

319

★ TELEDYNE

407

FIELD BOOK

INDEX

1-11	USFS	BURROWS LK
12	OT'S MC USFS	TOWNLINE LK
13-39	USFS	BURROWS LK
40	FLORENCE MINNETTE	2-30-178-29
41	ROBERTA RADCLIFF	35-142-30
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45	BOB JOHNSON	30-140-30
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55	JIM DE WERDT	24-142-28
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59	MILDRED BRANDT	9-139-30
61		5 + OUTLOT 29 HACK
62	LENGLE	28-140-29
63	MIKE SEMATUC	27-140-28
64	JIMMIES MITEL	LOTS 1 BLK 10 PARKSIDE AND WALKER

Mike

C/4 1902

29

54.93

Mike

68	R. GREEN	14-140-29
69	NACK CEMT.	
70	TOOTS BRENNEN	WEST. ADD NACK
71	VICTOR DAVIS	SANBURN MILLER PT
72	Jim GARNER	BRUCE EVELAND 5-138-30
73	Jimmies MOTEL	
75	V. DAVIS	
76	WADDE BRAMMER	BLKS 5 RIVER RIVER
77	SEACY	15-140-29
78	EVELYN MITCHELL	22-135-30
79	LONNIE JOHNS	33-139-30

C/4 1902

2A

54.93

BURROWS

NO1 SIGHT 2

set nail 1.49' wly of 3 on line = 4

NO4 BS 2

0-0-28
180-00-13
588-18-32
268-16-15

see page 3

4-2 F 1360.75
90-21-17 M 414.759
4-5 F 1360.75
4-5 F 1360.75
90-36-34 M 184.945

NO4 BS 5

0-0-20
180-00-10
271-34-07
91-34-06

see page 3

NO5 BS 4

0-0-19
180-00-18
180-00-18
0-0-16

5-4 F 606.72
89-32-35 M 184.929
5-6 F 307.91
91-41-10 M 93.852

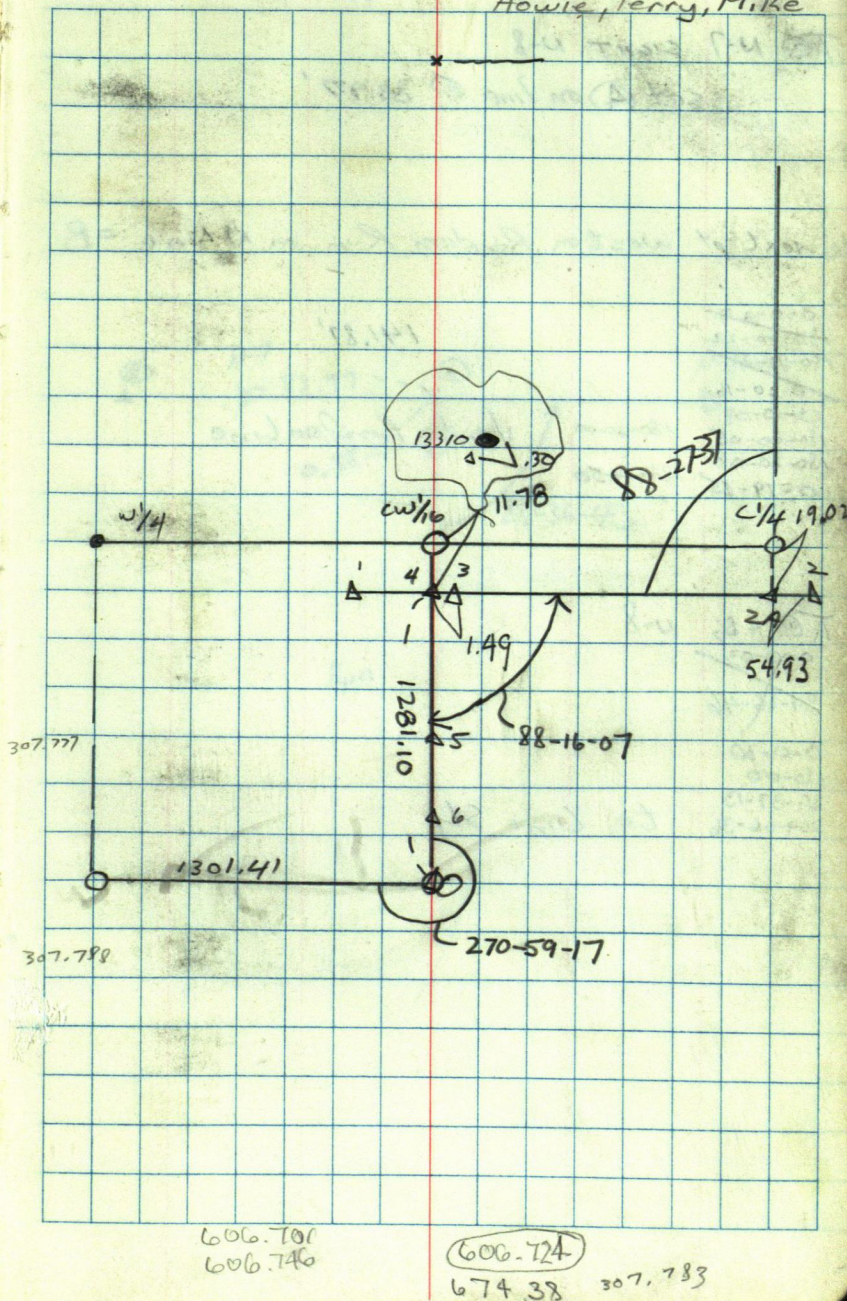
NO6 BS 5

0-0-35
0-0-27
180-00-27
0-0-21

88-36-00 F 307.88
M 93.810
93-53-00 F 367.42
M 111.988

March 1, 1988
P.C. 25°

Ken
Tom
Howie, Terry, Mike



2

π @ N-7 SIGHT N-8

set A on line @ 83.97'

To next pt Weston Random Run on N Line = B

141.87'

✓ into Random Line

π @ A B N-8

~~0-0-03~~

~~89-36-46~~

0-0-30

180-00

89-37-13

269-36-36

to Line Sk

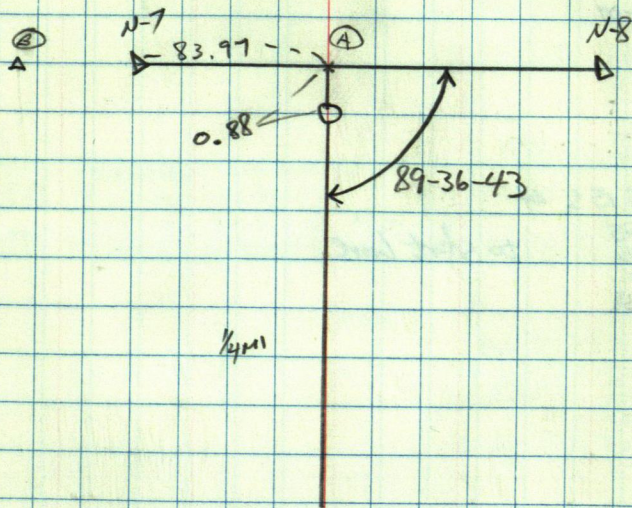
March 1, 1988

P.C. 32° PM

π Ken

Tom

2



3

π @ 4BS 2
 0-0-20
 180-00-13
 88-26-16
 ⑤ 268-26-12

π
 0-0-07
 180-00-05
 ⑤ 88-27-34-06
 268-② 91-34-07

π @ 2A BS 4

0-0-25
 179-59-46
 88-27-52
 268-27-38

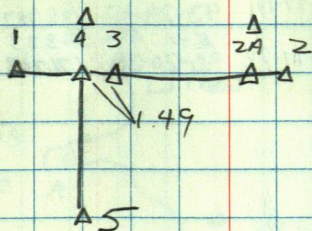
to start line

3/3/87

π Ken
 Tom

3

88-27-37
 25



4

Λ@ E-1 BS A

0-0-31	0-0-43	222-27-16	E-1-A	783.44 F	941
40	180-00-43		93-29-47	238.787 M	781.969
	822-27-59		E-1 E-2	563.33 F	
E-2	42-28-03	222-27-20	90-20-30	171.703 M	563.318
222-30-34					

Λ@ E-1 BS E-2

0-0-12		
180-00-00	137-32-29	
137-32-41		
A	317-32-4	137-32-41

Λ@ E-2 BS E-1

0-0-30	180-09-39	E-2 E-1	563.33 F	319
180-00-31		89-48-22	171.701 M	563.321
180-10-09		E-2 E-2A	180.71 F	
E-2A) 0-10-03	180-09-32	94-45-04	55.082 M	180.091

Λ@ E-2 BS E-2A

0-0-21		
180-00-27	179-50-31	
179-50-52		
E-1	359-50-54	179-50-25

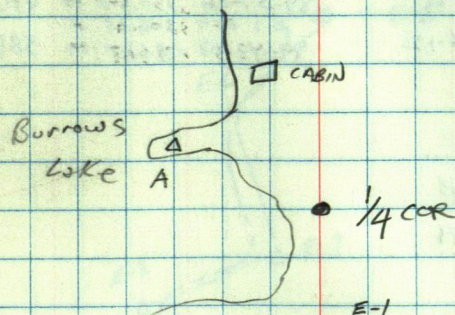
Λ@ E-2 BS E-1

0-0-36		
180-00-31	155-37-45	
155-38-24		
E-3	335-38-44	155-37-43
		2-3
		426.65 F
		90-14-08
		130.043 M
		426.644

Λ@ E-2 BS E-3

0-0-02		
180-00-10	204-22-27	
204-22-29		
E-1)	24-22-35	204-22-25

4



2 | 1
— | — f-5
11 | 12

5

T@E-3 BS E-2

0-0-07
 180-00-02 232-28-14
 232-28-21
 E-4) 52-28-14 232-28-12

E-3 E-2 426.65 F .146
 89-57-36 130.043 M 426.648
 E-3 E-4 586.23 F
 89-43-08 178.685 M 586.224

T@E-3 BS E-4

0-0-16
 180-00-19 127-31-48
 127-32-04
 E-2) 307-32-05 127-31-46

T@E-4 BS E-3

0-0-14
 180-00-15 143-21-46
 143-22-00
 E-3) 323-21-58 143-21-43

E-4-E-3
 586.25 F .229
 90-24-40 178.690 M 586.234
 E-4-E-5 678.04 F
 90-15-10 206.668 M 678.033

T@E-4 BS E-5

0-0-17 216-38-26
 180-00-26 216-38-43
 216-38-27
 E-3) 36-38-53

Ken Tom Cir 25°

March 3, 1988

T@E-5 BS E-4

0-0-24
 180-00-17 231-24-05
 231-24-29
 E-4) 51-24-33 231-24-06

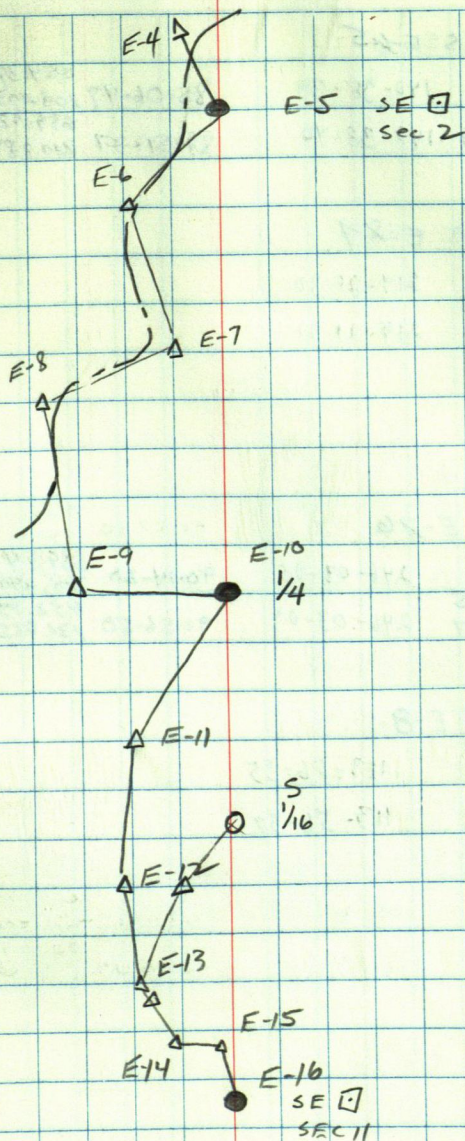
.035
 678.04 F
 89-53-00 206.668 M 678.038
 354.51 F
 95-06-32 102.056 M 353.102

T@E-5 BS E-6

0-0-27
 180-00-25 128-35-48
 128-36-15
 E-4) 309-36-15 128-35-50

Ken
 Tom

5



6

T@E-6 BS E-65

0-0-09

180-00-03 140-38-39

140-38-48

E-8) 320-38-43 140-38-40

85-06-47	354.34 F	.076
	108.003 M	353.051
	689.92 F	
89-51-37	210.287 M	689.914

T@E-6 BS E-87

0-0-25

180-00-28 219-21-30

5 219-21-55

E-8) 39-21-49 219-21-21

T@E-8 BS E-76

0-0-10

180-00-08 246-03-05

E-8) 246-03-15 246-03-09

90-14-20	689.94 F	.919
	210.290 M	689.924
	432.95 F	
90-56-50	131.965 M	432.892

T@E-8 BS E-8

0-0-30

180-0-32 113-56-55

6 113-57-25

E-8) 293-57-29 113-56-57

7

K@E-8 BS E-7

0-0-35	0-0-26			432.92 F	.886
180-00-22	180-00-18	104-00-42	89-13-15	131.955 M	432.88
124-01-10	104-01-08			1456.31 F	
E-9)	254-01-02	104-00-42	88-09-48	443.815 M	1455.558

K@E-8 BS E-9

0-0-18					
180-00-21		255-59-22			
E-7)	255-59-40				
	75-59-45	255-59-24			

K@E-9 BS E-8

0-0-32-25				1456.35 F	.557
180-00-18	105-33-21	91-53-30		443.899 M	1455.556
105-33-46				478.21 F	
E-10)	285-33-37	105-33-19	90-20-13	145.758 M	478.199

K@E-9 BS E-10

0-0-17					
180-00-22		254-26-45			
E-8)	254-27-02				
	74-27-05	254-26-43			

K@E-10 BS E-9

0-0-20				478.20 F	.200
180-00-18	299-54-01	89-51-43		145.758 M	478.201
299-54-21				947.04 F	
E-11)	119-54-15	299-53-57	90-20-47	288.65 M	947.019

K@E-10 BS E-11

0-0-05					
180-00-11		61-06-01			
E-9)	240-06-10	60-05-59			

March 4, 1988 T Ken

Clear 0° AM

Tom

E-10 = Aluminum Clp

I.P

GLD SIGN
YPOST

TS8N R2M

1/4	
5	5
11	12

$\pi @ E-11$ BS E-10

0-0-20

180-00-20 153-52-15

153-52-35

E-12) 333-52-36 153-52-16

89-43-45

90-39-05

947.06 F

288.162 M

543.68 F

165.76 M

1031

947.042

543.646

$\pi @ E-11$ BS E-12

0-0-19

180-00-27 206-07-54

206-08-13

E-10) 26-08-20 206-07-53

$\pi @ E-12$ BS E-11

0-0-24

180-00-05 134-20-37

134-21-01

E-13) 314-20-50 134-20-45

89-31-28

89-56-25

543.67 F

165.71 M

629.09 F

191.748 M

.648

543.64

629.089

$\pi @ E-12$ BS E-13

0-0-05

180-00-05 225-39-09

225-39-14

E-11) 45-39-12 225-39-07

$\pi @ E-13$ BS E-12

~~0-0-19~~

0-0-23 0-0-24

180-00-59 180-00-19

221-31-55 221-31-58

E-14) 41-31-58 41-31-58

221-30-49

221-30-54

221-30-54

221-30-54

221-30-54

629.13 F

191.763 M

384.56 F

117.212 M

.11

629.13

384.336

$\pi @ E-13$ BS E-14

0-0-22

180-00-27 138-29-08

138-29-33

E-12) 318-29-33

0-0-08

180-00-05

138-29-16

318-29-13

138-29-08

138-29-08

9

 $\pi @ E-13 \text{ BS } E-12$

0-0-45

180-00-43

56-46-10

56-46-55

 $E-13A) 236-46-48 \quad 56-46-05 \quad 93-23-47 \quad 415.92F \quad 173$

126.764M

415.174

 $\pi @ E-13 \text{ BS } E-13A$

0-0-40

180-00-42

303-14

303-14-40

 $E-12) 123-14-35 \quad 303-13-53$
 $\pi @ E-14 \text{ BS } E-13$

0-0-30

180-00-13

0-0-30

180-00-20

88-17-30

384.54 F

117.192 M

384.342

102-05-4924

102-05-25

90-37-35

358.17 F

109.170 M

358.147

 $E-15) 282-05-25$

282-05-20

90-37-35

358.17 F

109.170 M

358.147

 $\pi @ E-14 \text{ BS } E-15$

0-0-27

180-00-27

257-54-50

257-55-17

257-54-48

 $E-13) 77-55-15$

257-54-48

 $\pi @ E-15 \text{ BS } E-14$

0-0-22

180-00-18

241-00-40

89-36-20

358.17 F

109.171 M

358.161

241-01-02

241-00-39

92-24-10

320.96 F

97.829 M

320.677

 $E-16) 61-00-57$

241-00-39

92-24-10

320.96 F

97.829 M

320.677

 $\pi @ E-15 \text{ BS } E-16$

0-0-23

180-00-31

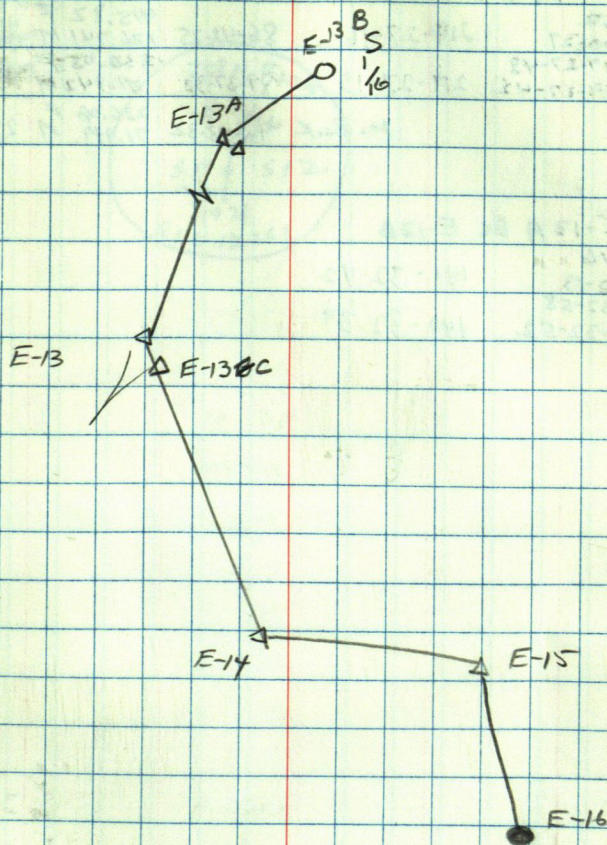
118-59-28

118-59-51

118-59-28

 $E-14) 298-59-59$

118-59-28



TQ E-13 A B S E-13

0-0-32			415.82 F	
180-00-27	219-27-16	86-48-25	126.741 M	415.171
219-27-48			236.05 F	
E-13B 39-27-42	219-27-15	89-37-30	71.942 M	236.034
			236.06 F	
	M. Back	90-43-32	71.999 M	236.037

TQ E-13 A B S E-13B

0-0-16	
180-00-13	140-32-42
140-32-58	
E-13 320-32-52	140-32-39

BRSS
CJP
MM

TSPN R250
5'16
511 512
1978
RLS 12261

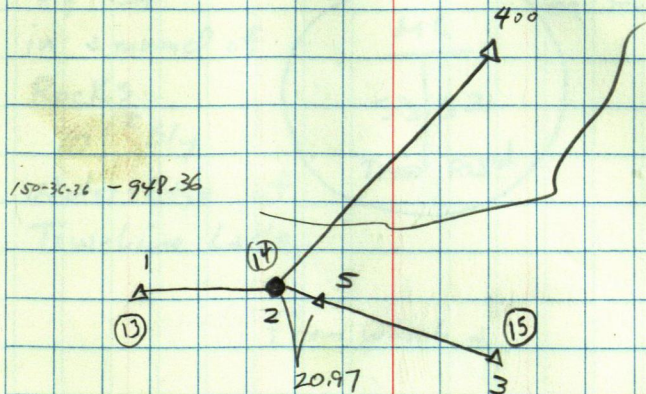
No 2BS1

0-0-06		939.49 F	
180-00-15	146-45-39	286.358 M	939.454
146-45-45		1546.95 F	
4) 326-45-50	146-45-35	477.506 M	1546.646

No 4BS2

0-00-00		1546.91 F	
	89-04-45	477.500 M	1546.706

1 180-12-40	2 150-36-36	2010.81	948.36
3 148-37		817.40	
4 138-50		481.4	
5 93-33		299.84	
6 56-34		496.5	
7 55-48		589.35	
8 39-39		751.7	
9 32-58		989.25	
10 13-57		1055.2	
11 8-24		1193.0	
12 0-57		1256.15	Just shy of Acc. Rd.



