>	<u>5.5</u>	<u>14</u>
	3.55	3.6	3.1	3.6
	<u>21</u>	<u>6</u>	<u>6</u>	<u>8.5</u>
				<u>11</u>
				<u>2.4</u>
				<u>20</u>

6.35	6.35	6.45	4.95
<u>20</u>	<u>13</u>	<u>7</u>	<u>6.8</u>
50	5.52	5.2	4.45
<u>20</u>	<u>10.5</u>	<u>7</u>	<u>20</u>
3.0	3.0	3.0	2.95
<u>20</u>	<u>12</u>	<u>5.5</u>	<u>7</u>
			<u>9</u>
			<u>2.95</u>
			<u>17</u>

J.P.				299+05	35 L
4.92	4.92	5.55	4.8	5.05	6.0
<u>20</u>	<u>14</u>	<u>12</u>	<u>9</u>	<u>5</u>	<u>8</u>
5.45	5.45	5.8	5.55	5.35	6.1
<u>20</u>	<u>14</u>	<u>10.5</u>	<u>8</u>	<u>7.5</u>	<u>10.5</u>
5.0	5.9	6.2	5.7	5.6	6.1
<u>20</u>	<u>14</u>	<u>11.5</u>	<u>10.5</u>	<u>6.5</u>	<u>9</u>
		4.0	4.3	4.0	4.4
		<u>14</u>	<u>10.5</u>	<u>8</u>	<u>9</u>
					<u>3.7</u>
					<u>13</u>
					<u>50</u>
					<u>20</u>

Small White Oak. 310+90 36⁵ R.

	FS	H.I.	B.S.	ELV.
		1191.83		
T.P.	0.40	1204.48	13.05	1191.43
T.P.	0.33	1212.62	8.47	1204.15
T.P.	5.67	1208.12	1.17	1206.95
T.P.	9.33	1179.49	0.70	1198.79
B.M.	1.10			1178.39
T.P.	13.0	1167.09	0.60	1166.49
T.P.	11.65	1155.97	0.53	1155.44
T.P.	12.27	1144.80	1.10	1143.70
T.P.	12.25			1132.55

Spike in 16" Oak stump 331+30 ~ 60' L.

Big Spring Cr.

H.I.

Rad.

27.5

7.6

19.9

100 FT. Down stream.

8.35

19.15

" UP

7.40

20.1

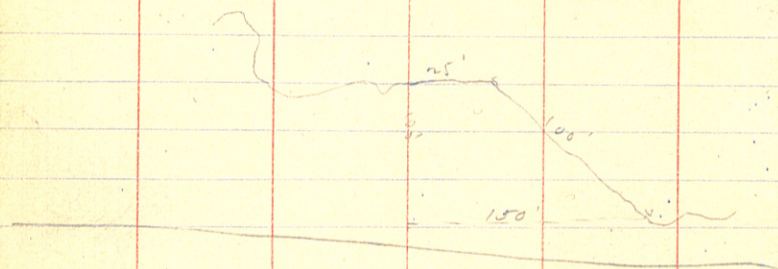
2 Ft. Sand & Wash

4" Sand & Black Limestone

2 Gravel & Sand.

L

P



Soundings

- 126 3' Peet 16' mark
- 129 5' Peet Then sang
- 128 4' " 13' of mark to Sang
- 124 3' " 11' mark to sang

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle
of Intersection or I. P.= $23^{\circ} 20'$ to the R. at Station
542+72.

Ext. in Tab. IV opposite $23^{\circ} 20'$ =120.87
120.87+12=132.87. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20'$ =1183.1
1183.1+10=1193.1.

Tab. V. correction for A. $23^{\circ} 20'$ for a 10° Cur.=0.16
1193.1+0.16=1193.26=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. $23^{\circ} 20'$ = 23.33° +10=2.3333=L. C.

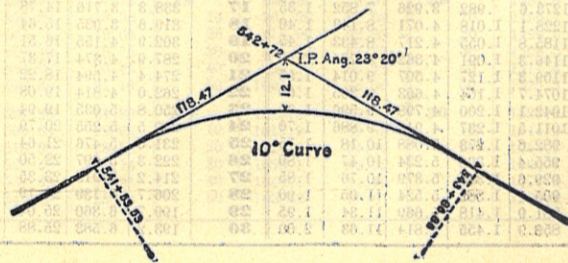
$2^{\circ} 19\frac{1}{2}'$ =def. for sta. 542	I. P.=sta. 542+72
$4^{\circ} 49\frac{1}{2}'$ = " " +50	Tan.= 1.18.47
$7^{\circ} 19\frac{1}{2}'$ = " " " 543	B. C.=sta. 541+58.53
$9^{\circ} 49\frac{1}{2}'$ = " " " +50	L. C.= 2.33.33
$11^{\circ} 40'$ = " " " 543+	E. C.=sta. 543+86.86
86.86	

$100-58.53=41.47 \times 3'$ (def. for 1 ft. of 10° Cur.)=124.41'
 $2^{\circ} 19\frac{1}{2}'$ =def. for sta. 542.

