

337

E	L	A	N
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Field Book

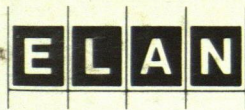
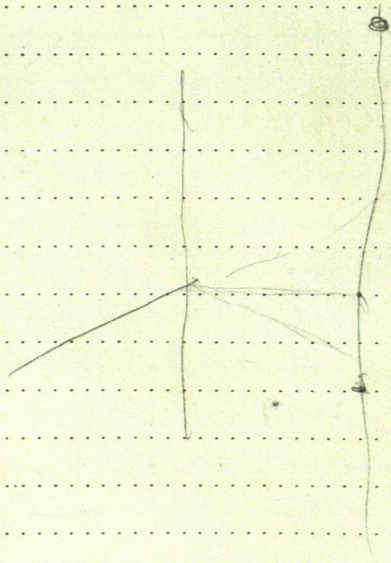
E 64-8x4

*small Red Field Book*

300,43

319,55

Projects



Publishing Co., Inc.

Meredith, N.H. 03253



7 0 4 3 3

10 6 B5 4

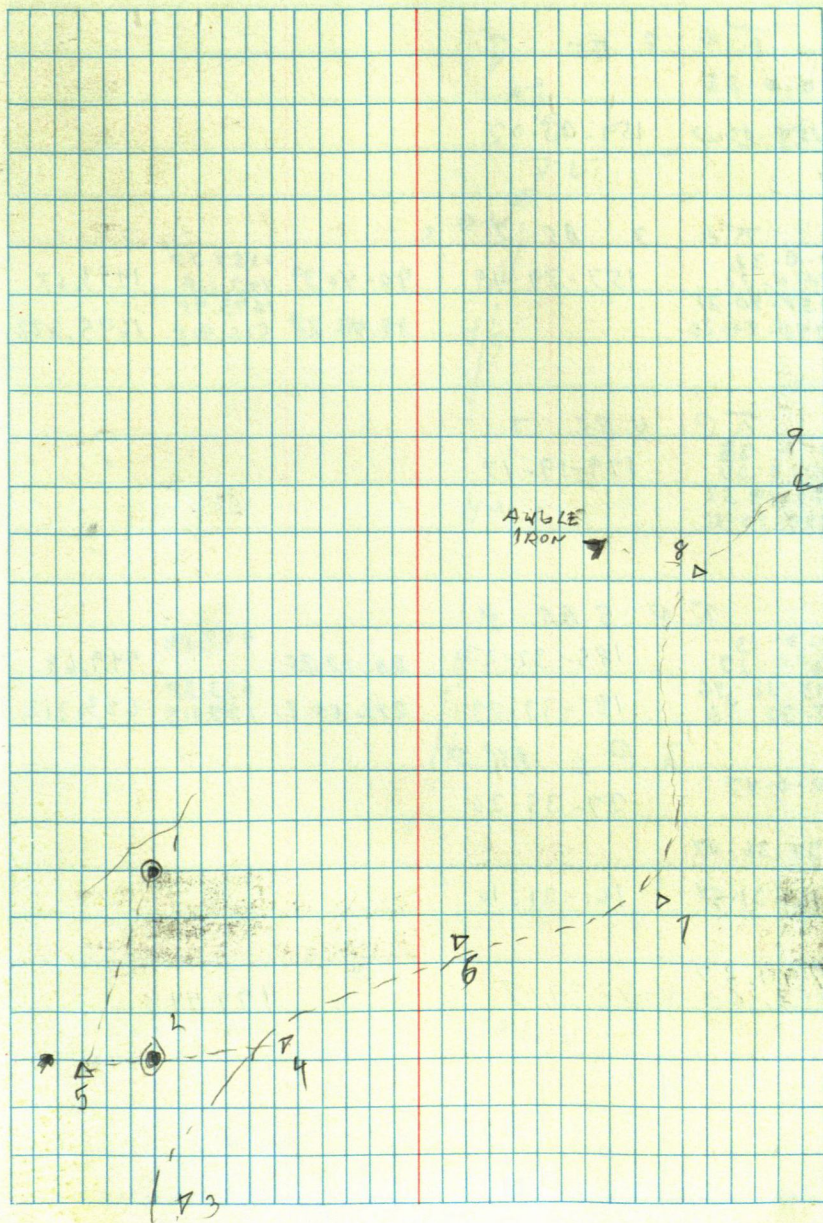
7	33	4
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$\overline{\Lambda} @ 8 \text{ BS } 7$

E EDGE POST

$\bar{\lambda}$  @ 5 BS

0.0.15		270.99	
180.0.16	58-30-57	90.41.34	270.966
58.31.12		82.596	
4238.31.13		149.828	
		89.14.39	149.828
		45.669	





$\pi @ 2 BS 3$

0-0-25

159-03-27 159-03-02

$\pi @ 3 BS 25$

0-0-32

180-0-31

157-40-21

4 347-40-20

157-39-49

90-40-39

1453.77

442.114

1695.91

1453.67

89-42-28

516.915

1695.883

$\pi @ 4 BS 3$

0-0-35

180-0-34

179-19-52

5 357-19-31

179-19-17

$\pi @ 5 BS 4$

0-0-13

180-0-13

185-32-36

6 5-32-36

185-32-23

88-12-25

449.89

449.69

185-32-23

271-55-21

633.57

192.113

633.212

$\pi @ 6 BS 5$

0-0-47

37-35-20

37-36-07

161-21-57

161-21-10

499.87

152.360

V-87.39.12

499.448

8  
36.49  
36.49  
36.49

5

4

3

2781.5 CULV



7+50	28" MAPLE	19' RT	
9+03	8' ASH	19' RT	
9+40	7" BIR	19' RT	
10+70	12" ELM DEAD	16' LT	
14+63	18" BASSWOOD	18.5 RT	
16+			
26+06	16" MAPLE	18' RT	
26+50	CLUMP 5 BASSWOOD	15' RT	
26+75	20" BASSWOOD	18' RT	
27+25	CLUMP 3-20" BASSWOOD	16' LT	
27+55	TWIN 20" BASSWOOD	16' LT	
28+45	CLUMP BASSWOOD	19' LT	
28+60	12 BASSWOOD	18' LT	
30+00	26" WO	12' LT	
<del>23+00</del> 23+50	14" ASH 8" MAPLE	15' LT	
23+70	20" BASSWOOD	15' LT	
BM	5.95	100.00	SPK IN 18" WO 25' LT
	HI: 105.95		32+60
32+0			
34+00			
32+55			
33+00			
TP	0.87	HI 93.57	13.25 92.70

TP	0,30			82,55	11,02		± 35+00
	8,2	8,2	5,6	5,05	5,2	7,0	7,2
	40	20	9	0	10	20	40
	79,7	77,7	82,3	82,90	82,70	80,9	80,7
							CULVERT
							36+43

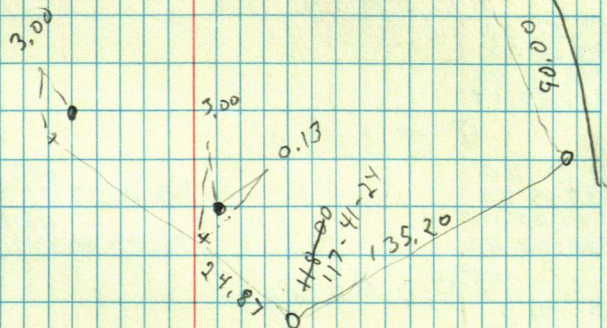
8,7	5,7	4,8	4,98	4,9	4,0	1,0
40	20	9		14	20	40
97,25	100,25	101,15	100,97	101,05	101,75	104,35
10,0	7,3	6,3	5,4	5,5	3,8	1,5
40	20	9,0	6	9,5	20	40
95,95	98,65	99,65	100,35	100,45	102,15	104,45
8,1	5,6	5,0	6,6	6,7	6,4	3,5
40	20	14	9,5	0	9,5	20
97,85	100,35	100,95	99,35	99,55	99,25	99,55
8,5	7,7	7,6	8,8	8,4	8,8	8,2
30	20	14	9	0	9	20
97,45	98,25	98,35	97,75	97,55	97,15	97,75



SHARON READ

PINE RIVER

4





BILL GANZ

0.0.28	1820.45
180.0.28	554.871
277.10.54	711.48
3 97.10.54	90.21.49 216.863

TE 3 B52

0.0.27  
180.0.27  
200.10.43  
4.20.10.43

TE 4 B53

0.0.22	1097.60
180.0.22	91.06.49 334.548
205.20.05	709.07
5 25.20.05	91.30.21 216.125

TE 5 B54

0.0.32  
180.0.32  
142.32.40  
6 322.32.40

TE 6 B55

0.0.20	843.17
180.0.22	90.20.37 257.000
144.03.04	484.74
7324.03.06	90.20.40 147.750

TE 7 B56

0.0.23  
180.0.23  
157.26.25  
8 337.26.25

TE 8 B57

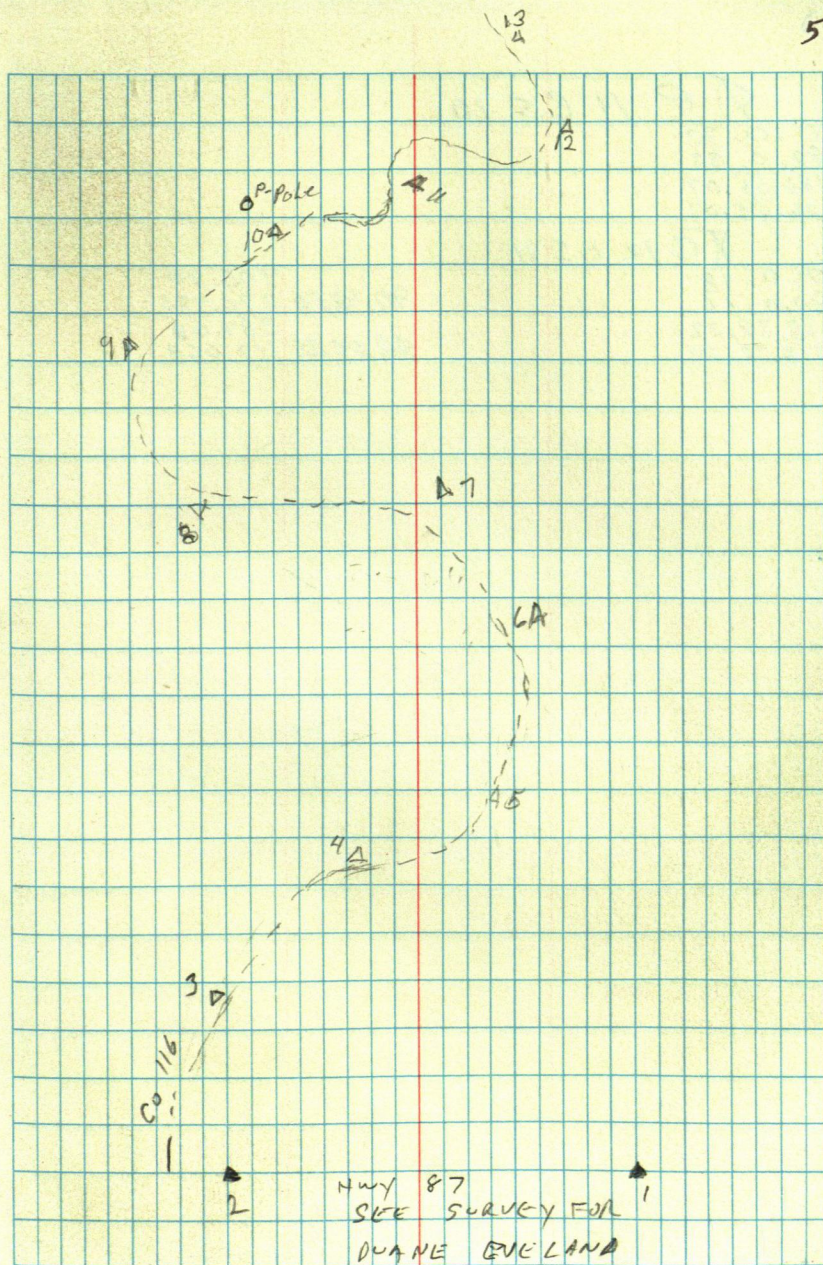
0.0.32	1268.72
180.0.33	91.27.52 386.705
201.06.07	636.72
921.06.08	92.13.06 194.071

TE 9 B58

0.0.17  
180.0.19  
193.36.54  
16 13.36.55

TE 10 B59

0.0.09	1703.05
180.0.09	91.46.20 519.091
188.09.52	754.31
11 08.09.52	91.57.28 229.914





DE 11 BS 10

0.0.33  
180.0.33  
184.55.07  
1206.55.07

XC 12 BS 11

0.0.18  
180.0.14  
138.32.22  
13318.32.20

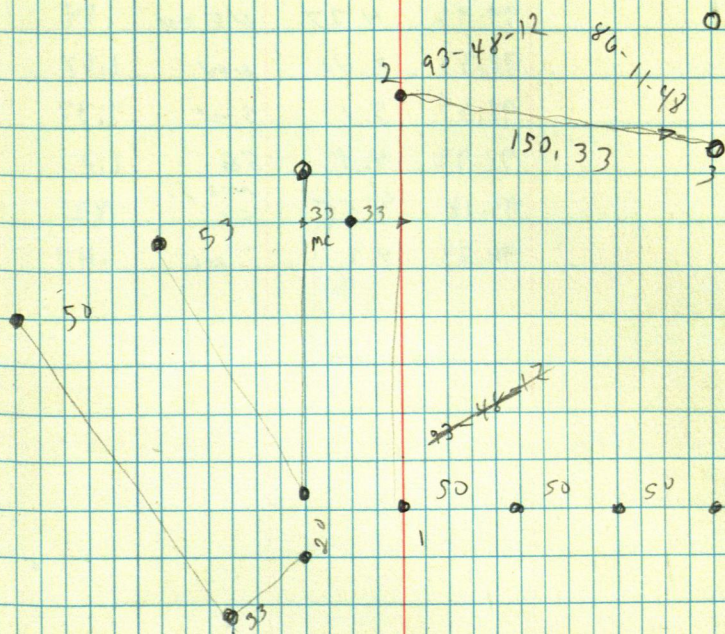
906.90  
90.4850 276.425  
384.08  
98.55.35 117.068



1 0 2 0 5 1

93.48.12

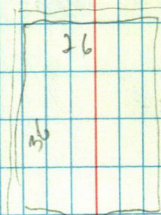
3





## BLDG CORNS

BM	3.73	FLOOR OF OFFICE		
	103.73			
	99.46	4.27	NE COR	.54
	98.33	5.40	NW	1.67
	98.63	5.1	SW	1.37
	98.93	4.8	SE	1.07
	99.18	4.55	MID PT SL	.82
	99.53	4.2	" NL	.47



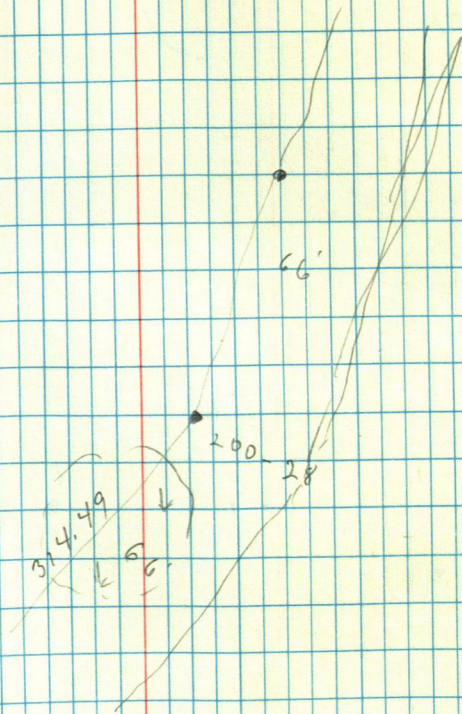






OTTER TAIL PEN. Twp

10





TC 2 BS 1 3

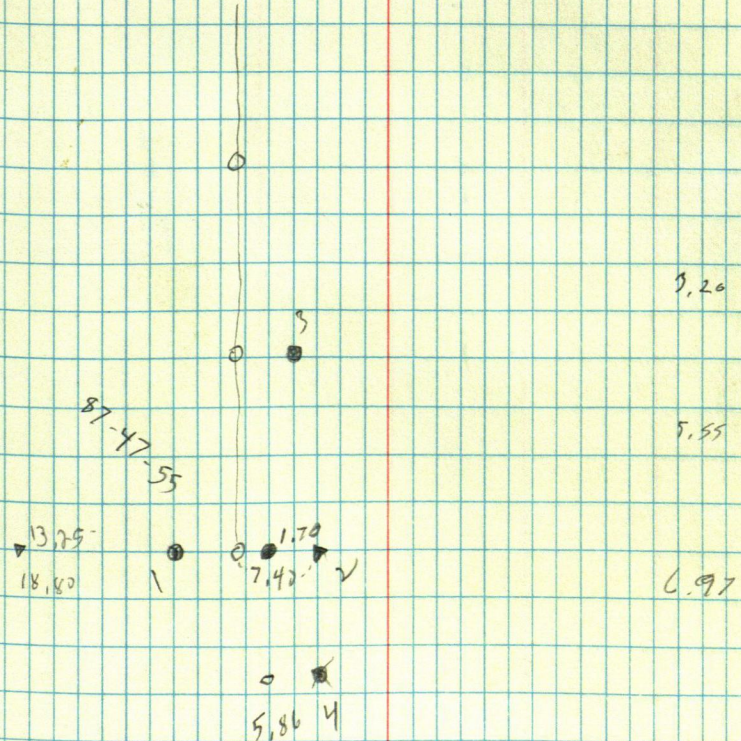
386.25,30

4257.51

155-41-15

90.05.30	131.65 40.126	131.646
7100.27.30	103.69 31.592	101.947
90.17.00	129.03 42.377	139.029

18.80  
13.25  
5.55





11  
T @ 1 BS 2

797.20  
902.24 242.985 797.194

2  
1.9

0

0

0

0

1

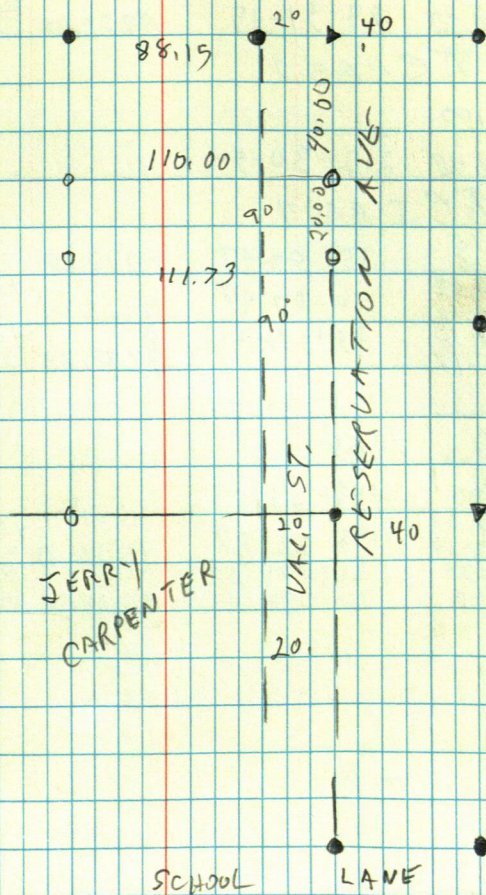
•



BILL HANSEN

LONGVILLE

13





BILL HANSON

T@ 2 BS 1

~~T@ 2 BS~~

266.51.30	158.32	158.088
	48.269	

3

269.29-18	1271.21	1271.161
	387.469	

T@ 2 BS 3

8321.36

4 167.02.30	83-31-15	89.23.42	234.25	236.236
			72.009	

T@ 4 BS 2

212.31.00

5 65.01.48 212-30-54

T@ 5 BS 4

0 0.15			155.51	
180.0.15	154-07-47	90.13.10	47.401	155.511
154.08.02			124.66	
6 234-08-02	154-07-47	90.13.14	38.005	124.673
7 234.13.18	234-13-03	94.32.38	172.40	
54-13-18			52.550	171.865