5 wly Edge Shank
Center Bent over

12

March 7, 1988

P.C. 38°

Ken

Tom

12

BRASS Cap Monument

up 29"

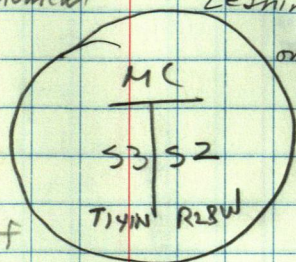
in a mound of

Rocks

10' Sly

Waters Edge of

Townline Lake

Leaning NELY
on Seawall

From which ↓

Birch Bears N71E 5.10'

SC. MC S2 BT

NAIL NLY BASE

Red Oak Bears S41E 21.28'

SC MC S2 BT

NAIL IN SWLY BASE

White Oak Bears N63W 41.75

SC MC S3 BT

NAIL IN SLY BASE

8' steel Post with F.S. Sign 54-9

~~54-9~~ swly 4.24' to Nly edge @ Mon.
Height

13

TP INT PT A BS B

0-0-02

179-59-51

57-26-35

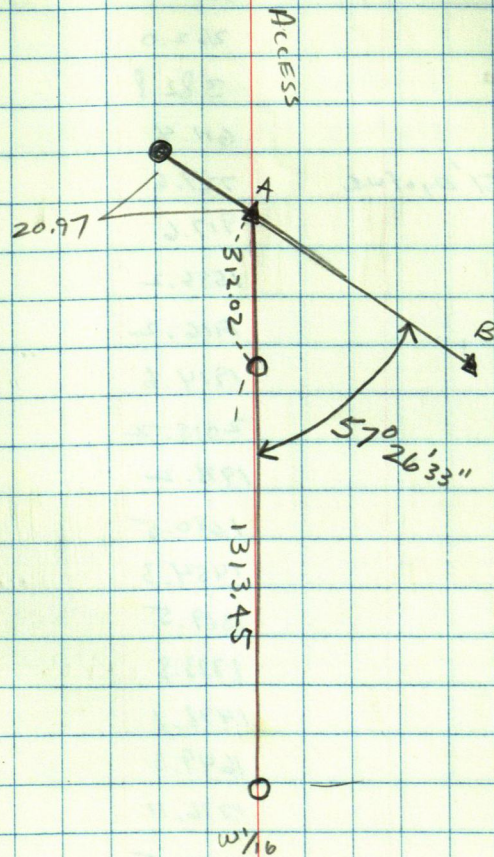
237-26-28

57-26-33

57-26-37

Ken
Tom

13



14

A@4 BS 2

¹³	356-39	1198.61
¹⁴	343-38	782.09
¹⁵	327-39	660.61
¹⁶	294-59	262.0
¹⁷	259-04	382.8
¹⁸	252-30	611.4
¹⁹	252-30 51' E of W.E.	727.6
²⁰	250-55	917.6
²¹	229-29	1556.2
²²	228-01	1916.2
²³	221-07	1914.6
²⁴	217-43	2015.2
²⁵	216-24	1978.2
²⁶	216-21	1680.5
²⁷	211-19	1454.3
²⁸	208-08	1369.5
²⁹	198-10	1373.8
³⁰	195-17	1478.1
³¹	194-49	1649.3
³²	186-49	1776.11
³³	183-01	2076.5
³⁴	180-13	2012.5

March 9, 1988

Clear 32°

A Ken

Tom

14

15

K@4 BS 2

0-8-05

180-00-01

173-40-47

35 173-40-52

35 353-40-48

173-40-47

90-02

2081.89 F

634.562 M 2081.884

K@6 BS 4

00-00

179-59-50

75-08-26

90-10-40

2081.93 F

7634.570 M

1425.68 F

435.767 M

.895

2081.907

36 75-08-26

7) 255-08-12

75-08-22

90—

1429.68 F

435.767 M

1429.674

37 240-71

243.7

Shot 26 times

38 221-26

179.6

39 199-32

457.2

APX
M C

40 127-33

1666.9

APX
M C

41 126-32

1614.4

42 118-37

1517.1

43 109-22

819.3

44 96-05

754.0

45 80-40

999.9

46 80-04

1112.1

47 79-40

1353.2

48 W ^{False} Waters

48 70-11

1571.0

49 64-56

1394.2

50 60-09

1354.0

5/9/88

15

16

T

0

18

35 17.51

2 35

60-20

1533.6

52 48-13

1642.8

T 53 44-05

1524.9

54 32-11

1458.1

55 30-24

1388.8

56 17-08

1264.9

✓ 2 times

57

58

59

60

61

62

63

64

65

66

67

68

69

70

71

72

73

74

75

76

77

78

79

80

81

82

83

84

85

86

3/9/88

16

T 7 BS 6

0-0-0148

351-06-12

70-03-05

1429.69 F

.679

435.720 M

1429.68 F

180-00-26

351-06-52

171-06-40

351-06-1F

T 7 BS 1/4

0-01-10

180-01

227-06-20

47-50-00

89-34-40

1859.20 F

566.688 M

1859.148

7.54

17

0-00-08

130-00-15

99-10-11

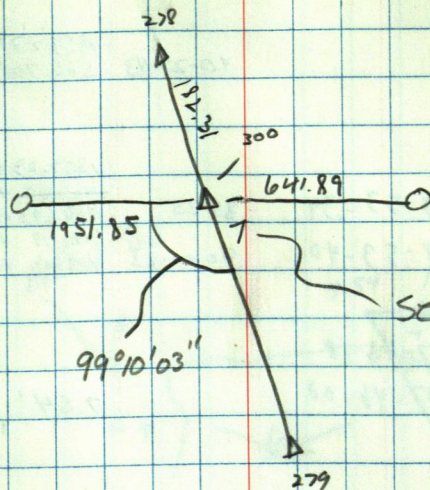
279-10-16

99-10-03

99-10-01

March 10, 1988
O.C. 35° AMTKen
Tom

17



18

1/4 to 7

90-27-43 1859.27 F
566.705 M 1859.20

T@ 7 BS 1/4

0-0-11			1859.23 F	.174
180-00-10	8-53-39	89-35	566.693 M	1859.172
8-53-50	8-53-40	90-01-28	1429.75 F	1429.785
188-53-50			435.801 M	

~~227-00-02~~

180-00-00

227-46-18

227-46-20

47-46-00

227-46-00

7.54'

~~0-0-20~~

134-57-29

0-0-14

134-57-01

180-00-07

134-57-15

314-57-10

134-57-03

88-00-15 1313.13 F
400.242 M 1312.328

T@ 8 BS 7

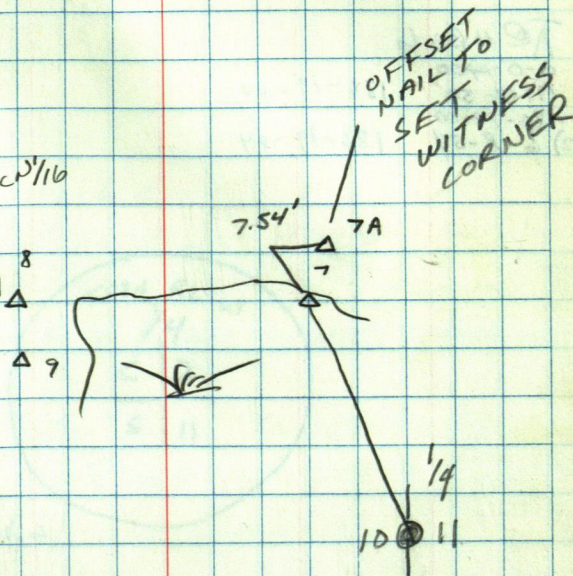
0-0-27			1313.17 F	.314
180-00-30	88-29-10	92-04-30	400.253 M	1312.301
88-29-37	88-29-05	83-06-40	125.35 F	124.445
268-29-35			38.207 M	

3/10

18

90-27-43 1859.27 F
566.705 M

APPR C 1/16



19

T@6657

0-0-22

180-00-37

284-51-27

284-51-49

4) 104-51-59

284-51-22

T@4356

0-0-400

179-59-50

186-19-00

✓ 86-19-00

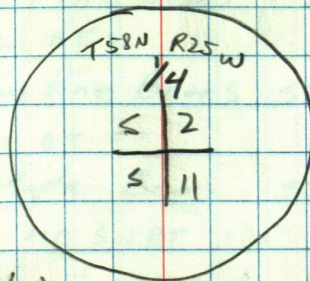
2) 6-8-54

186-19-04

3/10/88

T Ken
Tom

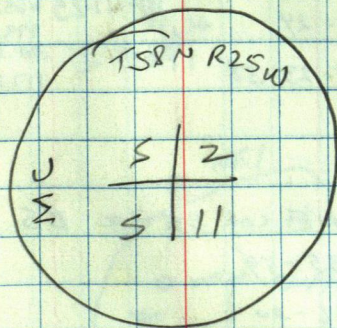
19

3/14/87
Aluminum
Capped
Monument

From which

9" Birch	S 70 E	9.47	Nly Base
old BT	1/4 S 11 BT		
6 1/2" Birch	N 20 E	10.87	Wly Base
old BT	1/4 S 2 BT		
6" Spruce	N 87 W	48.39'	48
old BT	1/4 S 2 BT		Sly Base

3/14/88
Aluminum
Capped
Monument



From which ↓

10" White Pine Bears N36E 23.57

OLD BT MC S2 BT

NW 1/4 Base

18" Norway Pine Bears S61E 30.60

OLD BT MC S11 BT

S1/4 Base

7" Twin Maple Bears S74E 65.62

NEW BT MC S11 BT

S1/4 Base

Mon is 10'± Ely Waters Edge of
Burrows Lake

21

T@NE COR SEC 2 BS wly

0-0-01		89-41-25	455.47 F	
180-00-10	272-24		199.788 M	655.459
08-24-07				
NE-1) 92-24-08	272-23-58	88-41-25	384.66 F	
			117.246 M	384.561

T@NE-1 BS NE COR SEC 2 BS NE-1

0-0-17				
180-00-20	87-35-59			
87-36-16				
NE-1) 867-36-20	87-36-00			

T@NE-1 BS NE COR SEC 2

0-0-10			384.70 F	.565
180-00-01	179-54-15	91-29-10	117.257 M	384.57
179-54-25			428.37 F	
NE-2) 359-54-14	179-54-13	91-40-55	130.566 M	428.182

0-0-10				
180-00-01	178-58-36			
178-58-40			565.89 F	
NE-3) 351-58-29	178-58-28	90-47-30	172.481 M	565.83

0-0-29				
180-00-19	178-25-46			
178-26-15			671.30 F	
NE-4) 351-26-10	178-25-51	88-22-20	204.616 M	671.022

T@NE-1 BS NE-2

0-0-22				
180-00-30	180-05-40			
180-06-02				
NE-5) 0-06-12	180-05-42			

T@NE-1 BS NE-3

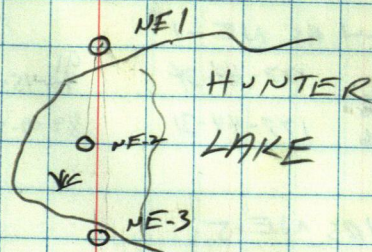
0-0-24				
180-00-33	181-01-34			
181-01-58				
NE-6) 1-02-04	181-01-31			

3/14/88

T Ken
Tom.

21

N-8

35 36
2 11

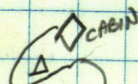
Δ NE4

NE6 ○ ← 1.4 Plastic Cap
RLS 9293

Δ NE5

Δ NE7

Δ NE8



○ 1/4

Δ X

22

T@ NE-1 BS NE-4

0-0-29

180-00-35

181-34-13

181-34-42

NE-5 7-34-46

181-34-11

T@ NE-4 BS NE-1

0-0-06

180-00-05

177-44-34

91

40-45-20

671.31 F

1.013

207.616 M

670.993

177-44-40

177-44-31

89-09-40

440.52 F

440.472

NE-5 35-44-36

134.27 M

T@ NE-4 BS NE-5

0-0-25

180-00-35

182-15-31

182-15-56

NE-1 27-46-03

182-15-28

T@ NE-5 BS NE-4

0-0-16

180-00-12

179-49-19

91-02-15

440.56 F

.479

134.283 M

410.486

179-49-35

NE-7 359-49-30

179-49-18

92-23-30

401.86 F

401.502

0-0-15

180-00-07

0-0-19

0-0-34

NE-6 180-00-25

0-0-18

93-40-50

153.94 F

153.622

46.921 M

T@ NE-5 BS NE-7

0-0-27

180-00-40

180-10-43

180-11-10

NE-4 0-11-16

180-10-36

T@ NE-5 BS NE-6

0-0-08

180-00-15

359-59-37

359-59-45

NE-4 359-59-52

359-59-37

3/15/88

22

23

K@NE-7 BS NE-5

0-0-16			401.80 F	.51
180-00-11	180-00-39	87-51-00	122.40 M	401.518
180-00-55			242.31 F	
NE-5) 0-0-45	180-00-34	87-40-20	73.854 M	242.106

K@NE-7 BS NE-8

0-0-43				
180-00-48	179-59-31			
180-00-14				
NE-5) 0-0-20	179-59-32			

K@NE-8 BS NE-7

0-0-02			242.40 F	.105
179-59-53	179-53-42	92-49-50	73.884 M	242.104
179-53-44			539.38 F	
1/4) 359-53-33	179-53-40	90-48-32	164.404 M	539.326

K@NE-8 BS 1/4

0-0-25				
180-00-37	180-06-12			
180-06-37				
NE-7) 0-0-50	180-06-13			

K@1/4 BS NE-8

0-0-25			539.34 F	.313
180-00-23	280-03-45	89-21-55	164.388 M	539.30
280-04-10			537.94 F	
A) 100-04-05	280-03-42	90-31-30	163.961 M	537.91

K@1/4 BS A

0-0-10				
180-00-16	79-56-15			
79-56-25				
NE-7) 259-56-30	79-56-14			

March 15, 1988

P.L. 20°

TKen

Tom

27

0-0-16		182.30
to X 180-02-52	77.22'	
180-02-36		

24

Port to f N Line
S 1/2 SE 1/4 Sec 11

0-0-07
180-00-01 304-51-20
304-51-27
124-51-23 304-51-22

N@ABS B

0-0-05
180-00-02 124-51-20
124-51-25
1) 304-51-23 124-51-21 92-08-30 621.55 F
0-0-18 124-49-44 189.447 M 621.11
180-00-08
124-50-02
2) 304-49-55 124-49-47 90-16-50 1129.35 F
344.230 M 1129.378

N@ABS 1

0-0-16
180-00-15 235-08-26
235-08-42
B) 55-08-42 235-08-27

N@ABS 2

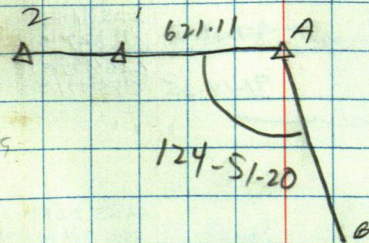
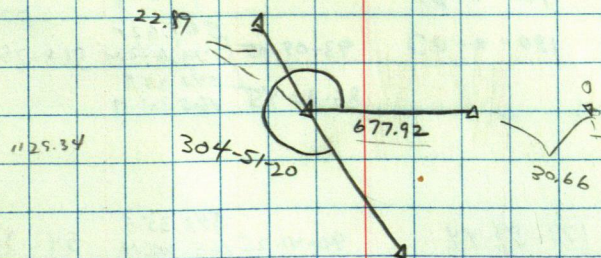
0-0-19
180-00-20 235-10-16
235-10-35
B) 55-10-39 235-10-19

3/15/88

24

91-40-25 678.57
206.825
83 35

91-40-25 678.20
206.712



25

$\pi @ \frac{1}{4} \frac{2}{11}$ BS Pt 209.72' Wly

0-0-05 179-59-55 267-57-47

267-57-52 267-57-50

87-57-45 267-57-50

87-01-20 569.56 F
173.603 M 568.79

$\pi @$ 1 BS $\frac{1}{4}$

0-0-13 180-00-06 180-0-03

180-00-16 180-0-03 93-09-05 569.62 F .774

2) 0-0-09 180-0-03 93-09-05 173.622 M 568.759

89-30-45 542.33 F
165.301 M

$\pi @$ 2 BS 1

0-0-21 179-59-44 90-41-25 542.35 F 542.303

180-00-10 179-59-46 92-53-00 165.305 M 225.88 F

3) 359-59-56 179-59-46 92-53-00 68.850 M 225.596

$\pi @$ 3 BS 2

0-0-14 91-26-24 87-28-40 225.81 F 225.59

180-00-11 91-26-19 91-14-25 68.827 M 1264.99 F

4) 91-26-38 91-26-19 91-14-25 385.571 M 1264.691

$\pi @$ 4 BS 3

0-0-10 180-01-22 88-50 1265.02 F .706

180-00-12 180-01-18 84-54-28 385.576 M 1264.751

5) 180-01-30 180-01-18 84-54-28 261.34 F 260.203

See page 27

March 16, 1988

O.C. 30°

π Ken

π Tom

25

267° 57' 47"

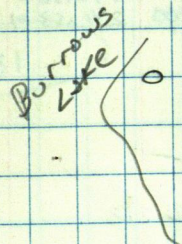
1336.68

FS

NY

568.79

568.76



542.31

91-26-40.

