

2

360

№ 162

SAR#	Job #	Data	Pg. to Pg.
2	2901	Transit Notes Line A	1-3
2	"	Level + X-Sec Notes Line A	4-8

Cass County S.A.R #2 Job # 2901
 Line A.
 From TH #19 South of Backus to Motley

Curve Notes

PT 1+87.93

0+00 = R 66°30' S31°30' W.
 TH Sta 674+98 $\Delta = 20^\circ$
 PC -1+44.67 T = 187.83
 L = 332.56
 E 56.09 S 35° E

Offsets
 +87.93 = 332.16
 +50 = 292.28
 1+00 = 242.35
 0+50 = 192.43
 0+00 = 142.51
 -50 = 92.59
 -1+00 = 42.67

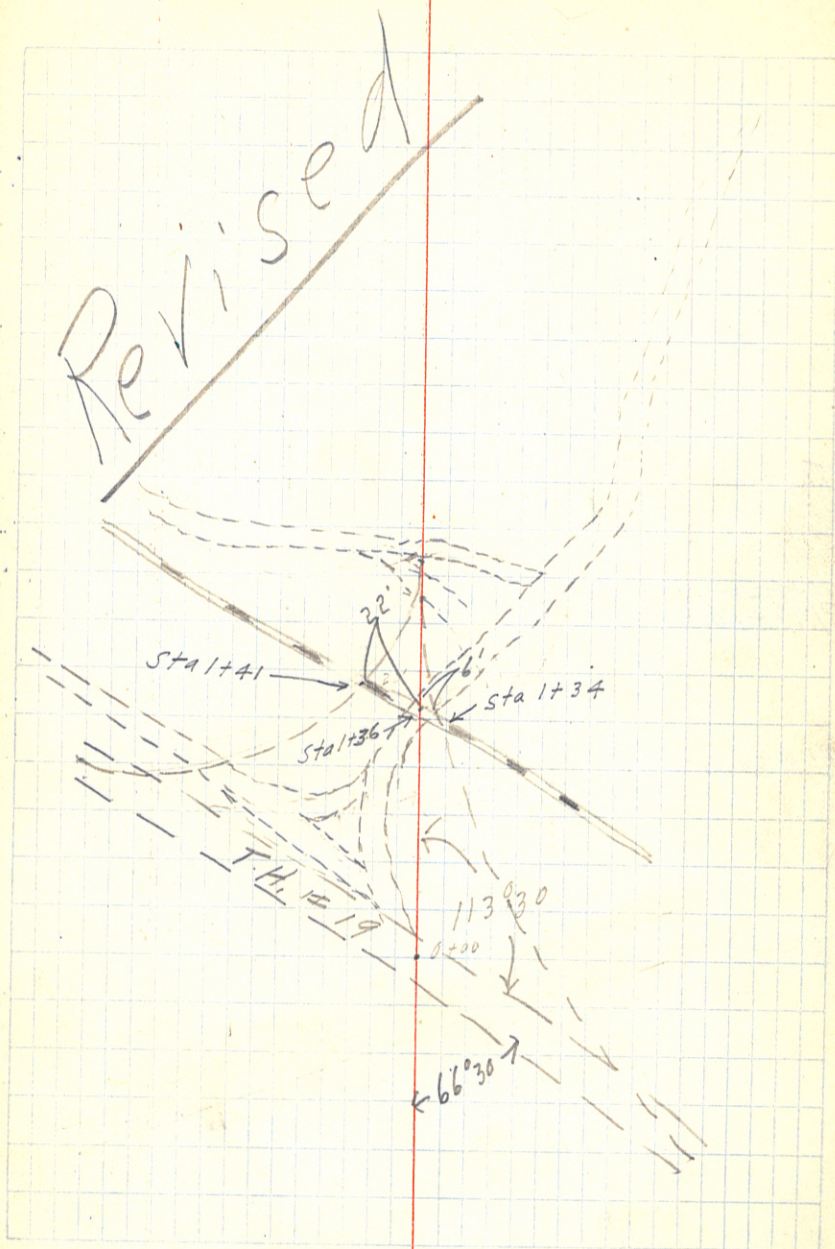
PT 2+18.48

0+00 L 113°30'
 PC -0+66.27 $\Delta = 40^\circ$
 T 218.48
 L 283.75
 E 118.01

Offsets
 +18.48 = 56.45
 2 = 53.03
 +50 = 43.13
 1+00 = 33.03
 +50 = 23.03
 0+00 = 13.03

PT 4+23.0

$\Delta = 20^\circ$
 T = 436.96
 L = 567.5
 E = 236.06



S.A.R #2 Job #
From Buckus toward Motley

Sta. Detl Angle Mag. Bearing

Revised

C.G.
O.D.