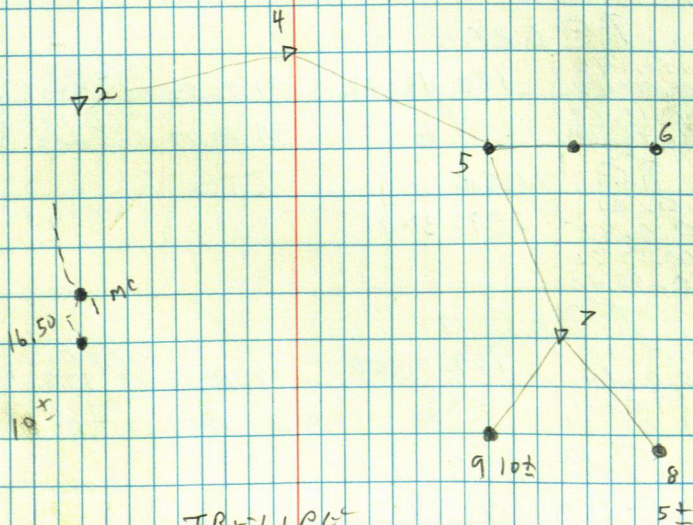
T@ 7 BS 5

0-0-33				
180-0-33	145-23-02			

8 145-23-35	145-22-57	90-32.43	138.19	138.164
385-23-30			42.109	
213-0-35	213-00-02		78.89	
9 33-0-15	212-59-42	91-35-38	27.562	73.972

3 SEC COR  
BACK OF OLD  
STONE PILLARS

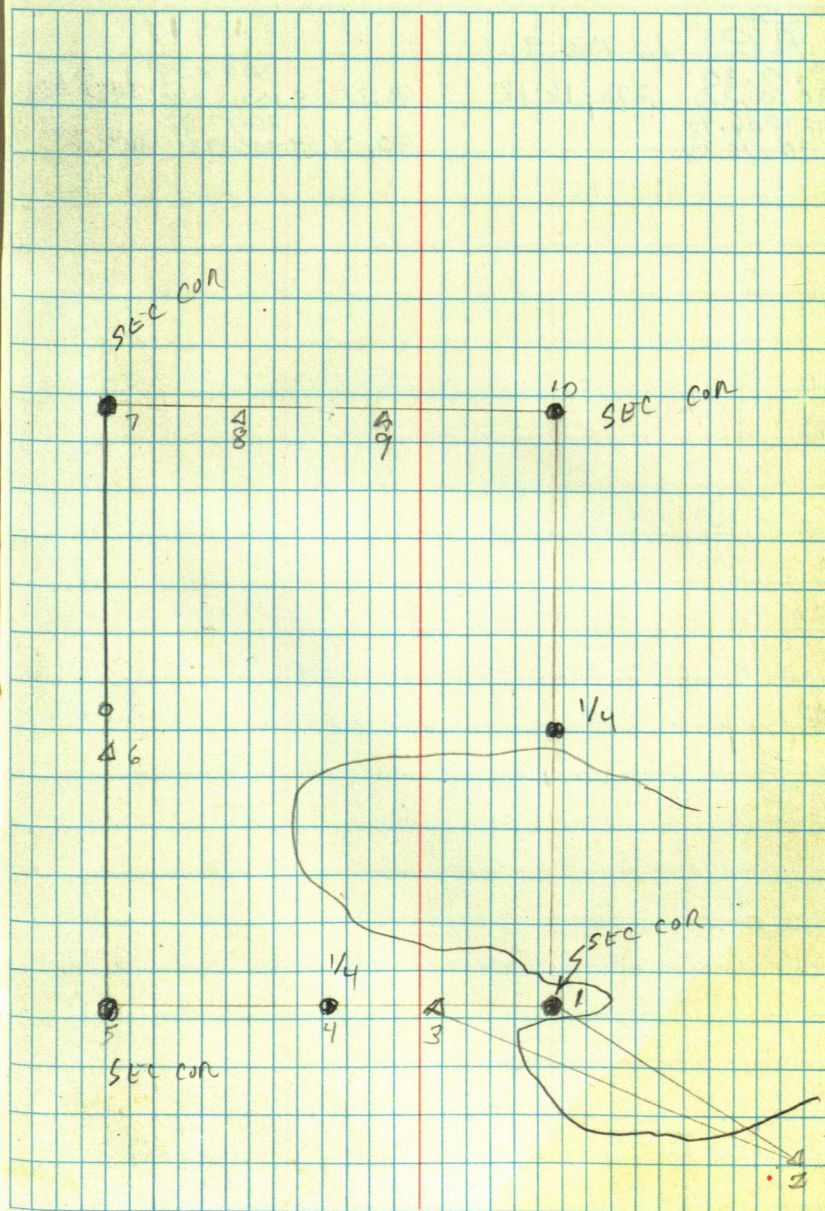
1429.24



TRELLIS

LH







0.0.30	10 1359	3422.14	
180.0.30	270-16-18	90.35.49	3421.953
11) 270.16.48		10.43.076	
90.16.48		2647.42	
		90.53.07	2647.093
		806.934	



2 BS 1

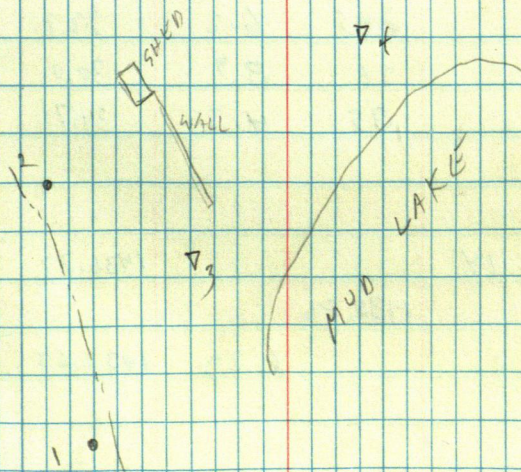
324-14			322.30	
3 288-28	324-14	90.53.36	78.236	322.258
		91-20-06	176.87	176.821
			53.91	
BM	5.15	HI=1437.78	1432.63	TOP PIPE #1 TRV. PT
224-10		78'	3.0	34.8
294-50		45	5.7	32.1 NW COR SHED
308-05		65	6.1	31.7 SW COR SHED
328-		70	4.2	33.58
TP		4.80	1432.98	TOP WALL END

3 BS 2

94.27.18				
4 188.53.36	94-26-48			
TP	0.81	HI=1433.79		TOP WALL
63-40		23	3.5	30.3
94-00		123	3.1	30.7
	50' LT		1.0	32.8
	3' HIGHER	90' LT		35.8
		8.0	1425.79	TOP WATER MUD LK
TP	6.31	4.75	1429.04	
		1435.35		

4 BS 3

147.42.00		90.12.54	435.15	435.146
5 295.23.40	147-41-54	89.08.30	132.634	
			227.40	
			69.312	227.374





187-10		285	2.8	32.6
156-04		160	2.5	32.9
41-		92	7.8	27.6
41-		185	7.4	28.0
TP	8:70	141 = 1438.91	5.14	1430.21
	A @	5 B 5 Y		1430.21
49-30		82	10.0	28.9
91-		180	<del>10</del> 6.7	32.2
115-20		178	2.9	36.01
146-0	88-16	200	5.0	40 <del>38.71</del>
172-10	88-24	200	5.0	40 <del>38.71</del>
193-20		208	3.7	35.2
221-40		205	6.2	32.71
96		56	8.9	30.0
0		35	4.2	34.71

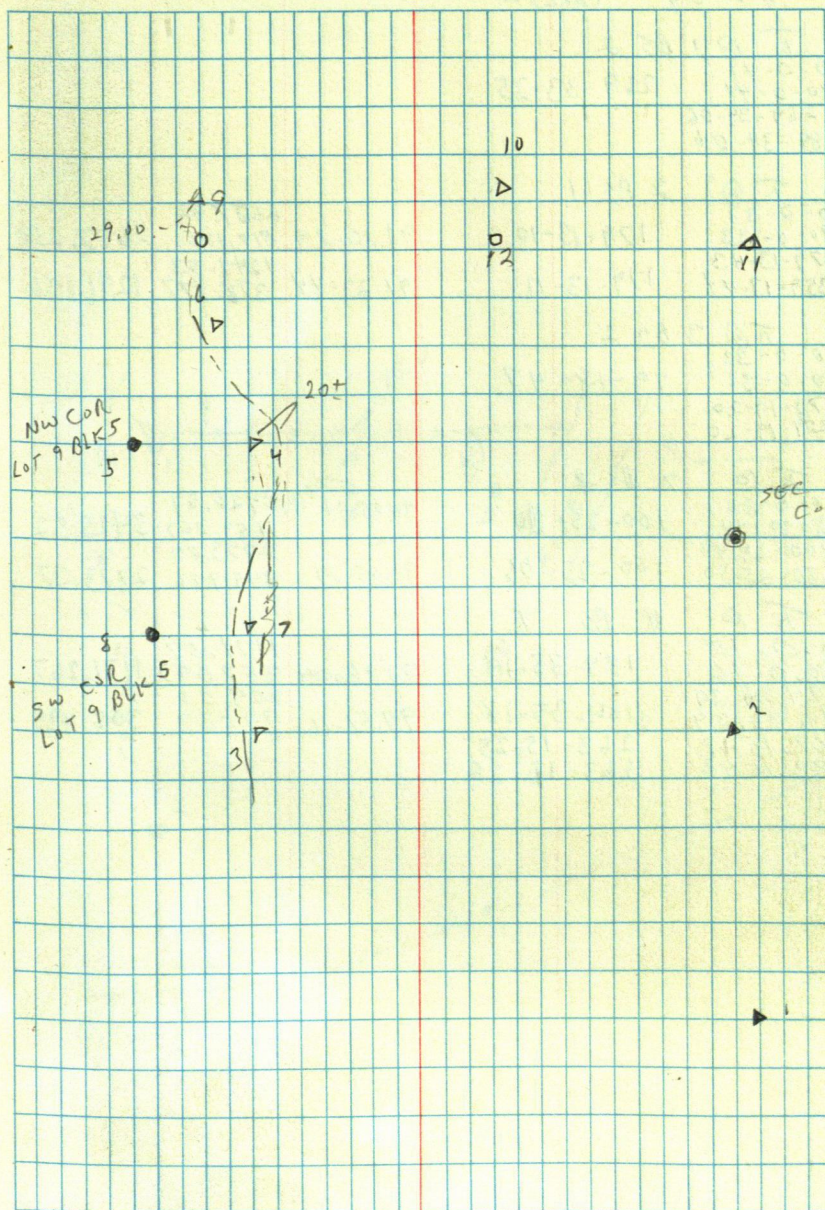
Bm	2.14		1436.72	Top 1440
		1438.86		
Bm		6.23	1432.63	Top Pipe



FRED Mc GREGOR

AKELBY

A @ 2 BS 1			
0.0.25		1056.15	
180.0.26	69-25-44	91.14.22	321.912
69.26.09			1055.894
3) 249.26.10		91.33.21	662.28
			201.866
Te 3 BS 2			
0.0.14			
180.0.16	265-58-22		
265.58.36			
4) 85.58.38			
Te 4 BS 3			
0.0.10			
180.0.10	100-20-56	92.09.27	431.56
100.21.06			131.539
5) 280.20.06			431.251
172.59.50	172-59-40		33.20
6) 352.59.50		90.47.39	124.11
			37.830
		270.10.59	203.26
			41.954
			203.259
A @ 7 BS 4			
0.0.08			
180.0.08	282-28-59		41.92
8) 282.29.07			
102.29.7			
Te 6 BS 4			
0.0.06			
180.0.07	202-55-58		
202.56.04			
9) 22.56.05			
Te 9 BS 4			
0.0.18			
180.0.18	268-47-27	91.37.41	236.91
268.47.48			72.218
10) 88.47.45		91.42.44	387.03
			117.966
			386.854
Te 10 BS 9			
0.0.06			29.00
180.0.06	280-24-19		
280.24.25			
11) 100.24.25	280-24-19	91.08.02	340.16
291.14.17	291-14-11		103.681
12) 111.14.17	291-14-11	91.08.00	44.49
			13.562
			44.484





NANCY CARLSON ?

1 @ 1 BS 2

0-0-41  
180-0-41 269-33-25  
269-34-06  
4 89-34-06

1 @ 2 BS 1

0-0-33  
180-0-33 179-13-10 91.10.29 2657.82 810.106 2657.254  
179-13-43 1241.53  
3 359-13-44 179-13-11 91.23-44 378.487 1241.156

1 @ 3 BS 2

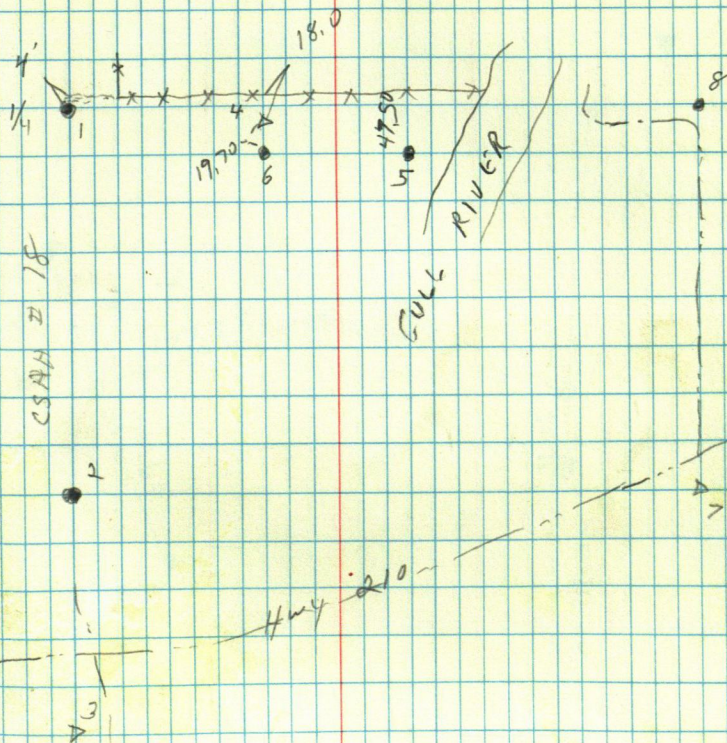
0-0-33  
180-0-33 79-18-47  
79-19-20  
7 259-19-20

1 @ 7 BS 3

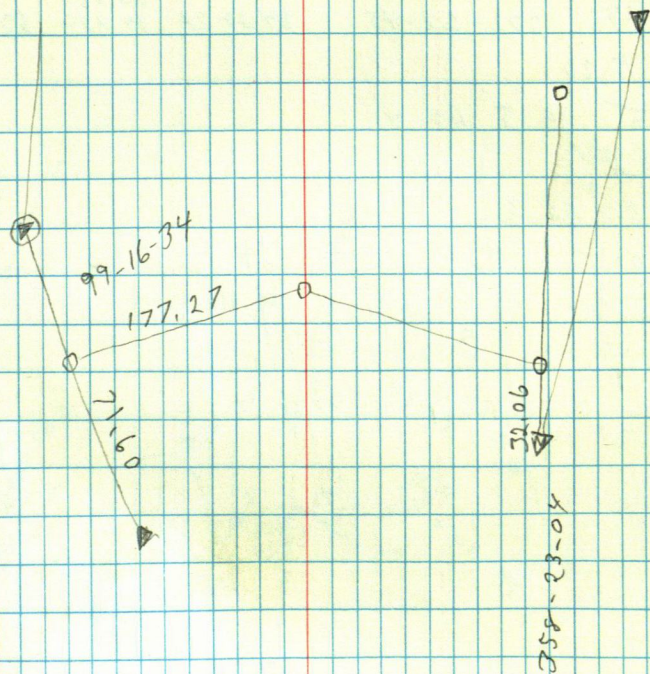
0-0-20  
180-0-44 100-25-90 91.05-11 5426.51 1654.007 5425.52  
100-25-40 2773.89  
8 280-25-50 100-25-06 91.05-11 845.476 2773.37

1 @ 4 BS 1

0-0-15  
180-0-16 184-35-19 91.12.04 1171.57 357.097 1171.267  
184.35.34 309.61  
54.35.34 184-35-18 94.51.11 74.267 308.495  
263.15.40 263-15-25  
6 83.15.40 263-15-25









VAC. PROP

140-29

SEC 23

T @	2 BS	1
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259,26.06      259-26-03

3 168.52.05

TC 3B52

109,54.30	109-54-43	88,37.06	89,49 27,280	89.469
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4 219,49,24	88,55,06	131,70	40,141	131,674
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7 @ 4 Bs 3

272-23	272-22-45	84.28.24	63,88 19,470	63,582
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5 184-45-30

T @ 5 BS 4

86-12-24

$\pi \in \mathcal{B}_S \quad 2$

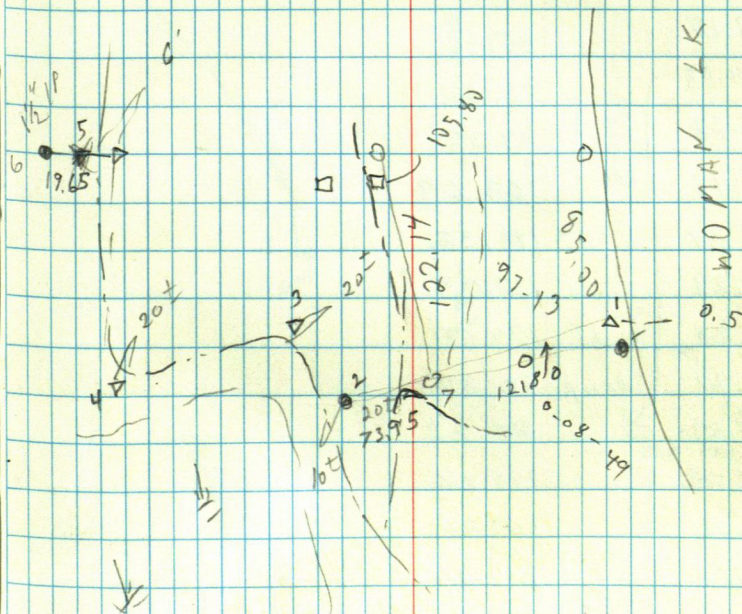
83-00

E. C. W. R.

B. CURD

7-20-95

22





BEASLEY

TEN MILL LK

T @ 2 BS 1

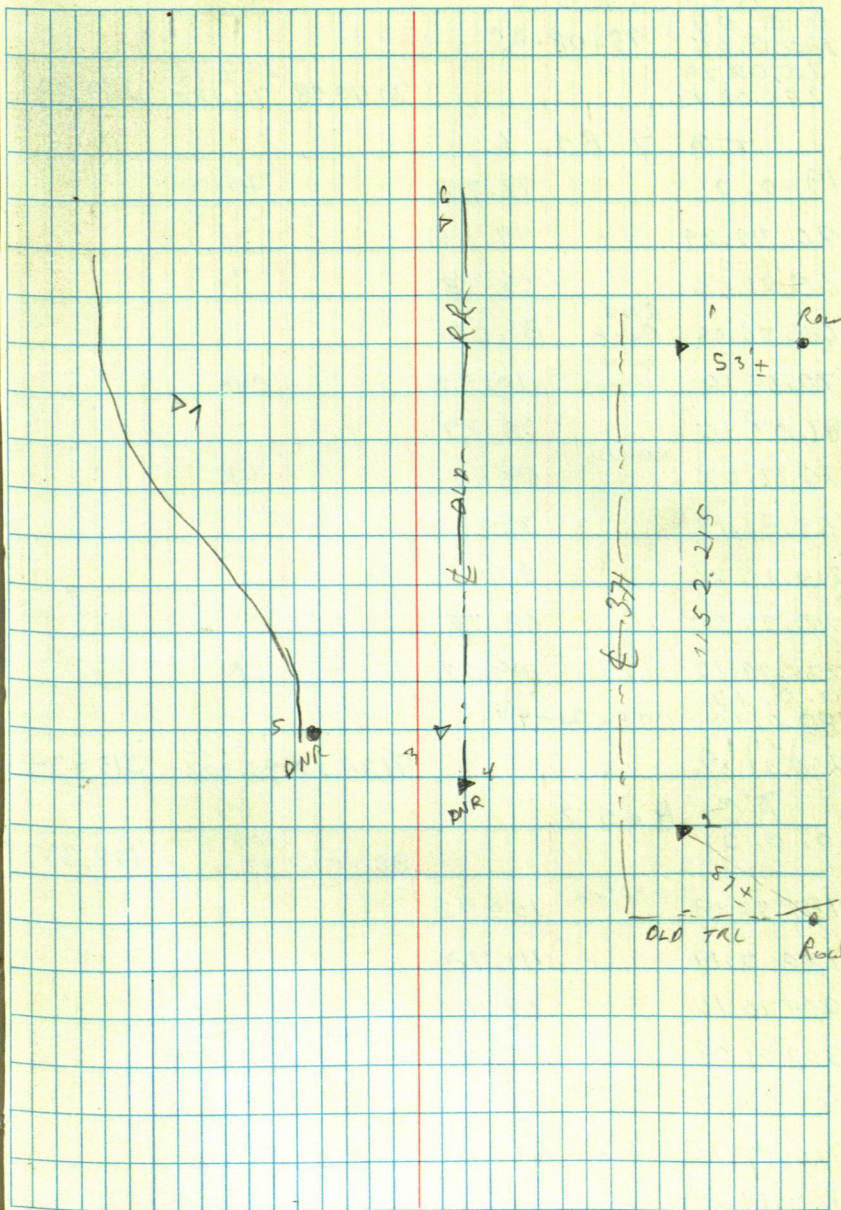
0-0-47  
 180-0-47 325-57-59  
~~325-58-46~~  
 3 145-58-46 325-57-59