2

CN

1/16

ROAD

4

5

26

 Pt of N Line S $\frac{1}{2}$ SE $\frac{1}{4}$
 Sec 11

NO 2BS A

00-28

180-00-26

180-00-27

0-00-24

179-59-59

179-59-58

89-48-10

1129.35 F

344.234 M

,345

1129.35

89-41-00

790.86 F

241.053 M

790.843

3/17/88

 T Ken
 Tom

26

790.81

28

N@2BS1

0-0-14			584.03 F	
180-00-10	179-59-56	90-27-55	178.010 M	584.004
180-00-10			486.55 F	
3) 0-0-05	179-59-55	90-30-25	148.30 M	486.53

N@3BS2

0-0-40			486.53 F	.523
180-00-35	179-59-50	89-41-20	148.292 M	486.517
180-00-30			244.73 F	
4) 0-0-26	179-59-51	93-02-30	74.593 M	244.383

N@4BS3

0-0-20			244.67 F	.390
180-00-00	90-10-12	87-18-50	74.575 M	244.399
90-10-32			255.08 F	
5) 270-10-15	90-10-15	92-14-15	77.750 M	254.887

N@5BS4

0-0-10			255.05 F	.898
180-00-12	179-59-59	88-05-53	77.738 M	254.906
180-00-09			292.07 F	
0-0-10	179-59-58	95-21-35	89.021 M	290.789

			291.88 F	.764
	84-56-40		88.963 M	290.74

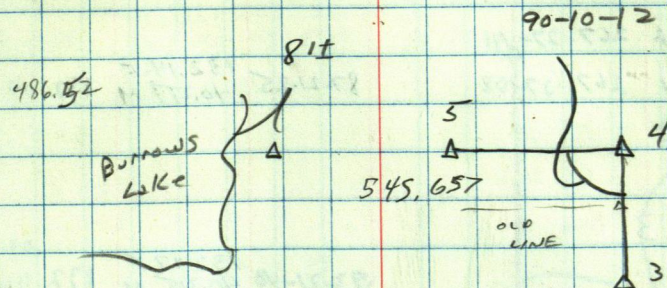
Ken
Tom

March 18, 1988

28

584.01

486.53



ROAD

2

1

TR 2 BS 1

180° set 3 @ 84.67'

TR 3 BS 1

~~0-0-50~~

~~267-27-11~~

0-0-08

180-00-06 267-27-11

267-27-19

4) 87-27-14 267-27-08

87-21-25 132.14 F
40.277 M 132.00

TR 4 BS 3

5) 180°

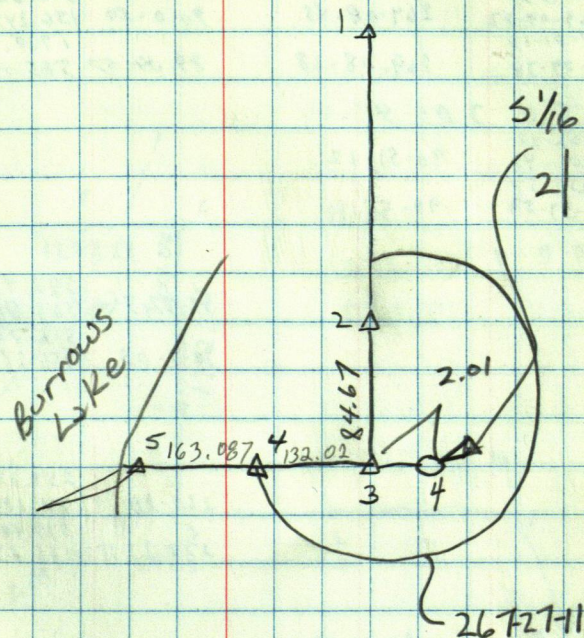
93-21-40 132.27 F
40.315 M 132.04

100-58-30 166.14 F
50.640 M 163.102
31-10 165.84 F
79-36 50.548 M 163.073

March 18, 1988
P.C. 30 Very Windy

T Ben
Tom

29



163.087
132.02
295.107

TE 2 BS 1

89-45-20 1129.36
744.233 1129.351

180-00

3 89-42-20 790.94 790.977

1920.328

TE 3 BS 1

0-0-57

269-09-42 269-08-45 90-0-50 512.62 512.615

180-01-10

4 89-09-38 269-08-28 89-09-57 565.449 1920.726

TE 3 BS 4

0-02-45

180-02-42 90-51-12

90-57-57

1 270-57-53 90-51-11

TE 4

5 92-37-31 547.46 546.884

3 90-1-05 512.73 512.729

1059.614

268-10-39 253.22 253.08

272-23-23 547.40 546.922

TE 6 BS 4

00-02-29

180-02-30 90-53-37 87-49-07 800.51 799.729

90-58-06

7 270-56-11 90-53-41 89-44-50 538.17 538.123

TE 6

BS 7

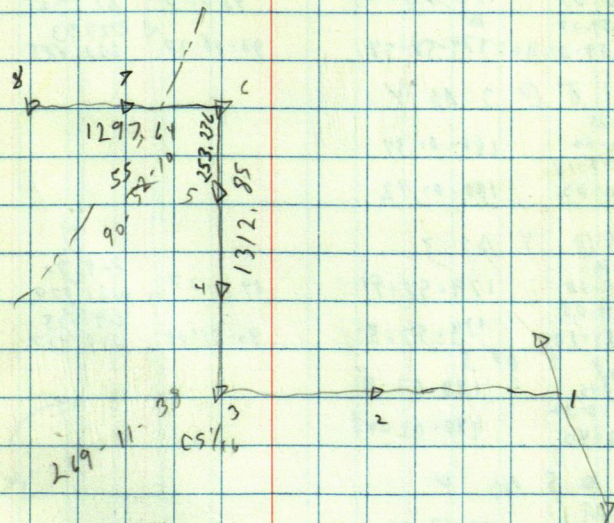
0-0-36

180-0-42 269-06-25

269-07-01

4 89-07-09 269-06-27

E. COLO
H. COOK
T. KUHEFSKI
M. KAMANN 3-23-88



π	1	135	2		
0-1-48				609.22	
180-1-48	57-27	48	88-31-17	185.689	609.006
57-27-38				202.07	
3 237-27-34	57-27-46		84-59-10	61.55	201.229

π	0	3	85	1			.262
0-0-01						202.21	
181-0-03		179-59-09			95-27-37	61.636	201.296
179-59-10						729.93	
4 359-59-01		179-58-58			90-46-27	222.485	729.863

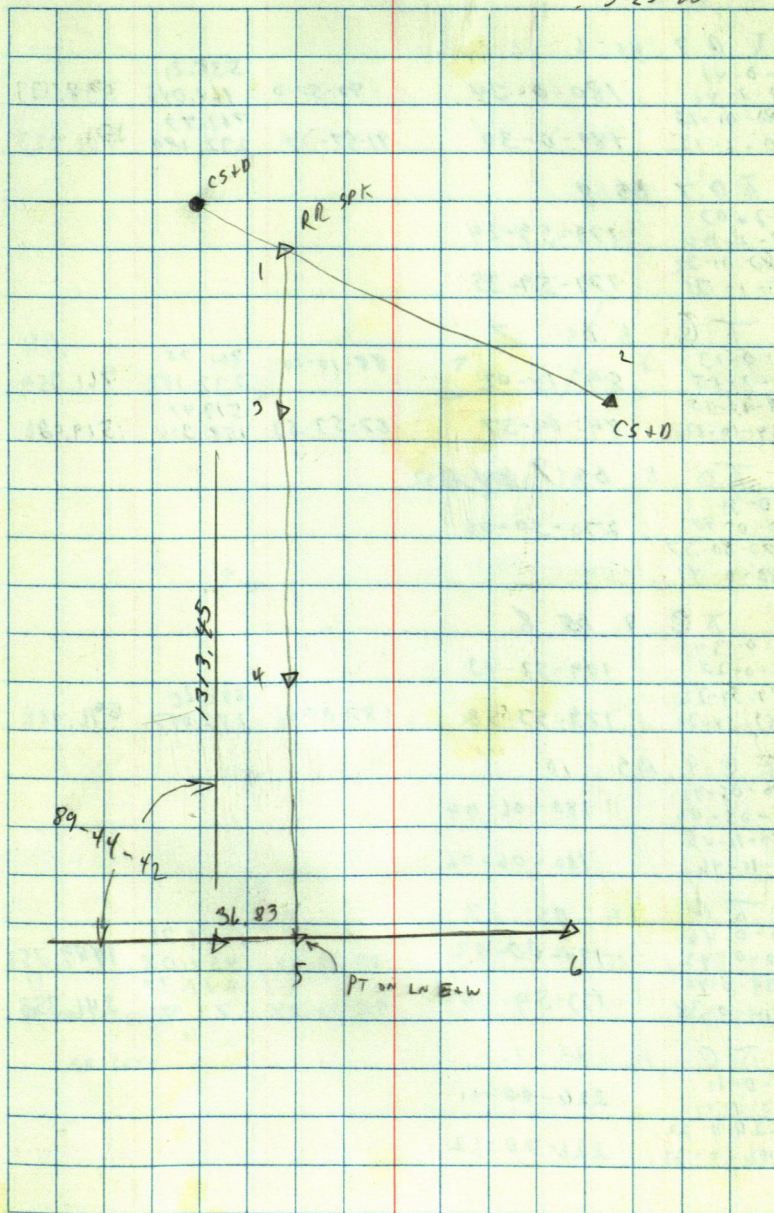
0-1-18	179-57-51	89-21-37	729.90	729.86
120-1-18			222.479	
129-59-06			692.15	
359-59-10	179-57-52	90-55-09	210.967	692.057

0-2-35	90-17-10
90-19-45	90-17-20
180-02-25	
270-19-45	

TC5 B5 C	
8-0-34	
180-0-34	269-42-53
269-43-32	
4 89-43-26	269-42-52

35° CLR

3-23-88



3-25-88

T 07 BS 6

0-0-41			538.21	
180-0-42	180-0-34	90-57-0	164.046	538.133
180-01-15			761.77	
0-0-1-12	180-0-30	91-57-32	232.189	761.323

T 07 BS 8

0-2-07				
180-2-06	179-59-29			
180-01-32				
0-1-35	179-59-35			

T 0

8 BS 7

0-0-13			761.75	.341
180-0-15	89-10-02	88-10-10	232.182	761.359
89-10-15			519.44	
9 264-10-12	89-09-57	87-57-53	158.324	519.086

T 0

8 BS 9

0-0-31				
180-0-40	270-50-06			
270-50-37				
7 180-0-41				

T 0

9 BS 8

0-0-39				
180-0-28	179-53-43			
179-54-22			597.26	
10 357-54-20	179-53-58	87-05-06	182.047	596.488

T 0 9

BS 10

0-0-5-41				
180-05-40	180-06-04			
180-11-45				
8 0-11-46	180-06-06			

T 0

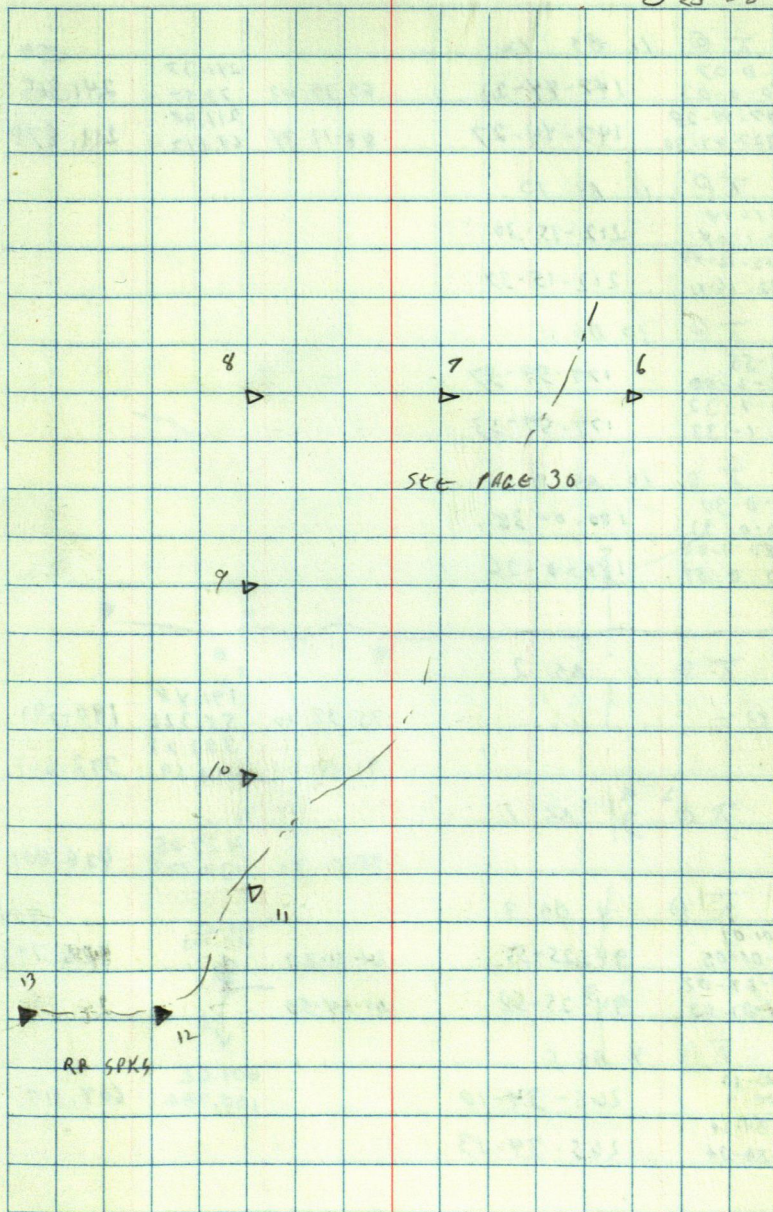
12 BS 13

0-0-46			1489.76	
180-0-42	134-00-02	89-53-54	454.08	1489.753
134-0-48			241.37	
11 314-0-38	133-59-56	90-46-04	73.57	241.353

T 0

12 BS 11

0-0-11				
180-0-11	226-00-11			
226-0-22				
13 46-0-23	226-00-12			



$\pi @$	11 BS 12			
0-0-07			241.37	359
180-0-03	147-44-21	89-39-02	27.57	241.365
147-44-28			211.98	
10 327-44-30	147-44-27	88-12-34	24.613	211.878

$\pi @$	11 BS 10	
0-1-14		
180-1-04	212-15-30	
212-16-44		
12 32-16-41	212-15-37	

$\pi @$	10 BS 11	
0-1-55		
180-2-00	179-59-37	
180-1-32		
9 0-1-33	179-59-33	

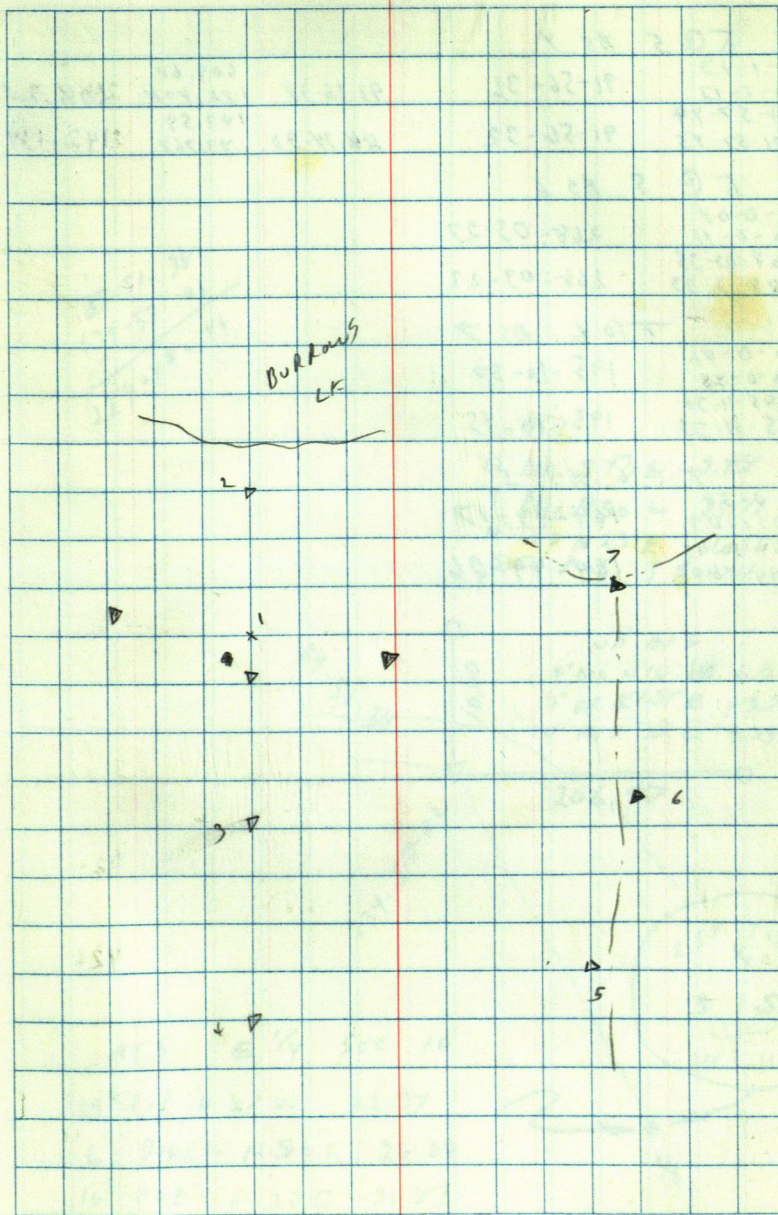
$\pi @$	10 BS 9	
0-0-30		
180-0-32	180-0-38	
180-1-08		
11 0-0-58	180-0-26	

$\pi @$	1 BS 2			
180-		95-32-10	191.48	
			58.326	190.591
3		91-17-40	392.71	
			119.696	392.604

$\pi @$	3 BS 1			
4		95-51-31	429.05	
			130.773	426.804

$\pi @$	4 BS 3			
0-01-07			428.83	774
180-01-05	94-25-55	84-21-27	130.703	426.743
94-27-02				
5374-27-03	94-25-58	87-34-50		

$\pi @$	4 BS 5			
0-00-14			609.62	
180-00-11	265-34-10		185.784	609.117
305-34-24				
385-34-24	265-34-13			



K @ 5 BS Y

0-1-13	91-56-36	92-36-38	609.60	608.968
180-1-13			185.808	
91-57-49	91-56-32	84-34-30	143.59	142.134
6371-57-45			73.268	

K @ 5 BS 6

0-0-08	268-03-27
180-0-11	
268-03-35	268-03-22
88-3-23	

K @ 6 BS 7

0-0-46	195-10-50
180-0-48	
195-11-36	195-10-45
515-11-35	

K @ 6 BS 5

0-0-58	164-49-17
180-1-09	
164-50-15	164-49-06
7344-50-15	

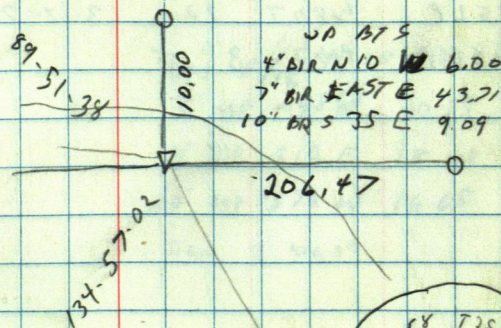
84-51-38
134-57-02
224-48-40

BT'S

12" DIR S 43 W 3.48
4" DIR N 50 W 25.72
4" WD N 23 E 66.52
SIGN POST 3' SOUTH

UP BT'S

4" DIR N 10 W 6.00
7" DIR E 45 E 43.71
10" DIR S 35 E 9.09



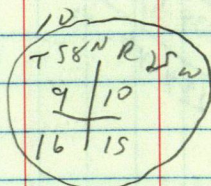
BT'S E 1/4 SEC 10

14" POP N 87 W 22.37
6" DIR N 50 E 26.00
16" POP S 30 E 31.73
7" DIR N 40 W
4" DIR S 88 E

OLD PTS

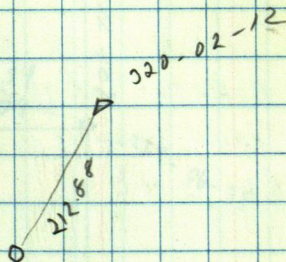
91-3-42 212.71 212.176
67.832

BTS SW COR SEC 10
5" BIRCH N 60 W 11.64 OLD
6" BIRCH N 25 E 24.09 OLD
6" BIRCH N 60 E 16.27 OLD
6" BIRCH S 45 W 21.95 OLD
6" BIRCH S 85 E 17.84 NEW



FSLP WEST 10' 3-17-22 12" ASP
SIGN POST 3' E

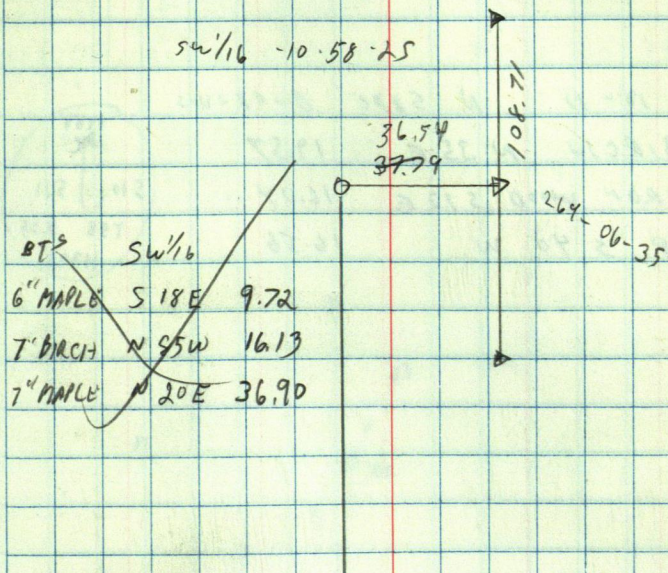
4-6-88



BTS W 1/4 N LN SEC 10
8" ASP N 48 E 20.25
5" BIR S 12 E 18.62
10" ASP S 70 W 16.65
SIGN 3' WEST

W 1/4 SEC 10 S LINE 10

BTS
6" BIRCH N 80 W 14.48
10" ASP N 25 W 12.19
10" ASP N 85 E 25.20



CY4 SOC 27-60-27

3" TAM N45 W 26.65

3" TAM S50 E 17.08

3" TAM S25 W 21.48

MC 10-11 N SCAPE BURROWS

8" BIRCH N35 E 19.57

4" IRON WOOD S12 E 16.04

6" ASP S40 W 16.56

1488
MC
S10 S11
758 R25
11995

n
D
43
= 0 mc
12
D

94-13-06 541.02
164.904 539.554

Σ 0 1 05 3

0-0-36
180-0-30 270-18-20 91-24.58 851.25
270-0-56 216.75 850.999
2 90-18-56 270-18-26 96-39-50 86.265 215.284