PT 16+10.81

13+21.42 Fed
P.I. 13+50.12 R 44°00' 57630'W

D = 8°
T = 289.39
L = 550.00
E = 58.25

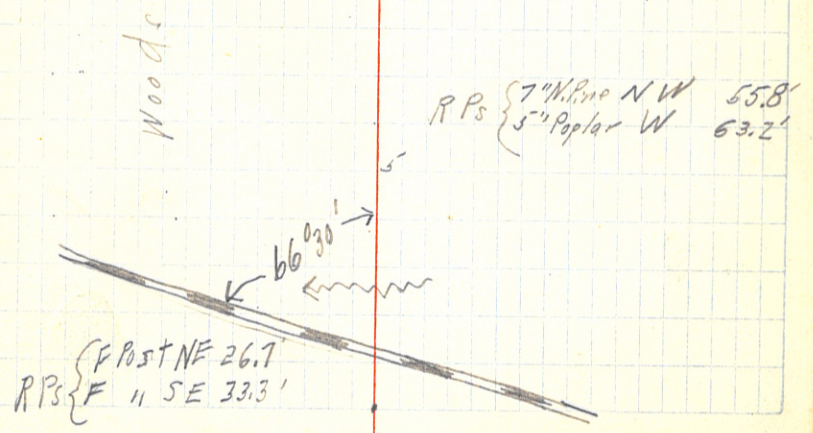
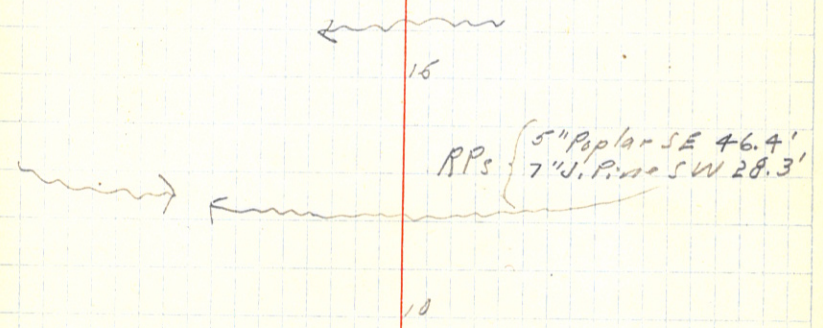
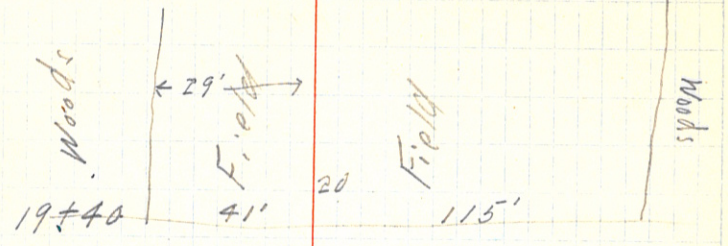
Defls.
16+10.81 - 22°00'
+50 = 190.34
15 = 17°34'
+50 =
14 = 13°34'
+50 =
13 = 9°34'
+50 =
12 = 5°34'
+50 =
11 = 1°34'