T @ 3 BS 2

0, 0, 22  
 180, 04, 22 88.50.49 358.16 358.07 4  
 13.55.56 13-51-33 20, 20  
 124, 01, 32 123-57-10 63.01  
 5 304, 01, 32 96.43.02 19.206 62, 578  
 217, 57, 51 217-53-29 398.24  
 6 37.57.51 90.02.10 121.381 398, 234

T @ 6 BS 3

0.0.04  
 2 73.08.17 35.01  
 3 56.54.38 48.11  
 4 59.56.32 84.33  
 5 62.51.45 108.63  
 6 68.13.07 118.38  
 7 80.21.29 132.03  
 8 91.46.23 Right 174.67  
 9 95.17.47 Swamp 201.82  
 10 98.30.39 185.27  
 11 104.55.08 175.66  
 12 111.48.21 159.84  
 13 123.04.32 146.90  
 14 34.47.03 Left Swamp 66.15  
 15 39.23.09 76.04  
 16 37.07.09 Mound 103.20  
 17 45.32.51 135.51





XC CBS 3

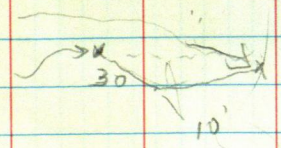
0.0.04  
180.0.04 75-08-25  
75.08.29  
7 255.08.29 90.40.08 249.95 76.184 249.931

XC 7 BS 6

18 19.0.0 73.74 H  
19 26.42.29 44.55 "  
20 60.21.56 69.78 "  
21 65.56.08 END Deck 83.64  
22 70.59.18 Small House 110.92 CAB  
23 86.07.16 98.72 "  
24 126.17.02 WATER 59.40 LK  
25 153.36.19 39.81  
26 214.16.26 37.91  
27 259.29.25 68.72  
28 275.23.12 109.72 LK  
0.0.10  
180.0.10 70-21-46  
90.21.56  
250.21.56 91.34.35 315.96 96.302 315.834

XC CBS 7

0.0.21 88.35.53 108.37 33.031 108.337  
29 187.52.18 water 153.72 LK  
30 188.0.19 111.90 "  
31 204.10.14 62.94 "  
32 302.21.03 63.83  
33 101.52.37 Swamp 94.82  
34 116.52.14 82.42  
35 154.19.24 82.91





36 170.19.34 Swamp 106.65

XC 9 B 57  
0.0.15

37 13.17.15 81.41 SwP

38 25.04.12 56.92 "

39 55.51.10 37.13 "

40 76.30.06 41.00 "

41 256.57.40 water 32.85 LK

XC 6 B 53

0.0.24  
180.0.24 101-45-36

101.46.00  
10281.46.00

XC 10 B 54

0.0.25  
180.0.25 88.07.00 233.43 233.301

253.52.01 253-51-36 46.13  
H 73.52.01 90.50.17 14.059 46.122



PINE RIVER

ALMIRA RILEY

5

Q

N

T @

1

BS 2

EDGE

DITCH

DITCH

EDGE

EDGE

DITCH

1	14.15				
	33	12.60	6.20	8.90	14.0
2	58.15	9.30	2.50	11.0	16.50
		<del>8.50</del>	<del>2.0</del>	<del>10.7</del>	<del>15.60</del>
3	127.40	9.50	2.0	10.7	15.60
4	204.20	13.50	8.0	8.0	15.0
5	248.30	10.0	17.0	0	11

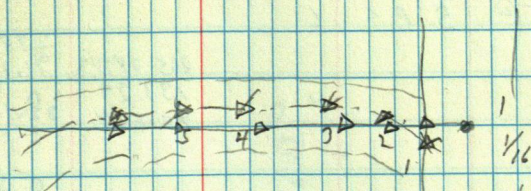
6

7

8

9

26



87-41-40

ALK  
TOP

2



T @ 1

3

T @ 5 B S L

85-17	523.86	522.08
	159.677	<u>66.026</u>
	278.90	588.109
265.08.42	91.110	297.834
133.29		
42.628	82-12-54	132.063
		429.898

184.42

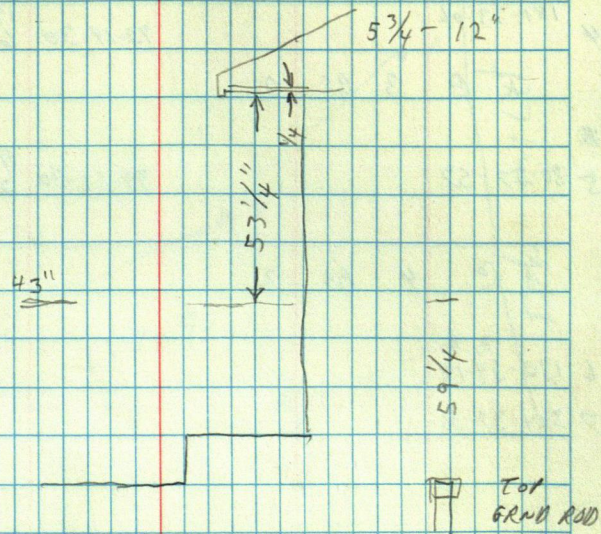
9  
8  
7  
6  
5  
4  
3  
2  
1

297.834

522.08

1







TONY PETERSON

T @ 2 BS 1

119-24-18

96-16-36

136.28

41.538

135.462

24.559

88-52-42

80.58

80.56

181-23-06

92-14-30

198.66

60.552

198.508

T @ 3 BS 2

80-27-57

94-52-30

97.40

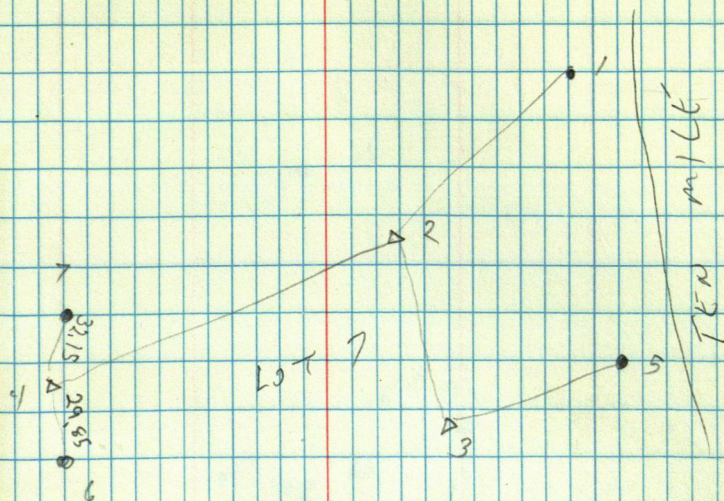
29.691

95.962

T @ 4 BS 2

130-54-18

324-37-36

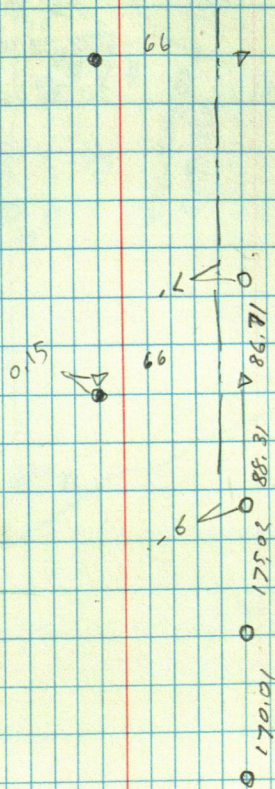




DON DOUGHTY

WOODLAWN EST.

30





GOLDIE WIESNER

204-45-06

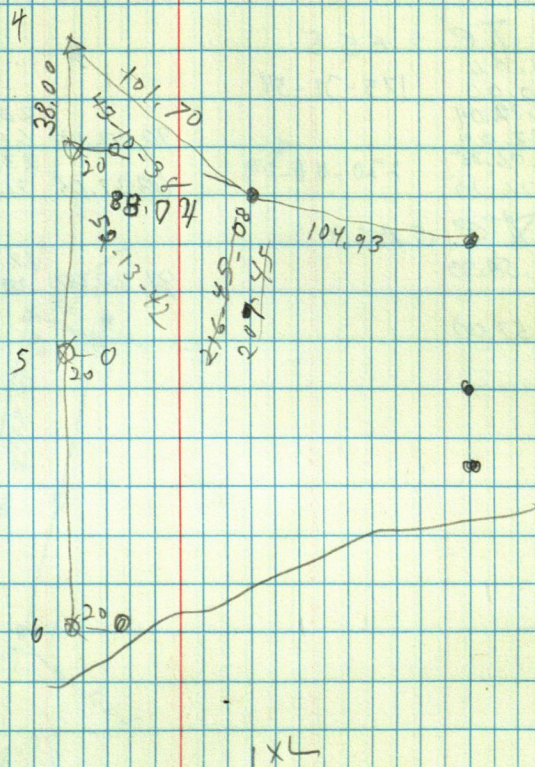
207-45

R 5 135 4

	105.95
272,38.42	32,294
	113.96
257.54,00	34.735

6

31





GEORGE KRUSNEY

T E 2 B S 3

86.46.30	230.21	71.999	235.839
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5	273.17.00	116.85	116.16
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T E 2 B S 5

0.0.06	175-31-58
--------	-----------

180.0.06

175.32.04

835.32.04

220.06.15

40.06.16

220-06-09

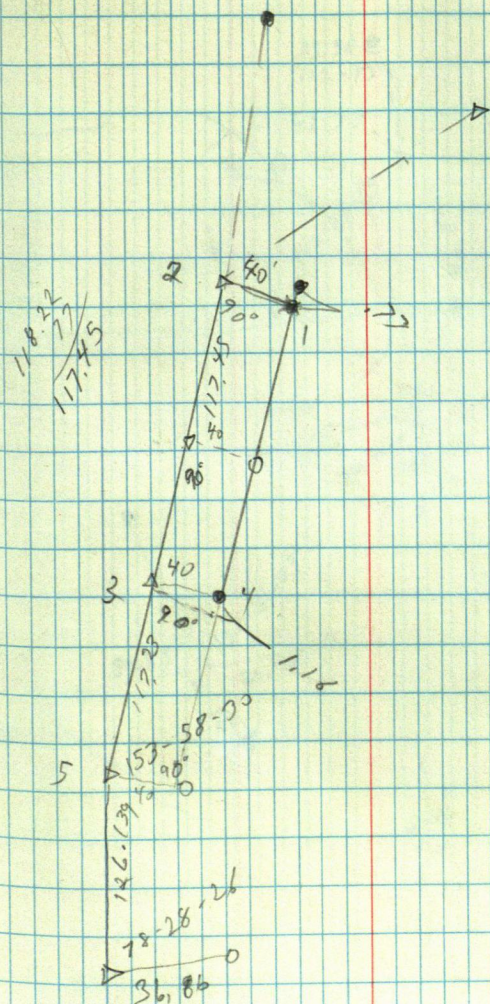
90.30.19	202.11	61.608	202.109
88.37.05	235.62	71.815	235.547

T E 5 B S 3

153.58.30

91.48.00	126.20	38.467	126.139
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307.57.00





DOROTHY BEASLEY

54-36-48

109-13

54-36-30

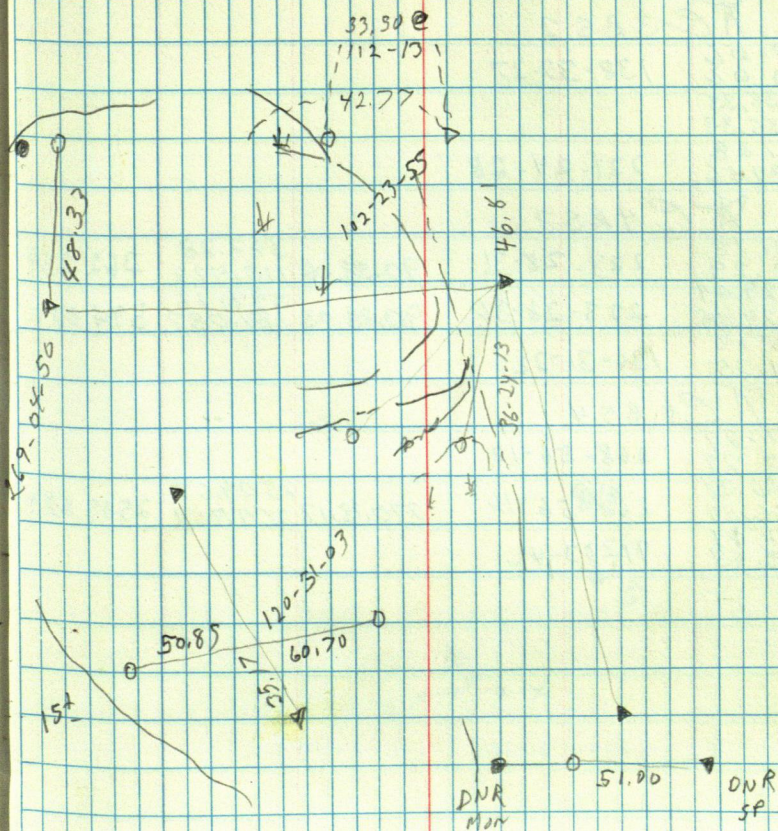
93-18-30

130.24

39.698

130.024

33





JIM SWANKER

$\pi$  C 2 B 5 1

0.0.12	140-43-16	90.10.53	452.13	452.127
180.0.12			137.810	
140.43.28			1383.89	
320.43.28		90.08.11	421.812	1383.884
0.0.20	219-16-50			
219.17.10				

$\pi$  C 3 B 5 2

0.0.06	138-35-27			
180.0.06				
138.35.33				
318.35.33				
0.0.28	221-24-28			
221.24.56				

$\pi$  C 4 B 5 3

0.0.28	223-28-36	90.38.08	362.28	362.254
180.0.29			110.422	
223.29.04			594.11	
543.29.05	223-28-36	90.38.03	181.087	594.074
0.0.13	136-31-22			
136.31.35				

$\pi$  C 5 B 5 4

0.0.27	268-56-10			
180.0.27				
268.56.37			2509.67	
88.56.37	268-56-10	270.18.17	764.951	2509.629
0.0.01	91-03-42			
91.03.43				

34

5/4  
5/4  
D

x x x x

D

D

CV 4



T 0 19 BS 18			
0-0-09	44-36-05	89,56.15	95.82
180-0-09			95.82
18 44,36.14	44-36-08	89,39.17	329.67
20 224-36-17			100,484
0-0-15	315-24-07		
315-24-22	315-23-41		
180-0-10	179-59-45		
135-23-56	179-59-45		

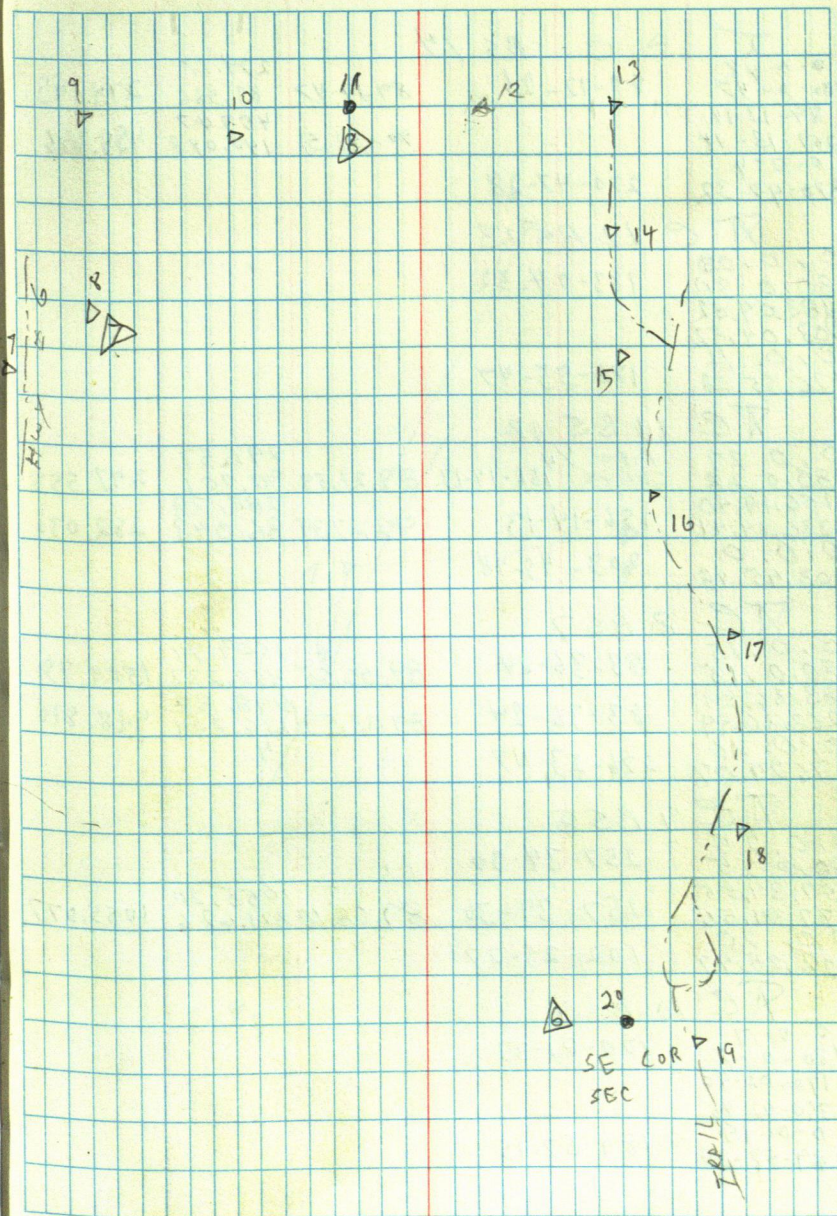
T 0 18 BS 19			
0-0-35	152-23-53		
180-0-35	18-35-19		
152,24.28			
17332,24.28			
0-0-25	207-36-04		
180-0-25			
207,36.29			
27,36.29			

T 0 17 BS 18			
0-0-05	167-16-08	87,50.46	568.29
180-0-05			173,213
167,16.13			417.68
347,16.13		86,23.41	127,309
			416,852

T 0 16 BS 17			
0-0-04	178-13-26		
180-0-04			
178,13.30			
358,13.30			

T 0 15 BS 16			
0-0-17	183-06-53	270,06.04	424.30
180-0-17			129,326
183,07.10			903.32
14 3,07.10		90,35.25	275,332
0-0-25	176-53-22		
124,53.40			

T 0 14 BS 15			
0-0-21	168-21-42		
180-0-20			
168,21.03			
1348,21.02			
0-0-15	191-39-10		
19139,25			





0-0-48	13 BS 14	274.17	
180-0-47	89-12-26	89-14-47	274.143
89-13-14		83,566	
12) 269-13-14		459.47	
0-0-4		140.048	459.416
270-47-32	270-47-28		

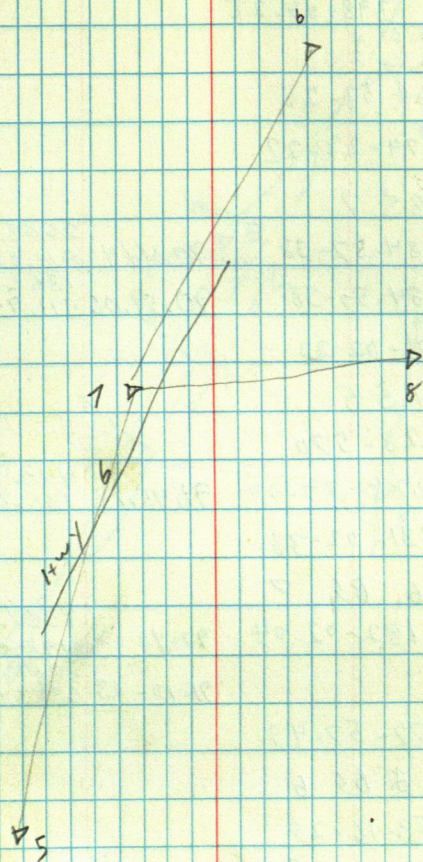
0, 0, 20	12 BS 13		
180, 0, 20	183-04-32		
183, 04, 52			
103, 04, 52			
0, 0, 11			
176, 55, 58	176-55-47		