Σ 0 4 05 3

100-0-0 96-17-54 289.80 288.084
91-27-47 88.33 191.96
58.509 191.896

535
52
E'16

3

4

2.52

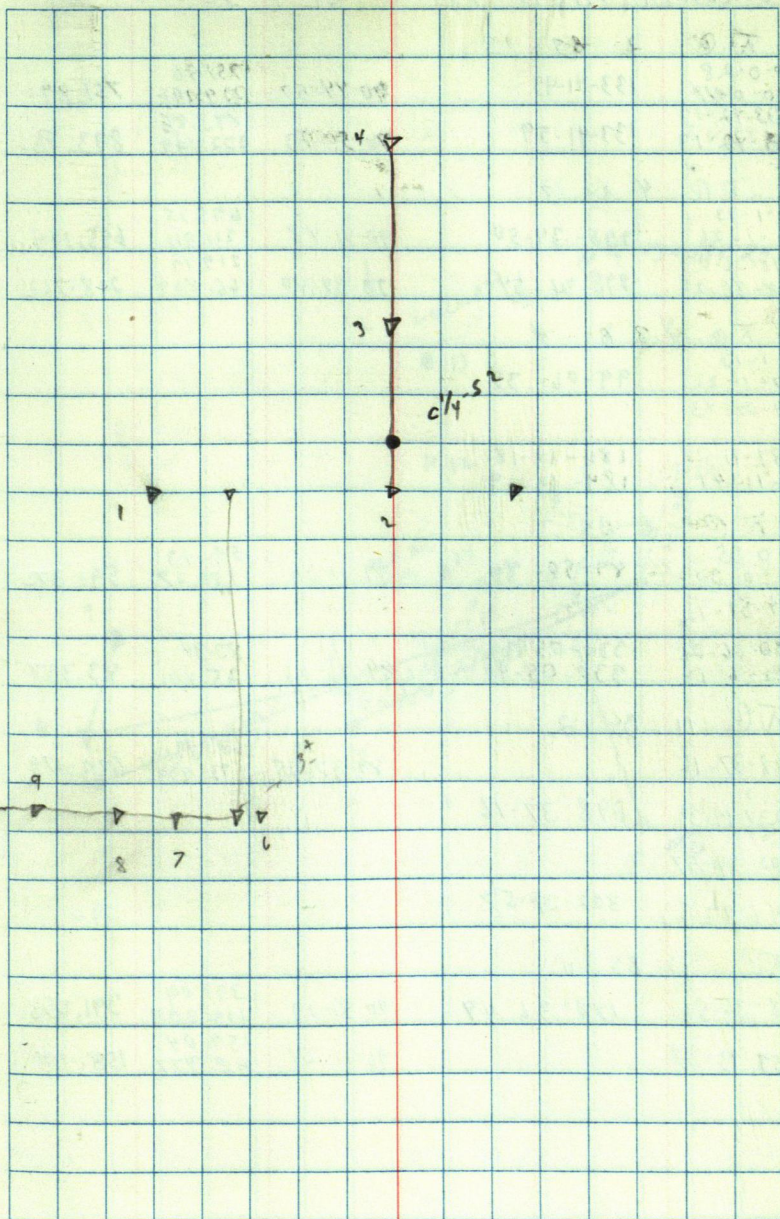
539.554
518.26
510
515
E'16

$\pi @$	2	BS	1
0-0-31			
0-0-32			
88-28-45			
3268-28-46	88-28-17	89-40-44	
4 88-28-48		88-08-48	1328.12
		89-22-59	404.812
			1328.039

$\pi @$	7	BS	6
180			
8			
		98-55-43	181.19
			58.228
		89-02-22	436.64
			133.087
			436.575

$\pi @$	8	BS	7
9	180-00		

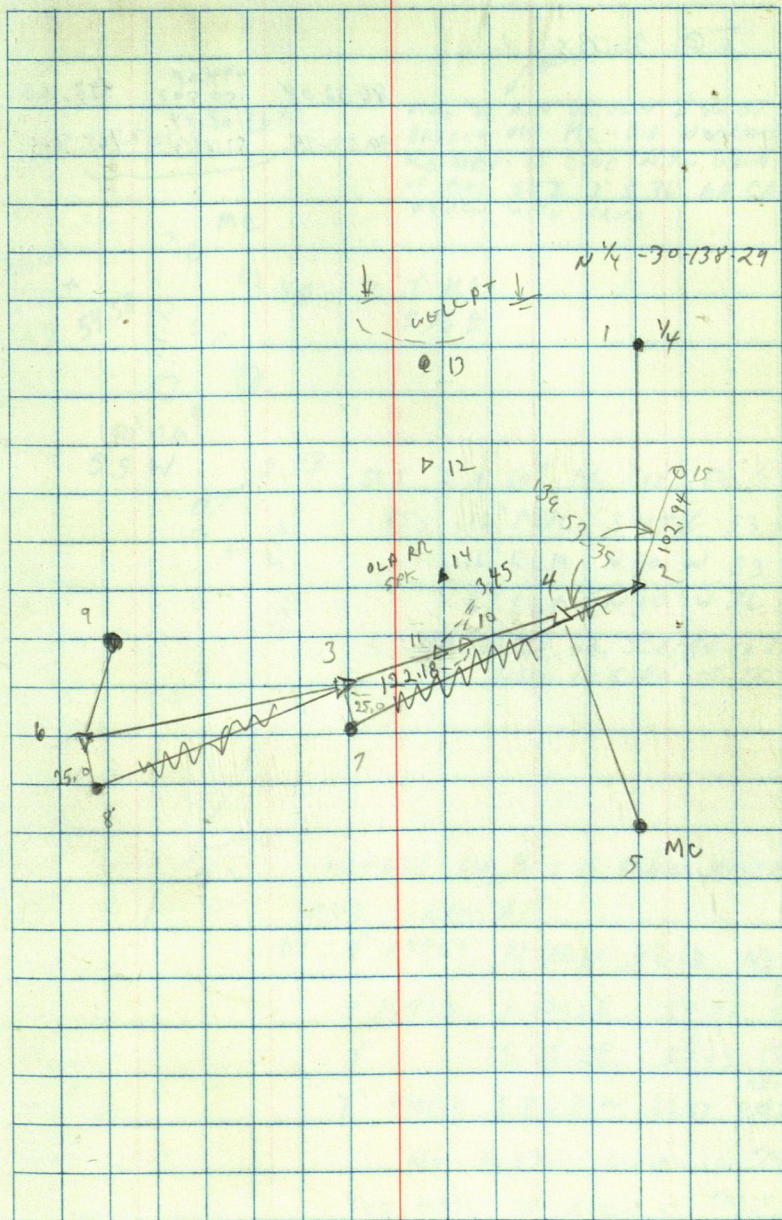
$\pi @$	9	BS	8
0-1-38			
180-1-28	179-20-34	88-25-50	361.01
179-22-12			110.033
10 359-22-10	179-20-42	97-0-50	323.86
			98.716
			321.441



FLORENCE MINETTE

GL 2 - 30-138-29

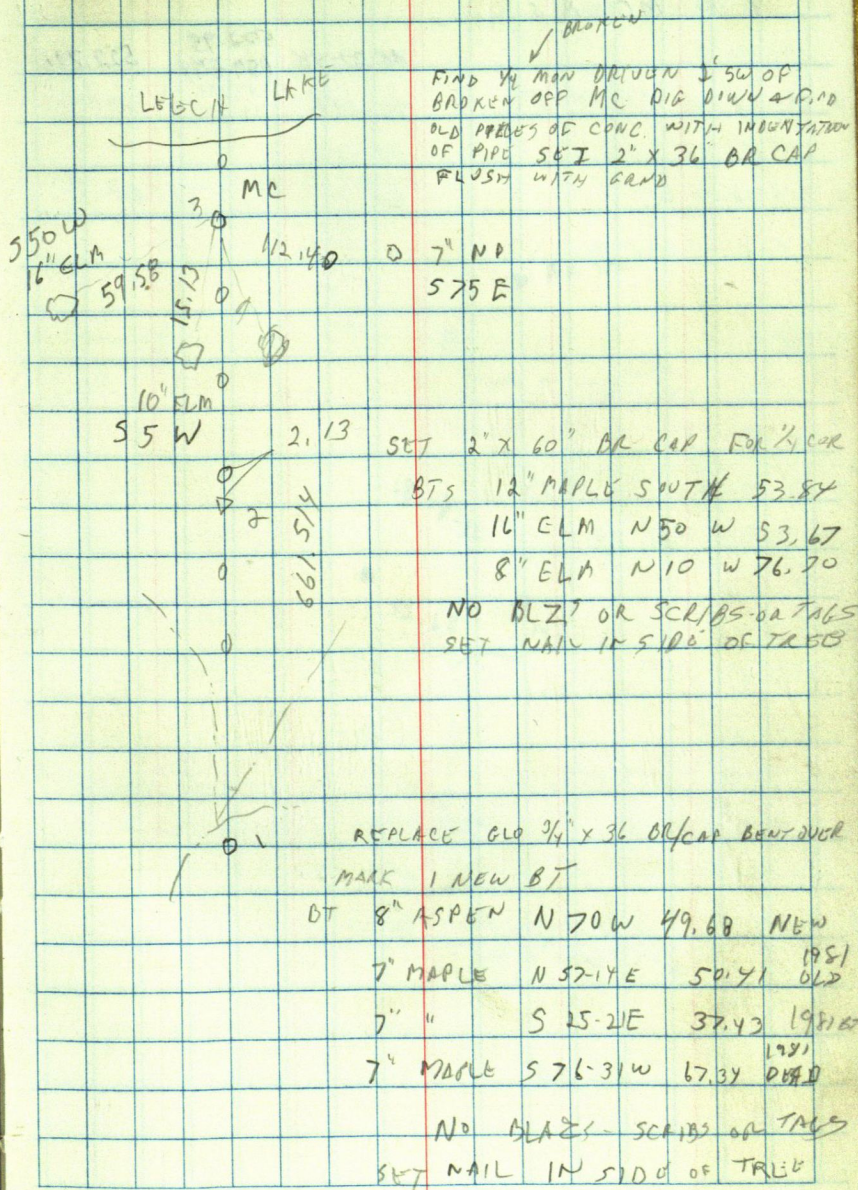
KQ 2 BS 3				
0-0-28	133-41-45	90-44-57	751.96	751.89
180-0-14			224.196	
133-42-13			843.86	
3 133-42-13	133-41-59	90-50-23	272.449	893.756
KQ 4 BS 3				
0-1-13			695.25	
180-1-26	298-34-50	90-41-48	211.911	695.194
298-36-03			219.19	
5 118-36-20	298-34-54	93-34-40	66.809	218.762
KQ 3 BS 4				
0-1-10				
180-1-22	99-06-35			
99-07-43				
7 184-11-28	184-10-18			
6 4-11-41	184-10-19			
KQ 6 BS 3				
0-0-35			591.43	
180-0-30	89-50-37	87-11-29	180.22	591.372
89-51-12				
18 330-06-06	330-05-31		83.34	
159 150-6-10	330-05-40	89-46-01	25.401	83.337
KQ 11 BS 2				
298-37-16		89-37-45	633.19	633.178
360			172.999	
12 237-14-33	298-37-16			
597				
302-24-57				
14 244-49-53	302-24-57			39.91
KQ 12 BS 11				
178-36-53	178-36-49	90-41-19	391.09	391.058
			119.203	
13 359-13-37		96-11-24	159.04	
			48.727	158.114



AO 2 05 1

3 180-00

86-32-04	494.08 150.592 168.84	493.168
94-27-15	51.463	168.345



ROBERT GREEN
A C MC B S

88.37-78 522.95 522.796
159.394

RR SPR

18.04-12

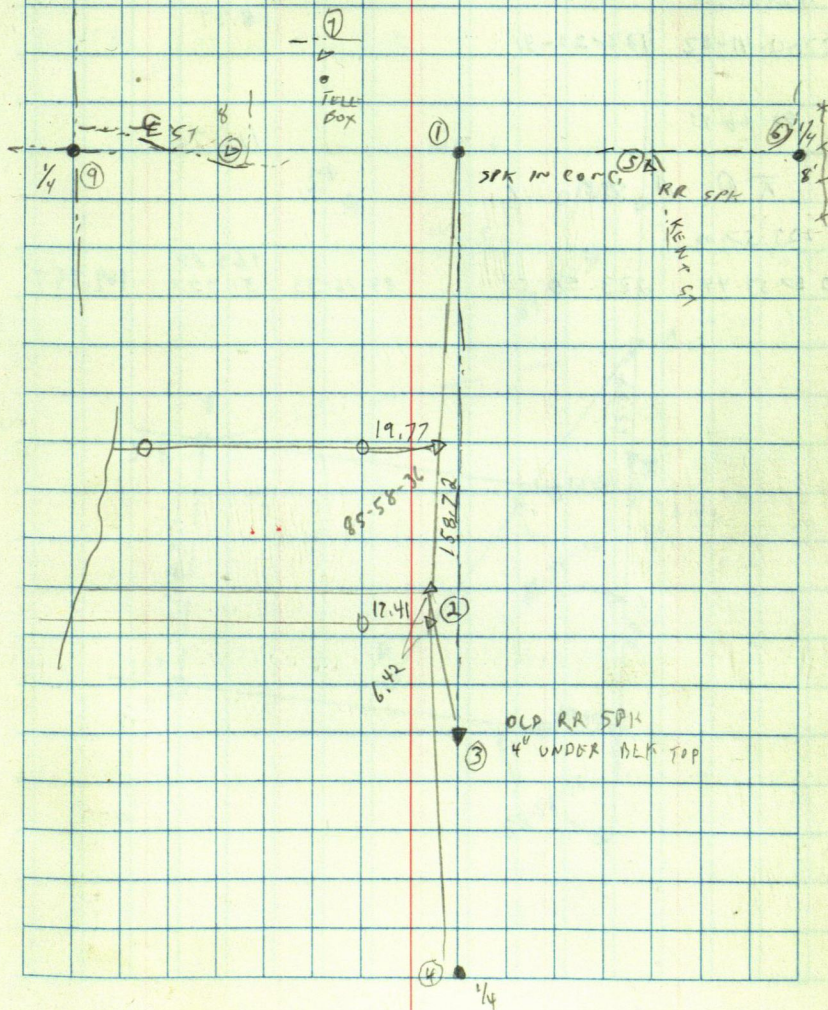
92.68

MC

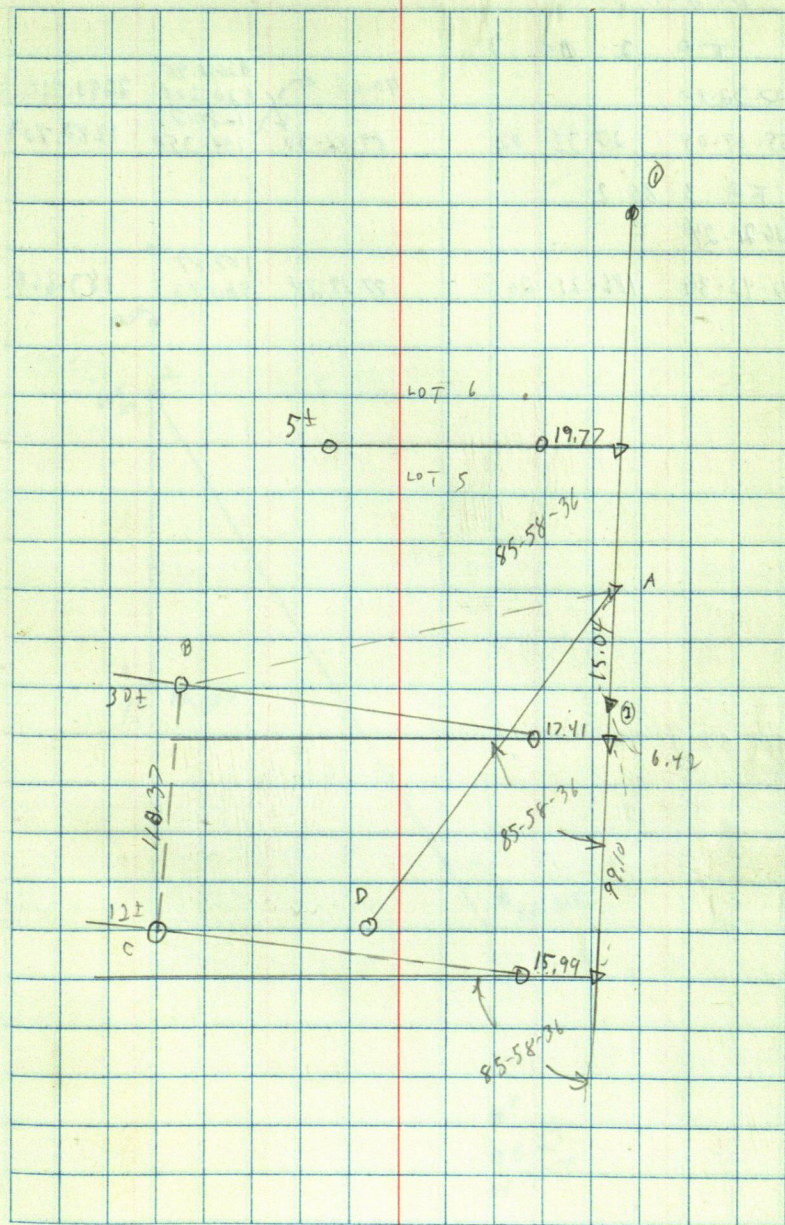
N1K6 ORTN		Lots 5-6 + N ¹ / ₂ 4	
5/25/88		WIDEWAYS ADD TO PINK RIVER	
K 0 2 BS 1			
175-31-33		90-0-17	1083.56 330.270 1083.557
3 351-02-30 175-31-19		90-14-05	243.30 74.159 243.299
172-37-08		88-18	
4 357-14		370-25-30	1564.76 478.156 1568.707
K 0 1 BS 5			
93-18-35			
2 186-36-50			
K 0 1 BS 2			
108-29-06			
7 216-57-54 108-28-57			
K 0 1 BS 7			
158-12-49			
5 316-25-48 158-12-54			
K 0 5			
172-45-19		90-26-03	1105.62 336.997 1105.58
6 357-30-42 172-45-21		90-08-39	1541.35 469.804 1541.339
K 0 7 BS 1			
133-06-43			
8 266-18-49 133-06-54		90-25-33	1161.35 353.983 1161.325
K 8 BS 9			
159-31-12		270-13-37	950.22 289.688 950.21
9 319-02-70 159-31-05		90-05-20	919.52 280.270 919.515

850 CLR LT WIND

E. EURO
T. KUCHARSKI 47
5-24-88



$\Delta \odot$ A B 1				
266-19-50				
B 172-39-20	266-19-40	90-24-18	209.97 24,004	209.972
$\Delta \odot$ B B 5 A				
102-20-39				
C 204-41-02	102-20-31		118.37	
90-26-45				
$\Delta \odot$ A B 5 1				
223-52-06				
D 82-53-44	223-56-52	89-16-33	169.87 51,777	169.857