P.O.T 6+86

Sta 1+36 R.R. X-ing
Q+00 = R 66°30' 531°30'W

10-25-1928
Cool a Fair

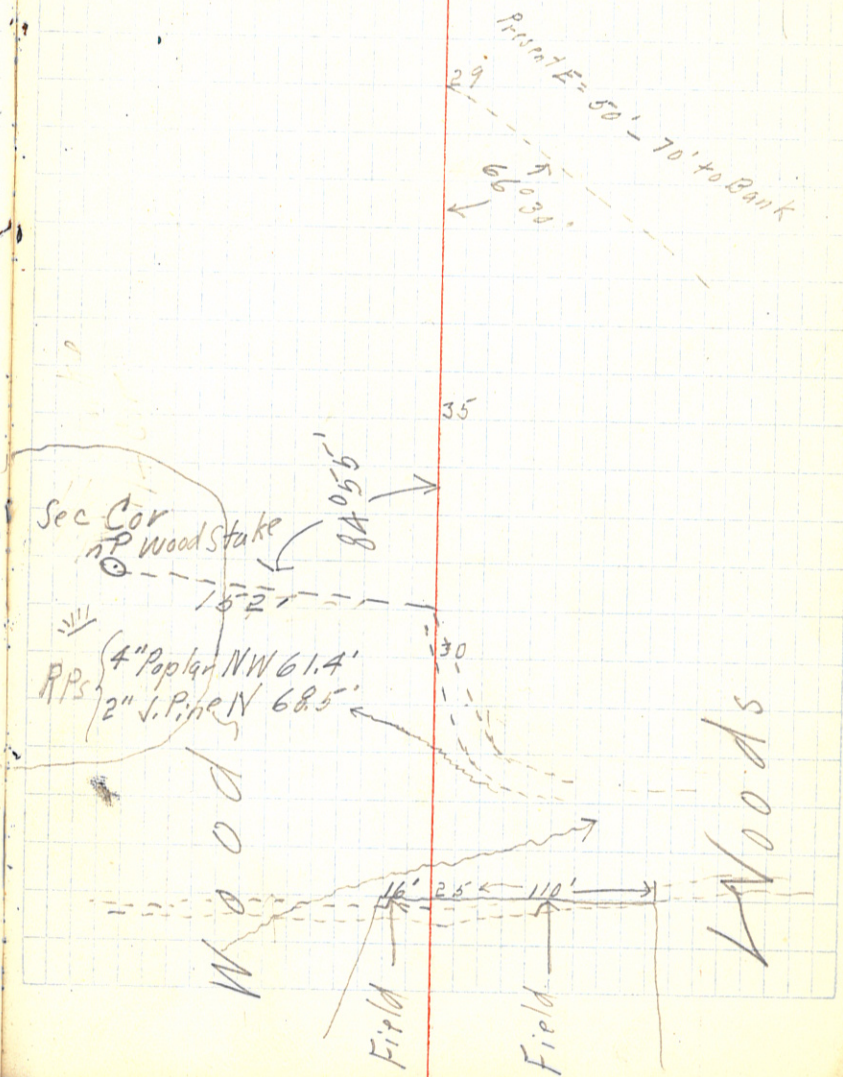
Party { Taubman *
L. French Rod
Verion Fox Chain
George Fox " } 2



Revised

P.O.T. 29473

Co. 6,
17



S.A.R #2 Job #2901

Level & X-Sec Notes

BM			
PC-0+65.27	12.7	1347.81	9.96 1337.85
0+00	13.6		35.1
+50	8.3		34.2
1+00	7.0		39.5
+50	5.5		40.8
2+00	5.9		42.3
PT+18.48	5.2		41.9
			42.6
PC-1+44.67	7.2		40.6
-1+00	7.5		40.3
-0+50	7.2		40.6
-0+00	6.0		41.8
0+50	4.8		43.0
1+00	4.9		42.9
1+34	4.5	Top of X-ing	43.3
1+50	6.2		41.6
PT+87.83	5.7		42.1
2+00	5.6		42.2
2+70	5.6		42.2
+90	3.9		43.9
3+00	1.6		46.2
TP	0.48		1347.33
+		1359.36	12.03

Revised

Party - Taubman Rod
L French Rod
Geo Fox Chain
(TH) 4

HI = 5.6

Spike in P Pole 65' R. Sta 677+30

4.3	6.6	7.1	4.6	6.6	7.0
Edge of R. 39	33	15	10	13	32
	1.4	2.3	4.7	3.4	3.7
	37	23	16	5	11
6.2	8.0	6.0	5.6	6.3	6.9
38	33	26	20	18	25
		5.8	5.3	5.6	4.5
		29	10	11	19
5.7	4.9			4.6	4.7
35	2			4	25
		6.1	5.8	5.2	3.6
		21	5	5	11
		6.6	6.4	4.7	CS
		27	18	27	
6.1	5.6	6.0	5.6	5.6	6.6
32	23	20	9	7	10
	5.7	4		9.5	2.8
	4			12	42
6.1	6.5	7.1	5.5	5.5	6.6
26	9	6	3	5	6
	7.4	7.7	8.4	4.5	4.0
	39	29	27	5	6
		8.9	6.2	13	31
		35	32	5.0	4.9
				10	23
				4.9	4.4
				14	23
				4.9	5.0
				14	28
6.1	6.0	6.4	6.0	4.6	3.6
35	25	12	10	14	28
				4.6	6.8
4.2	3.7		4.1	14	28
32	28		16	4.1	3.6
				6	23
				4.7	3.1
				10	22
				4.7	3.1
				10	22
				4.6	3.8
				18	25
				4.4	3.2
				22	30
5.7	4.8	6.1		6.2	6.2
31	23	2		1	15
					39