0, 0, 27	10 BS 12		
180, 0, 28	PIPE 1/4	297.57	
156, 14, 40	CONTR 156-14-13	90,701	297.553
10) 336, 14, 41	156-14-13	282, 29	
0, 0, 0		92,2734	86,043
203, 45, 48	203-45-48		282, 030

0, 0, 15	8 BS 7		
180, 0, 15	83-36-24	1509.94	
83, 36, 39		460,232	1509,751
9) 263, 36, 39	83-36-24	448, 83	
0, 0, 20		89,33,59	136,604
276, 24, 07	276-23-47		448, 816

0, 0, 25	9 BS 8		
180, 0, 25	257-34-30		
257, 34, 55		1055, 20	
10) 277, 34, 55	257-34-30	89, 08, 10	321, 626
0, 0, 20			1055, 077
102, 26, 47	102-25-27		

0, 0, 7	10 BS 9		
180, 0, 7	170-02-37		
170-02-40			
11) 350-02-40			
0-0-15			
189-57-30	189-57-15		





AC 7 BS 8

0.0.13  
180.0.13 117-29-03  
⑥ 117.29.16  
297.29.16 117-29-03  
⑤ 298.06.35 298-06-27  
118.06.35 298-06-22  
③ 0.0.18 BS 5

② 61.53.44 61-53-26  
⑥ 179.22.40 179-22-22

AC 5 BS 7

0.0.03  
180.0.03 184-57-38 90.31.14 2663.80 2663.68  
④ 184.57.41 184-57-38 90.51.06 1351.53 1351.374  
0.0.03  
175.02.24 175-02-22

AC 4 BS 6

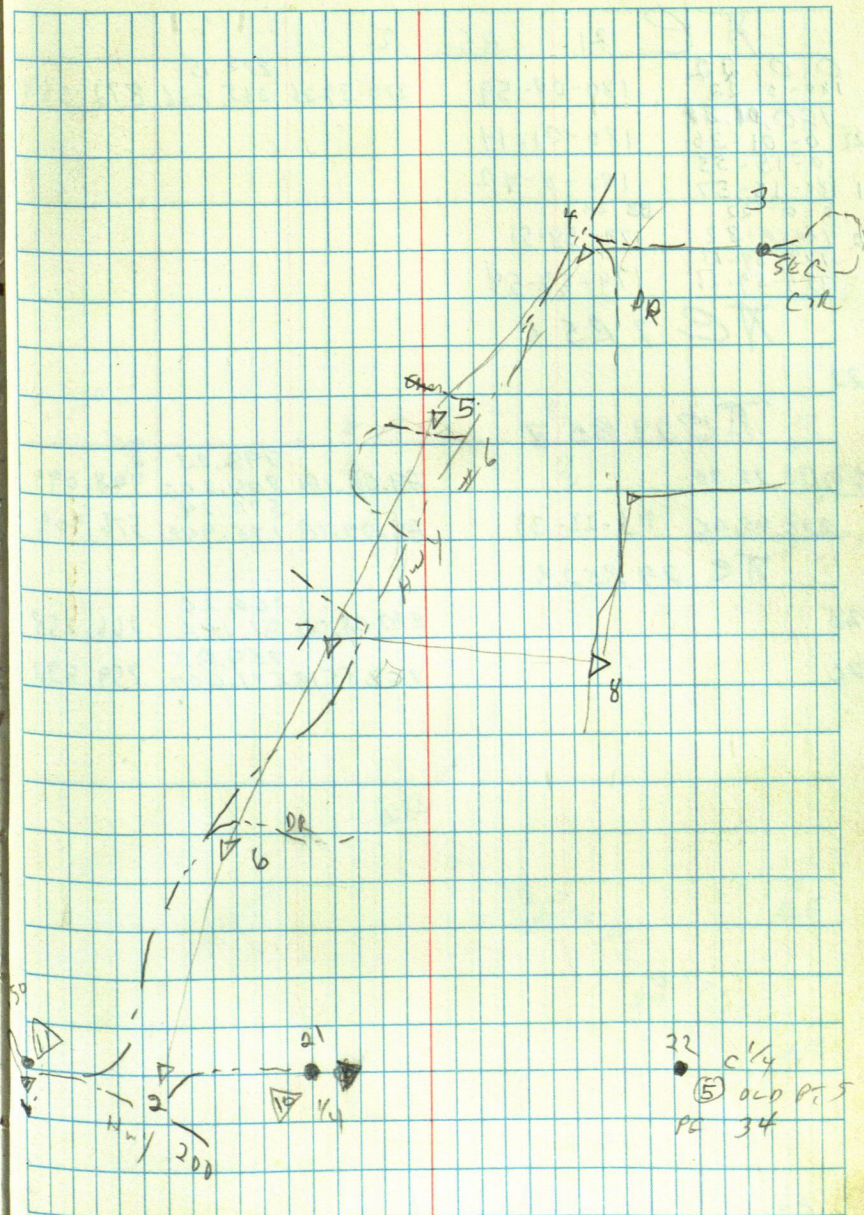
0.0.09  
180.0.10 228-570  
228.57.10  
48.57.11 228-57-00 91.45.13 443.98 443.773  
0.0.20  
131.02.58 131-02-38

AC 6 BS 7

0-0.33  
180-0.33 182-02-04 90.40-02 3582.73 3582.471  
182-02-37  
2 2-02-37 91-10-03 2085.12 2084.675  
0-0-08  
177-57-53 177-57-45

AC 2 BS 6

0.0.09  
180.0.09 53-16-25  
53.16.34  
21 233-16-34 53-16-25 90.33.14  
233.40.02  
1 0-0-13  
306-43-06 306-42-53





$\Delta C$  21 BS 2  
 0.01.22  
 180-0-32 180-00-59 270-39-26 872.15 265,826 872,080  
 180,01.21  
 22 8-01-36 180-01-14  
 0-15-55  
 1 180-15-57 180-0-02  
 0-0-22 BS 22  
 2 180-0-32 179-58-51  
 179-59-13  
 359-59-26 179-58-54

$\Delta C$  7 BS 5

23

$\Delta C$  23 BS 7

(24) 113.22.30 89.03.18 998.23 998.099  
 226.45.06 113-22-33 88.04.18 304.266 577.24 576.909  
 176,942

$\Delta C$  24 BS 23

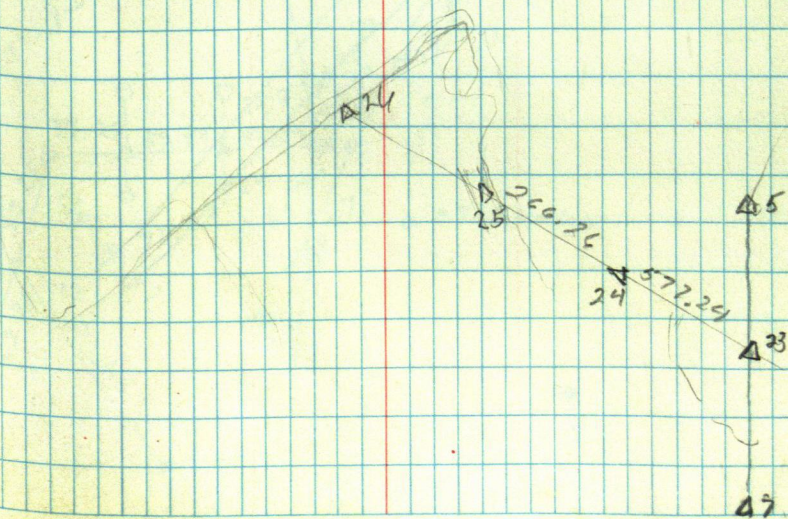
25 270.08.00 266.26 266.258  
 26 269.55.18 759.83 759.832  
 231.600

50  
1

$\Delta$   
 $\Delta$   
 $\Delta$   
 $\Delta$

21  
1/4

22  
 1/4  
 060 P7  
 5 PC





90.45

STEVE BOLTON

A 2 B5 3

179 59 60

① 223,47.00

90.45

49-18-28

4 162-42

13.71

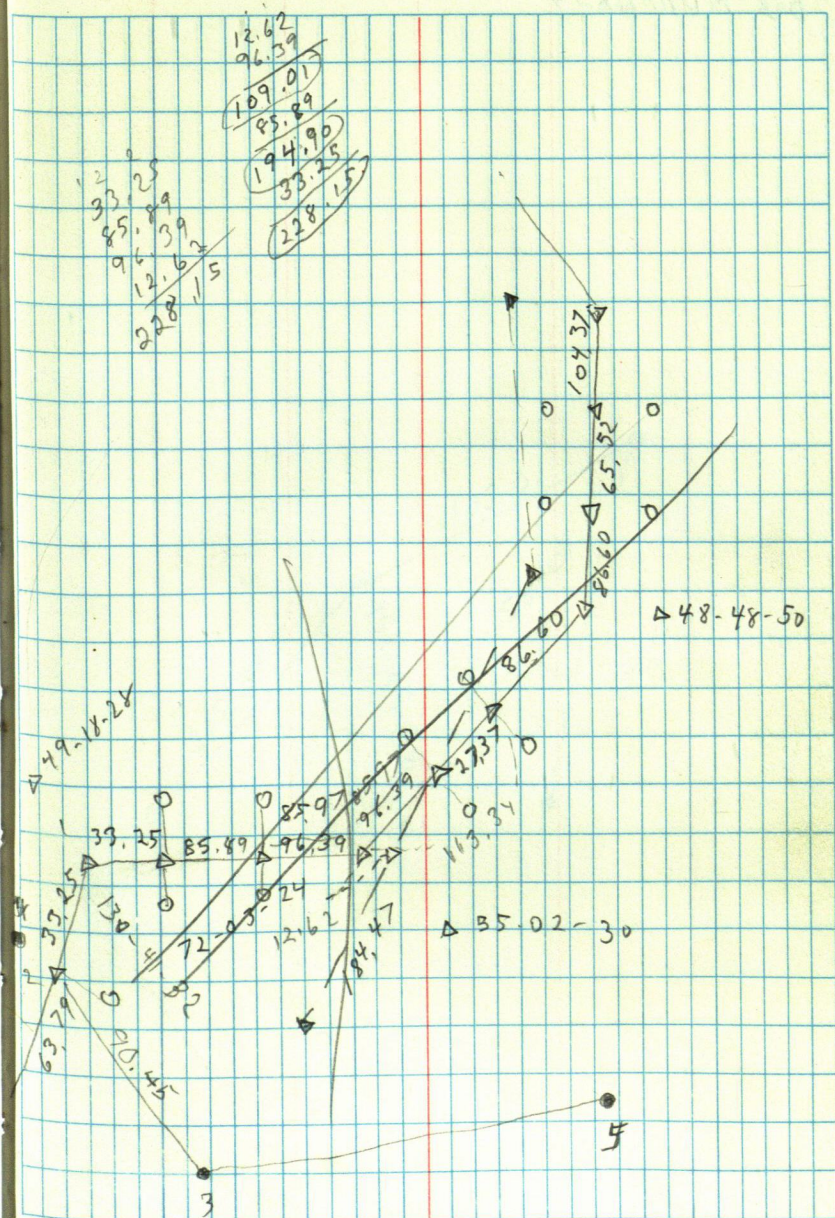
130 41-32

A 3 B5 5

217,44.06

5

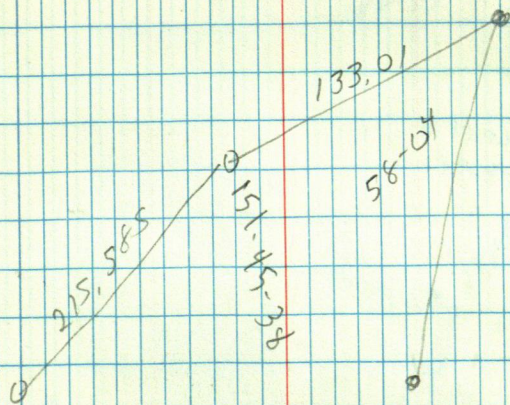
39





DOB MERCHANT

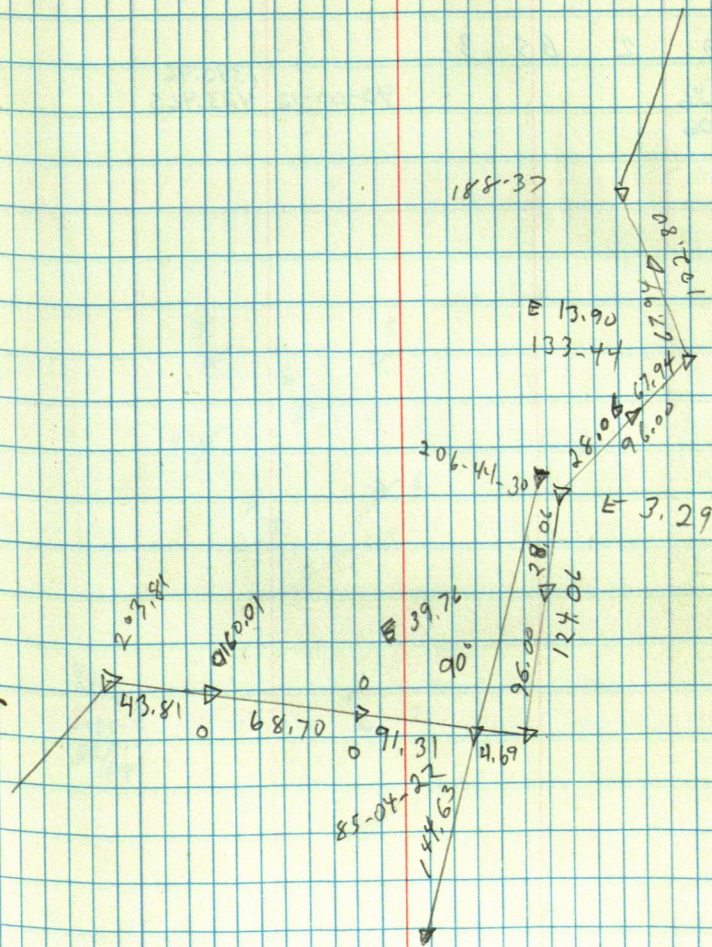
30





5 Bolton

41





STEVE HANSON

	T	Q	2	BS	1
0-0-52					2042.36
180-0-72			232-32-44		622.509
					587.23
9 180-				90-08-28	2042.34
232-33-36				90-53-47	587.146
4 52-33-30			232-32-48	90-09-09	1667.51
					508.235
					1667.461

	T	Q	2	BS	3
60-09-36					1390.96
4 120-19-06				90-00-12	423.965

1/4  
USFS  
BR/cap

2

1 sec  
cap



GORENTZ

	$\Delta$	2	B5	1			
	0-0-21		184-20-55		90-12-10	1732.37	
	180-0-21					528.028	1732.354
	184-21-16					281.920	
3	4-21-25		184-21-04.		90-31	924.93	924.89
	0-0-29						
	125-39-25		175-38-56				

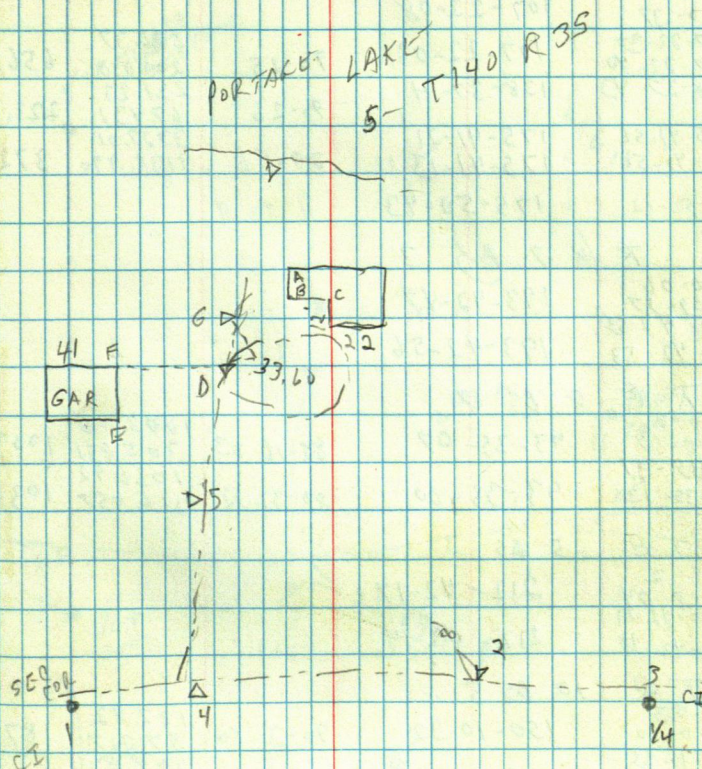
0.0.10	4 BS 2		
180.0.10	274-26-14		
274.26.34		89.59.28	266.99
74.26.34		90.33.00	266.988
0.0.14			1594.44
85.33.54	85-33-40		1594.362

	$\pi$	@ 5 Rs	4
	0-0-4		
	180-0-4	201-28-18	
	201-28-22		
b.	21-28-24	201-28-20	
	0-0-30		
	158-32-12	158-31-42	

TEG.BSS			
0.0.02	186-07-06	270.27.11	539.43
180.0.04			164.420
186.07.08	186-07-06	98.40.42	223.12
6.07.18			68.006
0.0.20	173-52-27		220.563
173.52.47			
0.0.12			

A 4-34-40	NW	cor Ho.	41.0
B 42-49.	SW	"	20.50
C 58-28	NE	cor	51

	$\pi @ 0$	B3	5
	0.		
E	39-24-12	63.35	
F	74-22	51.80	





# CALVIN SNOW

⌈ @ 2 BS 1

0-0-25			2229.37	
180-0-16	79-31-18	90-22-20	679.487	2229.272
79-31-43			690.78	
3 259-31-36	79-31-20	89-48-40	210.549	690.772
179-48-23	179-47-58		304.24	
4 359-48-20	179-48-04	90-19-50	92.237	304.241

⌈ @ 3 BS 2

0-0-29				
180-0-37	107-22-08			
107-22-37			656.37	
5 287-22-40	107-22-03	90-25	200.058	656.344
138-37-43	138-37-14		221.23	
6 175-41-50	175-41-21	90-26	67.431	221.223
7 355-41-50	175-41-13	89-56	3727.01	
			1135.990	3726.987
175-51-12	175-50-43	11 to 9		

⌈ @ 7 BS 3

0-0-06				
129-59-57	193-42-47			
193-42-53				
8 13-42-53	193-42-56			

⌈ @ 8 BS 7

0-0-0			1003.46	
180-0-13	93-35-07	89-16-03	305.851	1003.376
93-35-07			1036.92	
9 273-35-13	93-35-00	89-32-22	316.057	1036.899

⌈ @ 5 BS 3

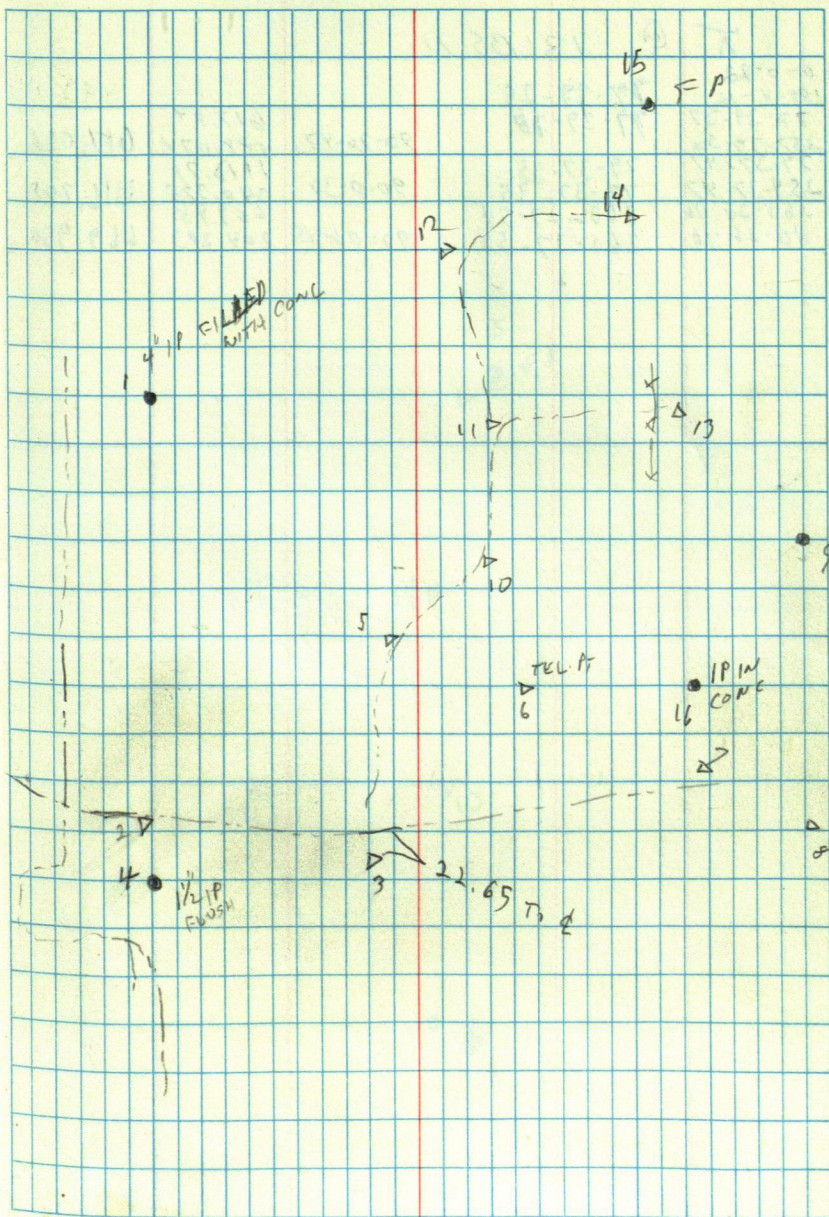
0-0-2				
180-0-04	212-42-17			
212-42-19				
10 32-42-18	212-42-14			