B. JOHNSON

TE 2 DS 3

27.32-10

90.05 ← 2690.95
820.226 2690.911
1280.73
89.42-30 390.358 1280.704

155-04-04 27-32-02

TE 3 DS 2

186-21-24

4 12-42-39 186-21-20 87-19-24 183.87
56.043 183.668

RR 5th

2
60° SPK

1

1/4 RR SPK

3 RR SPK

4

7B 23
M.V. DOT

174.176Z

AC 2 BS 1

212-55-30

90-05-06

2664.98

F12.222

2664.975

3 65-51-14

212-55-37

89-59-30

732.62

223.304

732.619

425

AC 3 BS 2

175-00-24

4 350-0-46

175-0-23

AC 4 BS 3

F 0-00

89-38-24

793.45

241.849

793.435

1 344.54

196.30

SHORE LINE

2 349-73

294.38

3 354-54

415.61

4 358-14

504.65

5 5-58

672.90

6

AC 2 BS 4

61-05-39

61-06-40

89-52-30

1335.76

407.143

1335.759

5 122-13-20

90-02-31

AC B BS A

0-0-42

93-11-17

90-0-44

2619.22

748.336

2619.204

180-1-10

93-11-59

C 273-12-08

93-10-58

90-8-57

2619.28

778.326

1303.22

397.224

1303.214

0-0-12

180-0-38

93-11-25

93-11-37

273-11-50

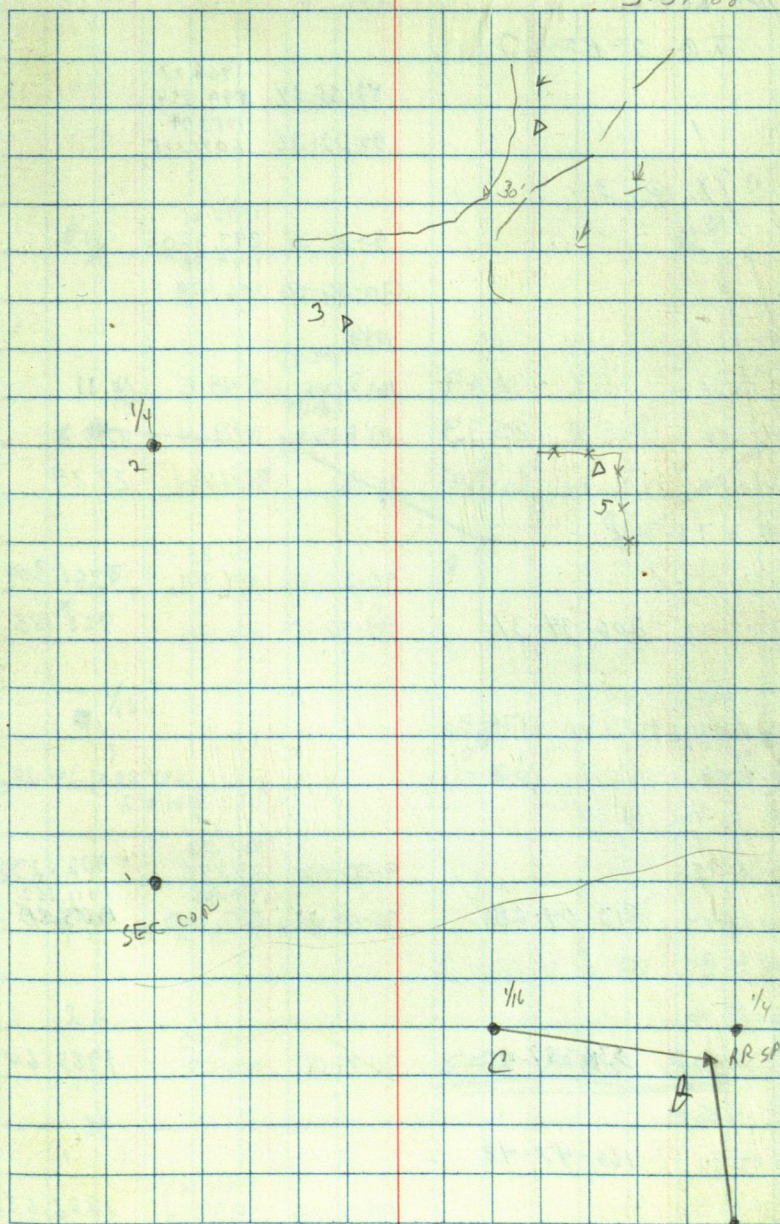
93-11-12

2.0020

TAVEHBSH

46

5-31-88



DOV KLINE

SEC 8 WILSON TWP

T@ 2 BS 3

3	89-55-54	1966.07	599.254
1	90-22-26	1983.94	604.705

T@ 3

4	90-25-38	1290.61	393.380
5	90-26-50	1169.38	356.428

5 1/4	N 1/4	116" R. Oak	S 48 E	9.11	
10" W. Oak	N 45 E	25.33	10" R. Oak	N 89 W	10.23
10" W. Oak	N 36 W	16.04	16" Pop	N 41 W	22.28

T@ 67 BS 6	90-25-30	1361.35	414.941	1361.309
206-34-31	88-32-23	922.49	281.176	922.188

10" B. sum.	N 27 W	174.80
18" W. Oak	S 42 W	168.51

T@ 8 BS 7	91-30-56	922.56	281.199	922.238
213-04-25	90-59-44	1911.95	582.708	1911.662

T@ 8 BS 10	91-37-00	1986.40	605.479	1985.64
316-59-46				

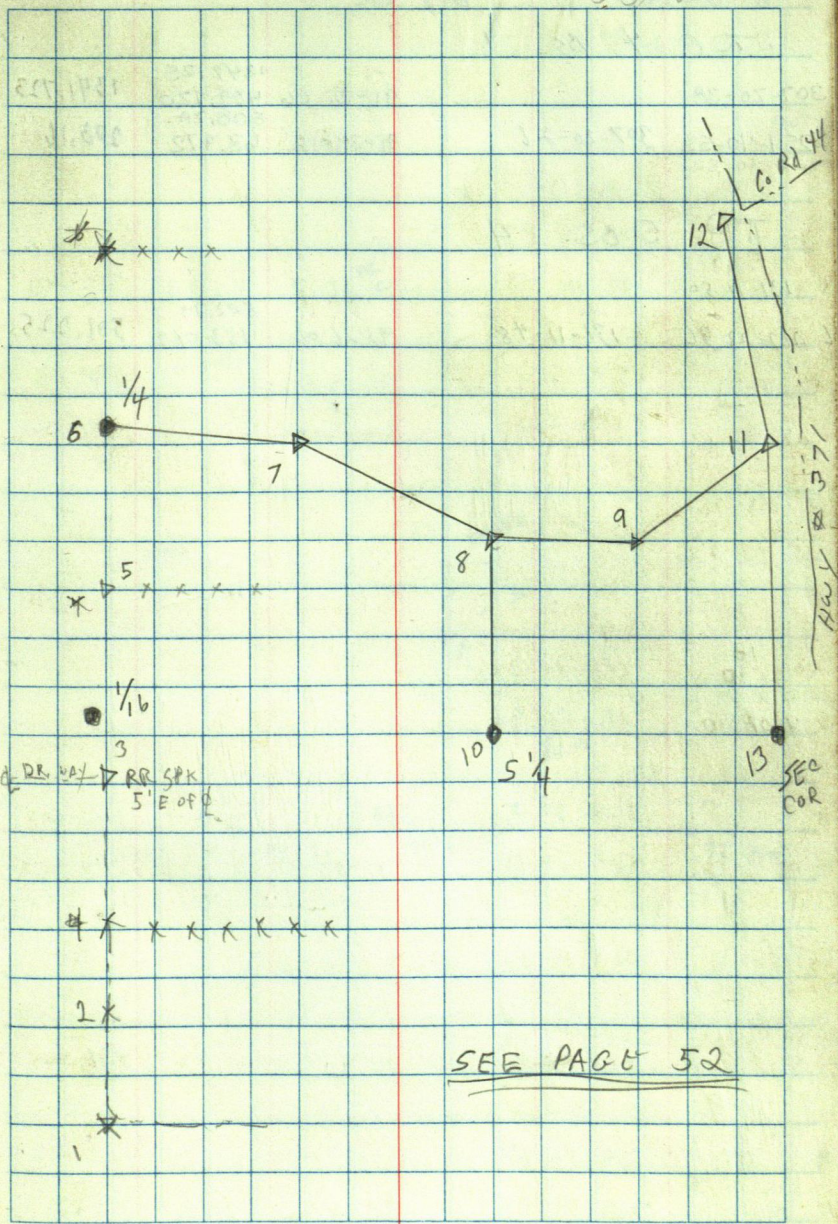
T@ 9 BS 8	90-06-36	1256.64	283.024	1256.632
160-47-54				
11321-35-36				

85° WINDY

E. CURD
T. KOCHERSKY

47

5-31-84



R. GREEN

Boy LK

π @ 4 BS 1

307-20-38

91-36-06

1342.25

1341.723

5254-40-52

307-20-26

91-35-12

409.120

208.24

63.472

208.16

614-40-52

π @ 5 BS 4

131-11-50

131-23-26

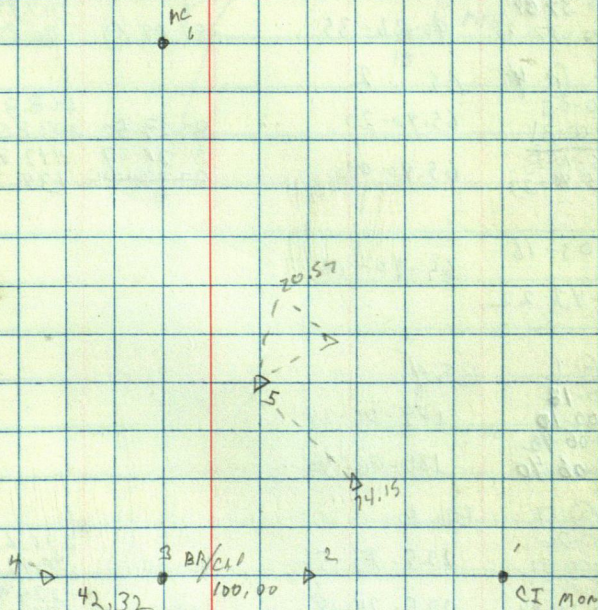
131-11-48

97-26-06

502.13

153.049

501.225



LIPPERT

T @ 2 BS 3

92-44-18	641.65 195.573	640.866
84-43-54	677.29 206.439	677.281

T @ 3 BS 2

0-0-26	90-36-43		
180-0-55			
90-37-89			
5 220-37-30	90-36-35	89-09-44	317.89 96.892 317.853

T @ 4 BS 2

0-0-05	65-40-20	87-23-52	668.82 203.858 668.13
180-00-31			
65-40-23			
6 245-40-33	65-40-02	89-28-29 87-19-02	442.85 134.797 442.219

0-03-16 65-40-06

65-43-22

T @ 6 BS 4

0-0-18	189-06-24
180-00-10	
129-06-48	
7 109-06-40	189-06-30

T @ 7 BS 6

0-0-26	225-23-56	90-35-33	296.67 90.425 296.653
180-00-31			
225-24-22			
8 45-24-49	225-24-18	89-36-42	229.93 70.085 229.928

T @ 8 BS 7

0-0-9	163-14-10		
180-0-19			
163-14-19			
10 345-14-29	163-14-10	93-20-55	223.05 67.986 222.669
263-31-58			
9 83-32-10	263-31-51	92-29-24	137.97 42.054 137.844

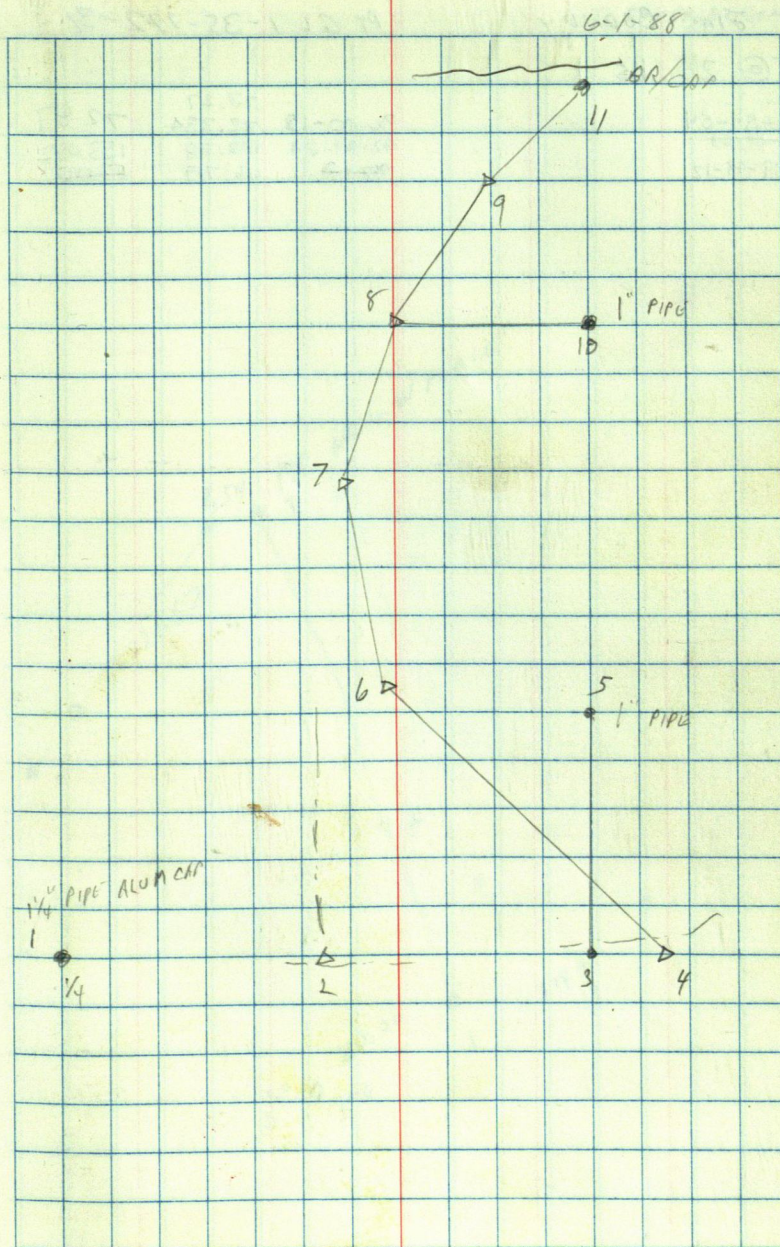
T @ 9 BS 8

0-0-55	206-13-48		
180-0-01			
206-14-43			
11 26-15-00	206-13-59	92-16-33	117.07 35.689 115.86

BS 1 - No 7

E 0020
T. KUCHEST

44



Jim COONLY

PT GL 1-35-142-31

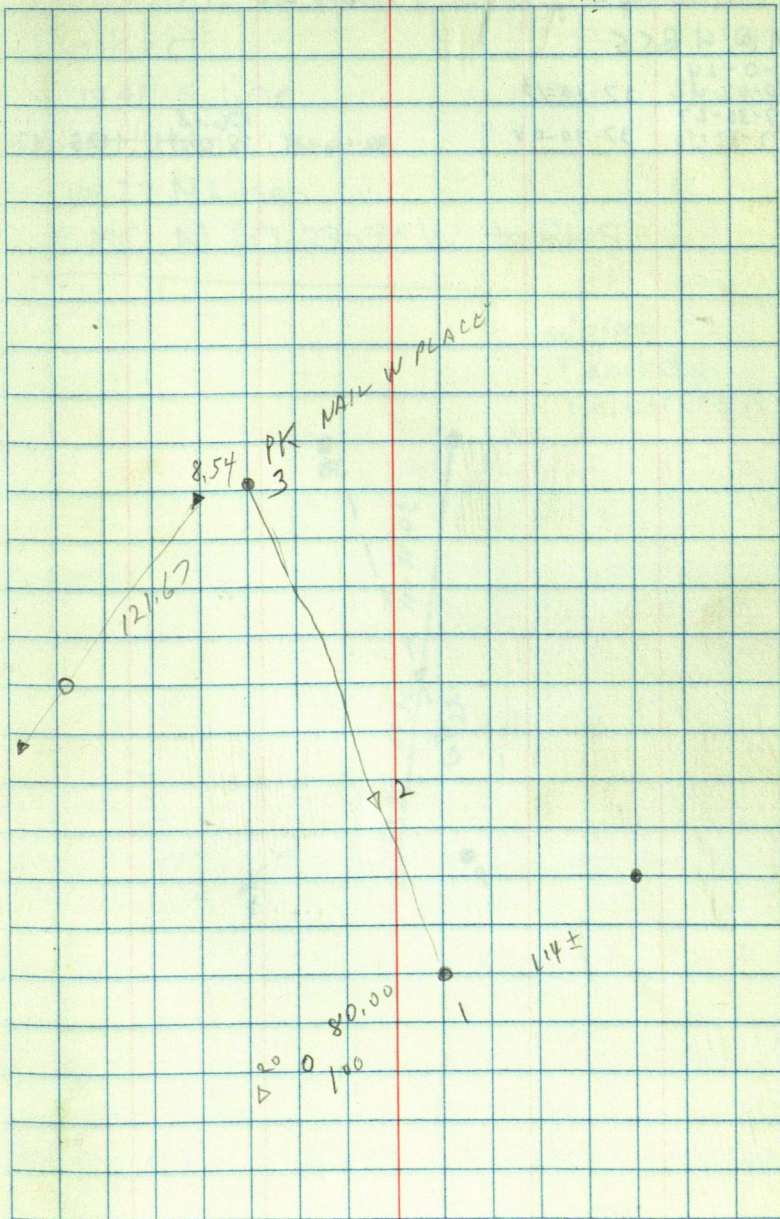
TA 2 BS 1

262
179-54-54
~~54-54-54~~
3359-49-12

96-00-18	73.27	72.87
92-49-34	22.334	153.092
92-7	153.28	46.719
		52.00

85' LOT

E. CURD 62-88
T. KUCHEFSKI 50
T. FREDERICKSON



R. GREEN

Boy L/C

K @ 4 BSS

0-0-14

180-02-42 37-30-13

37-30-27

9 217-32-50 37-30-08

88-46-45 126.18
38.461 126.153CERTIFICATE OF SURVEY GARY STEVENS & ASSOC.
Walker

79.41' S line

~~101.21~~

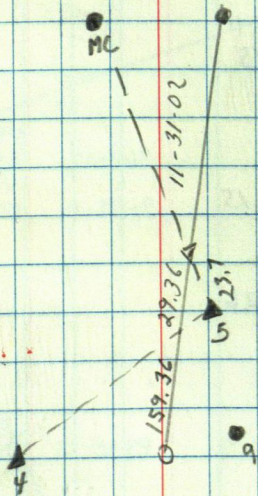
101.27 N Line

SMC N 67-27-35W to RLS

6/3/88

T. Kocher

T. Fredrickson



BS-1

	353.92	
89-24-58	107.875	353.90
	153.79	
92-03-54	46.883	153.702

BS 2

91-07-16	410.60 125. ¹³⁸ 125.138	410.531
----------	---	---------

BS 3

93-16-28	123.97 37.786	123.767
91-19-12	335.30 102.199	335.209

36

90-00-30	194.97	194.973
	59.429	

67

47.68
14,549

5

357

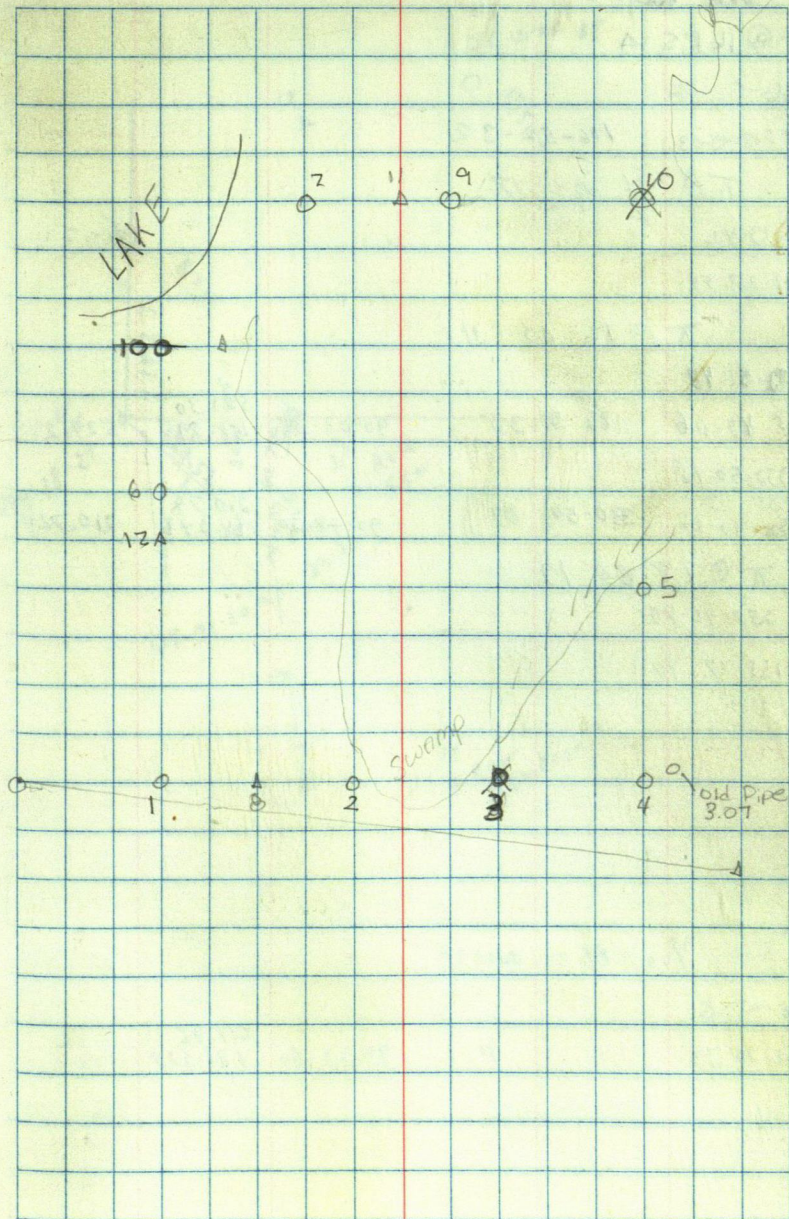
114.01			
34.750	94-30-24	113.657	

556.