Edge of Road

		1359.36		
+45	6.8		52.6	
4+00	2.3		57.1	
+25	0.6		58.8	
TP	0.96		1358.90	
+		1369.98	11.28	
+50	10.5		59.5	
5+00	11.2		58.8	
+50	7.4		62.6	
6+00	0.5		69.5	
BM	4.26		1365.72	
TP	0.36		1369.62	
+		1377.98	8.36	
+50	3.8		74.2	
+86	1.5		76.5	
7+00	1.4		76.6	
+50	3.1		74.9	
+90	3.8		74.2	
8+00	4.9		73.1	
+60	9.2		68.8	
+80	10.2		67.8	
9	12.2		65.8	
TP	12.20		1365.78	
+		1366.96	1.18	

Revised

H.I. = 56

CS	5.8	30	5.0	17	4.6	36	
CS	5.7	29	5.1	34	4.7	24	CS
					5.7	30	CS
CS	6.1	31	5.0	18	6.2	30	CS
L			5.0	8	6.3	68	CS
CS	4.8	22	4.8	22	16	31	CS
CS	4.9	25	5.0	9	6.3	6.2	
					18	29	
					6.6	22	CS

On 8" J. Pine N of Sta 6+00

CS	5.5	28	6.8	24	7.8	34	CS
	5.6	30	6.2	27			L
	5.6	31	5.4	17	5.7	5.6	6.0
CS	6.0	39	6.4	31	15	26	32
CS	5.1	34	6.9	17	4.0	3.8	
CS	3.9	31	6.2	11	26	32	L
CS	3.0	24	3.0	11	5.3	3.7	3.4
					10	3.1	3.9
CS	3.5	34	4.8	17		3.7	2.6
CS	4.0	32	4.7	17		2.0	3.2
					6.1	4.0	
					12	3.2	CS
					6.7	5.2	
					15	3.4	CS
					6.3	5.8	
					19	3.1	CS

	1366.96	
+ 35	4.7	62.3
+ 75	5.5	61.5
10	7.1	59.9
+ 30	7.9	59.1
+ 50	6.1	60.9
PC+60.81	5.8	61.2
11	6.5	60.5
+ 50	6.9	60.1
12	7.5	59.5
+ 50	7.3	59.7
13	7.3	59.7
+ 50	3.7	63.3
14	3.6	63.4
+ 50	7.3	59.7
TP	9.20	1357.76
+	1361.43	3.67
15	4.0	57.4
+ 50	4.4	57.0
16	5.3	56.1
PT+10.81	5.6	55.8
+ 35	6.4	55.0
+ 60	5.9	55.5

Revised

CS	4.7	
	31	
L		
CS	5.2	5.5
	32	17
CS	4.4	
	26	
L		
L		
L		4.6
		14
CS	5.8	
	25	
	5.9	
	31	
	6.5	
	25	
L		
	5.2	5.6
	34	16
CS	7.4	
	29	
CS	8.9	
	33	
	7.0	6.0
	32	23
CS		7.0
		28
	5.7	6.0
	30	15
	5.4	5.0
CS	32	18
	5.3	5.2
	28	16
L		
5.9	5.5	
22	35	
5.0	5.5	5.1
13	27	36
5.6	4.8	CS
14	31	
	6.1	6.6
	21	30
	6.3	
	24	CS
	4.9	4.7
	18	27
	5.1	5.1
	15	28
	4.9	
	28	CS
L		
4.5	4.7	
15	32	
5.1	4.9	CS
19	31	
4.4	4.0	CS
21	31	
	3.2	
	27	CS
	5.1	3.8
	16	30
	4.5	4.2
	19	36
	4.3	3.1
	24	32
	4.7	2.8
	14	33
	6.2	5.6
	11	25
		36
		CS