⌈ @ 10 BS 5

0-01-03			187.72	
180-0-30	150-10-32	90-21-50	57.217	187.715
150-11-35			248.89	
11 333-11-40	153-11-10 ?	89-39-45	75.860	248.882

⌈ @ 11 BS 10

0-0-53				
180-0-32	170-46-24			
170-47-17			430.99	
12 350-47-16	170-46-24	90-18-30	131.267	430.984
270-23-32	270-22-49		428.71	
90-23-35	270-22-43	269-44-04	130.976	429.707





$\bar{A}$		13 BS 11			
	0-0-12				
	120-0-12				
	77-39-37				
14	252-39-30				
	79-37-47				
15	259-37-47				
	260-28-06				
16	80-28-70				
	77-39-25				
	77-39-18				
	79-37-35				
	79-37-35				
	260-27-54				
	260-27-58				
		90-20-47	617.04		
			188.074	617.026	
			1116.71		
		90-0-30	340.325	1116.708	
			269.95		
		90-06-15	204.203	669.950	

15  
 $\Delta @ FP$

12  $\Delta$

14  $\Delta$

11  $\Delta$

13  $\Delta$

16



BILL HANSEN

XC 2 B 5 1

0.0.18		2642.70	
180.0.18	96-57-20	90.45.12	2642.453
96.57.38		755.08	
3) 276.57.38		90.58.13	754.964
0.0.18		260.146	
265.03.13	265-02-55		

XC 3 B 5 2

0.0.21			
180.0.21	177-21-44		
177.22.05			
4.357.22.05			
0.0.32			
182.38.56	182-38-53		

XC 4 B 5 3

0.0.20		1242.24	
180.0.20		90.56.12	1242.272
55.28.05	55-27-54	328.698	
98.53.21		202.90	
	98-53-01	61.843	202.671
187.28.06		190.82	
	187-27-46	58.163	190.214
326.09.88		103.76	
144.42.24	326-10-08	37.622	103.423
		58.15	
		99.36.58	57.324
		17.722	

88-26-54  
30-03  
47-56-51

14  
2

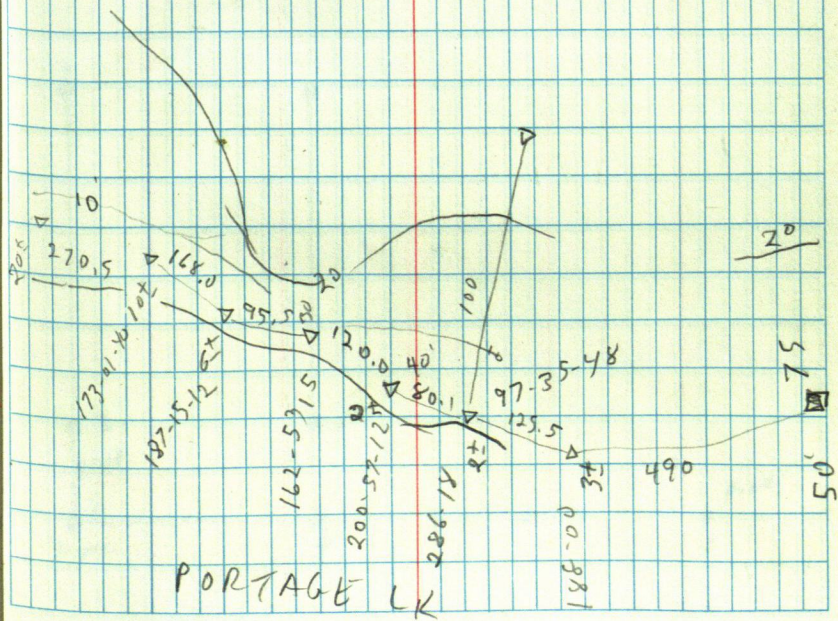
87-56-51  
1  
SBL CR

3  
SARD LIG  
No. DME

8  
4  
7  
5  
6



BERN - GORIENTZ





Te 2B51

4

390

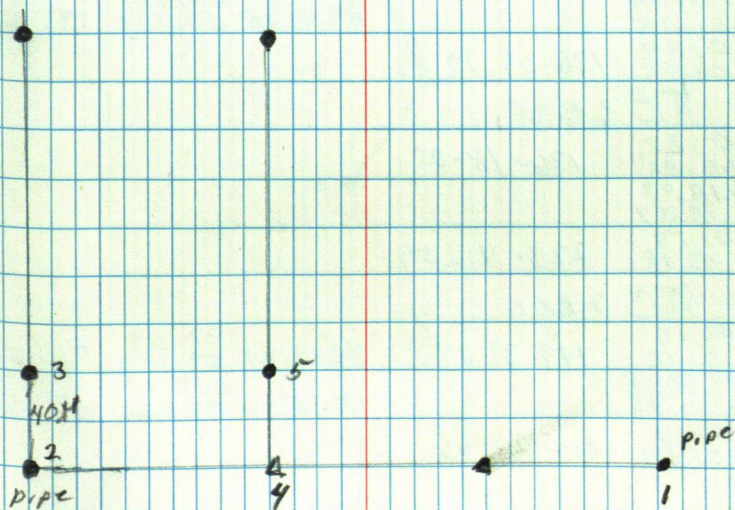
Te 4B51

590

75 ft

40 ft

40 ft





AC 3 B 5 2

47

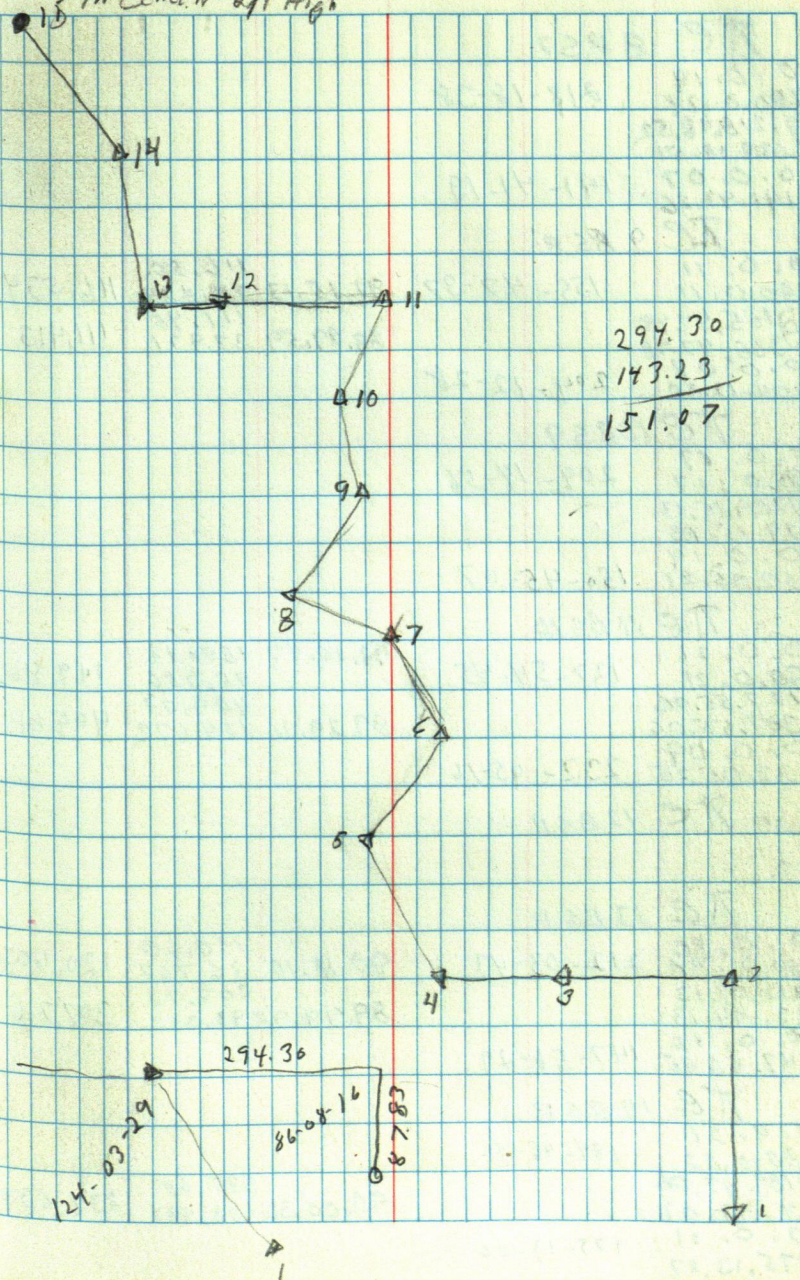
TE 5B54

TC 6 B55

TC 7 BSC

0, 0, 16	149-39-04	88.42, 01	97, 69	47, 668
120, 0, 16			29, 779	
8) 149, 39, 20			19, 03	
329, 39, 20		90.36, 410	42, 376	139, 02
0, 0, 28	210-20-56			
210, 21, 24				

pipe set  
15 in cement 2 ft high





Te 8B57

0.0.14 218-18-38  
180.0.14

9) 218.18.52  
38.18.51

0.0.07 141-41-19  
141.41.26

Te 9B58

0.0.11 155-47-37  
180.0.11

10) 155.47.48  
335.47.48

0.0.02 204-12-28  
204.12.30

Te 10B59

0.0.17 209-14-56  
180.0.17

11) 209.15.13  
29.15.13

0.0.14 150-45-07  
150.45.21

Te 11B510

0.0.21 127-54-45  
180.0.21

12) 127.55.04  
307.55.04

0.0.09 232-05-16  
232.05.25

Te 12B511

13

Te 13B511

0.0.30 212-03-43  
180.0.30

14) 212.04.13  
32.04.13

0.0.16 147-56-29  
147.56.45

Te 14B513

0.0.21 184-46-45  
180.0.22

13) 184.47.06  
4.47.07

0.0.11 175-13-06  
175.13.27

91.15.13 116.56  
35.529 116.534  
88.29.59 111.45  
33.971 111.413

93.20.47 150.12  
45.756 149.862  
89.29.16 409.03  
124.672 409.011

90.18.10 120.60  
34.762 120.603  
89.49.25 307.72  
93.792 307.716

90.00.32 832.65  
253.787 832.639



SWAN KIBR

TC 2 B 53

91.30.00

180.00.00

271.30.00

89.24.47 463.02 141.129 462.996

@ 4 B 5 2

0-0-14

180-0-18

177-19

177-18-46

177-18-40

90-16-10 684.48 208.626 684.464

5 352-18-58

TC 4 B 5 3

4A 139-19-08

TC 4A B 5 4

A 246-30 138.55

B 259-05 152.58

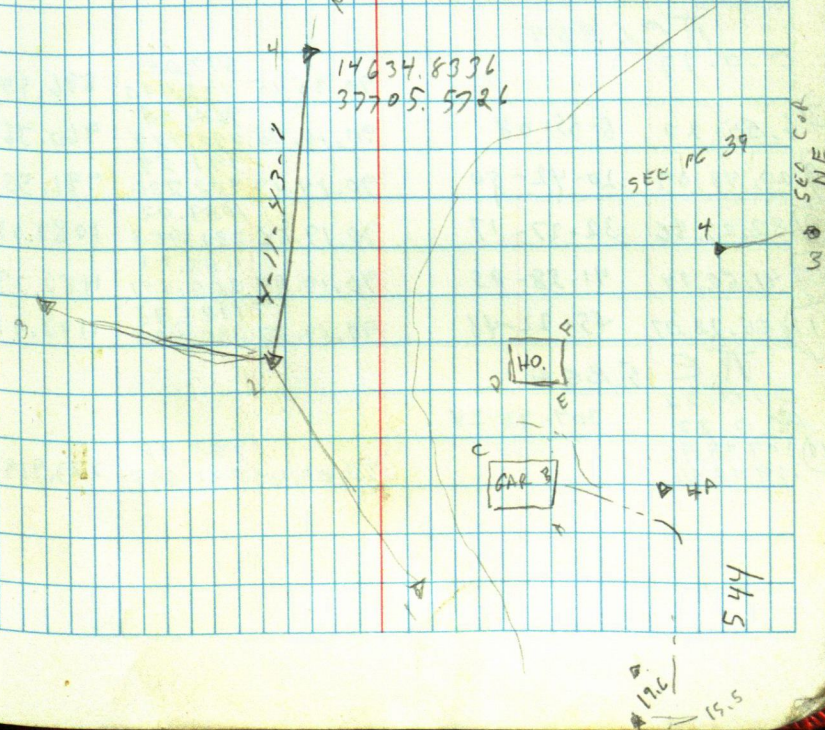
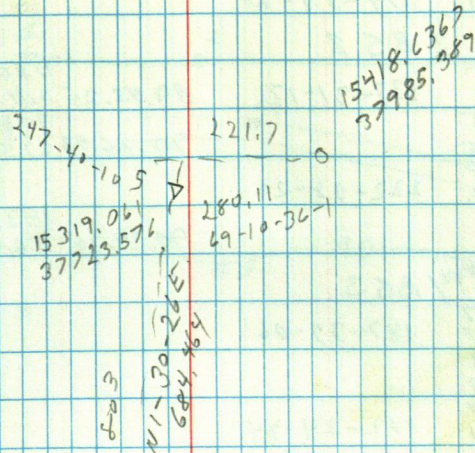
C 260-08 177.69

D 294-0 127.77

E 301-55 102.64

F 311-00 120.33

4 70-21-06 392.56 119.653 392.552





BEN OVERBOUGH

AC 2 B 5 1

0.0.35  
180.0.45 180-00-49  
② 180.01.29  
0.01.34  
0.0.33  
180.0.01 179-59-28

AC 3 B 5 2

0.0.18  
① 180.0.18 137-31-17 89.43.25 1186.47 361.637 1186.453  
137.31.35 903.65  
317.31.35 90.26.53 275.402 903.518  
0.0.29  
222.28.52 222-28-29  
5 90.34.25 183.89 56.049 183.879

AC 4 B 5 3

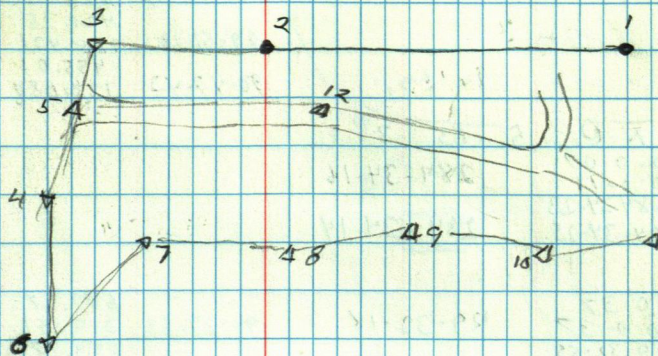
0.0.07  
② 180.0.07 187-35-06  
187.35.13  
07.35.13  
0.0.17  
172.25.01 172-24-44

AC 6 B 5 4

0.0.19  
⑦ 6.55.27 6-55-08 90.35.15 897.05 273.420 896.998  
⑧ 20.43.09 20-42-50 90.14.45 960.38 292.722 960.364  
⑨ 32.27.36 32-27-17 90.14.14 991.54 302.236 991.551  
⑩ 41.58.24 41-58-05 90.19.56 1089.02 331.953 1089.029  
⑪ 55.23.07 55-22-48 90.19.57 1182.77 360.501 1182.733  
12 55.23.07 55-22-48 90.19.57 1103.93 336.480 1103.91

AC 5 B 5 4

0.0.22  
180.0.22 309-38-24  
⑫ 309.38.46 773.92 235.879 773.919  
129.38.46



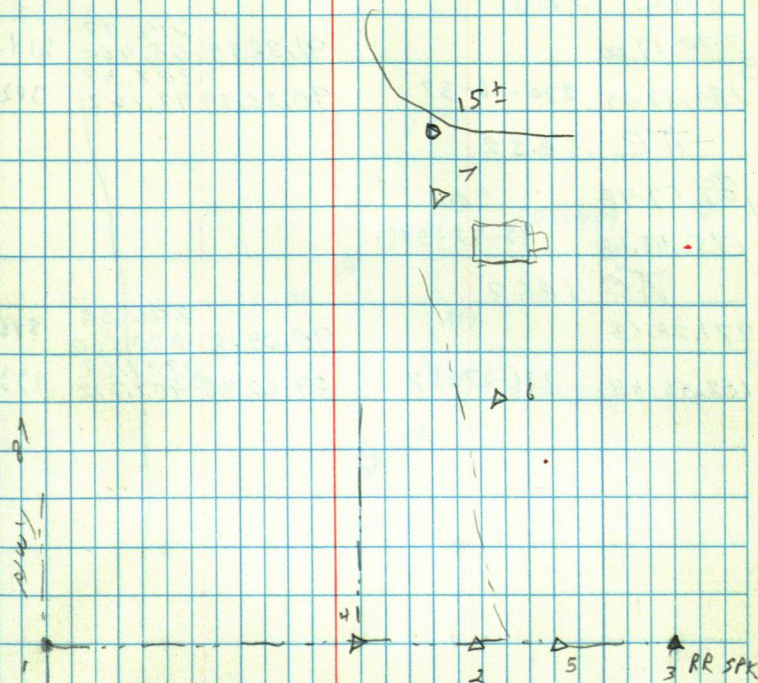


7 2 2 25 1

$\overline{A} \cap B$	5	B5	3
$A - A \cap B$			
$180 - 0 - 11$		284-34-16	
284-34-23			
6 104-34-25		284-34-14	

0-0-37	129-32-18	90-22-55	689.14	689.124
180-0-37			210.051	
129-32-55			593.98	
309-32-50	129-32-13	90-13	181.047	593.976

184-24-54		<del>98</del> + 2		
B-49-54	184-24-57	<del>98</del> - 12	96.20 29.323	95.218