91-44-57	63.95 19.455 29.24	63.859
----------	--------------------------	--------

35 10

91-56-46	255.97
	78.014



186.527

Hand-drawn surveying diagram on graph paper. The diagram shows a road layout with several points and distances:

- Top Right:** "JP SWAG BT" and "155.5" with a small square symbol.
- Top Center:** "12" with a small triangle symbol.
- Top Right (Lower):** "11" with a small triangle symbol.
- Left Side:** A vertical line segment labeled "147.31". To its left, "1/16" and "249-18-29" are written.
- Center:** A horizontal line segment labeled "120.53". Below it, "204-05-19" is written.
- Bottom Left:** A curved line segment labeled "134.31-20".
- Center (Lower):** A point labeled "PI SPR" with "18" and "23.22" nearby. Above it, "41.74" is written.
- Right Side:** A point labeled "20 ROW SIGN".
- Bottom Center:** A point labeled "12" with an arrow pointing to it.
- Bottom Right:** A point labeled "19 ROW SIGN POST".
- Bottom Center (Lower):** "11" with a small triangle symbol.

6/16/88

T. Kochefski
T. Fredrickson

55

Jim DeWorot

offset 10.00 @ in center of road running N

T @ 2 BS3

180-00-00

T @ 1 BS3

221-57-09

90-32-27

495.56

152.269

499.541

4243-54-14

90-48-48

594.26

181.134

594.203

121-57-12

121-57-12

243-54-24

T @ 4 BS 1

23-23-00

90-36-04

159.12

7106-31-56

90-36-04

48.498

159.108

22-22-58

233-22-59

2645-57

T @ 4

105.95

6

T @ 4

7

77.47

T @ 1 BS3

179-04-27

8352-08-34

179-04-17

91-23-20

607.65

185.213

607.471

T @ 1 BS3

180-52-31

901-44-44

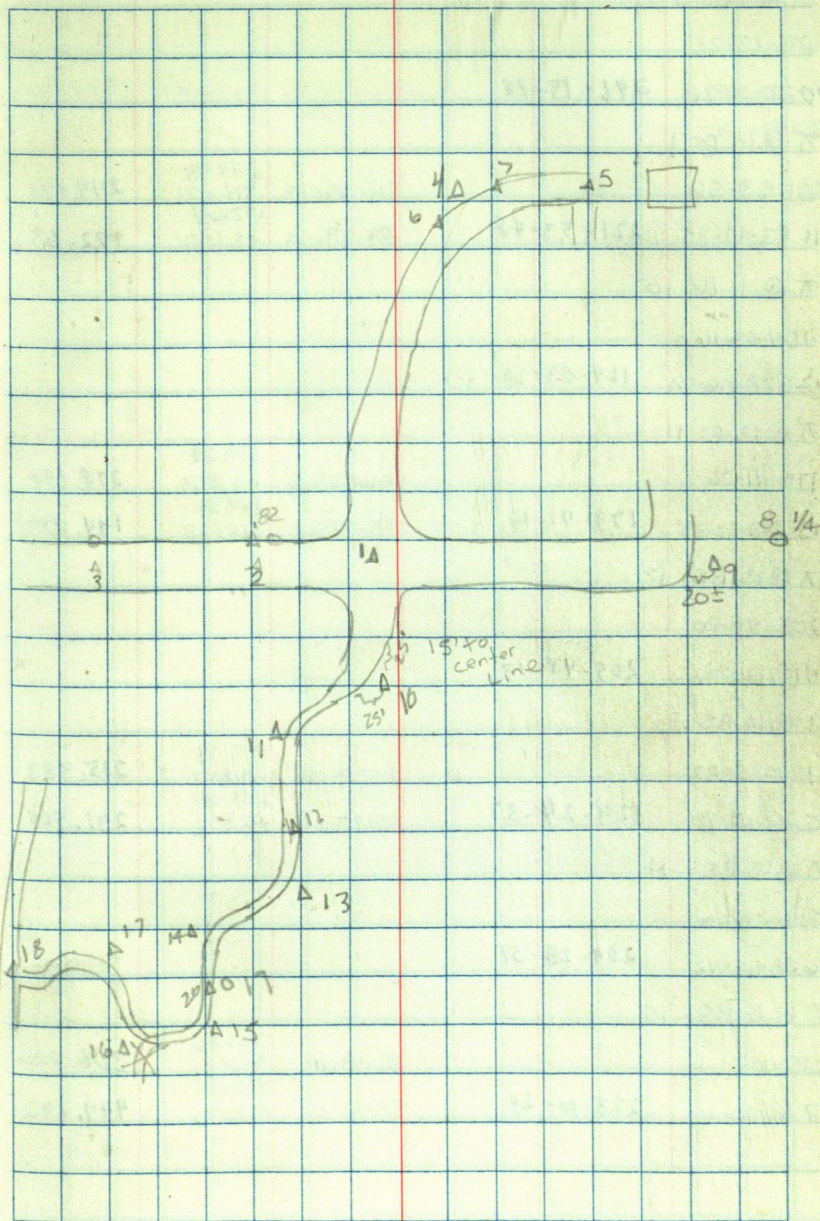
180-52-22

91-15-32

453.68

138.283

453.57



6/17/83

T. Kuchefski
T. Friedrichson

56

T@1BS3

C 296-15-25

A 10222-30-36 296-15-18

T@10BS1

7 221-53-56

2 1183-47-85 221-53-48

T@11BS10

12 164-03-16

2 12328-06-40 164-03-20

T@12BS11

179-41-26

13 359-22-88 179-41-19

T@13BS12

205-48-20

14 51-26-26 205-48-13

T@14BS13

129-25-02

15 268-49-40 129-25-53

T@15BS14

209-29-06

16 58-57-42 209-28-51

T@16BS15

225-10-21

17 90-20-45 225-10-24

244.98

74.671

172.64

52.417

244.191

172.63

278.29

84.823

144.89

64.163

278.154

144.889

215.98

65.817

291.58

88.873

215.383

291.568

306.86

92.531

450.00

127.177

306.824

449.692

12
T @ 17 DS 16

166-17-14

91

590.70

180.043

590.533

18 232-84-10 166-17-05

91-20-09

17 27' E 5' CL 27' W

16 30' W 10' CL 21' N

15 30' W 6' CL 15' N

14 39' S 12' CL 33' E

13 75' W 20' CL 58' N

11 20' S 4' CL 25' E

20 on line between 14 & 15

T @ 20 BS 15

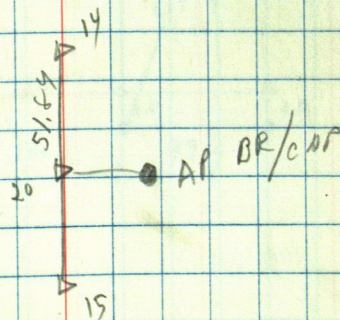
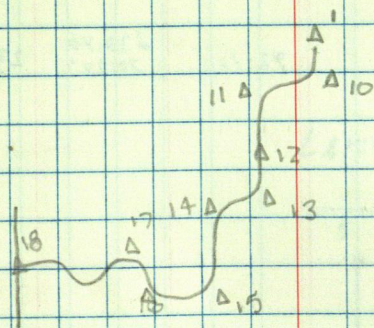
272-51-02

19 195-43-52

272-53-16

185-46-42 272-53-21

15.22



GARY GUMMON

LOT 9 ADA PINE BEACH

K@ 2 BS 1

269-57-48

3 179-54-24

295-4127

231-22-24 295-41-12

92-10

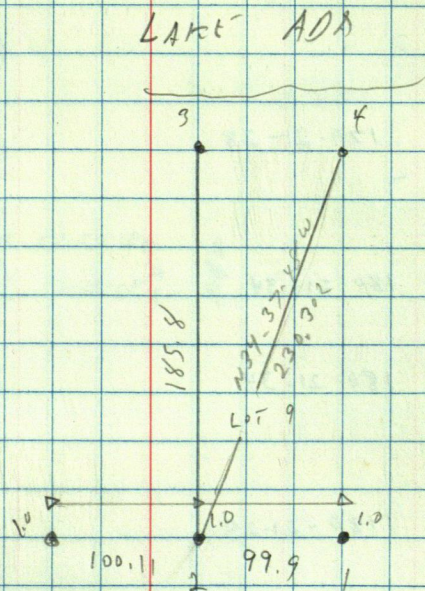
230.46
70.249

230.302

Hot 80°

E. euro
T. FRIDRICKSON

6-20-88



7@4BS 3

179-51-21

89-53-28

2651.03

809,867

2657.021

9 359-42-51

179-51-26

90-09-56

1695.13

316.67

1695.108

7@9BS 4

179-20-03

535889-56

179-19-58

7@5BS 9

90-12-46

88-52-46

952.42

290,340

952.436

6186-25-10

490-12-35

89-32-30

2643.65

805,784

2643.553

90-12-36

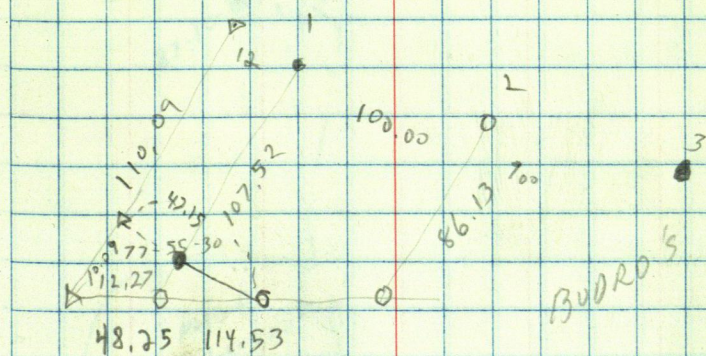
180-25-02

90-12-31

0A16 PLAT OC A/ACK
LOT 5+ PT LOT 29 AND PLT

TP 2 B5 3

90-10-14 199.40
60.778



ANGLE

AC 2 BS 1

208-26-39

356-52-54

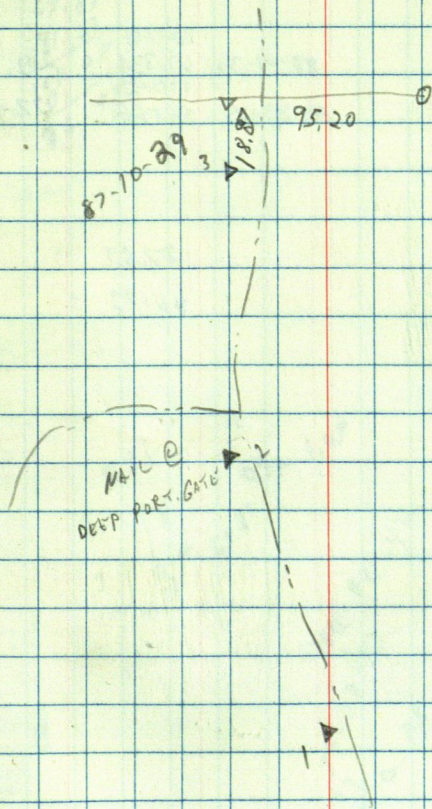
208-26-27

89-58-02

791.83

241.349

791.825



M.H.V. SONDYUK

π @ 2 BS 1

102-26-39

4 204-52-54

102-26-27

π @ 4 BS 2

259-38-57

83-01-30

280.91

67.334

219.275

177.45

54.088

177.44

5 ³⁶⁰
159-17-42
519-17-42

259-38-51

90-39-15

π @ 5 BS 4

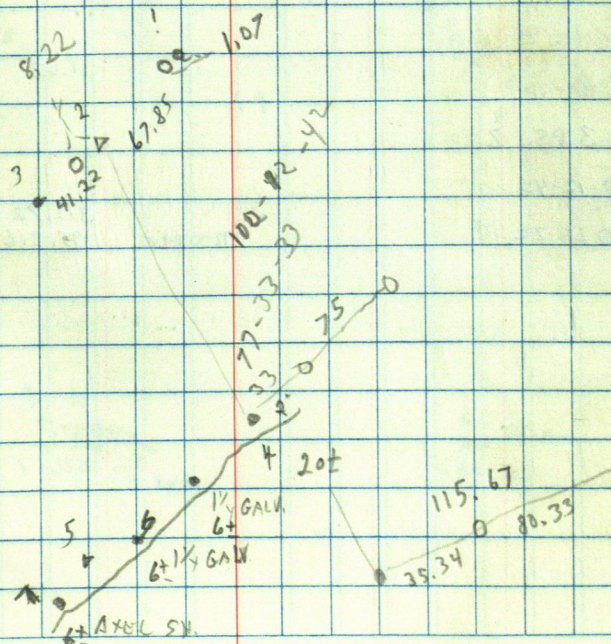
6 1-32-24

27.53

7 128-16-15

46.73

67.85
41.22
26.63
10.90
15.73
76.07



6-28-88

TIMMIES

AC 1 BS 3

267-51-09

72-16-38

600.83

183.136 600.358

4 4

AC 5 BS 3

25 253-25-18

89-56-34

297.79

90.769 297.793

5 1 176-50-24 253-25-14

93-08-32

370.51

112.925 369.94

9 233-19-15

7 106-40-42

6 AC 3 BS 5

7 69-41-20

2139-22-22

92-23-30

474.84

144.731 474.423

AC 3 BS 2

54-64-60

54-54-53

8 109-49-46

41.63

41.63

AC 3 BS 2

340-12-45

306-12-41

688-25-22

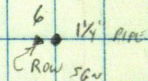
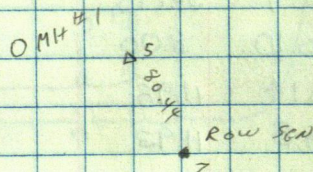
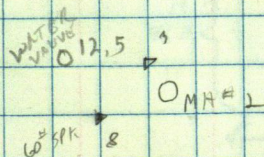
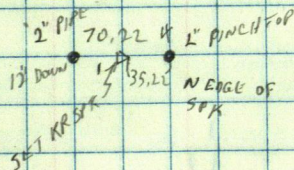
9320-25-22

92-07-00

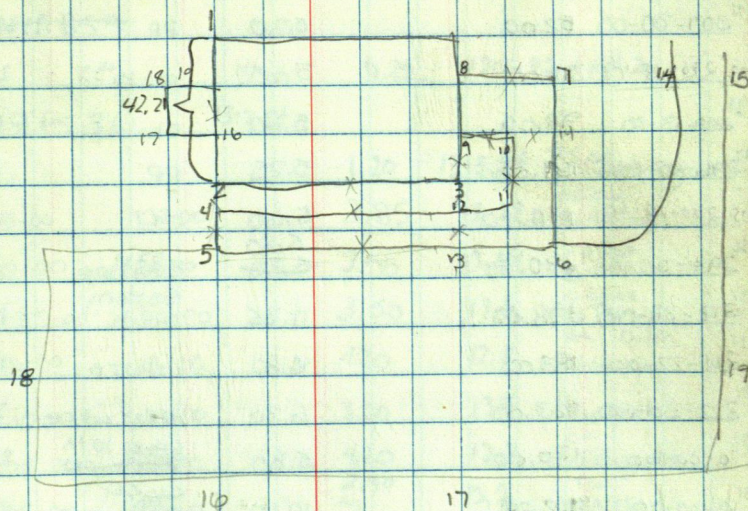
312.72

95.316

312.503



1 to 2	42.21
2 to 4	3.98
4 to 5	6.00
2 to 3	74.20
4 to 11	82.20
5 to 6	86.20
3 to 12	3.98
12 to 13	6.00
3 to 9	21.10 17.08
10 to 11	21.10
6 to 7	35.75
9 to 10	8.00
9 to 14	11.98
7 to 8	11.93
8 to 14	42.00
14 to 15	18.50
5 to 16	70.10
13 to 17	71.78
18 to 19	164.00
16 to 17	5.90