	1361.43	
17	6.1	53.3
+50	5.8	55.6
18	5.9	55.5
+75	7.7	53.7
TP	7.49	1353.94
+		
BM	1361.85 7.91	1355.57
19	6.9	55.0
+40	6.5	55.4
20	5.0	56.9
21	5.5	56.4
22	5.4	56.5
23	5.1	56.8
TP	5.04	1356.81
+		
	1358.77 1.96	
24	2.4	56.4
+85	3.7	55.1
25	4.1	54.7
+60	9.9	48.9
26	5.7	53.1
+30	4.6	54.2
+65	5.8	53.0

Revised

CS	5.5	5.2
	28	16
	5.9	5.8
	30	23
	5.8	5.6
	33	13
	4.7	4.3
	34	26

H.I. = 5.6

	6.0	6.6	6.3	CS
	10	21	32	
	6.2	7.4		CS
	1.2	2.7		
	5.3	6.8	6.1	CS
	14	23	33	
		5.0		
		2.8		

On 14" N. Pine No of Sta 18+00

L	5.6
	12
	5.4
	33
L	17
	6.1
	9
	5.2
	29
	5.1
	29
L	5.2
	24

	6.2	6.0
	1.5	3.3
	4.4	4.5
	14	30
		5.1
		30
	4.9	4.8
	14	29
		5.4
		39
		CS
	5.8	5.2
	6	3.2
	5.9	5.0
	6	2.9
		6.0
		3.5
		CS

	6.9	5.9
	30	20
	8.0	6.3
	29	10
		9.0
		32
CS	2.3	4.8
	22	9
L	4.4	4.8
	29	11
	5.9	6.0
	27	18
	5.3	5.4
	32	20

	5.6	5.3
	15	34
	4.5	4.3
	15	33
	5.0	4.0
	8	3.3
	5.4	3.2
	7	2.9
	7.5	9.9
	8	10.9
		34
	5.9	6.3
	8	9.3
	5.9	2.2
	17	3.1
		6.2
		2.9
		CS

27 11.7
 TP 11.60
 +
 + 30 8.7
 + 60 10.2
 28 11.8
 + 45 12.0
 + 75 13.2
 29 12.5
 + 55 8.3
 + 73 5.0
 30 4.9
 + 40 5.9
 31 8.4
 + 45 10.7
 32 13.6
 BM 11.13

1358.77

1351.17 4.00

Revised

47.1
 1347.17
 42.5
 41.0
 39.4
 39.2
 38.0
 38.7
 42.9
 46.2
 46.3
 45.3
 42.8
 40.5
 37.6
 1340.09

H.1 = 5.6

11.1

8

4.6 5.7
 36 10
 5.2
 17
 5.6 5.7
 11 32
 5.6 4.6 5.1
 13 20 29
 6
 6.0 6.0
 32 8
 5.4
 30
 8.0 6.7
 29 11
 10.2 9.8
 34 2.3
 CS 9.1 7.6
 27 12
 CS 8.7 6.9
 31 11
 CS 11.1 6.5
 27 6
 CS 12.3 6.4
 34 16
 CS 12.0 5.8 5.4
 36 24 9
 CS 10.9 5.9
 32 22
 CS 11.1 5.5
 27 14
 CS 11.6 5.8
 21 12
 6.0 5.6
 22 33 CS
 5.1 4.5
 25 36 CS
 4.2 4.3 3.2 CS
 14 20 31
 2.6 2.0
 20 32 CS
 3.6 2.4
 14 28 CS
 4.6 2.7 2.0 1.8
 10 17 30 40
 5.2 5.2 5.2
 13 29 39
 5.5 6.1 5.2 -1.0 -0.8
 12 26 27 38 48
 6.3 4.9 -2.9 -3.3
 13 15 30 37
 5.6 6.4 -6.8 -7.0
 4 9 31 35 L
 5.6 6.1 -6.9 -8.4 -9.1
 5 9 32 39 43 CS
 5.6 5.9 -2.0 -5.1
 6 11 27 42 CS

On Tel. Pole Soft Sta 30+00

Level Notes Line "B"