PAUL BECKMAN

~~AC~~ 2B51

71-42-36 269.20  
82.051 269.077

~~AC~~ 2B51

270.17.00

91.3854 214.79  
65.460 214.687

180.33.54 270-16-57

90.26.24 302.37  
92.162 302.359

~~AC~~ 3B52

4 87.57.48

175.35.48 87-57-54

~~AC~~ 4B53

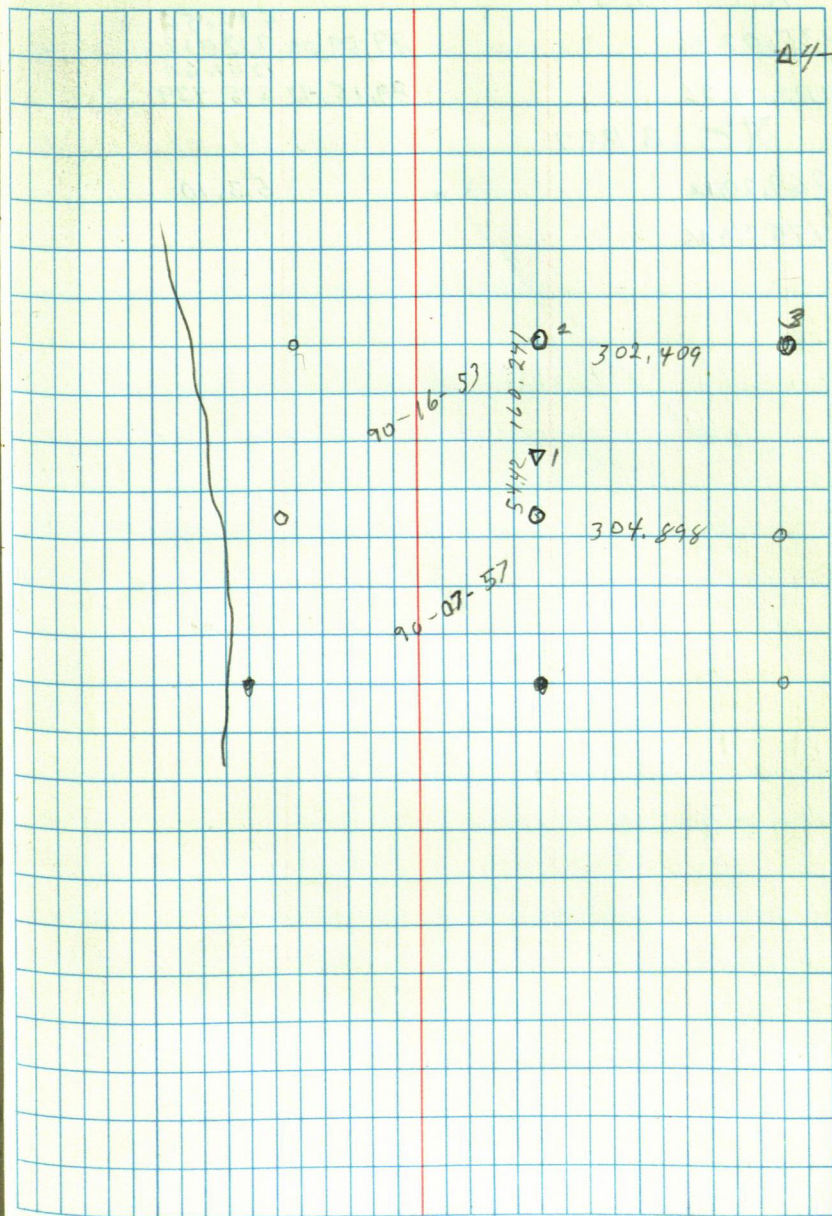
271.28.18

90.04.18 886.68  
270.260 886.675

5 182.55.54 271-27-57

89.56.48 1337.62  
407.712 1337.622

44-5





ΣC 2851

235,02,30

8

110,04,36

ΣC 31852

269,20,12

4 178,40,86

89,59,00

89,15,42

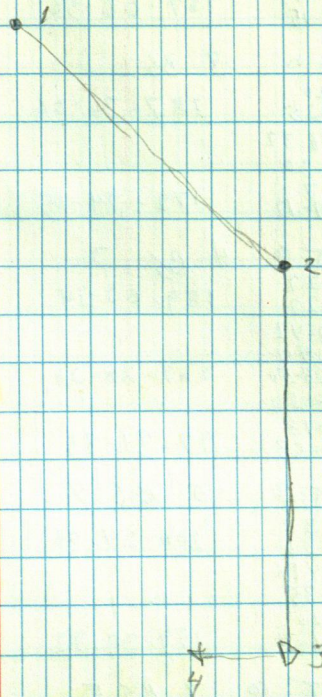
496,56

212,313

1241,60

378,439

53,10





# BERNARD GORENTZ

$\pi @$ 2 BS 1				
0-0-17	192-53-03	90-06-35	277.60	277.581
180-0-18			84.602	
192-53-20			212.55	
3 12-53-20		90-39-17	64.787	212.538
0-0-19	167-06-56			
167-07-15				
$\pi @$ 3 BS 2				
0-0-26	187-36-06			
180-0-25				
187-36-32				
4 7-36-30				
0-0-7	172-24-05			
172-24-12				
$\pi @$ 4 BS 3				
0-0-22	189-02-24	91-17-40	125.86	125.762
180-0-22			38.341	
189-02-41			80.21	
5 9-02-44		89-58-02	24.448	80.209
262-28-50	262-28-28			
6 82-28-50				
0-0-18	97-31-35			
97-31-53				
$\pi @$ 5 BS 4				
0-0-30	200-24-06			
180-0-30				
200-24-36				
20-24-35				
0-0-20	159-35-52			
159-36-12				
$\pi @$ 7 BS 5				
0-0-19	162-16-15	91-30-15	126.58	126.532
180-0-19			38.579	
162-16-34			88.48	
8 342-16-34		91 41-09	26.971	88.453
0-0-9	197-43-52			
197-44-01				
$\pi @$ 8 BS 7				
0-0-27	188-05-53			
180-0-27				
188-06-20				
9 8-06-20				
0-0-05	171-53-57			
171-54-02				



Ne 1852

3,

Ne 3851

490,00.00

Ne 4853

5

89,57.20	318.12 96,966	318.123
244.23.36	235.61 71.813	235.14

Ne 3852

2

91,03.00	207.52 63.246	207.474
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6

90,24.00	300.00 91,450	300.007
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Ne 4853

90.

268,94.24	236.03 71.946	235.979
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24H  
1

920

5 4 33 6 3

24

2

33 6 46



X @ 2 BS 1

3 180.00

4

81.43.54

5 163.27.24

126.51.54

6 26348.30

7 Xc 4BS2

8 106.33.18

211.06.42

Xc 7BS4

89.02.48 250.37 250.337

93.42.24 105.93 105.729

267.16.06 155.14 154.963

88.45.18 273.51 273.441

92.31.54 83.364 144.693

90.35.06 163.91 163.70

LEETCH

LAKE

7

4

49.23

3

1/2 BOLT  
w/ HOT NUT

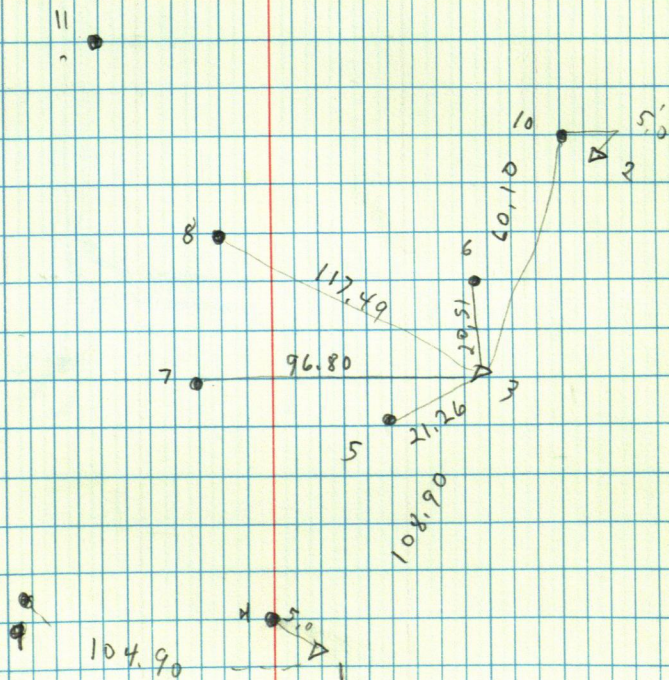
2

356.066

5



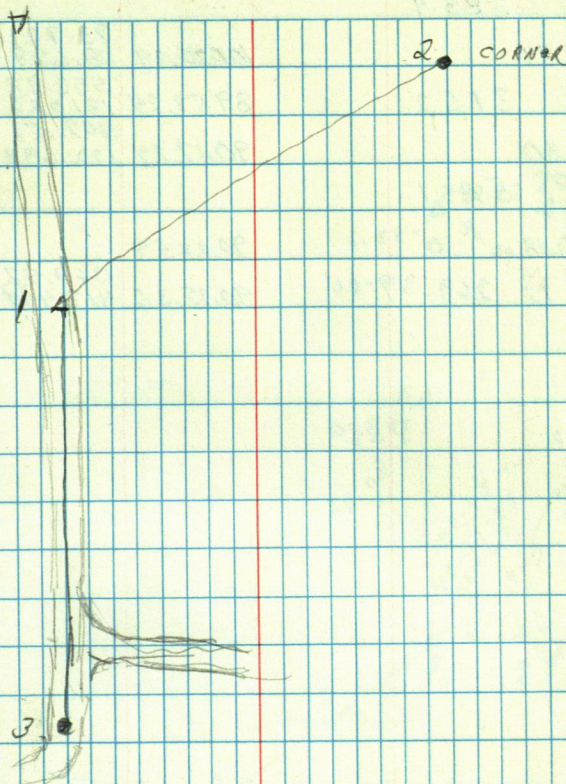
11	228-4-48	228-04-16	95-18-40	127,75	127,20
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8e 1852

③ 126.32.30	90.04.12	1566.13 472.353	1566.116
268.05.00	126-32-30	419.67 127.914	419.639





TC 3BS 4

101.30, 24

93.92	
28,629	92,036

Te 3952

8957.24

593.93	593,931
181.032	

2/20.10.30

90,17,24

402,57	
122,697	402,553

TE 5B51

7) 269,39.18

90,2854

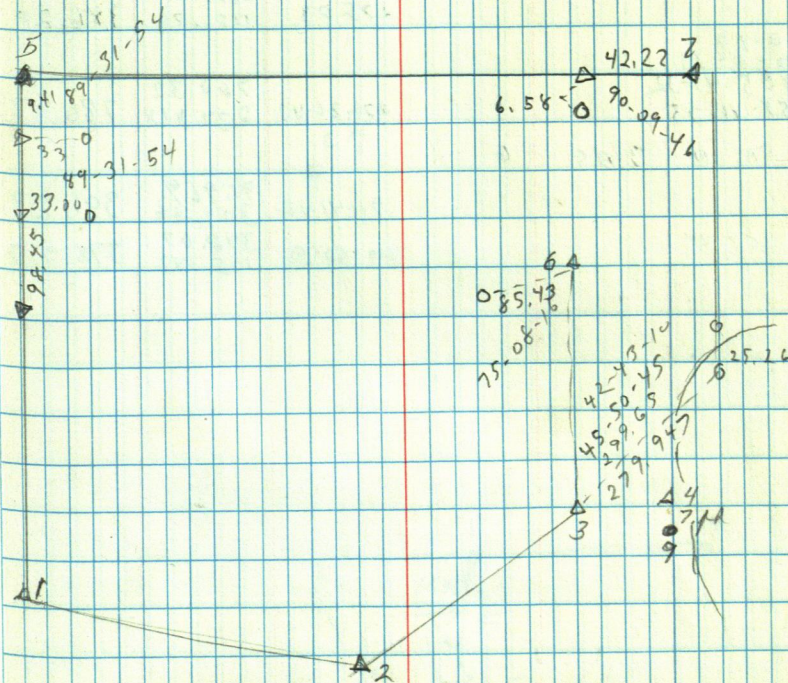
1349,57	1369,548
417,444	

179.18.12 269-39-06

90,15,36

1349,57	1369,548
417,444	

42-43-10





LARRY DRESON

SW-SE-32-140-30

90-08-50	1306.01 398.077	1306.008
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7 (a) 1 BS 2

275-03	387,70	
	118,175	386,20

4

0-0-10  
180-0-13  
385-41-32

5 155-41-35

271-26-42	780.32	
	237.818	780.03

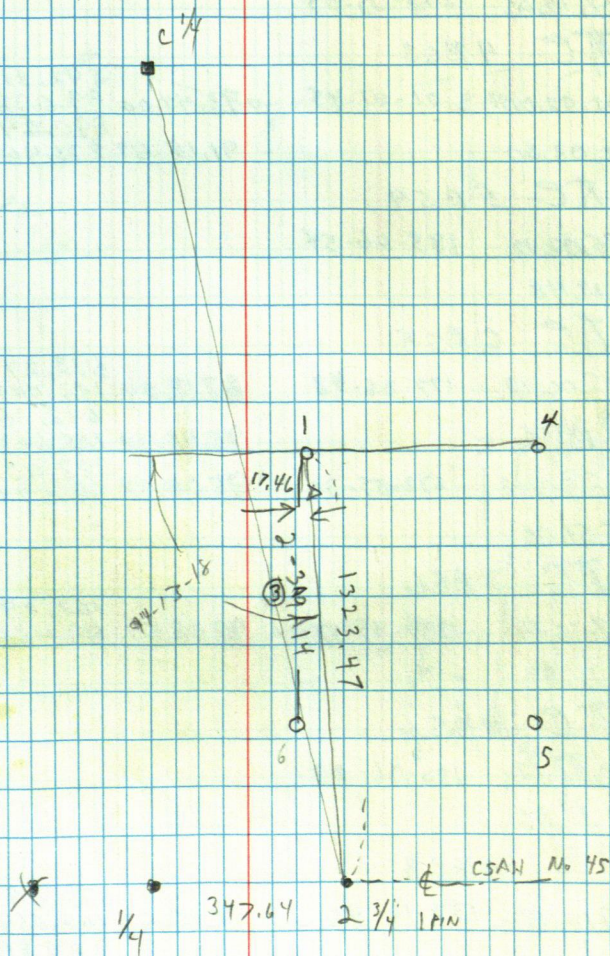
7 0 3 9 5 6

6	91-41-12	91, 967 301, 66	301, 558
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1 180.00

89-50-96	378.07 115.242	378.077
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E. CURR  
R. TURNER  
11-18-95





DAVE WILLIAMS

TC 2B51

3	178.23.30	734.86	704.849
		223.988	
350	46.24 175-23-12	1224.06	1223.547
		28.20.24	373.097

TC 3B52

4	273.35.06		
	182.10.06 273-35-03		

TC 4B53

5	001.02.00 01-01-45	292.31	291.693
		89.098	
		890.64	
	002.03.30	91.15.42	890.415
		271.464	

TC 5B54

6	185.07.12 185-06-54		
	10.13.48		

TC 6B55

7	177.06.48 177-06-48	513.27	512.947
		156.445	
		618.78	
	359.13.36	95.43.30	615.689
		188.603	
	8 282.55.42 232-55-30	323.40	322.098
		98.574	

105.51.00

TC 7B56

9	237.36.24 237-35-57	162.29	162.287
		49.465	
	115.11.54		

TC 8B57

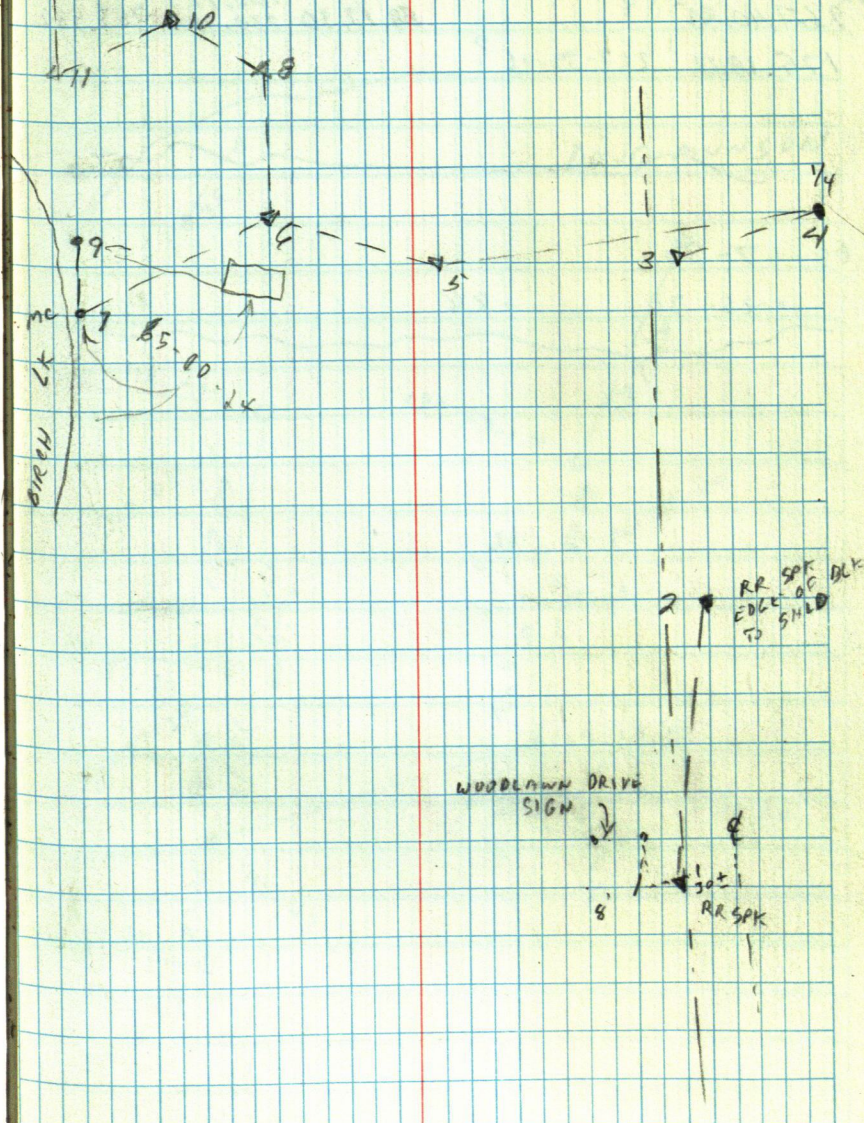
10	150.36.12 150-36-03		
	301.12.06		

TC 10B58

11	157.10.48 157-10-45	533.64	533.521
		142.654	
		320.86	
	314.21.30	90.22.24	320.852
		97.798	

1/16

AC SET FROM  
DT'S BK 298/154





12 267,40.30

175.18.12 267-39-06 ?

88.19,30	783,72	783,382
	238.878	

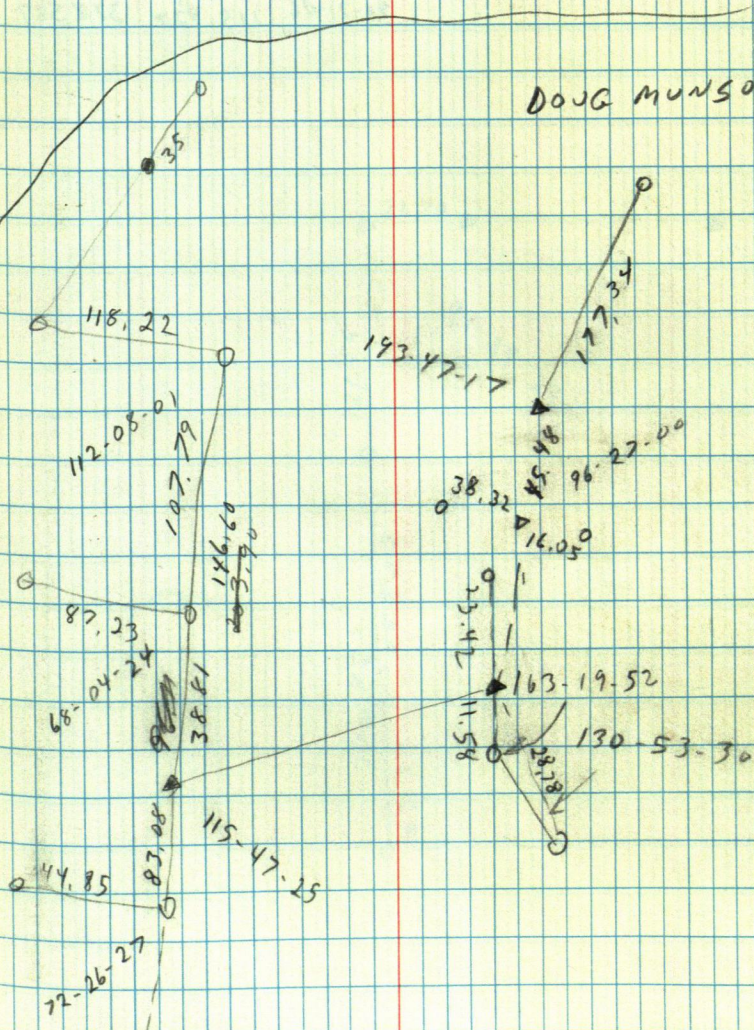
68-17-30

• -25- 30

184

89.20

DOUG MUNSON



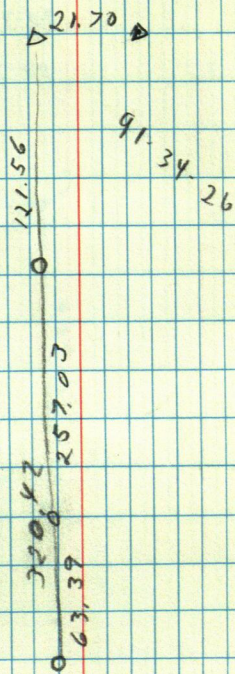


BBB F014261 W

140565NOE LK

90-21-06 378.69  
115.427 378.587

G. ORO  
R. TURNER  
11-9-95





DON KIRKE

SE-NE-8-137-29

π 2 B5 1

3 90.00

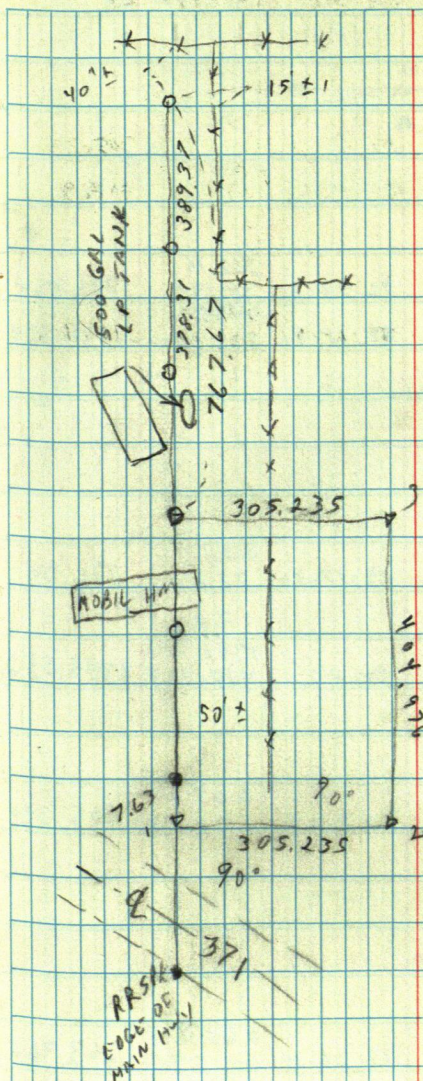
89. 34.0	305.24	
	93.037	305.235
	404.99	
89.35.12	123.44	404.976