ELC6V

BM #1 0.20

1327.98

NW COR MICH &
TOP NYD TENT

5.67

1322.51
RIM HH #1

5.09

1323.09 #2

SE COR SIDEWALK

TP +12.80

+12.64

BM #1

HT

0.22

1327.98

T @ 3 BS 2

1328.20

BM #1

265-02-00 40.00

40.00

0.22

BM #1

1327.98

309-00-00 52.00

5.30

PP

1322.9

295-18-49 98.00

5.65

CL 10th St

22.55

299-13-00 98.00

5.60

shoulder

22.60

296-40-00 169.00

5.25

PP

22.95

270-18-49 198.00

5.60

CL

22.60

294-00-00 230.00

5.80

6.80

shoulder

22.40

312-38-00 278.00

11.35

Bottom
Ditch

11.85

314-22-00 183.00

10.80

CORNER

17.40

322-50-00 163.00

6.30

APPROX Lot Cor

21.9

0-00-00 20.00

5.80

SHOULDER 10th
MICHIGAN

22.40

0-00-00 102.00

10.10

CL CL
MICHIGAN

18.10

350-25-00 128.00

11.60

16.60

333-25-00 104.00

11.20

3

Bottom
Slope

17.00

323-25-00 137.00

12.70

COR. PARK.
Lot

15.50

66

BM #1 0.50

1327.98

1328.48

BM #2 11.40

11.56

BOTTOM STUD ON E
OF TRASH AREA

1328.32

1316.92

BM #1

0.33

1327.99

~~BM #2 11.40~~

~~T @ 3 BS 9~~

H1

0.22

1316.92 BM #2

T @ 9 BS 3

1317.14

1.20

1315.94

#5 on
Boring

39 101-55-00

132.00

3.85

13.29

NE COR.
BLACKTOP

36 75-30-00

58.00

3.55

13.54

CB TOP
E-100

37 353-35-00

56.00

3.50

13.6

SE COR
B TOP

38 339-06-00

137.00

4.30

12.8

CL Ditch
Michigan

39 343-30-00

126.00

3.30

13.6

Top Bank
CL

40 335-05-00

150.00

4.20

12.9

CL
Michigan

41 319-45-00

91.00

3.90

13.2

TOP
BANK

42 319-45-00

105.00

6.90

10.2

Ditch

43 319-45-00

115.00

6.70

10.4

CL

44 282-30-00

107.00

9.20

07.9

CL

45 282-30-00

92.00

8.90

8.24

Ditch

46 282-30-00

71.00

5.40

1311.7

BANK

T@9 BS3

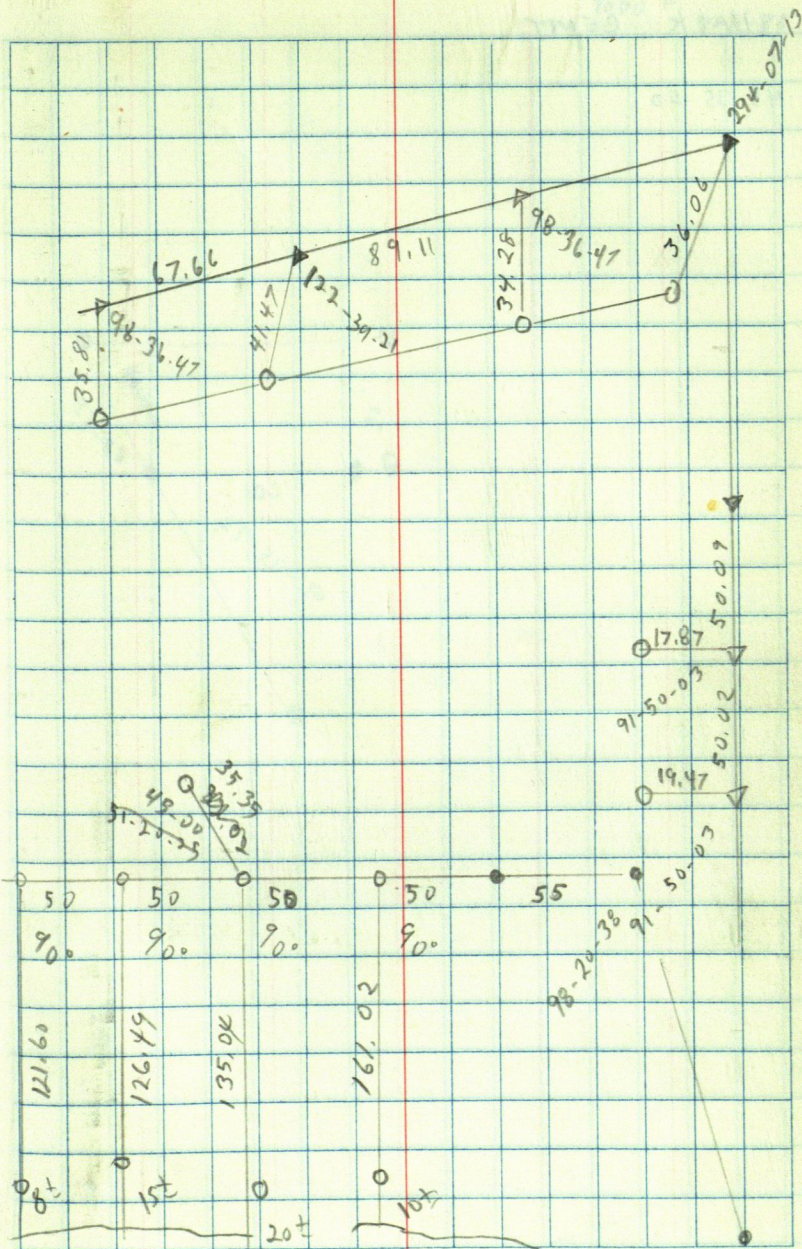
47	241-36-00	94.00	6.20	1310.9	Top Bank
48	247-50-00	103.00	11.20	5.9	Ditch
49	255-00-00	135.00	11.10	6.0	CL
50	239-25-00	175.00	12.40	4.7	CL
51	223-05-00	160.00	12.30	4.8	Ditch
52	224-15-00	150.00	7.90	9.2	Core of Fill
53	227-00-00	151.00	10.50	6.6	Bottom Bank
54	234-10-00	165.00	12.50	4.6	Shoulder
55	229-25	175.00	12.40	4.7	CL
56			13.20	3.9	CL SLine
57			13.20	3.9	Edge SLine Road
58	225-20-00	175.00	11.00	6.1	Core Fill at Bottom
59	221-55-00	170.00	8.60	8.5	Top Hill
60	209-35-00	164.00	8.50	8.6	Top of Fill
61	199-30-00	157.00	8.90	8.2	"
62	190-50-00	160.00	8.90	8.2	"
63	178-15-00	170.00	10.10	7.0	"
64	168-05-00	176.00	10.80	6.3	"
65	158-23-00	165.00	10.60	6.5	"
66	154-00-00	190.00	16.00	1.1	down in hole
67	149-15-00	222.00	15.20	1.9	Toe of Hwy
68	142-50-00	260.00	0.90	16.2	Shoulders of Hwy
69	131-13-00	235.00	0.00	17.1	"
70	131-40-00	195.00	10.50	6.5	Toe of Hwy
71	131-40-00	156.00	14.00	1303.1	"

T@9 BS3

72	131-40-00	141.00	7.90	1309.2	Edge of Fill
73	104-30-00	146.00	4.40	12.7	"
74	102-12-00	165.00	11.90	5.2	"
75	102-12-00	182.00	10.40	6.7	Toe of Hwy
76	84-44-00	157.00	2.20	14.9	Nedge of Stop
T@9 BS3					
77	27-26-35	137.708 122.69	1315.7	183.69	123.631
78	NE 59-07-20		1.40 88-04-04	37.708	141.16
79	10-57-00	120.00	2.10	87-54-00	43.028
	BM #2				141.07
					SW Cor B Top
80	265-30-00	73.00	0.20	16.93	Edge of Building toe
81	231-35-00	39.00	5.70	11.4	"
82	152-35-00	67.00	5.80	11.3	"
83	134-00-00	126.00	6.50	10.6	"
			6.70	10.4	"
			1.05	1316.09	Slab of Con in back

R. GREEN

WOMAN LK
SEMI-ON-SED

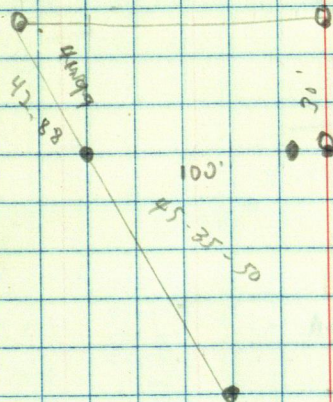


HACK CEMT.

45-35-50

G. CURD
Tom K
Todd F.
7-1-88

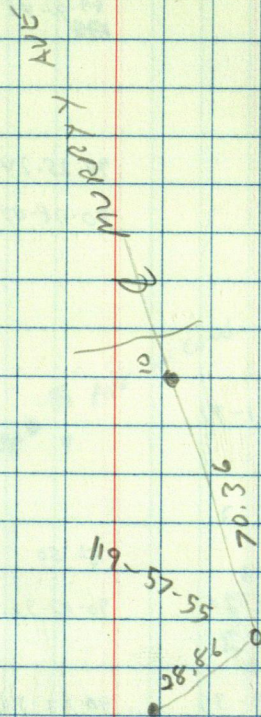
69



TOOTS BRENNER

E. CURD
Tom K
Todd F
7-1-88

70



VICTOR DAVIS

PT LOTS 2+3 MILLERS PT

T@ 2 BS 1

✓ 90-29-36

89-41-48	1323.17	
132	403.308	1323.155

T@ 5 BS 2

6 89-23-28

90-25-24	500.36	
	152.511	510.346

3

90-08-04	3461.07	
	1054.937	3461.05

T@ 2 BS 1

1110-22-08

116 53

7232-43-46

116-21-38

118-21-41

7 232-43-22

T@ 7 BS 2

221-29-36

82-50

146.89	
44.722	145.742

9 82-59

221-29-30

90-07-30

104.78	
31.936	104.778

202-59-48

145-59-18

202-59-39

90-42-48

351.21	
102.048	351.18

T@ 9 BS 7

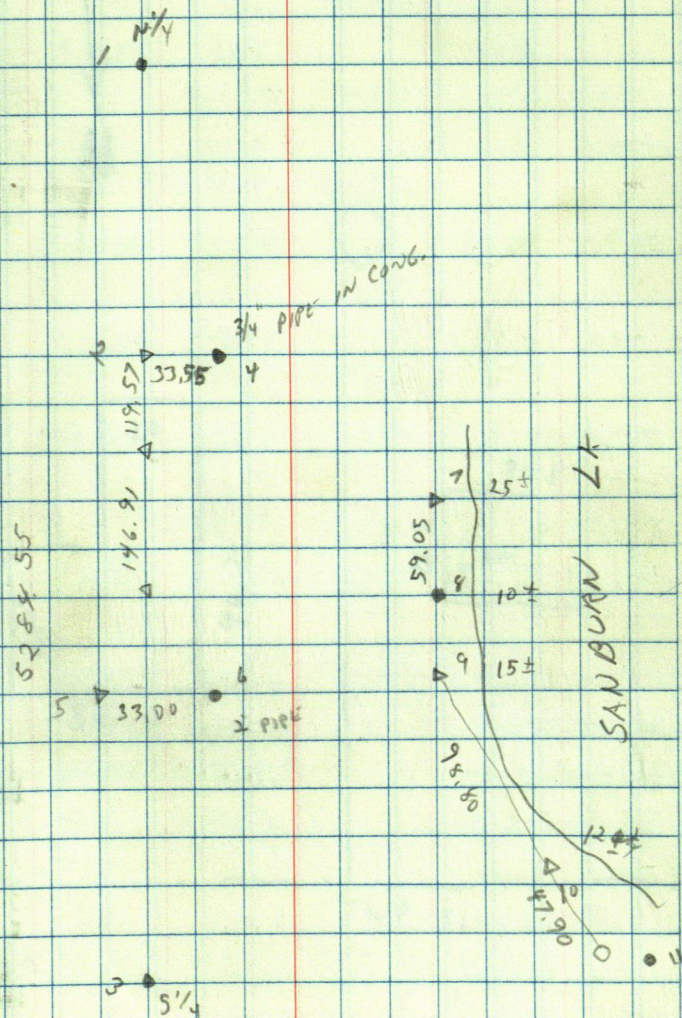
157-09-15

10 314-18-40

157-09-20

PRLY CLOY
40°E. CURD
TOM K
TODD F.
7-1-88

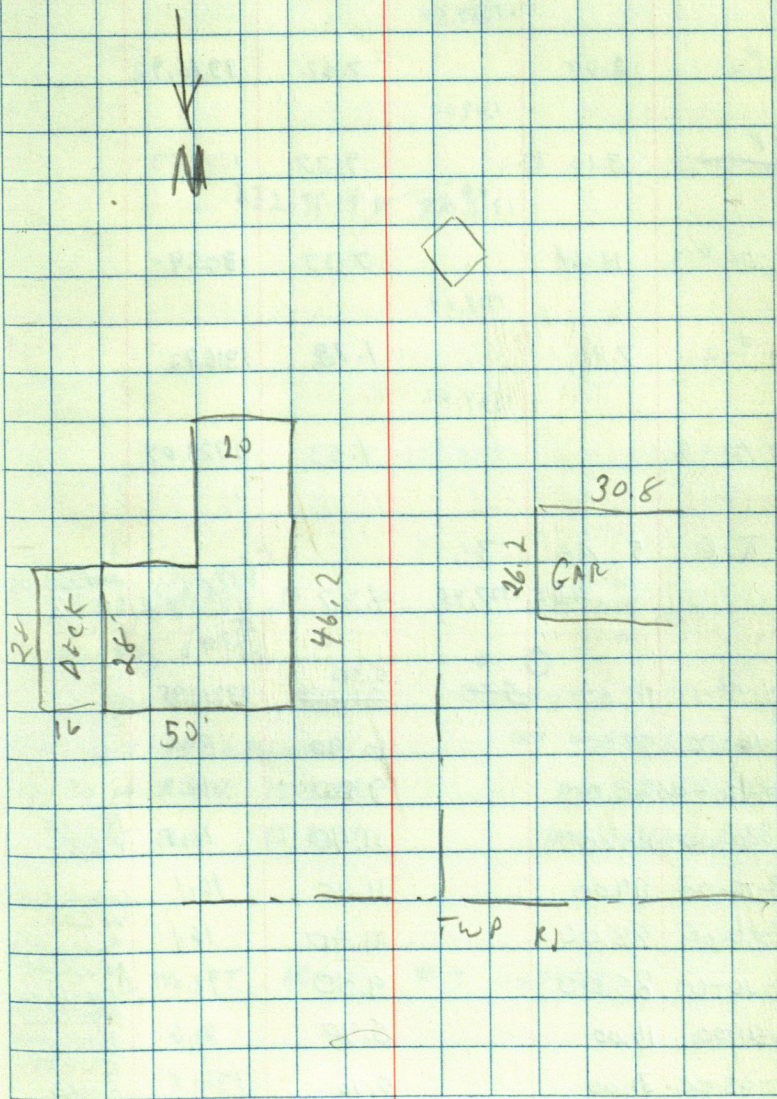
71



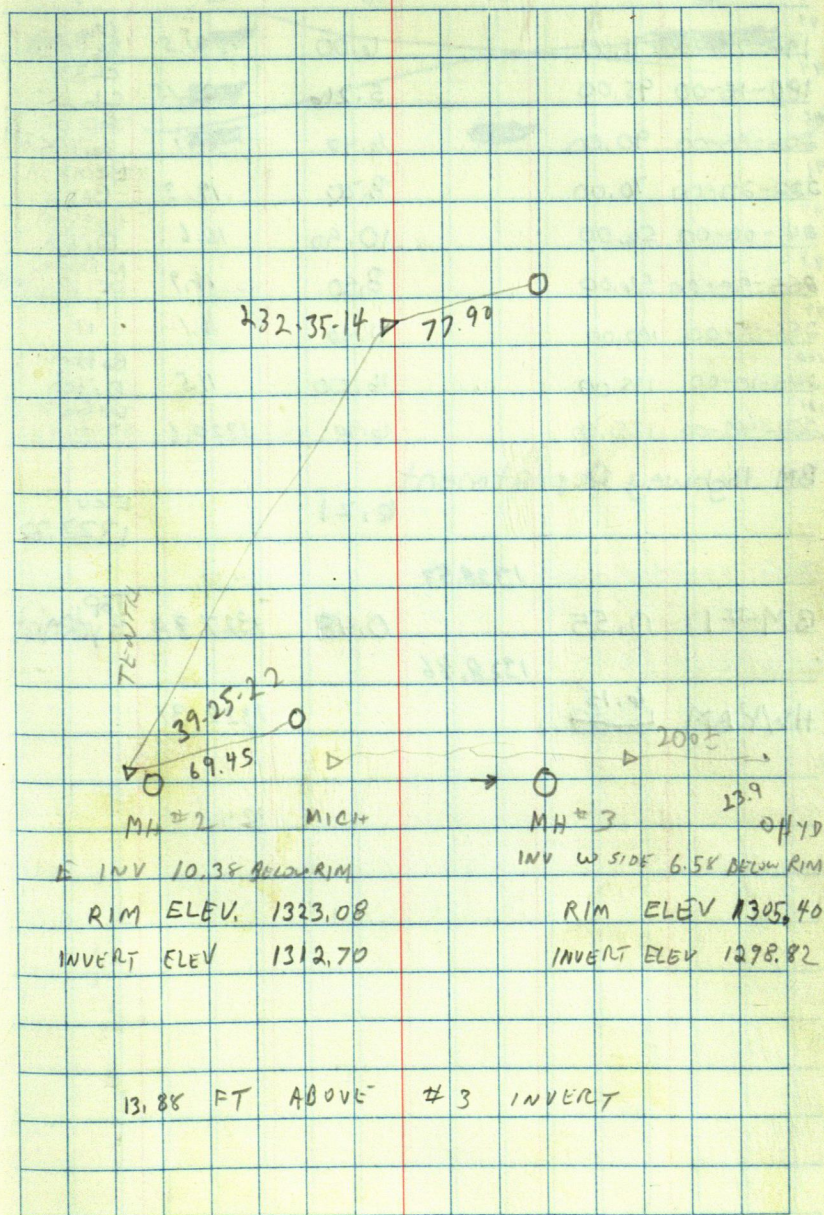
Jim Gamble

BR. EVELANDS HOUSE

72



JIMMBS	BS	HI	FS	
Rim Man H [#] 2	1.46		1.46	1323.08
		1324.54		
BM #2	2.08		7.62	1316.92
		1319.00		
TP				
Rim H [#] 3	3.10		9.37	1309.63
		1312.73		
Rim MH #3	12.64		7.33	1305.40
		1318.04		
BM #2	7.70		1.72	1316.92
		1324.62		
Rim MH #2			1.53	1323.09
TA @ 5 BS 3				
	HI = 1327.45	4.37		Rim of manhole BM #2
				1323.08
				BM #1 FIRE Hydrant
84 334-50-00	31.00	5.50	5.50	1321.95
85 286-16-00	57.00	6.90	20.6	SSide of Highway
86 277-50-00	88.00	9.20	14.3	"
87 277-50-00	108.00	11.40	16.4	N Side Plot
88 288-16-00	119.00	11.45	16.1	Covert side w/ W Cor.
89 298-50-00	88.00	11.40	16.1	Sidewalk
90 313-10-00	85.00	9.50	18.0	NW Cor Building
91 229-50-00	16.00	5.90	21.6	NW Cor Driveway
92 207-05-00	31.00	5.70	1321.8	END OF Curve



Angle	Distance	Rod Reading	S edge 371
95 194-20-00	71.00	6.00	1321.5 in gutter CL 371
97 180-15-00	95.00	5.26	22.15 CL 10th
95 206-55-00	90.00	6.40	21.1 Top of hill S 371
96 222-22-00	70.00	8.20	19.3 Break in Bank
97 241-00-00	56.00	10.90	16.6 Bottom Ditch
98 255-55-00	56.00	8.50	14.9 N Edge Dr. Bottom
99 255-55-00	100.00	11.40	16.1 LI
100 245-10-00	105.00	16.00	11.5 Bottom Ditch
101 221-45-00	125.00	6.90	1320.6 Top Bank S side 371

BM Highway Department

6.21

Elev

1322.32

1328.53

BM #1 0.55

0.48

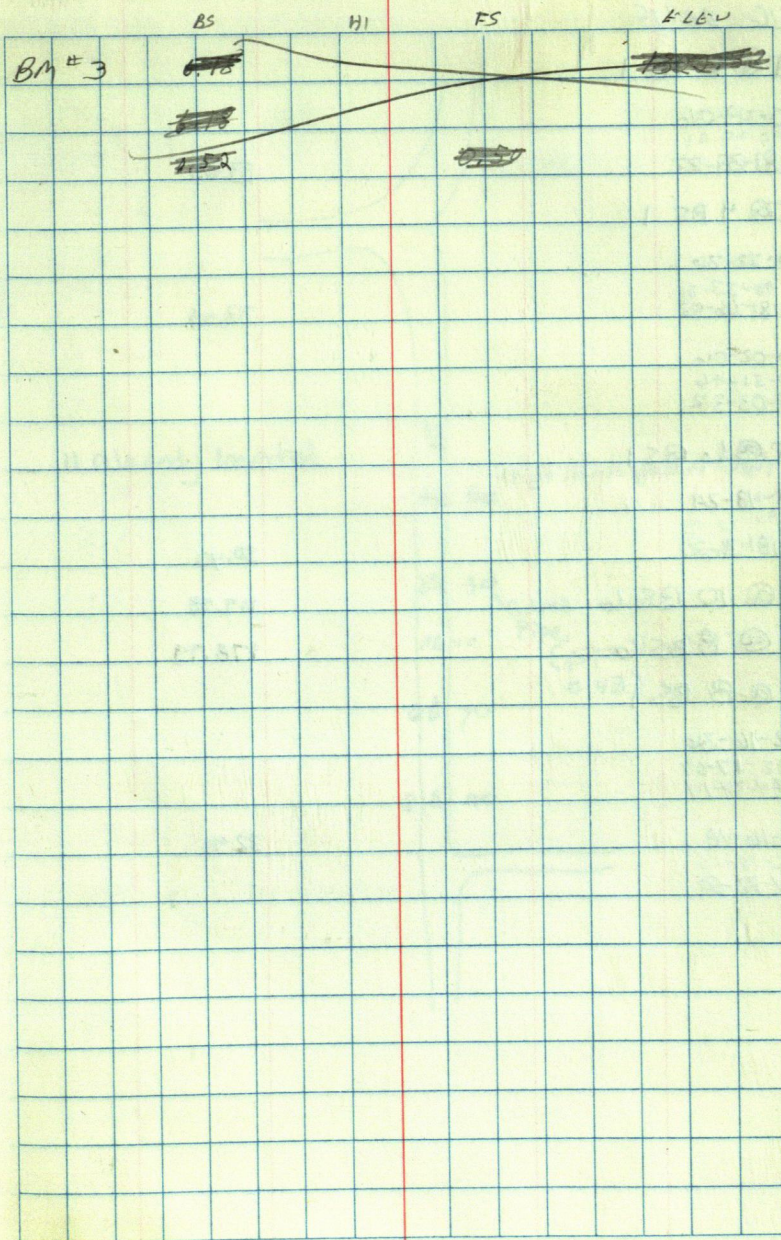
1327.98

Top Hydrant

1328.86

HWY BM 6.15

1322.31



7/5/88

T. Kochefski
T. Fredrickson

VIC DAVIS

T@2 BS 1

90-49-36
90-49-41

3181-39-22

33.05

T@4 BS 1

90-32-26

90-33-01

5181-06-03

33.05

90-02-06

90-31-46

181-03-32

T@6 BS 1

90-48-24

90-48-15

7181-36-30

30.40

T@10 BS 6

119.58

T@8 BS 6

178.79

T@8 BS 1

92-16-36

92-17-07

9184-34-14

32.91

92-16-18

92-16-25

184-32-50

75

11 already located

1A

4A 50

(pipe with yellow cap)