BM		1348.95	11.10	1337.85
0+00	7.5			41.5
1+00	6.4			42.6
1+27	5.6			43.4
2	5.8			43.2
3	0.4			48.6
TP	0.27			1348.68
+		1357.08	8.40	
+30	6.9			51.2
+75	7.1			50.0
4	4.4			52.7
+30	1.5			55.6
5	1.2			55.9
TP	0.97			1356.11
+		1368.49	12.38	
+40	12.5			56.0
6	5.8			62.7
TP	0.26			1368.23
+		1380.26	12.03	
+65	10.2			70.1
7	8.5			71.8
+20	6.8			73.5

~~Revised~~

P.R. X-ing

1390.24

+75	5.7
8	3.3
+25	2.2
+75	2.0
9	2.5
+55	4.2
10	7.0
BM	10.52

74.6
77.0
78.1
78.3
77.9
76.1
73.3

on 9" J. Pipe No. 2 Sta 8+60

12

S.A.R. #2 Job # 2901
 From T.H. #19 South of Backus - West
 Transit Notes

Sta	Defl	Angle	Mag B.	Com. Bearing
-----	------	-------	--------	--------------

PT 2+05.26				584°W
1+33				
P.I. 0+00 =				
TH 675+46	R	110°41'	575°15'W	
PC - 0+70.32	$\Delta = 40^\circ$			
	T = 205.26			
	L = 275.58			
	E = 107.22			

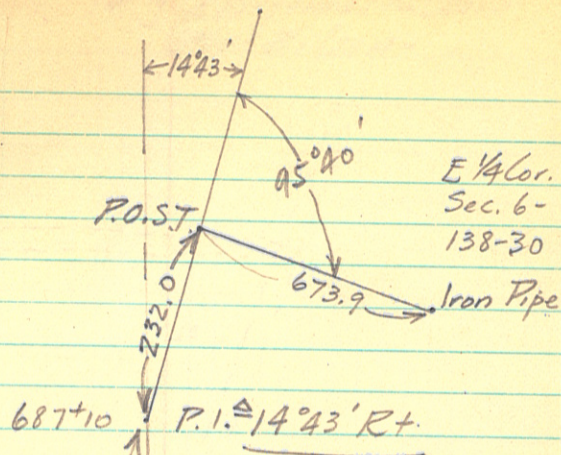
PT 1+99.74				
P.I. 0+00	L	69°46'		
	$\Delta = 20^\circ$			
	T = 199.74			
PC - 1+49.09	L	348.83		
	E	62.75'		

DEFLS

2+05.26	-55°07'
1+33	-40°04'
0+00	-34°04'
0+50	-24°04'
0+00	-14°04'
0+57	-40°04'

DEFLS

1+99.74	-34°53'
0+00	-29°55'
0+00	-29°55'
0+50	-19°55'
0+00	-14°55'
0+50	-9°55'
1+00	-4°55'



E 1/4 Cor.
 Sec. 6-
 138-30

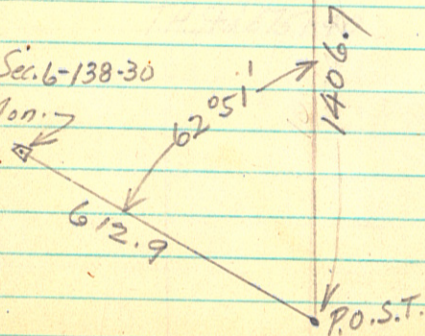
Iron Pipe

P.I. $\Delta = 14^\circ 43' RT$

675+40 P.O.T.