90-36-15	378.33 115.314	378.306
88-36		

25° snow

F CARD  
R. TURNER

11-13-95





## GORDY REHLER

11-140 29

A @ 2 BS 1

0-0-23  
 180-0-12 209-31-06  
 209-31-29  
 29-31-16 209-31-04  
 0-0-24  
 150-29-13 150-28-49

A @ 3 BS 2

0-0-19  
 180-0-21 170-28-42 92-28-38 322.16 321.864  
 170-29-01 1095.30  
 4 350-29-02 170-28-42 88-18-46 333.850 1094.824

0-0-20  
 180-0-16 227-24-33  
 327-24-53  
 47-24-42 227-24-26

A @ 6 BS 4

0-1-27 89-17-50 236.76 236.74  
 7 269-49-55 269-48-06 7.20  
 5 90-22 1346.59 1346.552  
 410.438

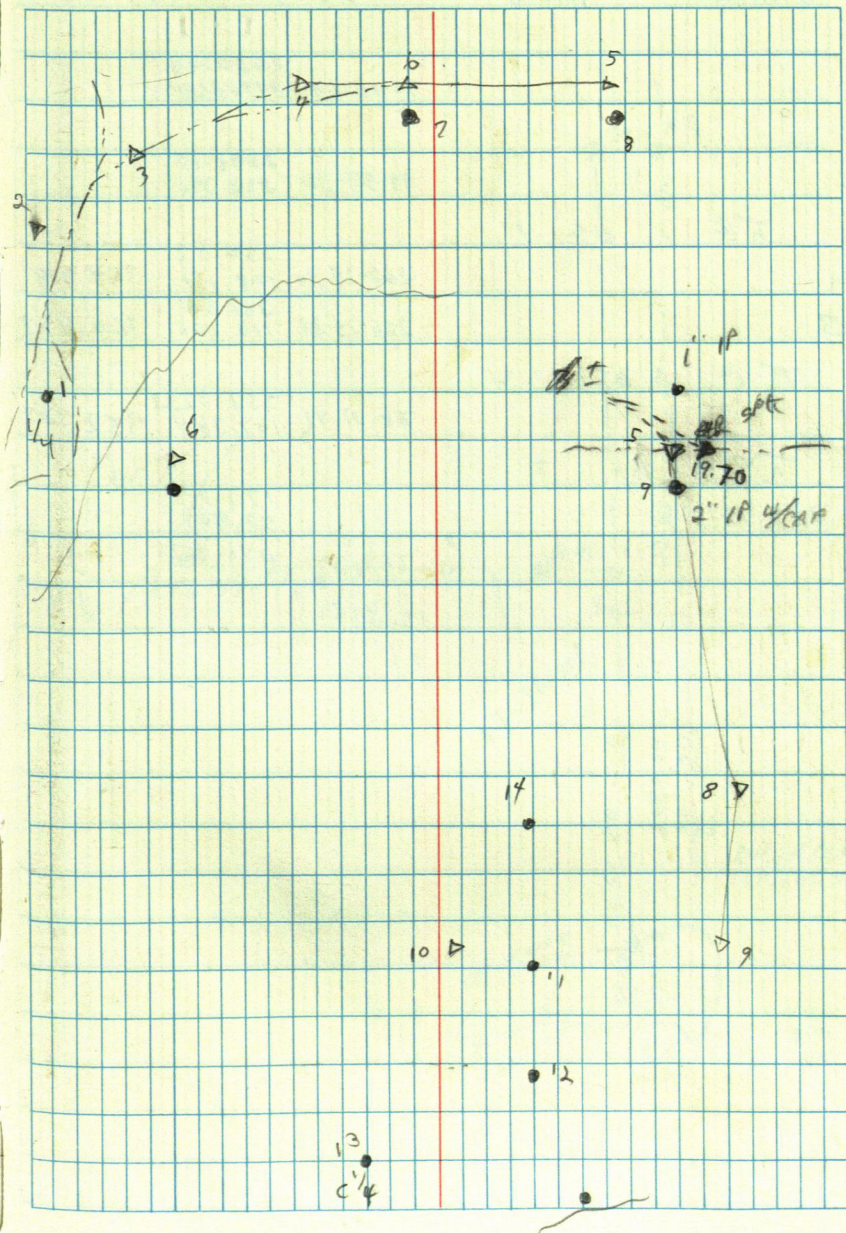
A @ 5 BS 4

0-4-01  
 180-03-42 256-54-22  
 256-55-22  
 8 76-55-03 256-51-21 91-4-56 605.45 605.341  
 184.542

A @ 8 BS 5

0-0-18  
 180-0-14 174-21-28  
 174-21-46  
 9 354-21-41 174-21-27

0-0-14  
 180-0-0-9 260-52-55 87-26-14 264.23 263.966  
 260-53-09 252.57  
 80-53-00 260-52-51 89-45-10 76.984 252.568





WARREN

FEARING

NE-SW-17-139-30

2680.99  
90-06-54 817.169

2698.15  
89-53-36 822.396

1 @ 2 BS 1

269-29-50 354.82 354.808  
108.151

3 266-24-24 361.56 360.852  
110.206

1 @ 3 BS 2

4 88-01-42 352.32 352.107  
107.384

1 @ 4 BS 3

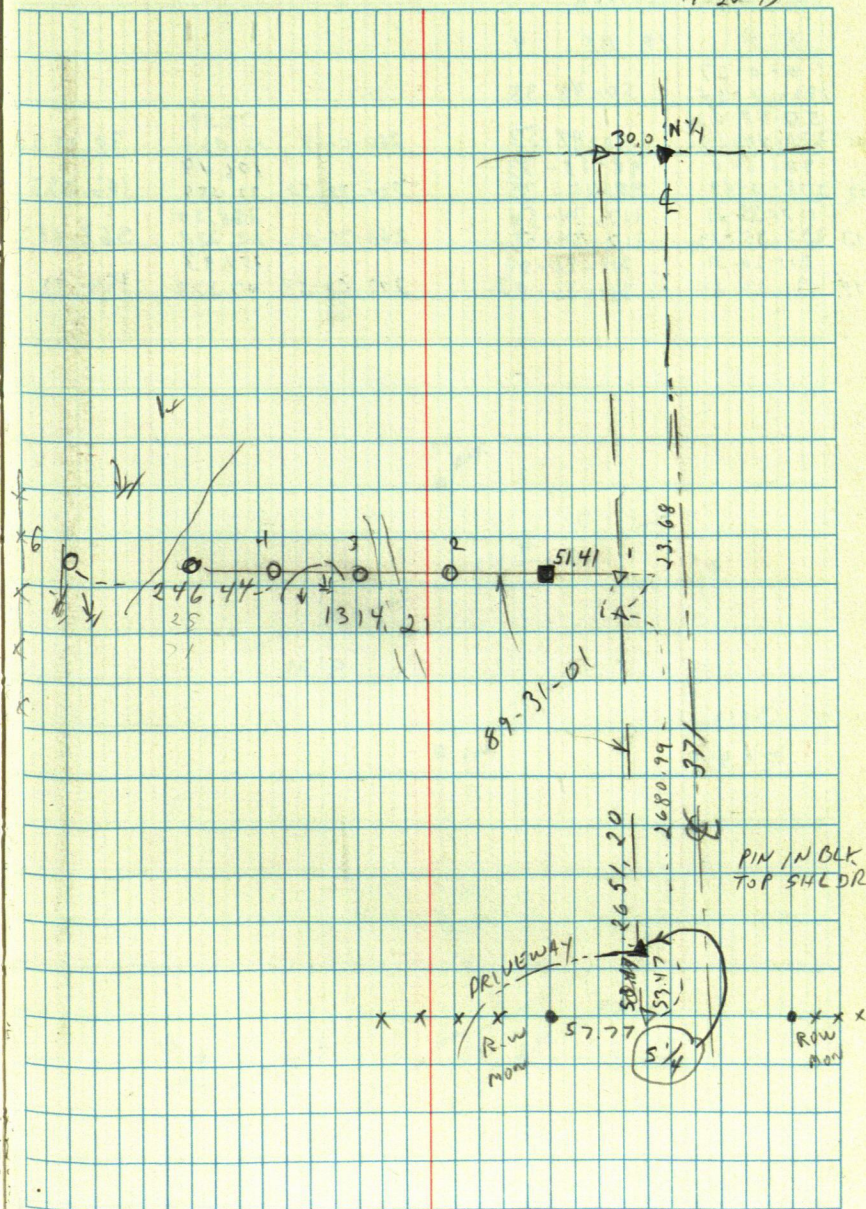
5 275-18-54 173.71 52.992

265.32 246.82

10° windy CLR

E. CUREO  
R. TURNER

11-20-95





GORDY

REHER

A @

10 DS 9

0-0-27

180-0-24

50-48-02

50-48-35

11 230-49-17

50-48-53

98-16-0

98-15-33

12 278-15-59

98-15-35

117-35-21

117-34-54

13 297-35-19

117-34-55

311-26-31

311-26-04

14 131-26-26

311-26-02

260-01-4

39.59

12.066

264-38-52

106.49

32.459

266-35-52

368.20

112.228

272-56-53

154.93

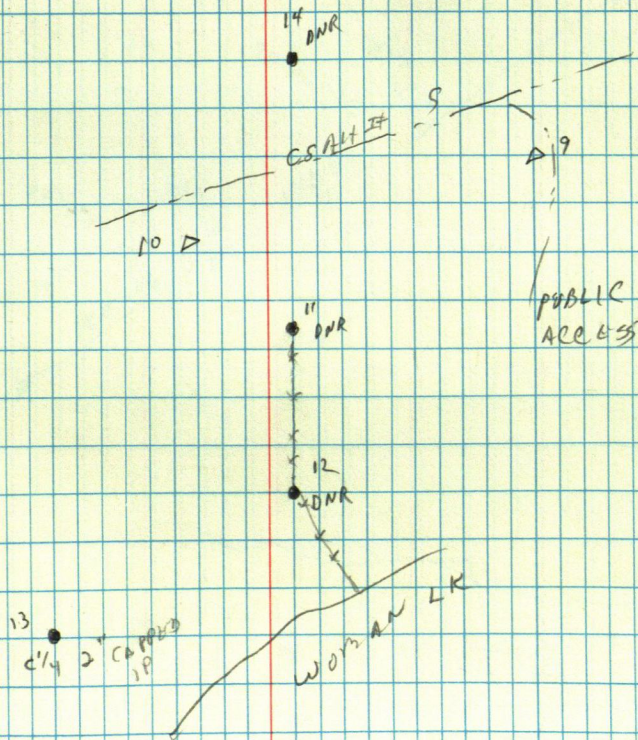
42.223

38.992

106.027

368.089

154.72





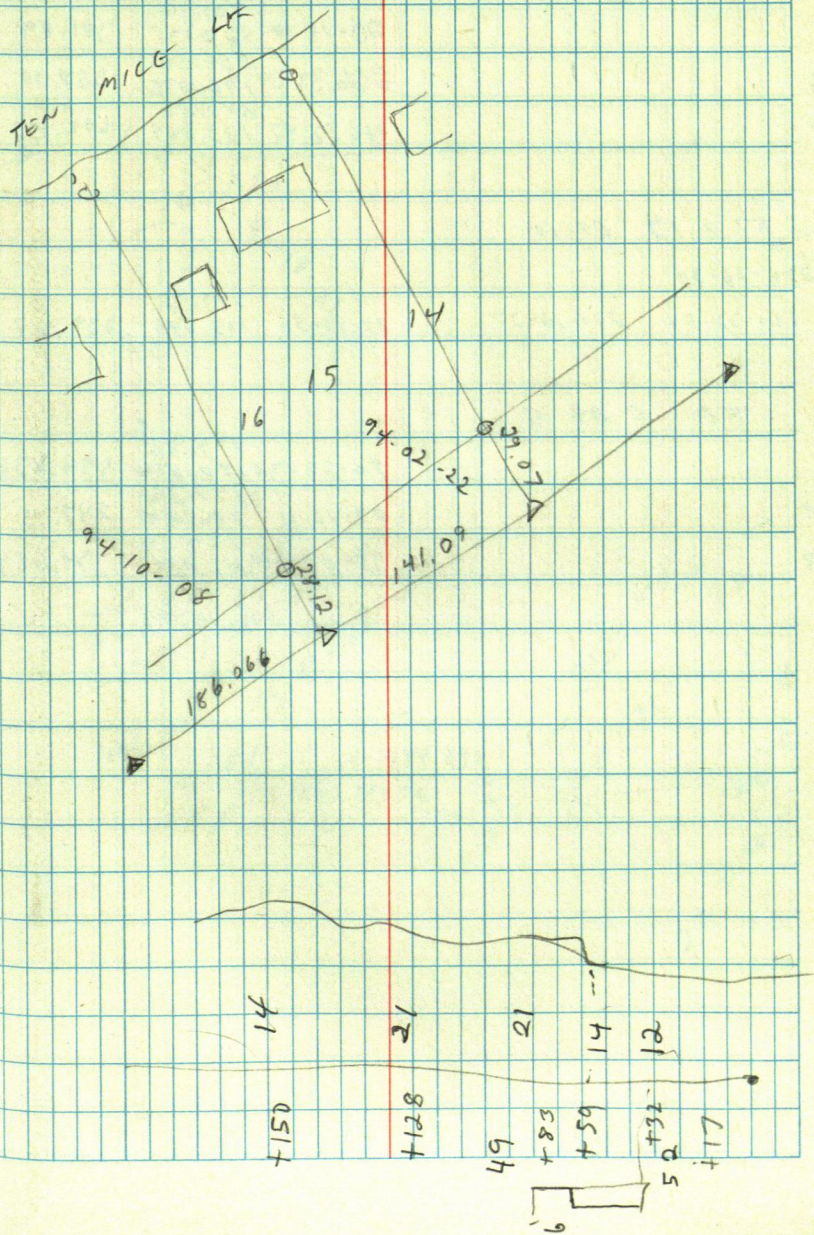
DAN FOSS

LOTS 15 + 16 + 5 1/2 14  
WHITE PINE BEACH

86-271 191.31  
58.312

91-09-42

ECURO  
R. TURNER  
12-3-95





GORDY REHER

T @ 2 BS 1

90-18-18	301.40 92.017	301.89
266.38-54	558.06 170.095	557.10
266.32-42	603.26 183.869	602.153

3

4

T @ 14 BS 10

270-16-30

5 180-32-54	270-16-27	82-45-36	340.05 103.645	339.785
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T @ C BS 5

90-32-36	494.86 150.834	494.836
89-46-12	247.72 75.525	247.75
95-03-30	134.59 41.035	134.084

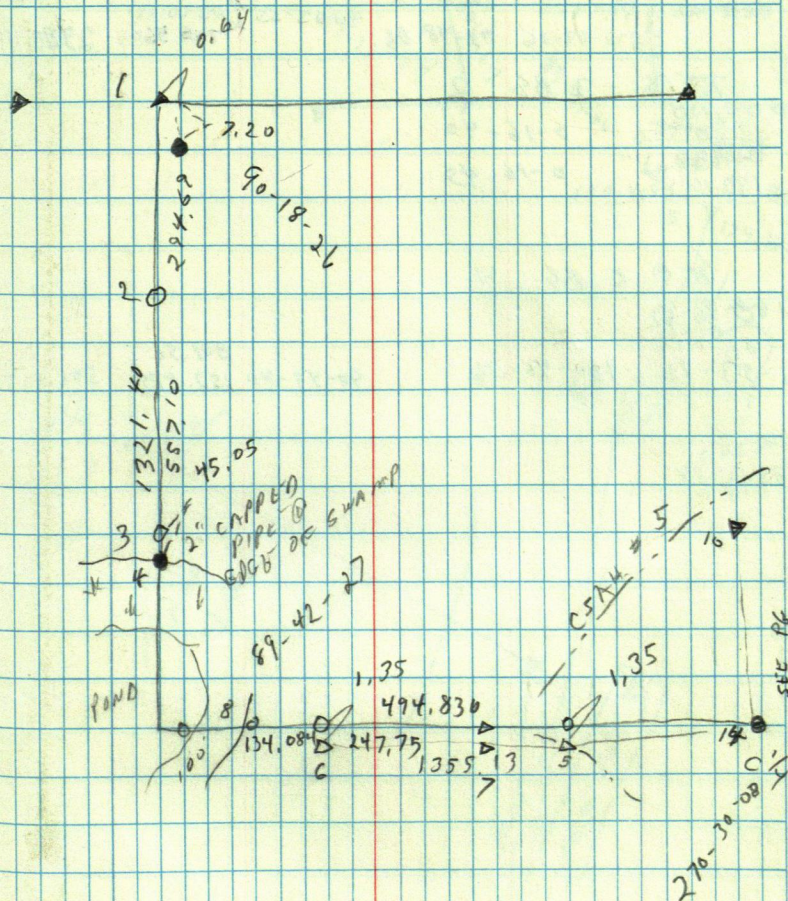
7

8

-13 CLR

G. CURR  
R. TURNER

12-7-95





$\pi$  2 BS 3

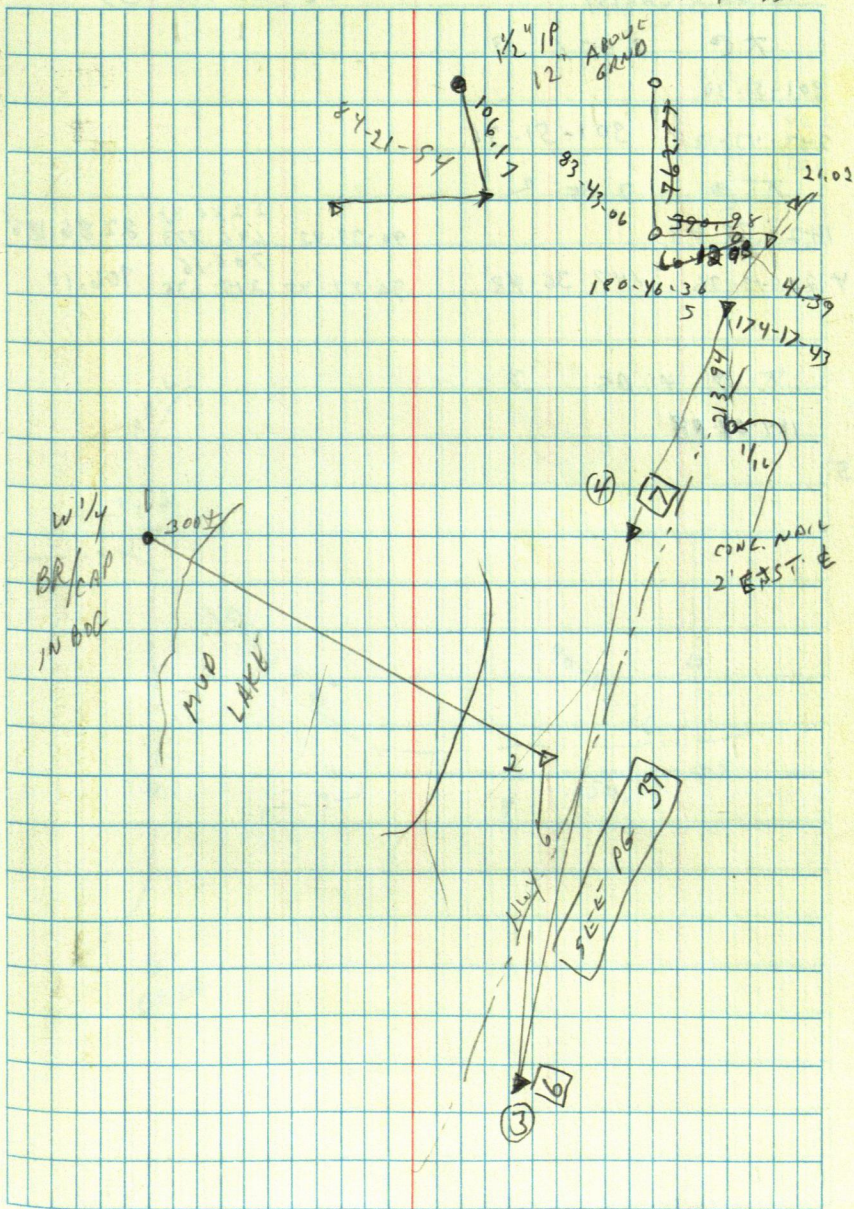
	$\Delta$	BS	2
	00.40		
	190.0		0-16-40
	0-1720		
4	190.16.45		0-16-45