2A 30

10A 110

Silver
Pipe(pipe N of #3
0.43)

4A 70

2A 90

WADE BRAMMANN

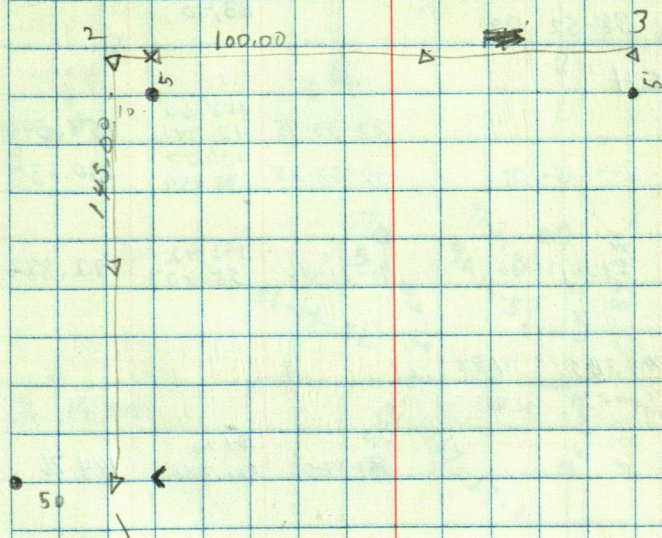
6-7-8 PT 9 BLK S ORG. PINK RVR

1 2 3 4 5

89-55-06

1 179-50-00 89-55-0

76



STACY

7 @ 2 BS 1

270-47-46	90-22-26	314.94 95.992 60.01	314.929
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3181-35-38 270-47-49

7 @ 4 BS 2

62-04-54	90-48-46	
----------	----------	--

38-52-16		88.70
----------	--	-------

5 77-44-18 38-52-09

7 @ 6 BS 4

204-05-30	89-37-45	158.60 48.341 130.77 39.859	158.594 130.633
-----------	----------	--------------------------------------	--------------------

7 48-11-10 204-05-35

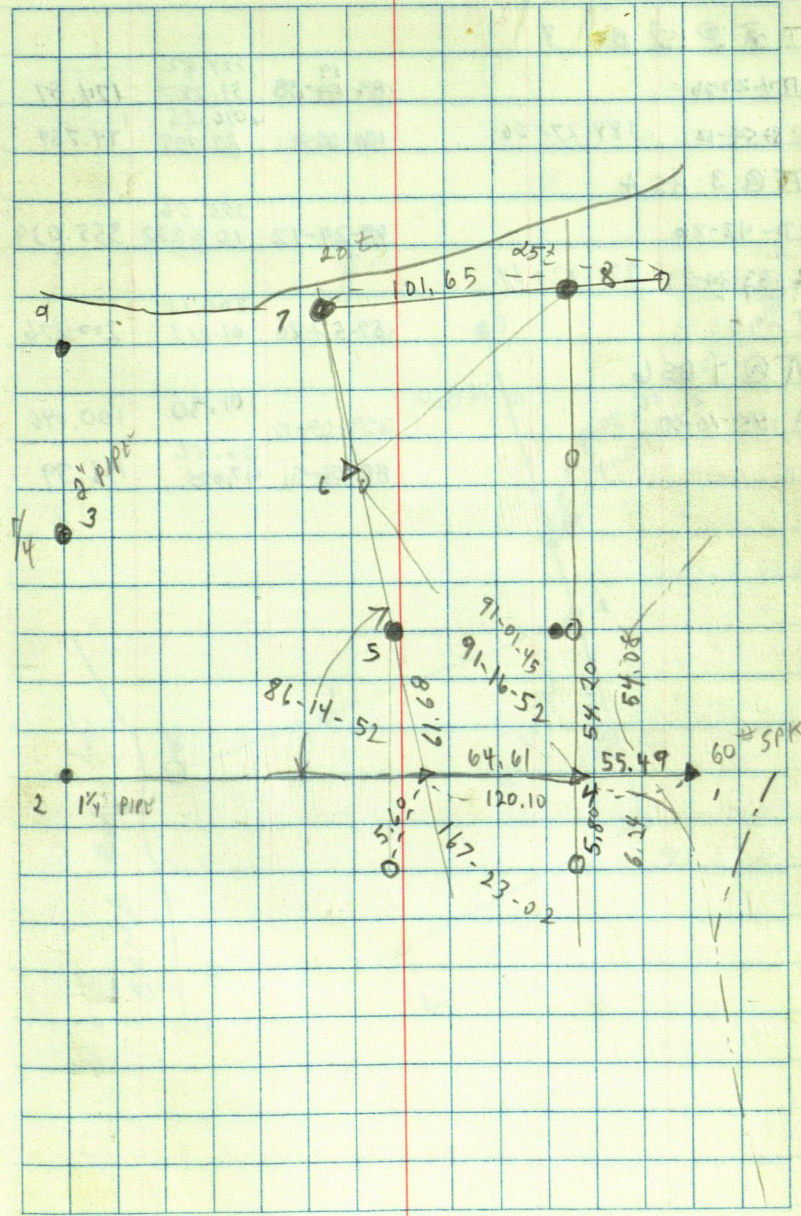
230-11-00		
-----------	--	--

8 100-22-01	230-11-00	91-21-46	192.92 58.803	192.866
-------------	-----------	----------	------------------	---------

7 @ 7 BS 6

73-56-26		
----------	--	--

9 147-52-34	89-53-02	184.76 16.316	184.76
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7/14/88

EVELYN MITCHELL

A @ 2 BS 3

184-27-06

89-¹⁹~~31~~-58

174.82

174.87

1 8-54-12 184-27-06

100-05-31

53.287

94.769

A @ 3 BS 4

271-42-26

89-24-12

355.06

355.039

2 103-24-27 271-42-14

4 271-42-13

89-52-20

200.18

200.176

A @ 7 BS 6

8 180-10-00

10' to H₂O

259-03-12

101.90

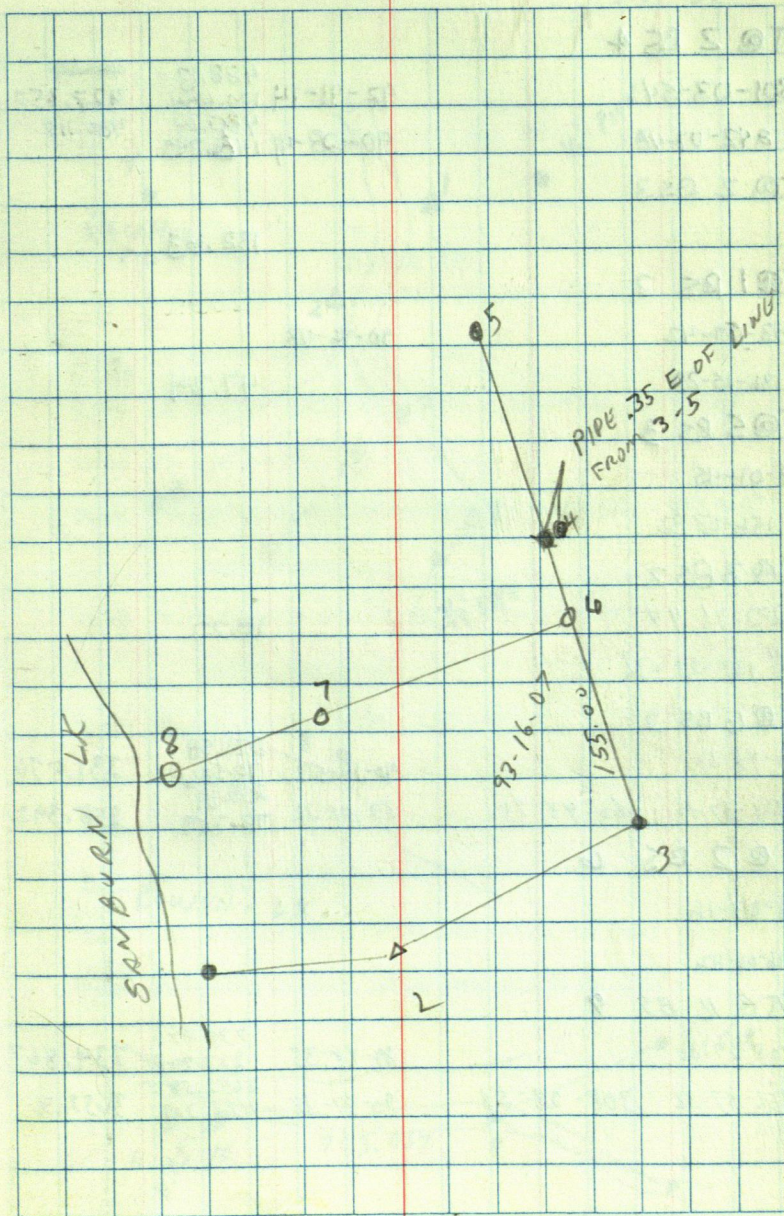
100.046

6

88-56-51

156.42

156.39

E. CURT
T. Kucharski

7/15/88

Lennie Johns

E. CURD
T. Kucharski

T@2 BS 4

301-03-54

92-41-14

428.13

~~428.13~~

130.474

427.657

3 242-07-40

90-28-41

480.14

480.118

T@2 BS 3

5

132.163

T@1 BS 2

243-07-42

90-36-48

1/2 126-15-28

47.34

T@5 BS 3

78-01-45

BL 156-03-32

T@3 BS 2

272-46-44

18.27

3/4 125-33-36

T@6 BS 2

60-48-51

90-18-57

231.58

231.576

7 121-37-13 66-48-40

89-58-12

70.586

258.39

258.392

T@2 BS 6

138-03-16

3276-06-42

T@11 BS 9

308-29-00

89-48-35

734.87

734.867

8 256-57-56 308-28-58

90-07-18

223.791

3652.58

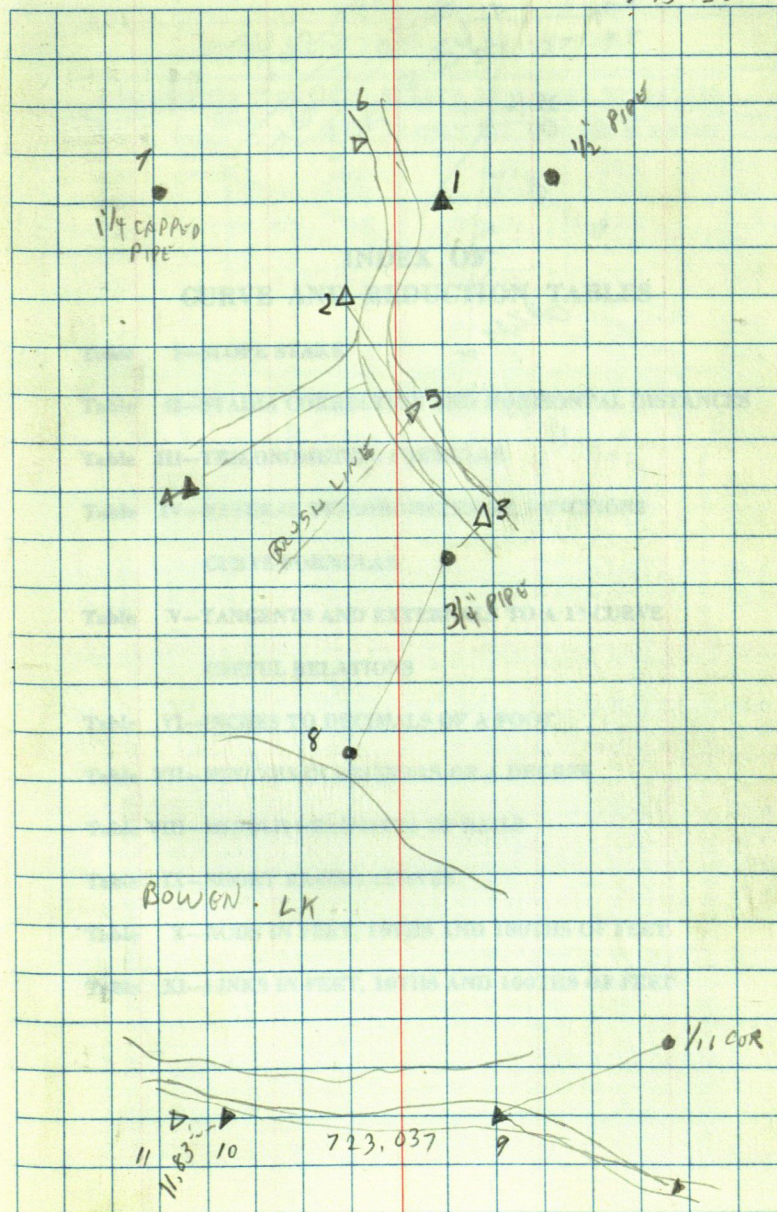
3652.56

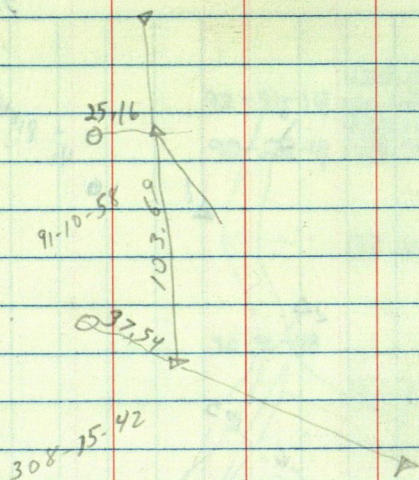
E. CURD

Tom K.

79

7-15-88





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CURVE AND REDUCTION TABLES**

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CURVE FORMULAE

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USEFUL RELATIONS

Table VI—INCHES TO DECIMALS OF A FOOT

Table VII—MINUTES IN DECIMALS OF A DEGREE

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Table IX—SHORT RADIUS CURVES

Table X—RODS IN FEET, 10THS AND 100THS OF FEET

Table XI—LINKS IN FEET, 10THS AND 100THS OF FEET

USEFUL RELATIONS

Lineal feet	$\times .00019$	= miles
Lineal yards	$\times .0006$	= miles
Square inches	$\times .007$	= square feet
Square feet	$\times .111$	= square yards
Square yards	$\times .0002067$	= acres
Acres	$\times 4840$	= square yards
Cubic inches	$\times .00058$	= cubic feet
Cubic feet	$\times .03704$	= cubic yards
Links	$\times .22$	= yards
Links	$\times .66$	= feet
Feet	$\times 1.5$	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = $0.667 (\text{Dist. in miles})^2$

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at center of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

SQUARE MEASURE

$$144 \text{ sq. inches} = 1 \text{ sq. ft.}$$

$$9 \text{ sq. ft.} = 1 \text{ sq. yard}$$

$$30\frac{1}{4} \text{ sq. yds.} = 1 \text{ sq. rd.}$$

$$40 \text{ sq. rds.} = 1 \text{ rood.}$$

$$4 \text{ roods} = 1 \text{ acre}$$

$$640 \text{ acres} = 1 \text{ sq. mile.}$$

SURVEYORS' MEASURE

$$7.92 \text{ inches} = 1 \text{ link.}$$

$$25 \text{ links} = 1 \text{ rd.}$$

$$4 \text{ rds.} = 1 \text{ chain.}$$

$$10 \text{ sq. chains or } 160 \text{ sq. rods} = 1 \text{ acre.}$$

$$640 \text{ acres} = 1 \text{ sq. mile.}$$

$$36 \text{ sq. miles (6 miles sq.)} = 1 \text{ township.}$$

0-0-07

304-51-27

TABLE VIII. MIDDLE ORDINATES OF RAILS

750.75

87-50

Length of Rail (feet)

C o /	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE IX. SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

182-00-28

265-34-10

265-34-24

0-00-14

265-34-10

225.94
68.866

182-15-30

177-44-34

360

92-24-08

452-2408

225.59

92.53

225.71

68.196

87-35-59

180-05-40

179-54-15

13

178-58-30

58-58-28

181-01-34

5

0-0-19

179-49-19

180-10

94-25-55

74.15

10-00-32

166-17-05
2 332-34-10

460-04-08

180-00-10

272-23-58

274-27-03

180-01-05

94-25-58

359-59-80

180-00-48

179 59 32

180-00-

359-59-60

8-53-39

351 06 21

87-36-59

-17

3616

260-26-16
89-25-48
171-00-38

272-24-00

180-06-12

179-53-42

267-36-20

180-00-20

87 36 00

79 56

180-00-41

85-34-24

94-22-47

144-21-02

0-01-07

94 25 55

484-15-28
243-07-44

349-9240
174-5360

2639-54-54
269-

209-28-36
2118-57-42

307-1000
21674 40-52-94-32
21359-49-12

140-38-39
130-38-40
219-21-30
219-21-21

233-22-50
2466-45-57

790.
241.091
02.05
20.24
1.21

230 85-68
179-59-51
572617

218-53
545-46-42
105-33-21

792.03
1129.35
1921.40

260-26.16
180-00-30
80-25-40

26979 2160-47-48
32135-36
529-54-54
369-

102-04 21
257-54-50
117-39-50

77117
70.74
13

10652-51
2113-15-03

270-01-43
540-03-34
2214

235-18-50
179-39-56
358-39-56
104-00-08

20826-214
416-52-64

89-39-44
179-19-30
270-01-40
540-03-20

219-22-16
140-32-42

89-25-64
360
254
618

179-33-33
206-34-31
2412-10-20
259-30-51
519-10-17

221-31-57
180-21-34
360-43-08

134 26-54
268-53-54
0-0-08
180-00-05

21485-55-12
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2180-10-20
259-30-51
519-10-17

0-0-24
180-00-19

221-31-13
41-31-43
177-37-10
2355-14-70
49-41-70
139-12-11

133-15-58
24063156-
134 26-54
268-53-54
0-0-08
180-00-05
138-29-16
318-29-13

221-30-49
221-29-02
242 5805

213-01-27
2426-08-05
93-02-30

244.36

273-59-24
360
2633-59-24
316-59-42

2174-50-29
2613-64-19
306-57-19
21345 49-57
253-2

222-27-16

222-27-63

222-27-20

0-0-43

93-53-10

367.30

367.40

271-33-47

271-33-46

143-21-46

88-16-07

143-21-43

88-16-02

216-39-26

93-53-20

179-59-62

179-55-55

00

30

137-32-29

88-26-14

222-28-14

127-31-48

179-41-19

2359-27-30

380-49-48

802-01-03

127-32-04

317-32-01

58

127-31-64

180-00-00

15

43

94-58-35

137-32-41

8

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