"V" line
 S.P. 19-24

NE Cor. Sec. 6-138-30
 Conc. Man. 7



S.A.R. #2 Job # 2901
 From T.H. #19 South of Backus - West
 Transit Notes

Sta Defl Angle Mag B. Com. Bearing

PT 2+05.26
 1+33
 P.I. 0+00 =
 TH 675+40 R 110°14' 575.75 W
 PC -0+70.32
 Δ = 40°
 T = 205.26
 L = 275.58
 E = 107.22

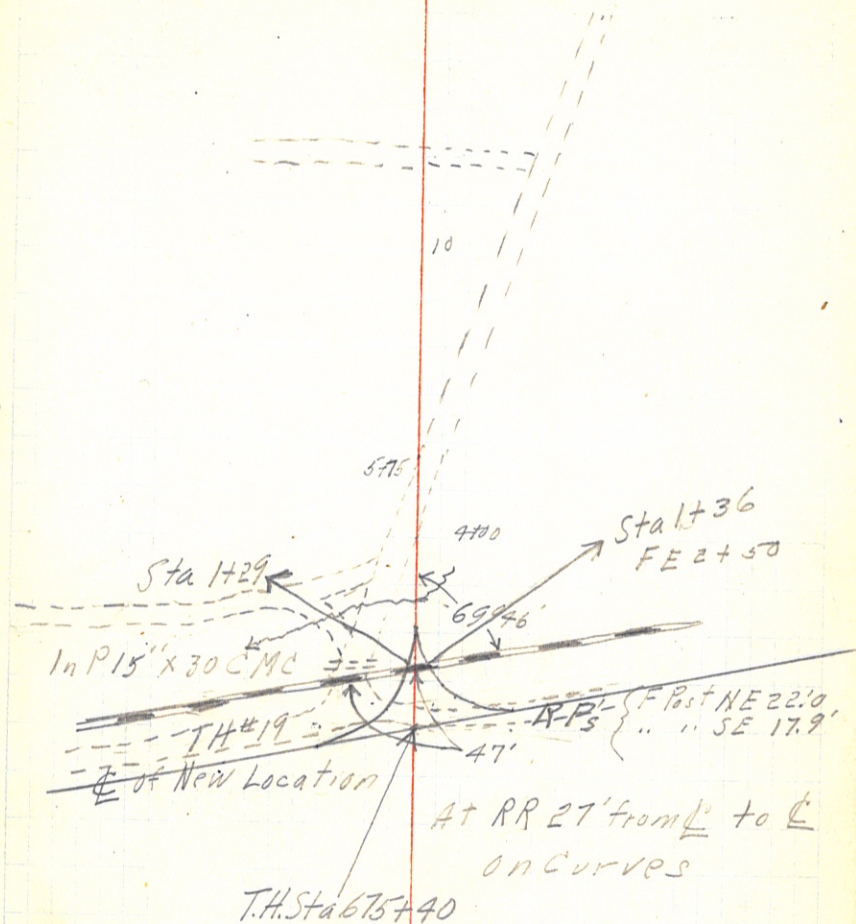
PT 1+99.74
 P.I. 0+00 L 69°46'
 Δ 20°
 T 199.74
 PC -1+49.09 L 348.83
 E 62.75'

584° W
 Details
 E+0526-55°07'
 +50-44°04'
 Δ = 32°04'
 0+50-24°04'
 0+00-14°04'
 -0+57-40°04'

Details
 +99.74-34°33'
 +60-29°55'
 Δ 20°
 1+00-29°55'
 0+50-19°05'
 0+00-14°55'
 -0+50-30°55'
 -1+00-40°55'

11-8-28

Party (A. R. Taubman - T 13
 R. Vaegemast - Chain
 Steve Wilson - "



PT 38+85.78

P.I. 36+52 = R 28°40' 58.195W

D=6°
T=244.0
L=17.78
E=30.68

PC 34+08

L=17.78
E=30.68

PT 27+64.4 = +77.4F

P.I. 25+92.4 = R 28°06' 55.2°00W

PC 24+13.15 D=8°
T=179.25
PT 23+69.99 L=35.125
E=22.1

P.I. 20+30 = L 51°20' 52.3°50'

D=7°
T=393.34
L=733.33
E=89.6

PC 16+36.66

P.O.T. 15+28.5

PT+85.78=1420'

38=114.6

37=84.6

36=54.6

35=24.6

34=24.6

33=12.5

Defls

PT+64.4=1403'

27=1102.8'

+35=80.42'

26=702.8'

+50=502.8'

25=302.8'

Defls

+85=2032'

+55=140'

PT+64.99=2024'

23=230.99'

+55=270.24'

22=190.24'

+50=180.04'

21=160.19'

+50=140.39'

20=120.49'

+50=110.04'

19=90.19'

+50=70.39'

18=50.49'

+50=40.04'

17=20.19'

+76=102.7'

Defls

Revised
Sta 19-40
Pg 15

R.P.S. { 4" Post SW 27.5'
" " SE 21.6'

← 263' → 30

R.P.S. { 10" Pine S 50.1'
3" " " SE 24.1'

Revised
Sta 16-40
Pg 15

In P 18" x 30' CMC

R.P.S. { 5" Poplar SW 44.2'
4" " " SE 50.2'

132
127'