70	5	BS	4
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60-12-08

E. CURD  
R. TURNER

12-12-95





LISA CHRIST

NW-SE-27-140-3)

T C 2 BS 1 3

301-51-30

243-47-12 301-51-36

T C 3 BS 2

142-36-48

90-35-42

2286.30

696.873

2286.186

4 285-13-36

142-36-48

90-42-45

706.16

215.236

706.10

T C 4 BS 3

184-01-18

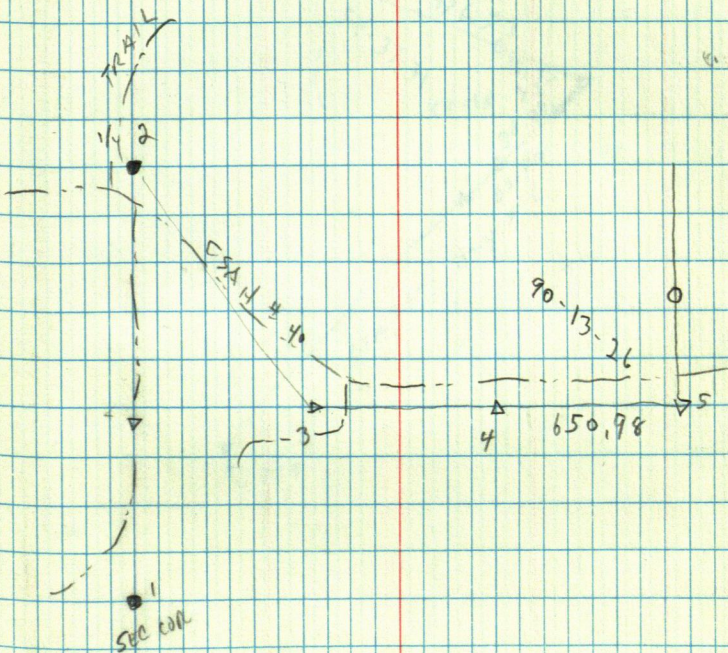
20' CLDY WINDY

20" SNOW ON GRND

E. CURRO

R. TURNER

12-14-95





JIM SWANKIER

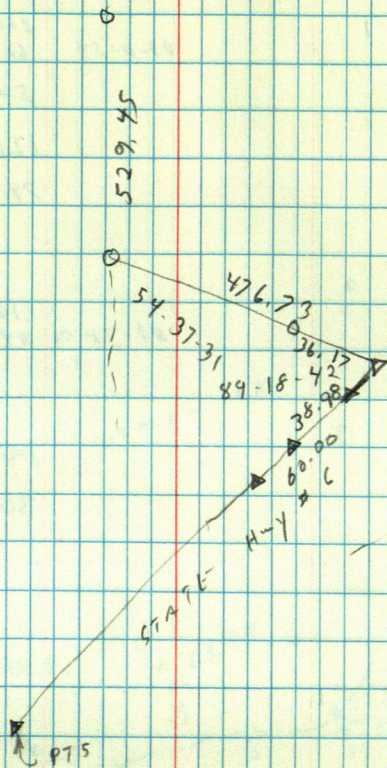
NE NE-31-142-25

25 CLOY

FIGURE  
R. TURNER

12-19-95

469.56





DON LARSON

2-18-140-28

K @ 2 BS 1

179-44-30

200.86

3

820-54

200.86  
61.220

4

304-25

54.55

5

340-03

121.46

6

182-20

74.43

K @ 3 BS 2

7

147-07-24

89-38-06

172.84  
37.997

8

K @ 7 BS 3

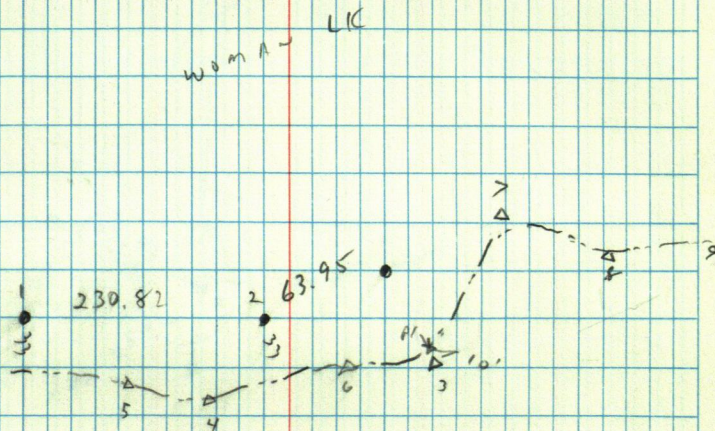
221.4736

189.16

9

218.0154

300.54





$\pi @ 2 \text{ BS } 1$

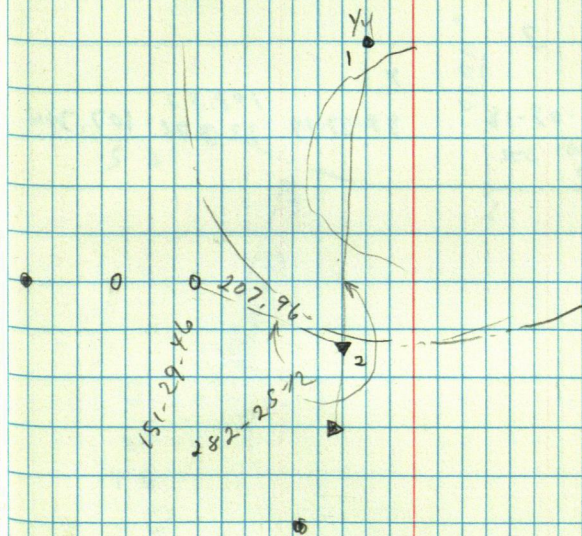
87.2054

207.38  
63.209

207.156

.80

207.96





JACOBS

TQ 2 BS 1

181-10-43

3 2-21-06 181-10-33

TQ 3 BS 2

140-23

90-12-36 713.41 126.006 413.403

4 280-45-48 140-22-54

91-10 339.26 103.404 339.184

210-31-12

92-06-54 168.04 51.218 167.924

5

TQ 4 BS 3

146-05-06

9

292-10-36 146-05-18

98-27-19 108.52 33.076 107.344

- 5 CLR

E. CURTO

R. TURNER

1-2-96

S D

221 N HASSO

SEC CON CSAH # 5

2

CSAH # 45

30-40

60 54



CHUCK ROBINSON

T @ 1/4 COR BS SEC COR

179-44-50

90-28-12 420.02  
128.019

T @ ~~SEC COR~~ BS 1/4 COR

269-46-53

~~370.09~~  
~~112.802~~

T @ 2 BS 1

89-19-12 370.09  
112.802 370.055

T @ 3 BS 1

89-42-12 644.55  
196.462 644.544

T @ 4 BS 3

85-28-24 237.39  
72.357 236.649

T @ 5 BS 4

90-33-12 264.65  
80.665 264.636

T @ 10 BS 11

89-10-00 303.96  
92.652 303.945

T @ 10 BS 11

273-43-18 129.36  
39.423 129.0769

T @ 6 BS 10

94-46-42 187.94  
57.279 187.2776

5 269-31-54

179-03-30

T @ 6 BS 10

271-44-54 161.75  
49.334 161.7274

12

T @ 9 BS 7

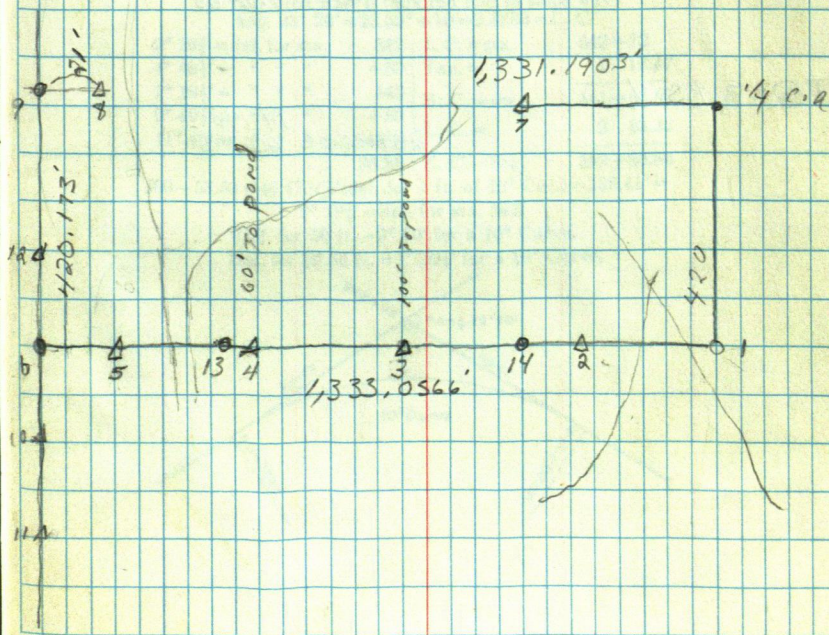
88-55-18 1169.70  
356.526 1169.4803

R. TURNER

T. TURNER

5-13-96

SEC COR





T@ 9 BS 7			
12 90-27-36	276-49-06	260.27 79.341	258.4456
180-55-24			

T@ 1/4 cor BS 7	93-03-24	161.94 493.60	161.7100
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T@ 31 BS 36			
44 84-31-35	90-39-18	1214.94 370.318	

T@ 36 BS 31			
45 286-53-14	89-21-06	868.86 264.126	

T@ 3 BS 2			
13	94-4606	245.62 74.860	

T@ 3 BS 4			
14	269-02-06	199.46 60.775	



334.58

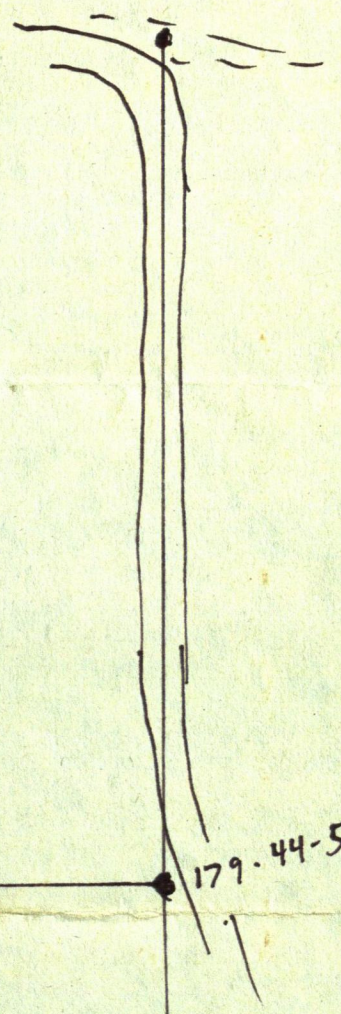
Tangents and Externals to a 1° Curve.  
Chord = 100 ft.

Int. Angle	Tangent	External	Int. Angle	Tangent	External	Int. Angle	Tangent	External
1°	50.00	.22	8°	400.66	13.99	15°	754.32	49.44
10'	58.34	.30	10'	409.03	14.58	10'	762.80	50.55
20	66.67	.39	20	417.41	15.18	20	771.29	51.68
30	75.01	.49	30	425.79	15.80	30	779.77	52.82
40	83.34	.61	40	434.17	16.43	40	788.26	53.97
50	91.68	.73	50	442.55	17.07	50	796.75	55.13
2	100.01	.87	9	450.93	17.72	16	805.25	56.31
10	108.35	1.02	10	459.32	18.38	10	813.75	57.50
20	116.68	1.19	20	467.71	19.06	20	822.25	58.70
30	125.02	1.36	30	476.10	19.75	30	830.76	59.91
40	133.36	1.55	40	484.49	20.45	40	839.27	61.14
50	141.70	1.75	50	492.88	21.16	50	847.78	62.38
3	150.04	1.96	10	501.28	21.89	17	856.30	63.63
10	158.38	2.19	10	509.68	22.62	10	864.82	64.90
20	166.72	2.43	20	518.08	23.38	20	873.35	66.18
30	175.06	2.67	30	526.48	24.14	30	881.88	67.47
40	183.40	2.93	40	534.89	24.91	40	890.41	68.77
50	191.74	3.21	50	543.29	25.70	50	898.95	70.09
4	200.08	3.49	11	551.70	26.50	18	907.49	71.42
10	208.43	3.79	10	560.11	27.31	10	916.03	72.76
20	216.77	4.10	20	568.53	28.14	20	924.58	74.12
30	225.12	4.42	30	576.95	28.97	30	933.13	75.49
40	233.47	4.76	40	585.36	29.82	40	941.69	76.86
50	241.81	5.10	50	593.79	30.68	50	950.25	78.26
5	250.16	5.46	12	602.21	31.56	19	958.81	79.67
10	258.51	5.83	10	610.64	32.45	10	967.38	81.09
20	266.86	6.21	20	619.07	33.35	20	975.96	82.53
30	275.21	6.61	30	627.50	34.26	30	984.53	83.97
40	283.57	7.01	40	635.93	35.18	40	993.12	85.43
50	291.92	7.43	50	644.37	36.12	50	1001.7	86.90
6	300.28	7.86	13	652.81	37.07	20	1010.3	88.39
10	308.64	8.31	10	661.25	38.03	10	1018.9	89.89
20	316.99	8.76	20	669.70	39.01	20	1027.5	91.40
30	325.35	9.23	30	678.15	39.99	30	1036.1	92.92
40	333.71	9.71	40	686.60	40.99	40	1044.7	94.46
50	342.08	10.20	50	695.06	42.00	50	1053.3	96.01
7	350.44	10.71	14	703.51	43.03	21	1061.9	97.57
10	358.81	11.22	10	711.97	44.07	10	1070.6	99.16
20	367.17	11.75	20	720.44	45.12	20	1079.2	100.75
30	375.54	12.29	30	728.90	46.18	30	1087.8	102.35
40	383.91	12.85	40	737.37	47.25	40	1096.4	103.97
50	392.28	13.41	50	745.85	48.34	50	1105.1	105.60

Corrections to be Added (T = Tangent. E = External.)

Int. Angle	Curve 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
5°	T = .02 E = .000	.03 .000	.05 .001	.06 .001	.08 .002	.10 .002	.11 .002	.13 .003	.15 .003	.16 .004	.18 .004	.20 .004	.21 .005	.23 .005
10°	T = .03 E = .001	.06 .003	.09 .004	.13 .006	.16 .007	.19 .008	.22 .009	.25 .011	.28 .012	.31 .014	.34 .015	.38 .017	.42 .018	.46 .020
15°	T = .04 E = .004	.10 .007	.14 .010	.19 .014	.24 .018	.29 .023	.34 .027	.39 .029	.45 .032	.51 .035	.53 .039	.58 .043	.63 .047	.68 .051
20°	T = .06 E = .006	.13 .011	.19 .017	.26 .022	.32 .028	.39 .034	.45 .038	.51 .045	.58 .051	.65 .057	.72 .063	.79 .070	.84 .076	.90 .083
25°	T = .08 E = .009	.16 .018	.24 .027	.33 .036	.40 .046	.49 .056	.58 .065	.67 .074	.75 .083	.83 .093	.90 .106	.99 .120	1.06 .127	1.14 .135





179.44-50

420.00

269.46.43

POND

KEEP THIS PART OF  
THE TRAV. CLOSE TO  
THE EDGE OF THE SWAMP

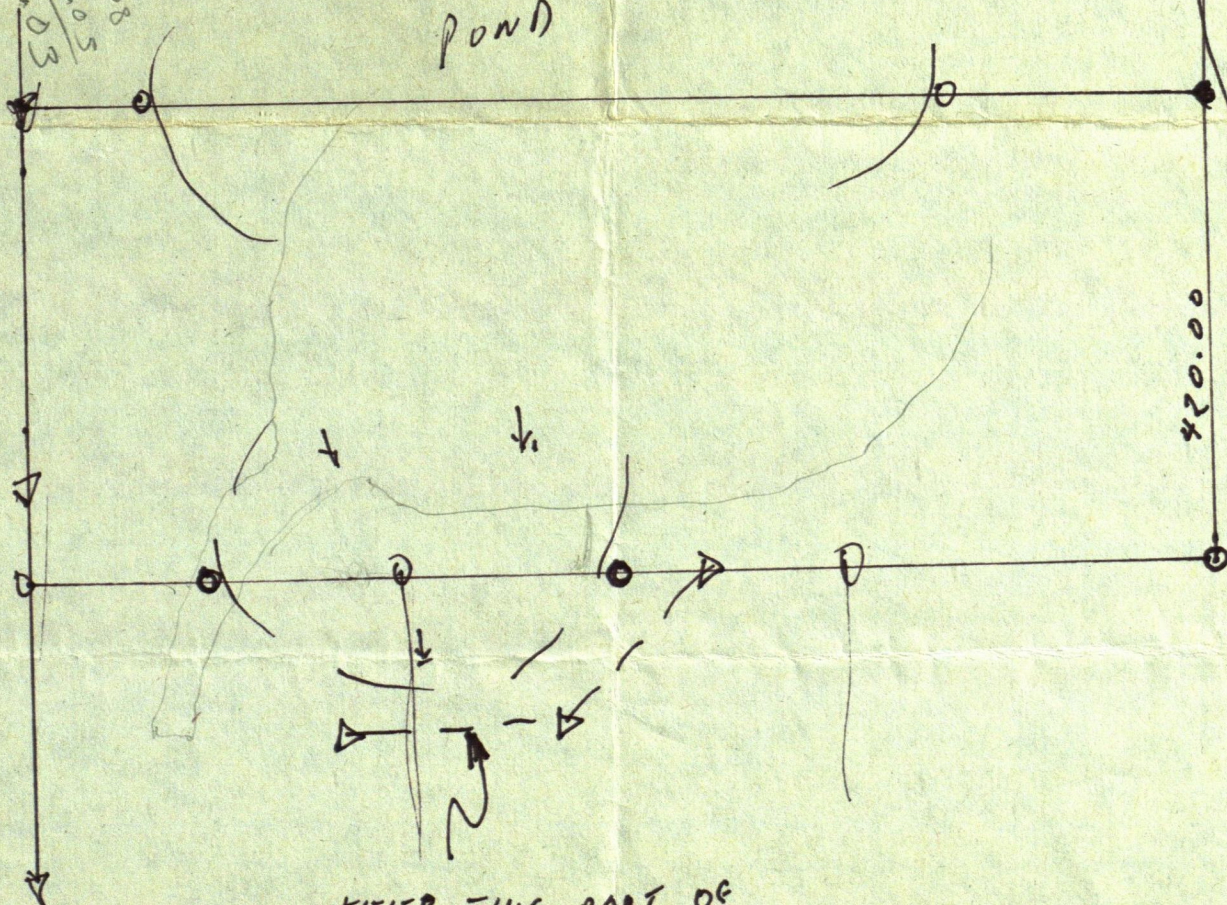
1046.81  
1190.83  
56.08  
1804.94  
1190.83  
246.11  
868.89  
264.823  
89-21-06  
868  
838  
30

90-39-18  
1214.94  
370.37

199.46  
60.775  
901-02-06  
445.08  
199.46  
445.69  
445.08  
890.116  
604.84  
285.62  
880.16  
055.612  
237.39  
18.83

255.62  
77.909  
94-46-06  
345.08  
370.05  
75.03

143.46  
245.68  
495.08





11	S	00-10-08	W	5290.704	9
9	S	89-28-31	W	2641.813	4
4	N	89-21-32	E	2345.650	31
31	S	39-31-47	E	13.107	7
7	S	89-36-26	W	2353.901	4



398.91



$$\begin{array}{r} 25 \\ 22 \\ \hline 13 \end{array}$$
$$\begin{array}{r} 402.57 \\ 122.697 \end{array}$$
$$\begin{array}{r} 4374 \\ 886 \\ \hline 5260 \end{array}$$

△ 334.08 ————— △ 204.69 △