Def. for 50 ft.= $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve

(These tables are published in Field Books of
KEUFFEL & ESSER CO., New York, N. Y.)



Natural Tangents

sec.	0'	10'	20'	30'	40'	50'	sec.	0'	10'	20'	30'	40'	50'	sec.	
0	0000	0020	0058	0108	0166	0245	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0538	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2300	2330	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10

sec.	0'	10'	20'	30'	40'	50'	sec.	0'	10'	20'	30'	40'	50'	sec.
80	5.6713	5.7094	5.7478	5.7865	5.8255	5.8648	100	0	8106	8157	8208	8259	8310	100
81	6.3138	6.4348	6.5566	6.6792	6.8026	6.9269	99	1	8406	8468	8530	8592	8654	99
82	7.1154	7.2687	7.4257	7.5857	7.7487	7.9147	98	2	8706	8779	8852	8925	8998	98
83	8.1443	8.3450	8.5555	8.7769	9.0008	9.2272	97	3	9006	9089	9172	9255	9338	97
84	9.5144	9.7882	10.078	10.385	10.711	11.059	96	4	9306	9399	9492	9585	9678	96
85	11.430	11.826	12.250	12.706	13.197	13.727	95	5	9606	9709	9812	9915	10018	95
86	14.300	14.924	15.605	16.350	17.169	18.073	94	6	9906	10019	10132	10245	10358	94
87	19.081	20.206	21.470	22.903	24.522	26.332	93	7	10206	10329	10452	10575	10698	93
88	25.636	31.242	34.368	38.189	42.964	49.104	92	8	10506	10639	10772	10905	11038	92
89	57.290	68.750	85.940	114.588	171.885	343.770	91	9	10806	11049	11302	11565	11828	91

Natural Cotangents

57.5
1204.48
33

57.47

1167.09
11.65

1155.44
1172.55
1.07

1171.48

1204.15
8.49

8735
11.24
98.59

1208.12
9.33

1198.70

16.48
7.9

81.35
11.24

1206.95
7.9

81.06
3.60

04.95
3.47

1144.80
12.25

84.65
5.31

42
3.2

12.25
5.55

78.35
98.8
98.23
9.53
78.70
5.17
84.27

$$\begin{array}{r} 71.01 \\ 10.2 \\ \hline 81.23 \\ 1191.43 \\ 13.05 \\ \hline 1204.48 \\ 1179.49 \\ 1.00 \\ \hline 1178.39 \\ 71.48 \\ \hline 0.47 \end{array}$$

$$\begin{array}{r} 60.60 \\ 0.39 \\ \hline 60.21 \\ 1206.95 \\ 1.17 \\ \hline 1208.12 \\ 20.35 \\ 7.95 \\ \hline 12.38 \end{array}$$

$$\begin{array}{r} 16.48 \\ 4.4 \\ \hline 12.08 \\ 16.48 \\ 5.9 \\ \hline 10.59 \end{array}$$

$$\begin{array}{r} 49.32 \\ 11.11 \\ \hline 40.01 \\ 1145.12 \\ 3.15 \\ \hline 1147.96 \\ 1142.27 \\ 6.4 \\ \hline 1160.21 \\ 1148.67 \\ 3.9 \\ \hline 1192.55 \\ 1144.77 \\ 3.09 \\ \hline 1192.18 \\ 1146.67 \\ 50.01 \\ 3.34 \\ \hline 1146.67 \\ 49.32 \\ 50.01 \\ 1.69 \\ \hline 49.32 \\ 47.88 \\ 21.48 \\ 10.70 \\ \hline 82.18 \end{array}$$

$$\begin{array}{r} 1148.67 \\ 3.90 \\ \hline 1150.47 \\ 40.98 \\ 2.5 \\ \hline 1195.42 \\ 27.5 \\ \hline 1222.92 \\ 1144.79 \\ 17.38 \\ 1.85 \\ \hline 1166.11 \\ 18.23 \\ 19.15 \\ \hline 1185.26 \end{array}$$

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	0
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.